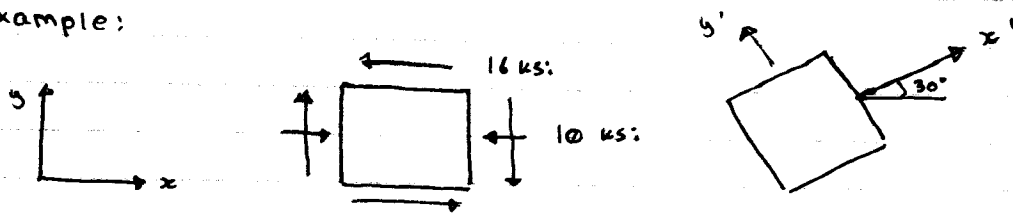


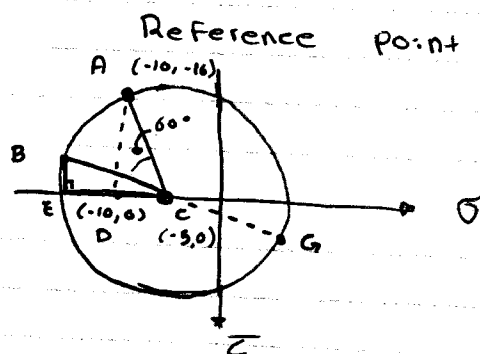
Example:



Determine the equivalent state of stress of an element if it is oriented 30° ccw from the element shown

Sol: $\sigma_x = -10$ $\sigma_y = 0$ $\tau_{xy} = -16$
 $\sigma_{avg} = \frac{\sigma_x + \sigma_y}{2} = \frac{-10 + 0}{2} = -5$

\therefore Centre = C (-5, 0)



$\sigma_x = -10$
 $\sigma_y = 0$
 $\tau_{xy} = -16$
 $\sigma_{avg} = -5$
 $R =$

$\Delta ACD \rightarrow CD = 5$ $AD = 16$

$\tan \angle ACD = \frac{AD}{CD} = \frac{16}{5}$

$\angle ACD = 72.646^\circ$

$\angle BCE = \angle ACD - \angle ACB = 72.646^\circ - 60^\circ = 12.646^\circ$

Since $BC = AC = R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$
 $= \sqrt{\left(\frac{-10 - 0}{2}\right)^2 + (-16)^2} = 16.763$

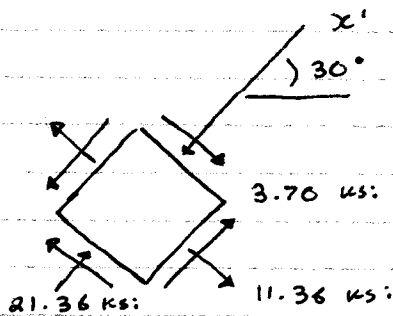
$\Delta BCE \rightarrow CE = BC \cos(\angle BCE) = 16.763 \cos(12.646^\circ)$
 $\therefore \sigma_{x'} = -(CE + OC) \Rightarrow -(16.763 \cos(12.646^\circ) + 5)$
 $= -21.36 \text{ ksi}$

$\tau_{x'y'} = -BE = -16.763 \sin(12.646^\circ)$
 $= -3.70 \text{ ksi}$

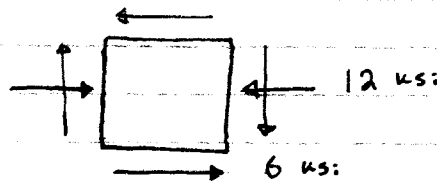
$$\frac{\sigma_B + \sigma_A}{2} = \sigma_c$$

$$\frac{\sigma_{x'} + \sigma_{y'}}{2} = \frac{\sigma_x + \sigma_y}{2}$$

$$\begin{aligned}\sigma_{y'} &= \sigma_x + \sigma_y - \sigma_{x'} \\ &= 10 + 0 - (-21.36) \\ &= 11.36 \text{ ksi}\end{aligned}$$



Example:



Determine the principal stresses and orientations.

