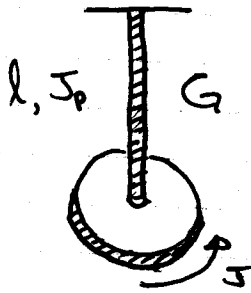


$$k = \frac{AE}{l}$$



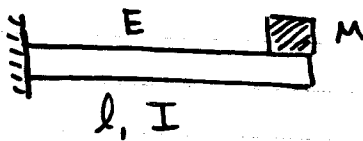
$$k = \frac{GJ_p}{l}$$

$$\omega_n = \sqrt{\frac{k}{J}}$$

natural frequency

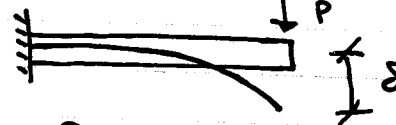
moment of inertia of disk

shorter spring, smaller "n", stronger spring  
longer spring, larger "n", softer spring



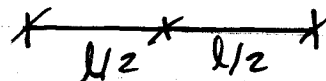
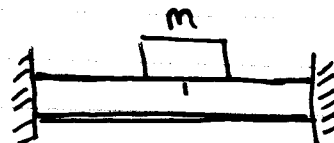
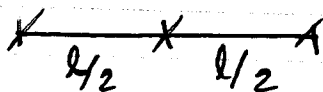
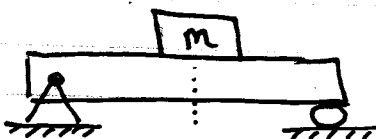
$$k = \frac{3EI}{l^3}$$

$$\omega_n = \sqrt{\frac{k}{m}}$$



$$\delta = \frac{Pl^3}{3EI}$$

$$P = \frac{3EI}{l^3} \delta$$



Page 53, table 1.3

Example

Consider front of airplane :

No Fuel,  $m = 10 \text{ kg}$ Full Fuel,  $m = 1000 \text{ kg}$ 

$$I = 5.2 \times 10^{-5}$$

$$l = 2 \text{ m}$$

$$E = 6.9 \times 10^9 \text{ Pa}$$

→ Find the Freq. of the wing for the two cases

Solution :

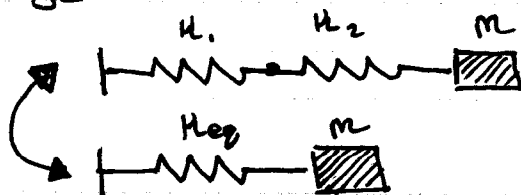
$$\begin{aligned} \text{Full Fuel, } \omega_n &= \sqrt{\frac{k}{m}} = \sqrt{\frac{3EI}{ml^3}} \\ &= \sqrt{\frac{(3) \times (6.9 \times 10^9) \times (5.2 \times 10^{-5})}{(1000) \times (2)^3}} \end{aligned}$$

$$\begin{aligned} \omega_n &= 11.6 \text{ rad/s} \\ \text{No Fuel, } \omega_n &= \sqrt{\frac{(3)(6.9 \times 10^9)(5.2 \times 10^{-5})}{(10)(2)^3}} \\ \omega_n &= 115 \text{ rad/s} \end{aligned}$$

↳ this doesn't consider mass of wing

Combining Springs

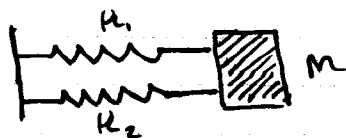
→ series



Each spring has the same force.

$$K_{eq} = \frac{1}{1/K_1 + 1/K_2} = \frac{K_1 K_2}{K_1 + K_2}$$

→ Parallel

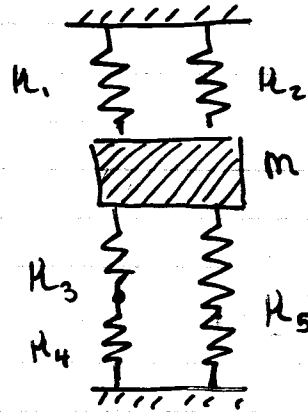


Each spring has the same deformation

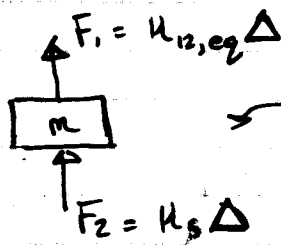
$$K_{eq} = K_1 + K_2$$

Example :

