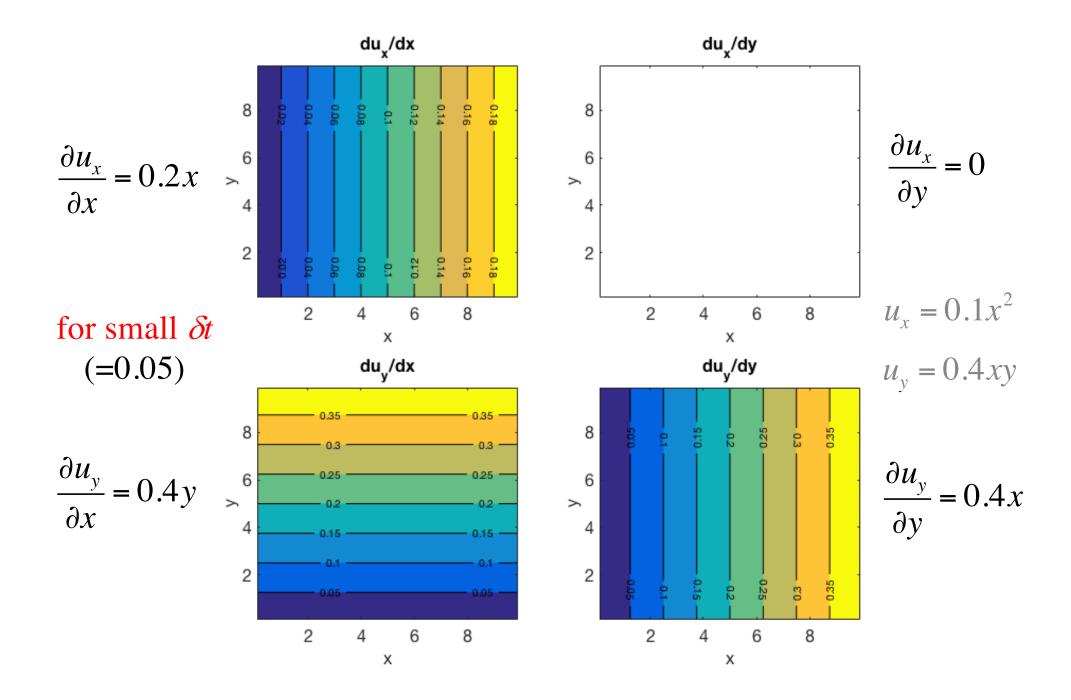
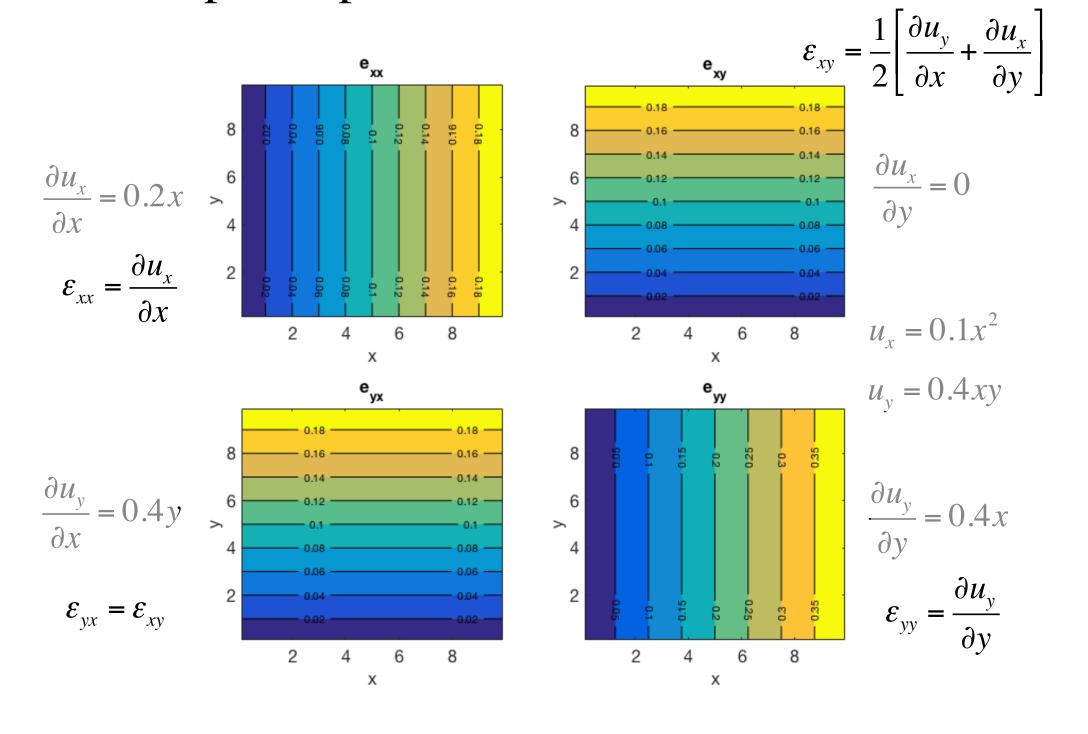
Learning Objectives

