Title

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#### Abstract

My very nice abstract

# Chapter 1

### Theoretical Development

### 1.1 Optical Cavity

We firstly introduce one of the most common object of quantum optic, namely, the *optical cavity*. It is mainly constitued of two mirrors mounted perpendicularly to the optical axis at a certain distance from each other. The idea behind this simple setup is to select a discret range of wavelengths defined by the space between the mirrors.

Indeed, one can modelize the cavity as an one-dimensional box, then apply the wave equation  $\Box \vec{E} = 0$  where  $\Box$  is the d'Alembertian operator and  $\vec{E}$  the electric field's amplitude, together with the Maxwell equation  $\nabla \cdot \vec{E} = \partial_x E = 0$ . As the wave must vanish at the boundaries of the box (meaning that the energy cannot propagate outside of the box's region) one would find that the solutions are linear combinations of sinuzoidale functions, each of them having a spatial frequency multiple of  $\frac{\pi}{L}$  where L denotes the length of the box/cavity. We shall consider that our model lies into a vacuum chamber, leading to the refractive index n=1 for the void and the well known constant c for the speed of light. Then, thanks to the relation  $\omega = ck$  we see that the angular frequency is also quantized. It is important to note that the argument is valid for other refractive index and higher dimensions (i.e in 2D, 3D, ...).

With a more pragmatic point of view, one can think of this wavelength selection as an interferometer. In fact, let's imagine for a while that we emplace a cavity in front of the sun, fast enough to capture a beam of sunlight. Then we stop the clock before further propagation. Mathematically, the waves which are differents from the selective frequency vansih instantaneously, because of the presence of the cavity. However, physically, the full spectrum of the sun still resides between the two mirrors. Then if we run the clock again, the light is reflected from the back mirror. As we captured a continous stream, the  $\pi$ -dephased reflected light encouters the incoming light: interference happens and after a couple of round-trips, only the waves generating an in-phase match at each round-trip (i.e with a space-frequency or wave-number  $\frac{n\pi}{L}$ ,  $n \in [0, +\infty[])$  remains by constructive interference, creating standing waves of the same frequency. On the other hand, all the other frequencies produce at reflection, in average on some round-trips, a random-like phase difference: the sum shall give a null coefficient in term of amplitude for those given frequencies. Although this is a simple explanation, two things are important to note:

• For the constructive interference case, we say that we need to be in-phase after one round-trip, meaning that after two reflections, which happens after hitting both back and front mirrors of the cavity, the wave must replicate the same

<sup>&</sup>lt;sup>1</sup>R.Loudon derives rigorous equations in sections 1.1 and 1.2 of Quantum Theory of Light.

amplitude at any position. However, the electric field is not static but moves in space. Then, it becomes more evident that twice the length of the cavity must be a multiple of the frequency in order to give the exact same phase, even with a space-motion of the wave.

• For all the other frequencies, the phase difference is not random but actually well behaved. Nevertheless, After a couple of round-trip, the set of generated phase difference is unformly distributed among  $[-\pi, \pi]$  reproducing a sort of randomness.

Thereby, that is why the device created by C.Fabry and A.Pérot in 1899 is called an *interferometer* as, in their case, the light hit the mirrors with an angle, creating the famous pattern of fringes. Equivalently, this category of instrument is often named *resonator* as the amplitude of the electric field is enhanced in the case of resonance with the cavity or decreases in other cases: by conception, it can be modelized as a classical harmonic oscillator or with the quantum equivalent. <sup>2</sup>

In real experiments, the device is static and one prefers to let the light enter partially, to feed the cavity, and exit partially to collect the selected waves. In that way, we use partially reflective mirrors parametrized by an electric field reflection coefficient r and an electric field transmission coefficient t obeying the relation  $r^2 + t^2 = 1$  (the squared terms are the respective coefficient for the intensity of the field), meaning that all the absorbed energy must be re-emitted by the mirror, which is of course not fully true as some amount of the energy is transformed into heat. However, current manufacturers creates mirror with less than 0.01% of loss and the above formula is sufficient for most of the applications.

The most commonly used approach to express the cavity response is the Airy distribution which represents the intensity ratio between the internal electric field and the *launching* electric field (i.e the amount of *feeding*-field succeding to transmit through the first mirror and penetrate the cavity), in function of the phase accumulated by round-trip:

Airy distribution : 
$$A(\phi) \stackrel{\text{def}}{=} \frac{I_{circ}}{I_{launch}}$$
 (1.1)

In other words, it just makes the link between the enhancment factor of the cavity field and the constructive-destructive interference phase pattern. In order to derive it, we shall use the circulating field approach <sup>3</sup>, represented in Fig (add figure!) and constitued of:

- A launching electric:  $E_{launch}$
- A round-trip electric field which is the field after one complete round-trip: one reflection on the back mirror plus another on the front mirror. We call it  $E_{RT}$
- A circulating electric field which is the sum of the launched field and the roundtrip one:  $E_{circ} = E_{launch} + E_{RT}$ . It is by definition the internal electric field.