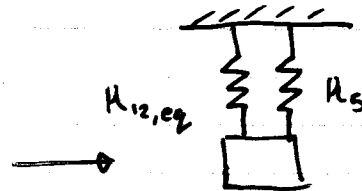
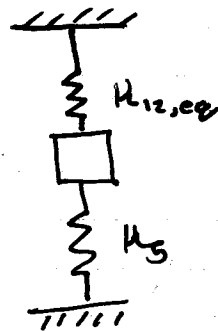
Find the equivalent stiffness ( $K_{eq}$ ) :



Solution :



consider :

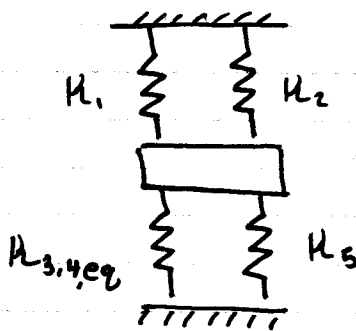


Thus, Same deformation

$$F = F_1 + F_2 = (K_{12,eq} + K_5) \Delta = K_{eq}$$

Springs  $K_3$  and  $K_4$  are in series.

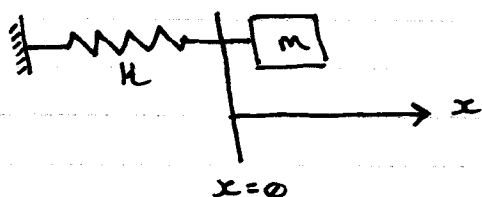
$$K_{34,eq} = \frac{K_3 K_4}{K_3 + K_4}$$



$K_1$ ,  $K_2$ ,  $K_{34,eq}$  and  $K_5$  are in parallel.

$$\begin{aligned} K_{eq} &= K_1 + K_2 + K_5 + K_{34,eq} \\ &= K_1 + K_2 + K_5 + \frac{K_3 K_4}{K_3 + K_4} \end{aligned}$$

# Harmonic motion



$$m\ddot{x} + kx = 0$$

(where:  $\omega_n = \sqrt{\frac{k}{m}}$ )

(Divide by  $m$ )  $\ddot{x} + \frac{k}{m}x = 0$

(Replace)  $\ddot{x} + \omega_n^2 x = 0$

Displacement:  $x = A \sin(\omega_n t + \phi)$

Velocity:  $\dot{x} = \omega_n A \cos(\omega_n t + \phi)$

Acceleration:  $\ddot{x} = -\omega_n^2 A \sin(\omega_n t + \phi) = -\omega_n^2 x$

Max displacement:  $x_{\max} = A$

Max velocity:  $v_{\max} = \omega_n A$  (or when  $\cos(\omega_n t + \phi) = 1$ )

Max acceleration:  $a_{\max} = \omega_n^2 A$  (or when  $x = A$ )

Complex number

$$c = a + ib$$

$$i = \sqrt{-1}$$

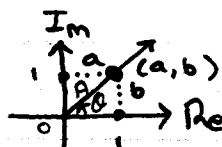
where  $a = A \cos \theta$

$b = A \sin \theta$

then  $c = A \cos \theta + i A \sin \theta = A(\cos \theta + i \sin \theta)$

$$c = A e^{i\theta}$$

$$e^{i\theta} = \cos \theta + i \sin \theta$$



Differential equation

$$m\ddot{x} + kx = 0$$

Solution of the ODE

$$x(t) \approx e^{\lambda t}$$

$$\dot{x} = \lambda e^{\lambda t} = \lambda x(t)$$

$$\ddot{x} = \lambda \dot{x} = \lambda^2 x(t)$$

Substitution:  $m\lambda^2 x(t) + kx(t) = 0$

$$(m\lambda^2 + k)x(t) = 0$$

(5)