- Be able to use material and spatial descriptions of variables and their time derivatives.
- Be able to compute infinitesimal strain (strain rate) tensor given a displacement (velocity) field.
- Know meaning of the different components of the infinitesimal strain (rate) tensor
- Be able to find principal strain(rate)s and strain (rate) invariants and know what they represent
- Understand difference between infinitesimal and finite strain
- Be able to use the conservation of mass equation

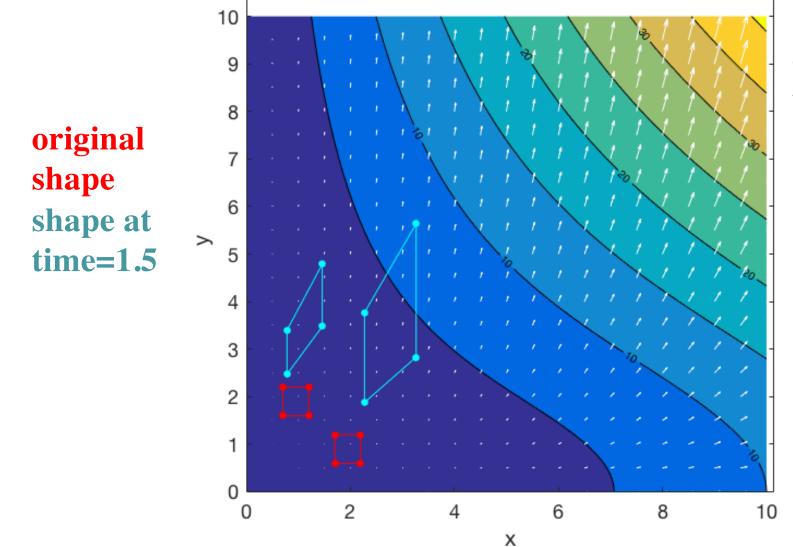
Example displacement – infinitesimal strain



Example displacement – infinitesimal strain



Deformation after finite strain

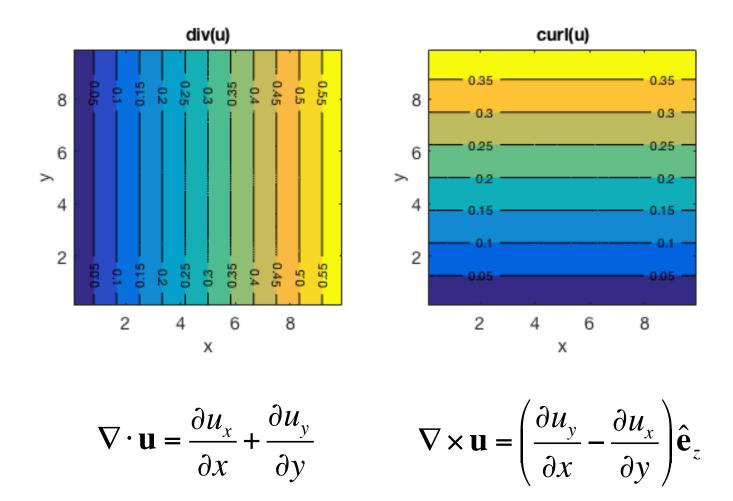


displacement in time interval =1

$$u_{r} = 0.1x^{2}$$

$$u_x = 0.1x^2$$
$$u_y = 0.4xy$$

Example displacement – infinitesimal strain



Try later: squarestrain.ipynb

Rotation tensor and rotation vector

For any antisymmetric tensor W, a corresponding *dual* or *axial vector* w can be found so that

$$\mathbf{W} \cdot \mathbf{a} = \mathbf{w} \times \mathbf{a}$$

How does vector w relate to the components of W?