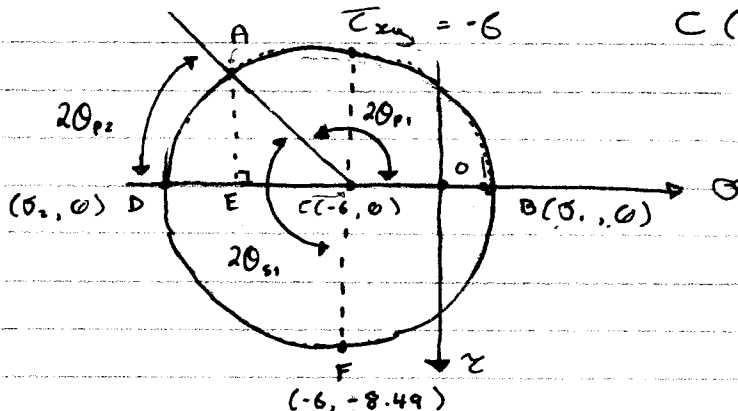
Solution: $\sigma_x = -12$

$\sigma_y = 0$

$\tau_{xy} = -6$

$$\sigma_{avg} = \frac{\sigma_x + \sigma_y}{2} = \frac{-12 + 0}{2} = -6$$

$C(-6, 0)$ $A(-12, -6)$



$$\begin{aligned}\text{Since } CA = R &= \sqrt{(-12 - (-6))^2 + (-6 - 0)^2} \\ &= 8.49\end{aligned}$$

$$\therefore \sigma_1 = R - 104 = 8.49 - 6 = 2.49 \text{ ksi}$$

$$\sigma_2 = -(R + 104) = -(8.49 - 6) = -14.49 \text{ ksi}$$

$$\triangle ACE : AE = 6 \quad CE = 6$$

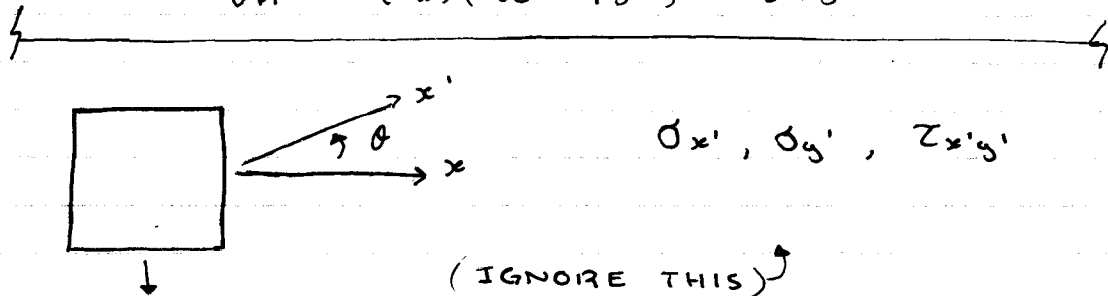
$$\therefore \tan \angle ACE = \frac{AE}{CE} = \frac{6}{6} = 1$$

$$\angle ACE = 45^\circ$$

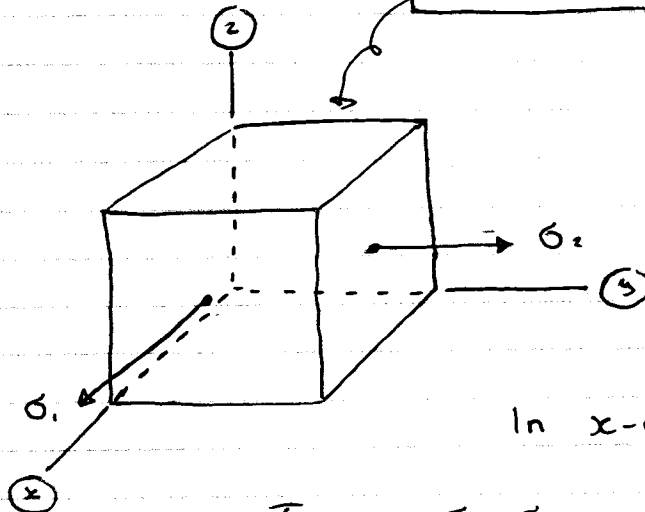
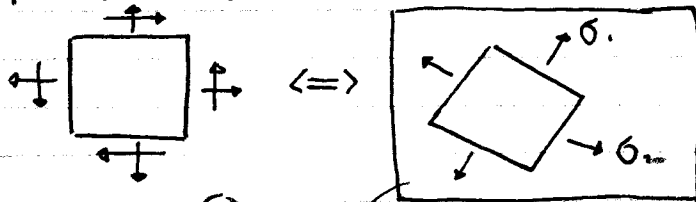
$$\therefore \theta_{p_2} = +(\frac{1}{2})\angle ACE = 22.5^\circ$$