Here, we use the phasor representation where the electric field (a real analytic signal) is splitted into two conjugate complex numbers:

$$E(x,t) = \overline{E}(x,t) + \overline{E}^*(x,t)$$
 s.t  $E(x,t) \in \mathbb{R}$ ,  $\overline{E}(x,t) \in \mathbb{C}$  (1.2)

$$=2\Re\{\overline{E}(x,t)\}\tag{1.3}$$

<sup>&</sup>lt;sup>2</sup>As we will see later, each resonant frequency owns a linewidth as a classical oscillator, in contrary to the quantum equivalent where the energy ladders (i.e the frequencies, in virtue of the relation  $\hbar\omega$ ) are well defined.

<sup>&</sup>lt;sup>3</sup>A. E. Siegman, section 11.3, *Lasers* 

Then, we consider fields evolving in time and in space along the optical axis x. Moreover, one considers only the amplitude of the fields and deals with scalar equation. However one can assume linearly polarized input field to get the same mathematical treament but the Airy distribution is valid for any kind of polarization and can be genelarized for vectorial equations instead (i.e at higher dimension). Note that (1.2) is not a definition sign " $\stackrel{\text{def}}{=}$ " as an analytic signal can be written is that form.<sup>4</sup>

Rewriting the equation for the circular field gives:

$$2\Re\{\overline{E}_{circ}\} = 2\Re\{\overline{E}_{launch}\} + 2\Re\{\overline{E}_{RT}\}$$
(1.4)

which, by linearity and analyticity of the signal, is equivalent to:

$$\overline{E}_{circ} = \overline{E}_{launch} + \overline{E}_{RT} \tag{1.5}$$

Now, one can express the round-trip field from the circular one, dephased by a certain angular amount. Indeed, one knows that each mirror add a phase of  $\pi$  to the original field and the amplitude is modulated by the reflection factor R. As a field of space-frequency k and propagating over a distance l is shifted by:

$$\omega \times$$
 "propagation time" =  $\omega \times \frac{l}{c}$  (1.6)

Then, after a complete round-trip, one obtains for the "RT" field a total angular shift of:

$$2\phi \stackrel{\text{def}}{=} \frac{2L}{c}\omega + 2\pi \tag{1.7}$$

Thereby:

$$\overline{E}_{RT} = r_1 r_2 e^{-i2\phi} \overline{E}_{circ} \tag{1.8}$$

where  $r_{1,2}$  are the reflection coefficients of front and back mirror respectively. In other words, instead of propagating the field from its original value  $\overline{E}_{circ}$  through time or space to get a phase, we compute the relative phase  $\phi$  from the length of the cavity L with the field's frequency  $\omega$ .

One can highlight that for a caracteristic space-frequency of the cavity  $k = \frac{n\pi}{L}$ , we have:

$$2\phi = \frac{2L}{c} \times \frac{cn\pi}{L} + 2\pi = 2\pi(n+1) \equiv 0 \quad [2\pi]$$
 (1.9)

meaning that those frequencies does not generate any phase shift after one complete round-trip, involving constructive inteferences then standing waves.

Putting (1.8) in (1.5) leds to:

$$\frac{\overline{E}_{circ}}{\overline{E}_{launch}} = \frac{1}{1 - r_1 r_2 e^{-i2\phi}} \tag{1.10}$$

Then, one uses the relation  $I \simeq |\overline{E}|^2$ , which is valid for an average of the intensity over some periods of the  $\overline{E}$ -field <sup>5</sup> and by the definition (1.1), one obtains:

$$A(\phi) = \frac{1}{(1 - r_1 r_2)^2 + 4r_1 r_2 \sin^2(\phi)}$$
(1.11)

Moreover, to get the actual distribution that we observe through the cavity, that is to say, the enhancment factor at the output of the cavity, we set:

$$A'(\phi) = (1 - r_1^2)(1 - r_2^2) \times A(\phi)$$
(1.12)

<sup>&</sup>lt;sup>4</sup>More explanations about the hypothesis and what an analytic signal implies in section ??

<sup>&</sup>lt;sup>5</sup>See section ??

where one uses the intensity transmission coefficients  $t_{1,2}^2 = 1 - r_{1,2}^2$ . Now, in order to sketch the function, independent of the size of the cavity L, we shall use the third term of the equality (1.9) to reparametrize the round-trip dephasing variable  $\phi$ :

$$\phi = \pi(x+1) \quad \equiv \quad \pi x \quad [\pi] \tag{1.13}$$

where the integer variable n has been replaced by the continuous one  $x \in \mathbb{R}$  so that one can also investigate the behavior of the enhancment factor  $A'(\phi) \sim A'(x)$  away from the resonant frequencies. Fig (??) is a normalized drawing<sup>6</sup> of the airy distribution for a short amount of negative and positive resonant frequencies through a couple of reflexion coefficient  $r_{1,2}$ .

