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Example
$$\frac{3}{5}$$
 $\frac{1}{5}$ $\frac{1}{5$

 \widehat{A}

IF Substitute II and III in I =>
$$P_{\omega} A_{t} \begin{pmatrix} dh/dt \end{pmatrix} - P_{\omega} V_{t} A_{t} - P_{\omega} V_{z} A_{z} = \emptyset => \frac{dh}{dt} = \frac{Q_{t} - Q_{z}}{A_{z}}$$

$$\frac{dh}{dt} = \frac{A_{t}}{A_{t}} \left[V_{t} \frac{D_{t}^{2} \pi_{t}}{4} + V_{z} \frac{D_{z}^{2} \pi_{t}}{4} \right]$$

Where
$$D_1 = 1$$
 in $D_2 = 3$:n

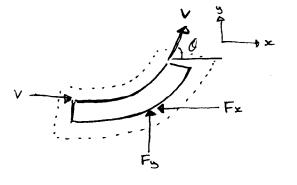
 $V_1 = 3 + 1$ for $\frac{dh}{dt} = \frac{1}{2} \left[3 \left(\frac{\pi}{4} \right) \left(\frac{1}{12} \right)^2 + (2) \left(\frac{\pi}{4} \right) \left(\frac{1}{12} \right)^2 \right]$
 $V_2 = 2 + 1$ for $A_1 = 2 + 1$

Example
$$Z\bar{f} = \frac{\partial}{\partial t} \int_{cv} P \bar{v} \cdot dv + \int_{cs} P \bar{v} (\bar{v} \cdot \bar{n}) dA$$
 $x: Zf_x = \frac{\partial}{\partial t} \int_{cv} P u d\bar{v} + \int_{cs} P u (\bar{v} \cdot \bar{n}) dA$
 $y: Zf_y = \frac{\partial}{\partial t} \int_{cv} P v d\bar{v} + \int_{cs} P v (\bar{v} \cdot \bar{n}) dA$

$$-f_{x} = -\rho VVA, + \rho(V\cos\theta)VA_{2}$$

$$-f_{x} = -\rho V^{2}A + \rho V^{2}A\cos\theta$$

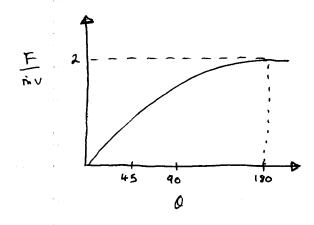
$$f_{x} = \rho V^{2}A(1-\cos\theta)$$

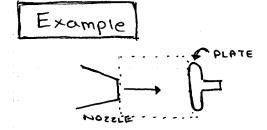


$$\frac{f_y = 0 + \rho(vs:n0)VAz}{f_y = \rho v^2 A s:n0}$$

b)
$$F = \sqrt{F_{x^{2}} + F_{5}^{2}} = \int \rho^{2} V^{4} A^{2} (1 - \cos \theta)^{2} + \rho^{2} V^{4} A^{2} \sin^{2} \theta \int^{1/2} d^{2} d^$$

- F = 2 m V sin(0/2)





$$\begin{array}{c} P_{\alpha} \\ P_{\alpha} \\$$

Special cases:

Steady Flow: ZF = Jes pV(V. R) dA

Mass Flow across inlet / putlet: m = Spe P(V-n) dAc = D Vong Ac

Momentum - Flux Correction Factor, β $\mathcal{E}F = \frac{d}{At} \int_{cv} \rho \nabla dN + \mathcal{E} \beta \dot{m} \nabla_{avg} - \mathcal{E} \beta \dot{m} \nabla_{avg}$ $\beta = \int_{Ae} \rho \nabla (\nabla \cdot \dot{n}) dAe \qquad (\beta \text{ always } \ge 1)$ $\dot{m} \nabla_{avg} \qquad (\beta \text{ close to } 1 \text{ for turbulent, not } 1)$ close For (aminor)

(momentum - Flux correction factor)

Example

$$V = 2V_{\text{ava}} \left(1 - \frac{r^{2}}{R^{2}}\right)$$

$$\beta = \frac{1}{H_{e}} \int_{A_{e}} \left(\frac{V_{\text{av}}}{V_{\text{av}}}\right)^{2} dA_{e} = \frac{\mu}{\pi R^{2}} \int_{0}^{R} \left(1 - \frac{r^{2}}{R^{2}}\right)^{2} 2\pi r dr$$

$$\Rightarrow \beta = \frac{\mu}{\pi R^{2}} \int_{A_{e}} \left(\frac{V_{\text{ava}}(1 - \frac{r^{2}}{R^{2}})}{V_{\text{ava}}}\right)^{2} 2\pi r dr$$

