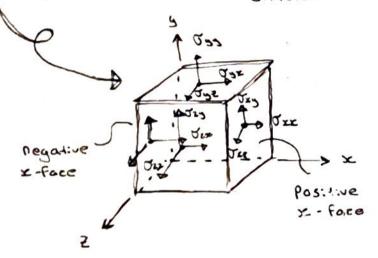
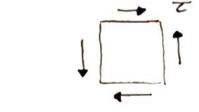


/ when subscripts are the same-normal stress \ "d: Fferent - Shear stress )



- 9 stress components at a point



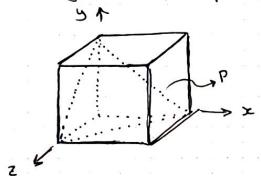
Pure shear Tyx: Txy; Txx: Txx: Txx: Txx

Only 6 of these components are independent

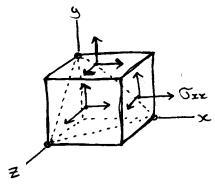
 $\begin{bmatrix} T \end{bmatrix} : \begin{bmatrix} G_{xx} & G_{xy} & G_{xz} \\ G_{5x} & G_{5y} & G_{5z} \\ G_{2x} & G_{2y} & G_{1z} \end{bmatrix}$ 

Symmetric matrix

arbitrarily oriented Plane



Find Tp on the inclined plane



Inclined plane:

Unit normal vector

$$\vec{N} = li + Mis + RH$$
 $l^2 + M^2 + R^2 = 1$ 

Stress vector  $\vec{\nabla} p = ?$ 
 $\vec{\nabla} p = \vec{\nabla} p \times \vec{i} + \vec{\nabla} p \times \vec{j} + \vec{\nabla} p \times \vec{k}$ 

Equilibrium of the small volume:

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz} \\
\nabla_{py} = L_{0xx} + M_{0yy} + n_{0yz} \\
\nabla_{pz} = L_{0zx} + M_{0zy} + n_{0zz}
\end{cases}$$

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0zz} \\
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0zz}
\end{cases}$$

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz} \\
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz}
\end{cases}$$

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz} \\
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz}
\end{cases}$$

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz} \\
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz}
\end{cases}$$

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz} \\
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz}
\end{cases}$$

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz} \\
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz}
\end{cases}$$

$$\begin{cases}
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz} \\
\nabla_{px} = L_{0xx} + M_{0xy} + n_{0xz}
\end{cases}$$

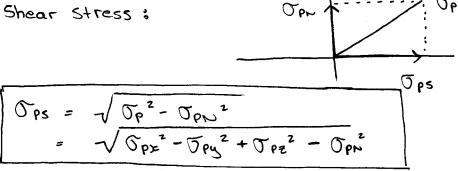
$$= l \partial_{px} + m \partial_{py} + n \partial_{pz} = \cdots$$

$$|\partial_{pn}| = l^{2} \partial_{xx} + m^{2} \partial_{yy} + n^{2} \partial_{zz} + 2 lm \partial_{xy} + 2 mn \partial_{yz} + 2 n l \partial_{zx}|$$

$$|\partial_{px}| = (l m n) (\partial_{px}) (\partial_{pz})$$

$$|\partial_{pz}| = (l m n) (\partial_{pz})$$

$$\begin{pmatrix}
\sigma_{m} = (l m n) & \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\
\sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\
\sigma_{zx} & \sigma_{zy} & \sigma_{zz}
\end{pmatrix}
\begin{pmatrix}
l \\
n
\end{pmatrix}$$



Direction of Shear stress: Tp = 5pn N + Jps 5

2.4 Transformation of Stress Principal Stresses

Define: 
$$\begin{cases} \vec{N_2} = l_1 \vec{i} + m_1 \vec{i} + n_1 \vec{H} \\ \vec{N_2} = l_2 \vec{i} + m_2 \vec{i} + n_2 \vec{H} \\ \vec{N_3} = l_3 \vec{i} + m_3 \vec{i} + n_3 \vec{H} \end{cases}$$

 $\int_{1}^{2} + M_{1}^{2} + R_{1}^{2} = 1 \qquad \int_{2}^{2} + M_{2}^{2} + R_{2}^{2} = 1 \qquad \int_{3}^{2} + M_{3}^{2} + R_{3}^{2} = 1$   $\int_{1}^{2} + M_{1}M_{2} + R_{1}R_{2} = 0$   $\int_{2}^{2} + M_{2}M_{3} + R_{2}R_{3} = 0$   $\int_{1}^{2} + M_{1}M_{3} + R_{1}R_{3} = 0$   $\int_{1}^{2} + M_{1}M_{3} + R_{2}R_{3} = 0$   $\int_{1}^{2} + M_{2}M_{3} + R_{2}R_{3} + R_{2}^{2} + R_{3}^{2} + R_{$ 

Stress vector on x-face  $\nabla x = \nabla_{xx} N_1 + \nabla_{xy} N_2 + \nabla_{xz} N_3$   $= > (\nabla_{xy} = \nabla_{x} \cdot N_2$   $\nabla_{xz} = \nabla_{x} \cdot N_3$   $\therefore \nabla_{xy} = \int_{1}^{1} \int_{1}^{1} \nabla_{xx} + m_1 m_2 \nabla_{yy} + h_1 h_2 \nabla_{zz}$   $\vdots + (l_1 m_2 + l_2 m_1) \nabla_{xy} + (m_2 h_1 + m_1 h_2) \nabla_{yz}$   $\vdots + (n_1 l_2 + n_2 l_1) \partial_{zx}$   $\nabla_{yz} = l_2 l_3 \nabla_{xx} + m_2 m_3 \nabla_{yy} + h_2 h_3 \nabla_{zz}$   $\vdots + (l_2 m_3 + l_3 m_2) \nabla_{xy} + (m_3 h_2 + m_2 h_3) \partial_{yz}$   $\vdots + (n_2 l_3 + n_3 l_2) \partial_{xy}$   $\vdots + (n_2 l_3 + n_3 l_2) \partial_{xy}$   $\vdots + (n_2 l_3 + n_3 l_2) \partial_{xy}$ 

Principal Stresses:

There exist three mutually perpendicular planes at the Point on which the shear stresses <u>vanish</u>

The remaining three normal stresses components on these three planes are called principal stresses.