(add figure!)

To clarify, the abscisse coordinate is the factor quantity between two caracteristic frequencies  $\frac{n\pi}{L}$ , which can be equivalently spatial or temporal as we get ride of the constant c in our calculation: then x is a frequency divided by the free spectral range (FSR) In other words, for  $x = \frac{1}{2}$ , one gets the enhancment factor A' for exactly a frequency halfway between two resonances, whereas x = 1 gives the A' factor for the first resonant frequency of the cavity.

From those previous results, we can now define the full width at half maximum (FWHM) which approximately represents how broad is the range around a resonant frequency where the field is modulated by more than one-half. Thanks to (1.11), one obtains A(0)/2 when the denominator respects:

$$(1 - r_1 r_2)^2 = 4r_1 r_2 \sin^2(\Delta \phi) \Rightarrow \Delta \phi = \arcsin\left(\frac{1 - r_1 r_2}{2\sqrt{r_1 r_2}}\right)$$
(1.14)

with, in virtue of (1.13):

$$\Delta \phi = \frac{\pi}{2} \Delta \nu \tag{1.15}$$

where FWHM  $\stackrel{\text{def}}{=} \Delta \nu$ .

Finally, one can sketch the FWHM in fonction of the mirror reflectivities  $r_{1,2}$  and obtains Fig ??

(add figure)

Two important points are noticeable:

- The linewidth of a cavity is invertly dependent on the mirrors reflectivity. In other words, more transmitive are the mirrors, broader is the frequency range around resonances, giving a less selective cavity, and reciprocally. Then, two perfectly reflective mirrors allow the FWHM to tend to zero: the cavity selects only and exactly the resonant frequencies  $\frac{n\pi}{L}$ . Formally, the selectivity of a cavity is defined by its finesse which reads  $F \stackrel{\text{def}}{=} \frac{\Delta \nu}{\text{FSR}}$ : one normalizes the linewidth by the distance (in term of frequency) separating two resonances. On Fig ??, as FSR is unity then the ordinate axis is also the finesse by definition.
- The function modelizing the FWHM tends to infinity below a certain value which can be evaluated to approximately  $r_1r_2 \approx 0.17$ . That is due to the behavior of the arcsin which is not defined beyond x = 1 for  $x \in \mathbb{R}^+$ .

<sup>&</sup>lt;sup>6</sup>One divides the whole graph by A'(0)

<sup>&</sup>lt;sup>7</sup>One could say that the first resonant frequency is x = 0 according to the figure or even the formula (1.11) itslef. However, x = 0 also means n = 0: the launched field would have null frequency, which is not a physical solution.

Nevertherless, it is always possible to build an experiment involving mirrors with high-losses (i.e very low reflection or very high transmission), without the output frequency going crazy. Thereby, what happens? Well, this is a limitation case of this Airy-model and in the common scientific description of a cavity, one utilizes the Lorentzian approach where one defines a coherent time of the light from the reflection coefficient and the cavity length, then gets a differential rate equation of the amount of photons (i.e an exponential decay of the electric field) which, by virtue of the Fourier transform, gives a Lorentzian as a spectrum around one resonant frequency. Then, to obtain the full cavity spectrum, one has to place each Lorentzian of a given resonance on top of each other on the same graph.<sup>8</sup>

The Lorentzian model is highly faithfull to the real world experiment for all the possible reflective coefficients and tends to give the same caracteristic values (linewidth, finesse, ...) than the Airy-model from half to full reflective mirrors. However, it may seem to be less intuitive even if the derivation is straigthforward and, after all, the goal here was to show the principle of interference inside a cavity due to the round-trip dephasing term.

Finally, the next step for an optical cavity is, as many of physical systems, to interact with its environment. In other words, what happens if one adds an element, let's say atoms, inside of it? Well, this is basically the principle of lots of current experiments and avdvanced optical tools, namely the *LASER* among others, and the next section is decidated to the mathematical formulation of one first model for a cavity filled with a gain medium.

### 1.2 Jaynes-Cummings model

As an introduction, it is important to remind that the Jaynes-Cummings (JC) approach is no more no less than a model, which means that it is based on some hypothesis and has limitations which leads to refinements for more complex physical systems. In the current section, we shall present as wide as possible the principles of this model which will be the foundments of all the next derivated/evoluted models<sup>9</sup>, even if the section is not supposed to be exhaustive but only a reference-like for further theoretical developments.

First of all, our system is composed of:

- An electric field inside a cavity: this E-field is quantized and can only be a superposition of resonances.
- A single two-level system: this system has a structure of ground-excited state and can represent a transition of an atom for example.