$$\mathbf{w} = \hat{\mathbf{e}}_1 \qquad \hat{\mathbf{e}}_2 \qquad \hat{\mathbf{e}}_3$$

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How does vector w relate to the components of W?

$$\mathbf{W} = \begin{bmatrix} \hat{\mathbf{e}}_{1} & \hat{\mathbf{e}}_{2} & \hat{\mathbf{e}}_{3} \\ & & \\ -W_{12} & W_{13} \\ -W_{13} & W_{23} \end{bmatrix} \begin{pmatrix} \alpha_{1} \\ \alpha_{2} \\ & \\ -W_{13} & W_{23} \end{pmatrix} = \begin{pmatrix} \alpha_{2} W_{12} + \alpha_{3} W_{13} \\ & & \\ & & \\ -W_{13} & W_{23} \end{pmatrix} \xrightarrow{\mathbf{e}} \begin{pmatrix} \alpha_{2} W_{12} + \alpha_{3} W_{13} \\ & &$$

Rotation tensor and rotation vector

For any antisymmetric tensor **W**, a corresponding *dual* or *axial vector* **w** can be found so that

$$\mathbf{W} \cdot \mathbf{a} = \mathbf{w} \times \mathbf{a}$$

Vector w relates to the components of W as:

$$\mathbf{w} = -\mathbf{W}_{23}\hat{\mathbf{e}}_1 + \mathbf{W}_{13}\hat{\mathbf{e}}_2 - \mathbf{W}_{12}\hat{\mathbf{e}}_3$$

For the rotation tensor, an equivalent rotation vector exists:

$$\mathbf{\omega} \cdot \mathbf{dx} = \mathbf{r}_{\omega} \times \mathbf{dx}$$
 where: $\mathbf{r}_{\omega} = \frac{1}{2} \nabla \times \mathbf{u}$

Note that ω only describes the overall rigid body rotation, not the total rotation of each individual segment dx, which is also influenced by ε

infinitesimal strain tensor properties

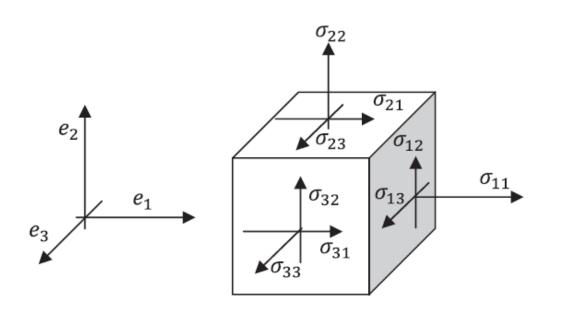
transform to fault plane coordinate frame:

$$\begin{array}{ll} \epsilon_{nn} & = \epsilon_{11} cos^2 \phi + \epsilon_{21} sin \phi cos \phi + \epsilon_{12} sin \phi cos \phi + \epsilon_{22} sin^2 \phi \\ \epsilon_{ns} & = \epsilon_{11} sin \phi cos \phi + \epsilon_{21} sin^2 \phi - \epsilon_{12} cos^2 \phi - \epsilon_{22} sin \phi cos \phi \end{array}$$

 ε_1 , ε_2 , ε_3 - *principal strains* : minimum, maximum and intermediate fractional length changes

isotropic, deviatoric strain: $\varepsilon_{ij} = (\theta/3)\delta_{ij} + \varepsilon'_{ij}$

- $tr(\varepsilon) = \theta = sum of normal strains=volume change$
- ε'_{ii} is deviatoric strain, change in shape, involves no change in volume
- $tr(\varepsilon') = 0$, does not imply $\varepsilon'_{ij} = 0$ for i=j
- $\varepsilon_{ij} = 0$ for $i \neq j$ does not ensure no volume change