Here the principal plane has a unit normal vector:

$$\Rightarrow \boxed{\overrightarrow{O_{p_1}} = \overrightarrow{O_{p_1}} \overrightarrow{N}} = \overrightarrow{O_{p_2}} \overrightarrow{N} = \overrightarrow{O_{p_3}}$$

$$\Rightarrow \boxed{\overrightarrow{O_{p_1}} = \overrightarrow{O_{p_1}} \overrightarrow{N}} = \overrightarrow{O_{p_2}} \overrightarrow{N}$$

$$\Rightarrow \boxed{\overrightarrow{O_{p_1}} = \overrightarrow{O_{p_2}} \overrightarrow{N}} = \overrightarrow{O_{p_3}} \overrightarrow{N}$$

$$\Rightarrow \boxed{\overrightarrow{O_{p_1}} = \overrightarrow{O_{p_2}} \overrightarrow{N}} = \overrightarrow{O_{p_3}} \overrightarrow{N}$$

$$\Rightarrow \boxed{\overrightarrow{O_{p_1}} = \overrightarrow{O_{p_2}} \overrightarrow{N}} = \overrightarrow{O_{p_3}} \overrightarrow{N}$$

$$\Rightarrow \sigma_{px}i + \sigma_{py}i + \sigma_{pz}k$$

$$= \sigma(li+mi+nk)$$

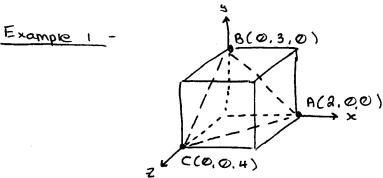
$$\sigma_{px} = \sigma l$$

$$\sigma_{py} = \sigma m$$

$$\sigma_{pz} = \sigma n$$

$$\Rightarrow \begin{cases} \nabla p_x = l \sigma_{xx} + m \sigma_{xy} + n \sigma_{xz} = \sigma l \\ \sigma_{py} = l \sigma_{yx} + m \sigma_{yy} + n \sigma_{yz} = \sigma_{m} \\ \sigma_{pz} = l \sigma_{zz} + m \sigma_{zy} + n \sigma_{zz} = \sigma_{n} \end{cases}$$

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Find the unit normal vector of the plane through A. B., and C.

Solution: 
$$0x + by + Cz = d$$

The normal vector is  $(a, b, c)$ 

A  $(2, 0, 0)$   $2a + 0 + 0 = d$ ;  $a = d/2$ 

B  $(0, 3, 0)$   $0 + 3b + 0 = d$ ;  $b = d/3$ 

C  $(0, 0, 4)$   $0 + 0 + 4c + d$ ;  $c = d/4$ 

=>  $1/2 + 1/3 + 1/4 = 1$ 

The normal vector  $(\frac{1}{2}, \frac{1}{3}, \frac{1}{4})$ Length =  $\sqrt{(\frac{1}{2})^2 + (\frac{1}{3})^2 + (\frac{1}{4})^2}$ ... the unit normal vector is:  $(\frac{1}{2}, \frac{1}{3}, \frac{1}{4})$ 

Given by

The state of stress at a point is

Unit: KPa

Determine the stress vector on the plane with unit normal vectors:

N = 1/2i + 1/2i + 1/2 R

```
Also find the normal stress and shear stress
  Solution: Oxx = -50 Oxy = -20 Oxz = 40
              Tyx = -20 Tyy = 20 Tyz = 10
              Ozx = 40 Ozy = 10 Ozz = 30
 and: l = 1/2 m = 1/2 n = 1/2
  Stress vector: Op = Opzi + Opy i + Opzil
        Here
    OPE = LOXX + M Dxy + N Dxz
        = (\sqrt[4]{2})(-50) + (\sqrt[4]{2})(-20) + (\sqrt[4]{2})(40)
        = -25.36
   Jpg = logz + Mogy + Nogz
        = (1/12)(-20) + (1/2)(20) + (1/2)(10)
        = 0.8579
  JPZ = lozx + mozy + nozz
       = (1/12)(40) + (1/2)(10) + (1/2)(30)
       = 48.78
.. Jo = -25.36 i + 0.8579 3 + 48.78 R
 Mormal Stress
  JPN = 1 ° Jxx + M2 Jyy + N2 Jzz
  ··· + 2lm Oxy + 2mn Gyz + 2nl Ozx
     = (1/\sqrt{2})^2(-50) + (1/2)^2(20) + (1/2)^2(30) ...
    ... + (2)(\sqrt{2} \times 1/2)(-20) + (2)(1/2)(1/2)(10) ...
    ··· (2)(12)(1/v2)(40)
```

Shear stress:

Ops = V Opx + Opy + Op2 - Op2