When quantizing the E-field inside of a box of volume  $V = L^3$  (i.e the cavity in three dimensions), one finds that the corresponding hamiltonian operator is [??Loudon

<sup>&</sup>lt;sup>8</sup>Note that when treating the spontaneaous emission of an atom (or more formally, a two-level atomic system), one also deals with differential rate equations, which represents the exponential lifetime decay of the excitation, giving a Lorentzian as a spectrum: longer it takes to the system to decay, broader is the bandwidth. However, the analogy stops here: for a cavity, the whole electric field spectrum is affected by the linewidth, whereas, for a two-level atom, the spectrum represents the frequency uncertainty as the atom can spontaneously emit a photon with frequency slightly different from what the atom has been excited with.

<sup>&</sup>lt;sup>9</sup>As written, the JC-model may seem to be a pre-model or even a *toy tool* in view of introducing other legitimate models. Nevertheless, the JC-model is an actual physical approach, currently used for real use-cases in Quantum Optics, especially whith single atom interactions.

p143]:

$$\hat{H}_{cav} = \int_{cavitu} \left[ \epsilon_0 \hat{E}(\vec{r}, t) \cdot \hat{E}(\vec{r}, t) + \mu_0^{-1} \hat{B}(\vec{r}, t) \cdot \hat{B}(\vec{r}, t) \right] dV$$
 (1.16)

$$= \sum_{\vec{k}} \sum_{\lambda} \hbar \omega_{c,\vec{k}} \left( \hat{a}^{\dagger}_{\lambda \vec{k}} \hat{a}_{\lambda \vec{k}} + \frac{1}{2} \right) \tag{1.17}$$

where  $\hat{E}(\vec{r},t)$  and  $\hat{B}(\vec{r},t)$  are respectively the electric and magnetic operators;  $\epsilon_0$  and  $\mu_0$  the electric and magnetic susceptibility of the vacuum respectively,  $\omega_{c,\vec{k}}$  the frequency mode;  $\lambda = \pm 1$  the polarization;  $\hat{a}^{\dagger}_{\lambda\vec{k}}$  with  $\hat{a}^{\dagger}_{\lambda\vec{k}}$  the ladders operator of the field.

Now, we define the electric field as exactly a unique mode with a unique polarization. Thereby:

$$\hat{H}_{cav} = \hbar \omega_c \left( \hat{a}^{\dagger} \hat{a} + \frac{1}{2} \right) \tag{1.18}$$

where we dropped the subscripts  $\vec{k}$  and  $\lambda$ . In other words, we represent the electric wave as a perfectly coherent field which fits a resonance of the cavity at frequency  $\omega_c$ . As we can see, this one-mode cavity system is treated as a quantum harmonic oscillator.

Then comes the choice of the model for the ground-excited system. Sometimes, in the litterature [??MandelWolf], one utilizes another quantum harmonic oscillator with bosonic modes, namely:

$$\hat{H}_{atom} = \hbar \omega_a \left( \hat{b}^{\dagger} \hat{b} + \frac{1}{2} \right) \tag{1.19}$$

where  $\hat{b}$  is the bosonic operator of the two-level system. However, this model allows multiple excited levels and the energy of the atom-system is artifically restrained to the first two levels.

In fact, an advantageous choice is to use the spin-half quantum system:

$$\hat{H}_{atom} = \hbar \omega_a \hat{\sigma}_z \tag{1.20}$$

where  $\hat{\sigma}_z$  is the third Pauli matrix. This model allows us to use the spin-down  $|\downarrow\rangle$  as the ground state with an energy:

$$E_g \stackrel{\text{def}}{=} \langle \downarrow | \hat{H}_{atom} | \downarrow \rangle = -\hbar \omega_a \tag{1.21}$$

and  $|\uparrow\rangle$  as the excited state with an energy:

$$E_e \stackrel{\text{def}}{=} \langle \uparrow | \hat{H}_{atom} | \uparrow \rangle = \hbar \omega_a \tag{1.22}$$

Moreover, the Pauli matrices can exponentiates to the Lie algebra of SU(2) then follows similar commutator relations, namely:

$$[\hat{\sigma}_j, \hat{\sigma}_k] = 2i\varepsilon_{jkl}\,\hat{\sigma}_l \tag{1.23}$$

where  $\varepsilon_{jkl}$  is the Levi-Civita symbol. For the ladder operators  $\hat{\sigma}_{\pm} = \hat{\sigma}_x \pm i\hat{\sigma}_y$ , one can esasily prove the following projections:

$$\hat{\sigma}_{+}|\downarrow\rangle = |\uparrow\rangle \qquad \hat{\sigma}_{-}|\downarrow\rangle = 0 \qquad \hat{\sigma}_{-}|\uparrow\rangle = |\downarrow\rangle \qquad \hat{\sigma}_{+}|\uparrow\rangle = 0 \qquad (1.24)$$

which means that one can excite a ground state or damp an excited state but one cannot excite an already excited state or damp a ground state: the spin-1/2 model is restrained to a pair of states by definition.<sup>10</sup>