and

$$\theta_{p_1} = -(\frac{1}{2})(180^\circ - 45^\circ) = -67.5^\circ$$

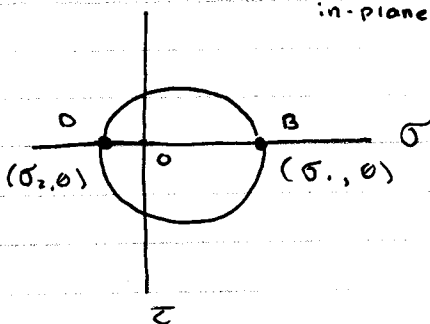
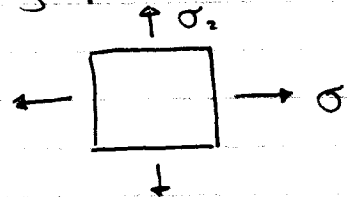


9.5 - Absolute Maximum Shear Stress Plane Stress

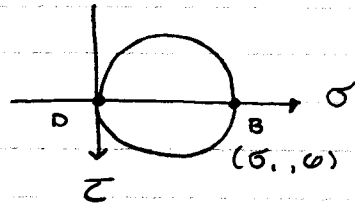
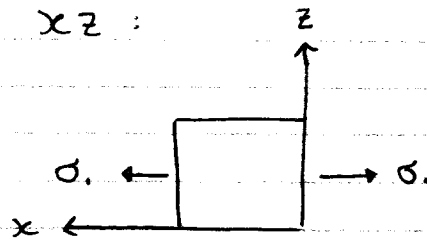


In x-y plane:

$$\tau_{\max \text{ in-plane}} = \frac{\sigma_1 - \sigma_2}{2}$$

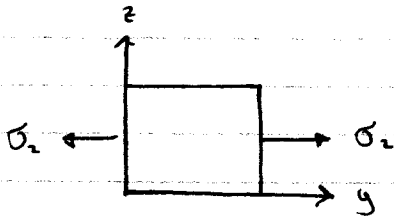


In xz :



$$\tau_{\max \text{ in-plane}} = \frac{\sigma_1}{2}$$

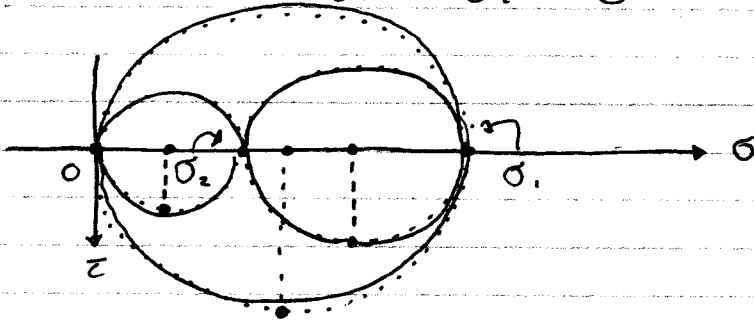
In yz :



$$\tau_{\max \text{ in-plane}} = \frac{\sigma_2}{2}$$

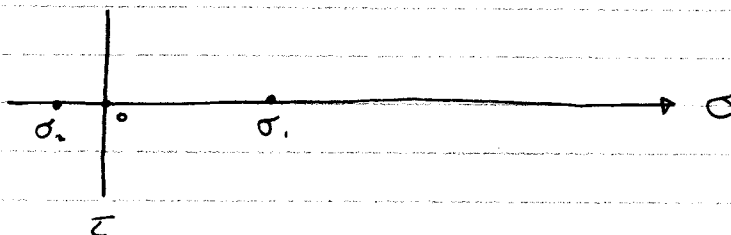
$$\tau_{\max \text{ abs}} = \max \left(\left| \frac{\sigma_1}{2} \right|, \left| \frac{\sigma_2}{2} \right|, \left| \frac{\sigma_1 - \sigma_2}{2} \right| \right)$$