$$= \frac{8}{R^{2}} \int_{0}^{R} \left(1 - \frac{r^{2}}{R^{2}}\right) r dr = \frac{8}{R^{2}} \int_{1 - 2\frac{R^{2}}{R^{2}}} + \frac{r^{5}}{R^{4}} r dr$$

$$= \frac{8}{R^{2}} \left[\frac{r^{2}}{2} - \left(\frac{2}{R^{2}}\right)\left(\frac{r^{4}}{\mu}\right) + \left(\frac{r^{6}}{6R^{4}}\right)\right] \int_{0}^{R} dr$$

$$= \frac{8}{R^{2}} \left[\frac{R^{2}}{2} - \left(\frac{2}{R^{2}}\right)\left(\frac{R^{24}}{\mu}\right) + \left(\frac{R^{6}}{6R^{4}}\right)\right]$$

$$= \frac{8}{1.333}$$

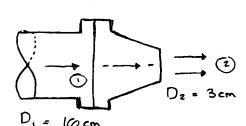
Steady linear momentum

EF = EBmV - EBmV

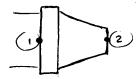
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One inlet and outlet:
$$\angle \vec{F} = m(\beta_2 \vec{V}_2 - \beta_1 \vec{V}_1)$$

$$F_x = \dot{m}(\beta_2 V_2 - \beta_1 V_1 \cos \theta)$$



$$Q = 1.5 \, \text{m}^3/\text{min} = 0.025 \, \text{m}^3/\text{s}$$

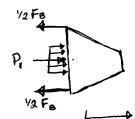


$$\frac{P_1}{\rho} + \frac{V_1^2}{2} + g_{Z_1}^2 = \frac{P_2}{\rho} + \frac{V_2^2}{2} + g_{Z_2}^2$$

$$V_{i} = \frac{Q_{i}}{A_{i}} = \frac{Q_{i}Q_{25}}{(\pi/4)(10\times10^{-2})^{2}} = 3.2 \,\text{m/s}$$

$$V_2 = \frac{Q}{A_2} = \frac{0.025}{(\pi/4)(3\pi 10^{-2})^2} = 35.4 \text{ m/s}$$

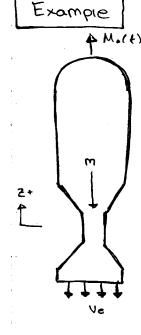
$$P_1 = (1/2)(1000)(35.4^2 - 3.2^2) = 6200000 Pa (gage)$$



620 KPa (gage)

$$\angle F_z = \dot{m}(V_z - V_i)$$

- $F_B + P_i P_i = \dot{m}(V_z - V_i)$



$$m(t) = M_0 + mt$$

$$(M_0 - mt)(g + \frac{dv}{dt}) = mve$$

$$g + \frac{dv}{dt} = \frac{mve}{M_0 - mt}$$

$$= dv = mve =$$

M = rF = rmax = mr2 x



Magnitude of torque: M = Smass 12 x & m
=> [Smass 12 & m] a = I x



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$$\frac{6-24}{V_{1}} = \frac{1}{45} + \frac{1}{45} + \frac{1}{45} = \frac{1}{12} + \frac{1}{12} = \frac{1}{12} = \frac{1}{12} + \frac{1}{12} = \frac{1$$

$$\frac{P_1}{p} + \frac{V_1^2}{2} + gZ_1 = \frac{P_2}{p} + \frac{V_2^2}{2} + gZ_2$$

$$V_1 = \frac{m}{PA_1} = \frac{(30 \text{ kg/s})}{(1000)(150 \times 10^{-4})} = 2 \text{ m/s}$$

$$V_{A} = \frac{\dot{m}}{PA_{2}} = \frac{(30 \text{ kg/s})}{(1000 \text{ X}25 \times 10^{-4})} = 12 \text{ m/s}$$

$$P_{1} = P(g(Z_{z}-Z_{1}) + \frac{Uz^{2}-U_{1}^{2}}{2}) = 1000(9.81(40 \text{ mg}^{-2}) + \frac{12^{2}-2^{2}}{2})$$

$$= 73.9 \times 10^{3} \text{ Pa}$$

9:
$$ZF_y = (\beta_1 \hat{m} \vee y_2) - (\beta_1 \hat{m} \vee y_1)$$

 $ZF_x = F_{P_1} - F_x$
 $F_{P_1} = P_1 P_1 = (73.9 \times 10^3)(150 \times 10^{-4})$

$$\begin{aligned}
\mathcal{E} F_{x} &= F_{0} - F_{x} \\
F_{p_{1}} &= P_{1} P_{1} = (73.9 \times 10^{3})(150 \times 10^{-4}) \\
(73.9 \times 10^{3})(150 \times 10^{-4}) - F_{x} &= (30)(1.03)(12(\cos 45^{\circ})) - 1.03(1)) \\
&= 30(1.03)(12\cos 45^{\circ} - 2)
\end{aligned}$$