Now that we got the hamiltonian operators for the cavity field and the two-level system, we use the tensor product in order to create a quantum system all-encompassing those two systems:

$$\hat{H}_{JC} = \hat{H}_{atom} \otimes \mathbb{1}_{cav,2} + \mathbb{1}_{atom,n} \otimes \hat{H}_{cav} + \hat{H}_{int}$$
(1.25)

where  $\mathbb{1}_{cav,2}$  and  $\mathbb{1}_{atom,n}$  are the identity operators for the Hilbert-space of the cavity and the atom respectively. Naturally, by their definition the Hilbert-space of the atom is of dimension 2 (i.e two states form the basis) whereas the Hilbert-space of the cavity is of dimension n as the quantum harmonic oscillator is associated to a Fock-space of the same dimension (i.e one has n possible different levels of energy for the electric field). In other words, we build another Hilbert-space of dimension 2n from two separated system. We also defined  $\hat{H}_{int}$  as an additional hamiltonian operator belonging to an Hilbert-space which is of dimension 2n by construction: this new term arises from the physical interaction of the two systems but not by the mixture of the cavity and atom systems (i.e there is nothing related with the tensor product). This interaction term can be mathematically formulated with the electric field's acting on the dipole constitued by the atom:

$$\hat{H}_{int} \stackrel{\text{def}}{=} -\hat{d} \cdot \hat{E}(\vec{r}, t) \tag{1.26}$$

where  $\hat{d}$  is the dipole operator in term spin-half operators (using Pauli matrices) and  $\hat{E}$  the quantized electric field of the cavity. After centering the frame on the atom with  $\vec{r} = 0$ , the interaction hamiltonian transforms as:

$$\hat{H}_{int} = \hbar g \left[ (\hat{\sigma}_{+} - \hat{\sigma}_{-}) \otimes (\hat{a}^{\dagger} - \hat{a}) \right]$$
(1.27)

where g is the coupling constant arising from multiple constant terms belonging to the dipole and electric operators: g defines how strong/often the cavity field and the atom will exchange energy. Finally, one obtains the complete hamiltonian operator for the Jaynes-Cummings model:

$$\hat{H}_{JC} \stackrel{\text{def}}{=} \hat{H}_0 + \hat{H}_{int} \tag{1.28}$$

$$= \hbar\omega_c \left( \hat{a}^{\dagger} \hat{a} + \frac{1}{2} \right) \otimes \mathbb{1}_{cav,2} + \mathbb{1}_{atom,n} \otimes \hbar\omega_a \hat{\sigma}_z + \hbar g \left[ (\hat{\sigma}_+ - \hat{\sigma}_-) \otimes (\hat{a}^{\dagger} - \hat{a}) \right]$$
(1.29)

$$= \hbar \omega_c \hat{a}^{\dagger} \hat{a} + \hbar \omega_a \hat{\sigma}_z + \hbar g \left[ (\hat{\sigma}_+ - \hat{\sigma}_-)(\hat{a}^{\dagger} - \hat{a}) \right]$$
(1.30)

where we omit the tensor product on the last line and remove the  $\frac{1}{2}\hbar\omega_c$ , which is only a choice of reference for the vacuum energy (i.e here we set zero). In the future, the *atomic* operators will lies on the right of the *field* operators in order to remind the implicit tensorial structure of the system.<sup>12</sup>

<sup>&</sup>lt;sup>10</sup>From an autor to another, the eigenvalues may differ from a constant (in particular by a factor of 2). Keep in mind that the Pauli matrix operators are taken from  $\hat{\sigma}_i = \frac{2}{\hbar} \hat{S}_i$  where  $\hat{S}_i$  is the spin operator.

 $<sup>^{11}\</sup>hat{H}_{atom}$  and  $\hat{H}_{cav}$  are often referred to the energy of the atom and the cavity field respectively, which is a bit tendencious as this is only true when one takes those two systems separately, but falls down as soon as we mix them and add the interaction term: the eigenvalues (i.e energies) with an interaction are very different from the eigenvalues of the separated systems. Moreover, a hamiltonian operator corresponds to the energy if and only if it is explicitly independent of time (which is the case here but it is always nice to precise the reason).

<sup>&</sup>lt;sup>12</sup>Note that we can reverse the tensor product order as long as one does not involve the coefficient of the states and this artifical sort is only present to clarify the notation and equations.