Since  $x(t) \neq 0$

$$m\lambda^2 + k = 0$$

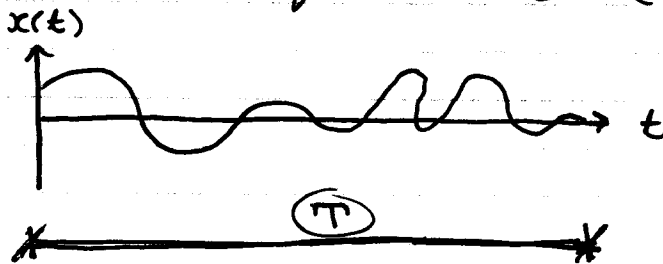
$$\rightarrow \lambda = \pm \sqrt{-k/m} = \pm i\sqrt{k/m}$$

$$\lambda = \pm i\omega_n$$

$$x(t) = a_1 e^{i\omega_n t} + a_2 e^{-i\omega_n t} \quad ; \quad a_1 \text{ and } a_2 \text{ are constant}$$

$$x(t) = A \sin(\omega_n t + \phi)$$

Root mean square values (RMS):

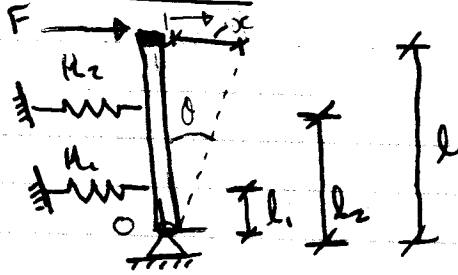


$$\lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T x(t) dt = \bar{x} \quad \text{average value}$$

$$\bar{x}^2 = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T x^2(t) dt \quad \text{mean square value}$$

$$x_{rms} = \sqrt{\bar{x}^2}$$

9/11/19

**Example**

Find the equivalent stiffness of the system that relates the applied force to the resulting displacement  $x$

$$F = K_{eq} x$$

Solution potential energy in the real system equals to the energy stored in the equivalent spring:

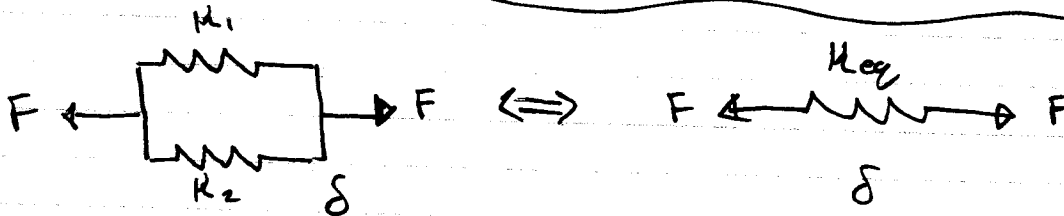
For small disp.  $x$ , angle  $\theta$  is small as well.  
 $x_1 = l_1 \theta$  ;  $x_2 = l_2 \theta$  (only when  $\uparrow$ )

$$(1/2)K_1 x_1^2 + (1/2)K_2 x_2^2 = (1/2)K_{eq} x^2$$

Since  $x = l\theta$ :

$$(1/2)K_1 (l_1 \theta)^2 + (1/2)K_2 (l_2 \theta)^2 = (1/2)(l\theta)^2 K_{eq}$$

$$K_{eq} = K_1 (l_1/l)^2 + K_2 (l_2/l)^2$$



$$(1/2)K_1 \delta^2 + (1/2)K_2 \delta^2 = (1/2)K_{eq} \delta^2$$

## The decibel dB scale

measure the vibration relative to some reference value:

$$10 \log_{10} \left( \frac{x}{x_0} \right)^2 \leftarrow \text{dB}$$

Reference power  $P_0$ , the sound produces twice as much as the reference.