Case 1: $\sigma_1 > \sigma_2 > 0$



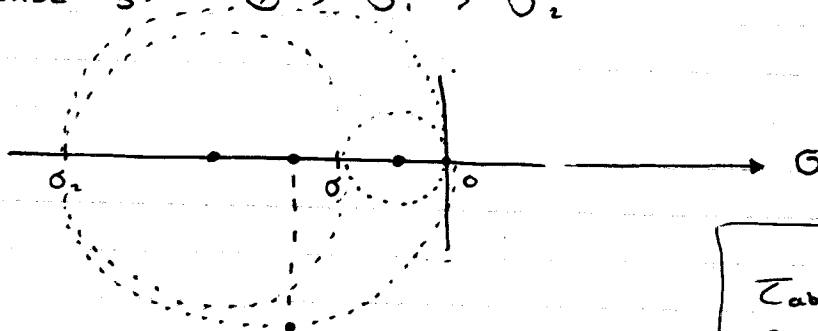
$$\tau_{\max \text{ abs}} = \frac{\sigma_1}{2}$$

Case 2: $\sigma_1 > 0 > \sigma_2$

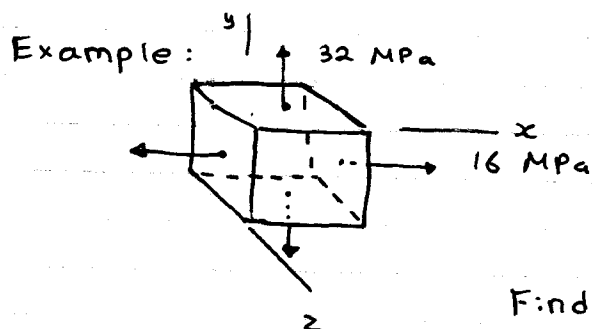


$$\tau_{\max \text{ abs}} = \frac{\sigma_1 - \sigma_2}{2}$$

CASE 3: $0 > \sigma_1 > \sigma_2$



$$\tau_{abs \max} = -\frac{\sigma_2}{2}$$



Find the absolute max shear stress.

Solution: Since

$$\sigma_1 = 32 \text{ MPa}$$

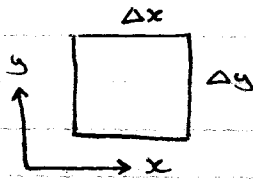
$$\sigma_2 = 16 \text{ MPa}$$

$$\sigma_1 > \sigma_2 > 0$$

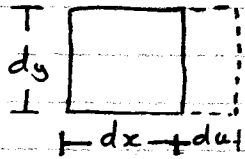
$$\therefore \tau_{abs \max} = \frac{\sigma_1}{2} = \frac{32}{2} = 16 \text{ MPa}$$

$$\text{and } \tau_{\max \text{ in-plane}} = \frac{\sigma_1 - \sigma_2}{2} = \frac{32 - 16}{2} = 8 \text{ MPa}$$

Ch. 10 - Strain Transformation 10.1 Plane Strain



Sign convention notes:
elongation : (+)
compression : (-)



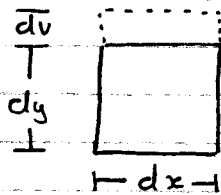
$\epsilon_x = \frac{du}{dx}$ = Normal strain
of a line segment
in x-direction

3.72

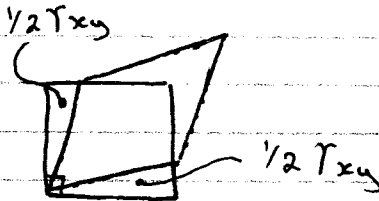
4.43

6.62

7.3



$\epsilon_y = \frac{dv}{dy}$ = Normal strain
of a line segment
in y-direction

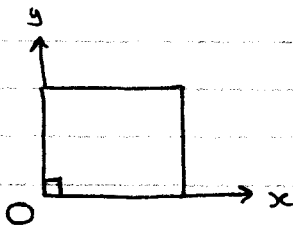


γ_{xy} = the shear strain

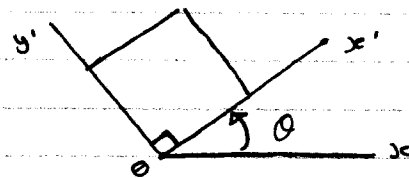
10.2 General Equations of plane-strain transformation Sign convention :

Normal strain: positive if elongation

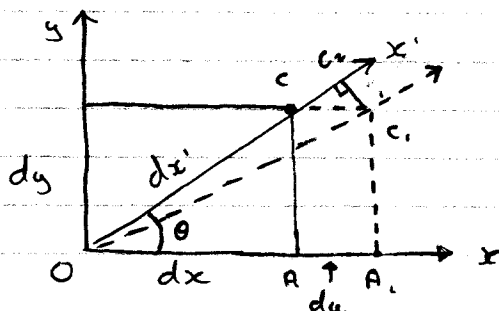
Shear strain: positive if the deformed
angle is less than 90°