Then, we shall change the reference frame of the hamiltonian in order to deal only with the frequency difference  $\Delta\omega \stackrel{\text{def}}{=} \omega_c - \omega_a$ , called *detuning*. It will be advantageous for the simulation part and also allow us to apply a very common approximation. In this way, we use a U(1) symmetry for the JC-hamiltonian in this manner:

$$\hat{H}_{JC} \to U \hat{H}_{JC} U^{-1} + i\hbar \dot{U} U^{-1}$$
 (1.31)

$$|\psi\rangle \to U|\psi\rangle$$
 (1.32)

where  $|\psi\rangle$  is a solution of the Schrödinger equation for the JC-hamiltonian; U is a unitary operator with its inverse  $U^{-1}$  belonging to its dual space, involving  $U^{-1} = U^{\dagger}$ ;  $\dot{U}$  is the one-time derivative of U. It can be proven that the transformed hamiltonian and  $U|\psi\rangle$  vector plugged into the Schrödinger equation, give the same equation as the JC-hamiltonian and  $|\psi\rangle$ . Thereby, if one finds a solution  $|\phi\rangle$  of the transformed system, then  $U^{\dagger}|\phi\rangle$  gives  $|\psi\rangle$  which is a solution of the original system.

In our case, we choose the unitary transformation as:

$$U \stackrel{\text{def}}{=} e^{\frac{i\omega_a t}{\hbar} \hat{H}_0} = e^{i\omega_a t(\hat{n} + \hat{\sigma}_z)} \tag{1.33}$$

where we utilize the common photon number operator of the field,  $\hat{n} = \hat{a}^{\dagger}\hat{a}$ . As the U(1) symmetry is essentially a rotation along the complex unitary circle, we explicitly choose here a rotation of  $\omega_a t$  which means that the transformed hamiltonian will be placed in the same frame as the atom: one calls this frame the *rotating frame*.

From Annexe (??) one finally obtains the following parts for the transformed hamiltonian:

$$i\hbar \dot{U}U^{\dagger} = -\hbar\omega_a(\hat{n} + \hat{\sigma}_z) \tag{1.34}$$

$$U\hbar\omega_c\hat{n}U^{\dagger} = \hbar\omega_c\hat{n} \tag{1.35}$$

$$U\hbar\omega_a\hat{\sigma}_z U^{\dagger} = \hbar\omega_a\hat{\sigma}_z \tag{1.36}$$

$$U\hbar g\hat{\sigma}_{+}\hat{a}U^{\dagger} = \hbar g\hat{\sigma}_{+}\hat{a} \tag{1.37}$$

$$U\hbar g\hat{\sigma}_{-}\hat{a}^{\dagger}U^{\dagger} = \hbar g\hat{\sigma}_{-}\hat{a}^{\dagger} \tag{1.38}$$

$$U\hbar g\hat{\sigma}_{+}\hat{a}^{\dagger}U^{\dagger} = e^{2i\omega_{a}t}\hbar g\hat{\sigma}_{+}\hat{a}^{\dagger} \tag{1.39}$$

$$U\hbar g\hat{\sigma}_{-}\hat{a}U^{\dagger} = e^{-2i\omega_{a}t}\hbar g\hat{\sigma}_{-}\hat{a} \tag{1.40}$$

As we shall us the detuning  $\Delta\omega$  for the transformed hamiltonian instead of the respective cavity and atom frequency, it makes sense to write down a strong hypothesis on the system:  $\omega_a \sim \omega_c$  which means that one assumes that the cavity and atom frequencies have the same order of magnitude. Thereby, the terms (1.39) and (1.40) are rotating extremely fast compared to our reference frame, about twice the cavity or atom frequency, and are qualified of anti-resonant. Then, those terms average to zero over some cycles and can be discarded. This approximation is called the rotating wave approximation (RWA).<sup>13</sup>

At the end of the day, one finds the transformed hamiltonian:

$$\hat{H}_{JC} \to \hbar \Delta \omega \,\hat{n} + \hbar g \left(\hat{\sigma}_{+} \hat{a} + \hat{\sigma}_{-} \hat{a}^{\dagger}\right)$$
 (1.41)

that we rename by convenience and without ambiguity  $\hat{H}_{JC}$ . One may first notice that the atomic hamiltonian term vanished and only the field operator remains of  $\hat{H}_0$ : that

<sup>&</sup>lt;sup>13</sup>Here, we firstly change the reference frame in order to introduce the RWA. However, this is not necessary. Indeed, the RWA only influence the interaction hamiltonian and one can apply this approximation directly in (1.30) through the interaction picture evolution.