IF  $P = 2P_0$ :

$$10 \log_{10} (P/P_0) = 10 \log_{10} 2 = 3 \text{ dB}$$

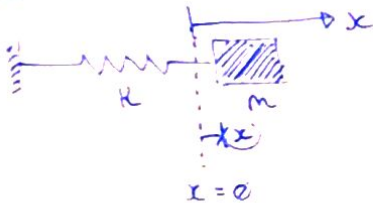
IF  $P = 10P_0$ :

$$10 \log_{10} 10 = 10 \text{ dB}$$

IF  $P = 10^6 P_0$ :

$$10 \log_{10} (10^6) = 60 \text{ dB}$$

## Modeling and Energy Methods



Potential energy

$$\rightarrow U = (1/2) k x^2$$

Kinetic energy

$$\rightarrow T = (1/2) m \dot{x}^2$$

For rotating about a fixed axis:

$$\rightarrow T = (1/2) J \dot{\theta}^2$$

Conservation of energy:

$$\rightarrow T + U = \text{const.}$$

$$T_1 + U_1 = T_2 + U_2$$

$$T_{\max} = U_{\max}$$

$$d/dt (T + U) = 0$$

Spring-mass:



$$T = (1/2) m \dot{x}^2$$

$$U = (1/2) k x^2$$

$$d/dt (T + U) = 0$$

$$\rightarrow d/dt ((1/2) m \dot{x}^2 + (1/2) k x^2) = 0$$

$$1/2 m \cdot 2 \dot{x} d\dot{x}/dt + 1/2 k \cdot 2x dx/dt = 0$$

$$m \dot{x} \ddot{x} + k x \dot{x} = 0$$

$$\dot{x} (m \ddot{x} + k x) = 0$$

Since  $\dot{x}$  cannot be zero all the time,

$$\rightarrow m\ddot{x} + kx = 0$$

**Example** Find the natural frequency from the energy:



The displacement :  $x = A \sin(\omega_n t + \phi)$   
 $x_{\max} = A$

Velocity :  $\dot{x} = A\omega_n \cos(\omega_n t + \phi)$   
 $\dot{x}_{\max} = A\omega_n$

$T_{\max} : \frac{1}{2}m(\dot{x}_{\max})^2 = \frac{1}{2}m(A\omega_n)^2$

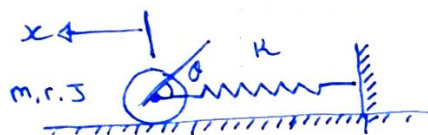
$U_{\max} : \frac{1}{2}k(x_{\max})^2 = \frac{1}{2}kA^2$

Since  $T_{\max} = U_{\max}$ ;

$$\frac{1}{2}m(A\omega_n)^2 = \frac{1}{2}kA^2$$

$$\omega_n = \sqrt{k/m}$$

**Example**



Assume it is a conservative system and rolls without slipping  
 Find the natural frequency of the disk.

Solution: rolling w/o slipping

$$x = r\theta$$

$$(x = A \sin(\omega_n t + \phi))$$

$$\dot{\theta} = \dot{x}/r$$

The kinetic energy

$$\begin{aligned} T &= \frac{1}{2}J\dot{\theta}^2 + \frac{1}{2}m\dot{x}^2 \\ &= \frac{1}{2}J(\dot{x}/r)^2 + \frac{1}{2}m\dot{x}^2 \\ &= \frac{1}{2} \underbrace{\left[ \left( \frac{J}{r^2} \right) + m \right]}_{\text{equivalent mass}} \dot{x}^2 \end{aligned}$$

$$\therefore T_{\max} = \frac{1}{2} \left[ \left( \frac{J}{r^2} \right) + m \right] (A\omega_n)^2$$



Potential energy

$$U = (1/2) K x^2$$

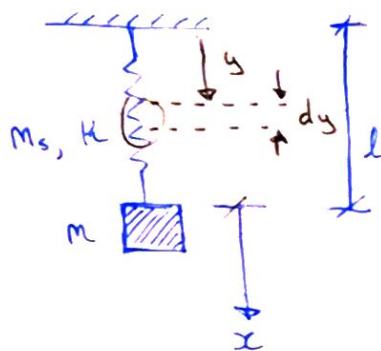
$$U_{\max} = (1/2) K A^2$$

$$\Rightarrow (1/2) \left[ \left( \frac{3}{l^2} \right) + m \right] (A \omega_n)^2 = (1/2) K A^2$$