$\epsilon_x, \epsilon_y, \gamma_{xy}$



$\epsilon_{x'}, \epsilon_{y'}, \gamma_{x'y'}$



$$\begin{cases} dx = \cos\theta \cdot dx' \\ dy = \sin\theta \cdot dx' \end{cases}$$

$$\epsilon_x = \frac{du}{dx}$$

ΔCC_1C_2 : $\angle C_1CC_2 = \theta$ $CC_1 = AA_1 = du$

$\therefore CC_2 = CC_1 \cos \theta = \cos \theta du$
 $C_1C_2 = CC_1 \sin \theta = \sin \theta du$

Normal Strain of OC :

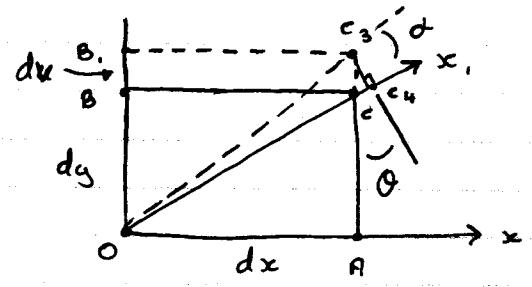
$E_{x'} = \frac{CC_2}{OC} = \frac{\cos \theta du}{dx'}$

ΔOC_1C_2 :

angle is clockwise
 $\tan \alpha = - \frac{C_1C_2}{OC_1} = - \frac{C_1C_2}{OC + CC_2} = - \frac{C_1C_2}{OC}$

Since α is small :

$\alpha \approx \tan \alpha = - \frac{C_1C_2}{OC} = - \frac{\sin \theta du}{dx'}$

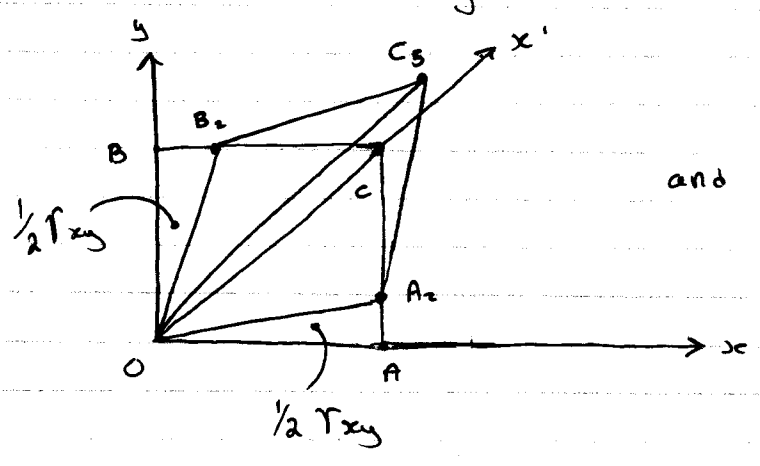


ΔCC_3C_4

$CC_4 = CC_3 \sin \theta = \sin \theta dv$
 $C_3C_4 = CC_3 \cos \theta = \cos \theta dv$

$E_{x'} = \frac{CC_4}{OC} = \frac{\sin \theta dv}{dx'}$, $\beta = \frac{C_3C_4}{OC} = \frac{\cos \theta dv}{dx'}$

$E_y = \frac{dv}{dy}$



Horizontal displacement :

$BB_2 = \frac{1}{2} T_{xy} dy$

and Vertical displacement :

$AA_2 = \frac{1}{2} T_{xy} dx$

Normal Strain of OC

$$E_{x'} = \frac{\cos \theta}{dx'} \cdot \frac{1}{2} \tau_{xy} dy + \frac{\sin \theta}{dx'} \cdot \frac{1}{2} \tau_{xy} dx$$

Rotation

$$\alpha = -\frac{\sin \theta}{dx'} \cdot \frac{1}{2} \tau_{xy} dy + \frac{\cos \theta}{dx'} \cdot \frac{1}{2} \tau_{xy} dx$$