is due to the new frame which follows the atomic frequency, then the transformed  $\hat{H}_{cav}$  is proportional to the detuning. It is also interesting to see how a generic JC-state (i.e  $|\uparrow\rangle\otimes|n\rangle$  or  $|\downarrow\rangle\otimes|n\rangle$  which are also called bare states) is influenced by the transformed interaction hamiltonian:

$$\hat{H}_{int} \cdot |\uparrow\rangle \otimes |n\rangle = \hbar g \left[ (\hat{\sigma}_{+} \otimes \hat{a}) \cdot (|\uparrow\rangle \otimes |n\rangle) + (\hat{\sigma}_{-} \otimes \hat{a}^{\dagger}) \cdot (|\uparrow\rangle \otimes |n\rangle) \right]$$
(1.42)

$$= \hbar g \left[ \hat{\sigma}_{+} | \uparrow \rangle \otimes \hat{a} | n \rangle + \hat{\sigma}_{-} | \uparrow \rangle \otimes \hat{a}^{\dagger} | n \rangle \right] \tag{1.43}$$

$$= \hbar g \left[ 0 + |\downarrow\rangle \otimes \sqrt{n+1} |n+1\rangle \right] \tag{1.44}$$

$$= \hbar g |\downarrow\rangle \otimes \sqrt{n+1} |n+1\rangle \stackrel{\text{def}}{=} \hbar g \sqrt{n+1} |\downarrow, n+1\rangle \tag{1.45}$$

where we used (1.24). Equivalently:

$$\hat{H}_{int} \cdot |\downarrow, n\rangle = \hbar g \left[ \hat{\sigma}_{+} \hat{a} |\downarrow, n\rangle + \hat{\sigma}_{-} \hat{a}^{\dagger} |\downarrow, n\rangle \right]$$
(1.46)

$$= \hbar g \sqrt{n} |\downarrow, n - 1\rangle \tag{1.47}$$

In other words, in the first case, an excited two-level system decays into its ground state, releasing a photon into the field (i.e the total energy is conserved), whereas in the second case, an atom *at rest* absorbs a photon of the field and ends up in its excited state: this is intuitively how one may imagine the interaction between the atom and the cavity field system.

In order to solve the system evolution, one wants to diagonalize the hamiltonian by finding the eigenstates and the eigenvalues. It turns out that  $\hat{H}_{JC}$  can be written by  $2 \times 2$  blocks in the JC-states:<sup>14</sup>

$$\hat{H}_{JC} = \bigotimes_{n} \begin{bmatrix} \hbar \Delta \omega (n-1) & 2\hbar g \sqrt{n} \\ 2\hbar g \sqrt{n} & \hbar \Delta \omega n \end{bmatrix}$$
 (1.48)

where n under the tensor product is the fock space dimension associated to the cavity system.

After diagonalizing each block of (1.48) (Annexe??), one finds the following egein-values and eigenstates:

$$E_{n,\pm} \stackrel{\text{def}}{=} \hbar \Delta \omega \left( n - \frac{1}{2} \right) \pm \frac{\hbar}{2} \sqrt{4g^2 n + \Delta \omega^2}$$
 (1.49)

$$|n, +\rangle \stackrel{\text{def}}{=} \cos\left(\frac{\theta_n}{2}\right) |\uparrow, n-1\rangle + \sin\left(\frac{\theta_n}{2}\right) |\downarrow, n\rangle$$
 (1.50)

$$|n, -\rangle \stackrel{\text{def}}{=} \cos\left(\frac{\theta_n}{2}\right) |\downarrow, n\rangle - \cos\left(\frac{\theta_n}{2}\right) |\uparrow, n-1\rangle$$
 (1.51)

with:

$$\tan\left(\theta_n\right) = -\frac{4\sqrt{n}g}{\Delta\omega} \tag{1.52}$$

To finish with the JC-model, we shall demonstrate one relevant case: the *Rabi* flopping (or more explicitly the Rabi oscillations) when the detuning is null or can be assimilated as vanishing (i.e  $\Delta\omega = 0$ ). Thereby, one starts with the two-level system as excited with an *empty* cavity field:

$$|\psi(0)\rangle \stackrel{\text{def}}{=} |\uparrow, n = 0\rangle = \cos\left(\frac{\theta_1}{2}\right)|1, +\rangle - \sin\left(\frac{\theta_1}{2}\right)|1, -\rangle$$
 (1.53)

The reason comes from the bare states being degenerated with eigenvalue n+1 when applied on the non-transformed base hamiltonian  $\hat{H}_0$ .

where we rewrite the initial state in terms of eigenstates.

Then, applying the spatial evolution operator, one finds (see Annexe??)

$$|\psi(t)\rangle = e^{-\frac{i}{\hbar}E_{1,+}t}\cos\left(\frac{\theta_1}{2}\right)|1,+\rangle - e^{-\frac{i}{\hbar}E_{1,-}t}\sin\left(\frac{\theta_1}{2}\right)|1,-\rangle \tag{1.54}$$

$$= \cos(\Omega t) |\uparrow, 0\rangle - i \sin(\Omega t) |\downarrow, 1\rangle \tag{1.55}$$

where we defined the Rabi frequency  $\Omega = 2g$ . Making the projection (i.e a measurment) along  $|\uparrow, 0\rangle$  or  $|\downarrow, 1\rangle$  and one ends up with the Rabi oscillations sketched on Fig ??. (add figure!!)