$$\Rightarrow \omega_n = \sqrt{\frac{K}{\left( \frac{3}{l^2} \right) + m}}$$

**Example**

The effect of including the mass of the spring on the value of the frequency



Solution: The mass per unit length of the spring

$$\frac{m_s}{l}$$

The mass element  $dy$ :

$$\frac{m_s}{l} dy$$

the velocity:

$$\frac{y}{l} \dot{x}$$

Assumptions

$$\begin{aligned} T_s &= \int_0^l (1/2) \left[ \left( \frac{m_s}{l} \right) dy \right] \left[ \left( \frac{y}{l} \right) \dot{x} \right]^2 \\ &= \left( \frac{1}{2} \right) \frac{m_s}{l} \left( \frac{\dot{x}}{l} \right)^2 \int_0^l y^2 dy \\ &= (1/2) (m_s/3) \dot{x}^2 \end{aligned}$$

The total kinetic energy:

$$T = (1/2) (m_s/3) \dot{x}^2 + (1/2) m \dot{x}^2$$

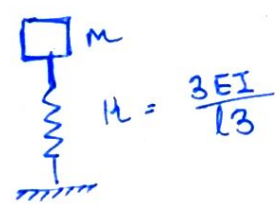
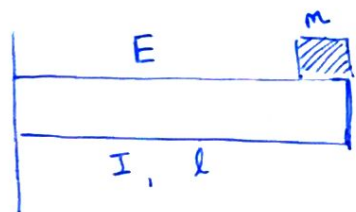
$$T = (1/2) \left[ (m_s/3) + m \right] \dot{x}^2$$

$$\rightarrow T_{\max} = (1/2) (m_s/3 + m) (A \omega_n)^2$$

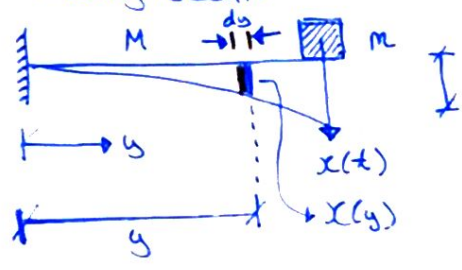
$$U_{\max} = (1/2) K A^2$$

$$\rightarrow T_{\max} = U_{\max}$$

$$\omega_n = \sqrt{\frac{K}{\left( \frac{m_s}{3} + m \right)}}$$



"Heavy beam"



The deflection at position y is:

$$x(y) = \frac{Py^2(3l-y)}{6EI}$$

The maximum deflection occurs at  $y = l$

$$x_{\max} = \frac{Pl^3}{3EI} \quad ; \quad P = \left( \frac{3EI}{l^3} \right) x_{\max}$$

$$\rightarrow x(y) = \frac{3EI}{l^3} x_{\max} \cdot \frac{y^2}{6EI} (3l-y)$$

$$= \frac{y^2}{2l^3} (3l-y) \cdot x_{\max}$$

$$\dot{x}(y) = \frac{y^2(3l-y)}{2l^3} \dot{x}_{\max}$$

For a small beam segment  $dy$ ,

$$T_{\text{beam}} = \int_0^l \left( \frac{1}{2} \right) \left( \frac{M}{l} dy \right) (\dot{x}(y))^2$$

$$\Rightarrow \int_0^l \left( \frac{1}{2} \right) \left( \frac{M}{l} dy \right) \left( \frac{y^2(3l-y)}{2l^3} \dot{x}_{\max} \right)^2$$

$$= \left( \frac{1}{2} \right) \left( \frac{33}{140} M \right) \dot{x}_{\max}^2$$

The total kinetic energy:

$$\rightarrow T = \left( \frac{1}{2} \right) \left[ \left( \frac{33}{140} M \right) + m \right] \dot{x}_{\max}^2$$

The equivalent mass of the system is:

$$\rightarrow M_{\text{eq}} = \left( \frac{33}{140} M \right) + m$$

$$\therefore \omega_n = \sqrt{\frac{\frac{3EI}{l^3}}{\frac{33}{140} M + m}}$$