Total normal strain

$$E_{x'} = \frac{\cos \theta}{dx'} du + \frac{\sin \theta}{dx'} dv + \frac{\cos \theta}{dx'} \cdot \frac{1}{2} \tau_{xy} dy + \frac{\sin \theta}{dx'} \cdot \frac{1}{2} \tau_{xy} dx$$

$$\text{Since } E_x = \frac{du}{dx} \Rightarrow du = E_x dx$$

$$E_y = \frac{dv}{dy} \Rightarrow dv = E_y dy$$

$$\Rightarrow E_{x'} = \cos \theta \cdot E_x \frac{dx}{dx'} + \sin \theta E_y \frac{dy}{dy'} + \frac{1}{2} \tau_{xy} \cos \theta \frac{dy}{dx'} + \frac{1}{2} \tau_{xy} \sin \theta \frac{dx}{dx'}$$

$$\frac{dx}{dx'} = \cos \theta \quad \frac{dy}{dy'} = \sin \theta$$

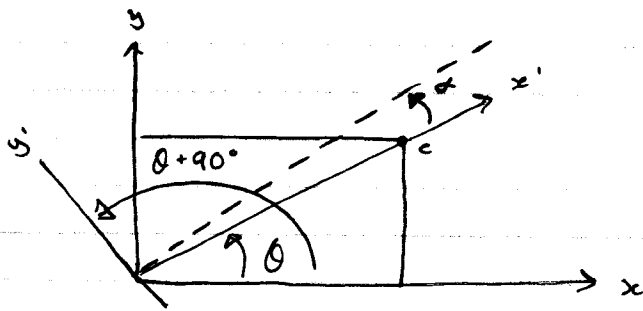
$$E_{x'} = E_x \cos^2 \theta + E_y \sin^2 \theta + \tau_{xy} \sin \theta \cos \theta$$

Rotation of x' axis (OC)

$$\alpha = -\sin \theta \frac{du}{dx'} + \cos \theta \frac{dv}{dx'}$$

$$= -\frac{1}{2} \tau_{xy} \sin \theta \frac{dy}{dx'} + \frac{1}{2} \tau_{xy} \cos \theta \frac{dx}{dx'}$$

$$= (E_y - E_x) \sin \theta \cos \theta + \frac{1}{2} \tau_{xy} (\cos^2 \theta - \sin^2 \theta)$$



$$\begin{aligned}
 & E_x, E_y, \tau_{xy} \\
 \therefore E_{y'} &= E_x \cos^2(\theta + 90^\circ) + E_y \sin^2(\theta + 90^\circ) \\
 & \quad + \tau_{xy} \sin(\theta + 90^\circ) \cos(\theta + 90^\circ) \\
 &= E_x \sin^2 \theta + E_y \cos^2 \theta - \tau_{xy} \sin \theta \cos \theta
 \end{aligned}$$

$$\begin{aligned}
 \beta &= (E_y - E_x) \sin(\theta + 90^\circ) \cos(\theta + 90^\circ) \\
 & \quad + \frac{1}{2} \tau_{xy} (\cos^2(\theta + 90^\circ) - \sin^2(\theta + 90^\circ)) \\
 &= -(E_y - E_x) \sin \theta \cos \theta + \frac{1}{2} \tau_{xy} (\sin^2 \theta - \cos^2 \theta)
 \end{aligned}$$

$$90^\circ \rightarrow 90^\circ - \alpha + \beta$$

The shear strain

$$\begin{aligned}
 \tau_{x'y'} &= 90^\circ - (90^\circ - \alpha + \beta) \\
 &= \alpha - \beta \\
 \tau_{x'y'} &= 2(E_y - E_x) \sin \theta \cos \theta + \tau_{xy} (\cos^2 \theta - \sin^2 \theta)
 \end{aligned}$$

$$E_{x'} = \frac{E_x + E_y}{2} + \frac{E_x - E_y}{2} \cos 2\theta + \frac{1}{2} \tau_{xy} \sin 2\theta$$

$$E_{y'} = \frac{E_x + E_y}{2} - \frac{E_x - E_y}{2} \cos 2\theta - \frac{1}{2} \tau_{xy} \sin 2\theta$$

$$\frac{\tau_{x'y'}}{2} = -\frac{(E_x - E_y)}{2} \sin 2\theta + \frac{\tau_{xy}}{2} \cos 2\theta$$

Stress \longleftrightarrow Strain

$$\sigma_x \longleftrightarrow E_x$$

$$\sigma_y \longleftrightarrow E_y$$

$$\tau_{xy} \longleftrightarrow \frac{1}{2} \tau_{xy}$$