Stress components

Reminder

traction on a plane

$$\mathbf{t} = \begin{bmatrix} \sigma_{11} & \sigma_{21} & \sigma_{31} \\ \sigma_{12} & \sigma_{22} & \sigma_{32} \\ \sigma_{13} & \sigma_{23} & \sigma_{33} \end{bmatrix} \cdot \hat{\mathbf{n}}$$

what is $\hat{\mathbf{e}}_1 \cdot \mathbf{t} = \hat{\mathbf{e}}_1 \cdot \mathbf{\sigma}^T \cdot \hat{\mathbf{n}}$? \mathbf{t}_1 on plane with normal $\hat{\mathbf{n}}$

what is $\hat{\mathbf{e}}_1 \cdot \boldsymbol{\sigma}^T \cdot \hat{\mathbf{e}}_1$? σ_{11}

what is $\hat{\mathbf{e}}_1 \cdot \mathbf{\sigma}^T \cdot \hat{\mathbf{e}}_2$? σ_{21}

$$\mathbf{\varepsilon} = \begin{bmatrix} \varepsilon_{11} & \varepsilon_{12} & \varepsilon_{13} \\ \varepsilon_{21} & \varepsilon_{22} & \varepsilon_{23} \\ \varepsilon_{31} & \varepsilon_{32} & \varepsilon_{33} \end{bmatrix}$$

$$\hat{\mathbf{e}}_1 \cdot \mathbf{\epsilon} \cdot \hat{\mathbf{e}}_1 = \varepsilon_{11}$$

$$\hat{\mathbf{e}}_1 \cdot \mathbf{\epsilon} \cdot \hat{\mathbf{e}}_2 = \varepsilon_{12}$$

 $\mathbf{\epsilon} \cdot \hat{\mathbf{p}} = \mathbf{p}'$ the unit vector $\hat{\mathbf{p}}$ after deformation by $\mathbf{\epsilon}$ $\hat{\mathbf{p}} \cdot \mathbf{\epsilon} \cdot \hat{\mathbf{p}} = \text{elongation by } \mathbf{\epsilon} \text{ of unit vector } \hat{\mathbf{p}} \text{ in direction } \hat{\mathbf{p}}$ $= \hat{\mathbf{p}} \cdot \mathbf{p}' = |\mathbf{p}'| \cos \alpha$

Strain Rate Tensor

In similar way as strain tensor, a tensor that describes the rate of change of deformation can be defined from **velocity gradient**:

$$\frac{\mathbf{D}}{\mathbf{D}t}\mathbf{dr} = \nabla \mathbf{v}$$

$$\nabla \mathbf{v} = \begin{bmatrix} \frac{\partial \mathbf{v}_1}{\partial \mathbf{x}_1} & \frac{\partial \mathbf{v}_1}{\partial \mathbf{x}_2} & \frac{\partial \mathbf{v}_1}{\partial \mathbf{x}_3} \\ \frac{\partial \mathbf{v}_2}{\partial \mathbf{x}_1} & \frac{\partial \mathbf{v}_2}{\partial \mathbf{x}_2} & \frac{\partial \mathbf{v}_2}{\partial \mathbf{x}_3} \\ \frac{\partial \mathbf{v}_3}{\partial \mathbf{x}_1} & \frac{\partial \mathbf{v}_3}{\partial \mathbf{x}_2} & \frac{\partial \mathbf{v}_3}{\partial \mathbf{x}_3} \end{bmatrix} \quad \nabla \mathbf{v} = \frac{1}{2} (\nabla \mathbf{v} + \nabla \mathbf{v}^T) + \frac{1}{2} (\nabla \mathbf{v} - \nabla \mathbf{v}^T)$$

$$\nabla \mathbf{v} = \mathbf{D} + \mathbf{W}$$
Velocity gradient tensor is the sum of **strain rate** and **vorticity** tensors

$$\nabla \mathbf{v} = \frac{1}{2} \left(\nabla \mathbf{v} + \nabla \mathbf{v}^T \right) + \frac{1}{2} \left(\nabla \mathbf{v} - \nabla \mathbf{v}^T \right)$$

$$\nabla \mathbf{v} = \mathbf{D} + \mathbf{W}$$

vorticity tensors