As we can see on Fig??, the probabilities of finding one photon with the atom in its ground state, while no photon with the atom in the excited state, oscillate in opposite phase.

Numerically, if one puts a small detuning (i.e  $\omega_a$  is still about the same order of magnitude of  $\omega_c$ ), one can numerically sketch Fig ?? where we see that the energy transfer is progressively discarded as we increase the detuning: the probabilities of inversing the intial state decreases.<sup>15</sup>

As we can notice, this model is mainly limited by its atomic level capability which is of number of two. Thereby, one would probably like to theoretically predict the behavior for many two-level systems (or equivalently several spins). Then, we shall introduce an extension of this model in the next section.

### 1.3 Tavis-Cummings model

In order to include more atoms, one needs to extend the Hilbert space involved into the JC-model. In fact, there are two ways of coupling more two-level systems, linked to the question: "Are the sub-systems distinguishable?". Indeed, here is the first  $na\"{i}ve$  idea to introduce N atoms:

$$\hat{\sigma}_i \to \hat{\sigma}_i^1 \otimes \mathbb{1}^{2,\dots,N} + \mathbb{1}^1 \otimes \hat{\sigma}_i^2 \otimes \mathbb{1}^{3,\dots,N} + \dots + \mathbb{1}^{1,\dots,N-1} \otimes \hat{\sigma}_i^N$$
 (1.56)

$$\stackrel{\text{def}}{=} \sum_{j=1}^{N} \hat{\sigma}_i^j \tag{1.57}$$

where  $i \in [x, y, z]$  and the upper indices indicate the Hilbert spaces involved into the operator owning them:  $\mathbb{1}_{k,\dots,m}$  is the identity operator for the group of spaces from k to m.<sup>16</sup> As this transformation is made of linear combination of two-level system and as the unitary transformation in the previous section, involving commutator rules from the Pauli matrices, are still valid by independency of a system to another (i.e (1.23) can be upper indexed for each Hilbert space), this leads to an equivalent hamiltonian of (1.41):

$$\hbar\Delta\omega\,\hat{n} + \hbar g \sum_{j=1}^{N} \left(\hat{\sigma}_{+}^{j}\hat{a} + \hat{\sigma}_{-}^{j}\hat{a}^{\dagger}\right) \tag{1.58}$$

Thereby, this extended system is composed of N+1 independent sub-system with dimension scaling as  $2^N \times N_{Fock}$  where  $N_{Fock}$  is the space dimension of the cavity

<sup>&</sup>lt;sup>15</sup>Of course, it depends on the initial state. Here we choosed to work with the pair  $|\uparrow,0\rangle$  and  $|\downarrow,1\rangle$  but similar behaviors happen for other states.

<sup>&</sup>lt;sup>16</sup>We intentionally split the tensor product in the transformation (1.56) for the sake of clarity even if the tensor product can be reversed. However, we drop the tensor notation in definition (1.57) for simplicity.

system. By *independent*, we mean that each atom-like system is distinguishable from another. However, we do not have good reason to modelize our original experiment with independent atoms. Even worse, the superradiant effect is allowed by a collective ensemble, that is to say the atoms are indistinguishable and react as a whole multi-level system.<sup>17</sup> Indeed, R.H. Dicke, in its original paper [??] of coherent radiation process, states that the atom to atom distance (hence the gaz volume) must be much smaller than the wavelength of the surrounding electric field in order to reach an enhanced and coherent radiation. Nevertheless, in our experiment, the atomic cloud does not respect this condition for superradiance but as the atoms are enclosed into a cavity, this leads to collective interaction from the field to the cloud of atoms, hence indistinguishability.

Therefore, as the spins are assumed to be identical in (1.57), one uses instead the collective spin operator:

$$\sum_{j=1}^{N} \hat{\sigma}_i^j \to \frac{\hbar}{2} \hat{S}_j \tag{1.59}$$

where  $\hat{S}_j$  follows the spin algebra similar to the Pauli matrices with, among other relations, the commutator:

$$[\hat{S}_j, \hat{S}_k] = i\hbar \varepsilon_{jkl} \,\hat{S}_l \tag{1.60}$$

Then, one obtains the following hamiltonian for indistinguishable N two-level systems:

$$H_{TC} \stackrel{\text{def}}{=} \hbar \Delta \omega \, \hat{n} + g \left( \hat{S}_{+} \hat{a} + \hat{S}_{-} \hat{a}^{\dagger} \right) \tag{1.61}$$

where the constant g swallows a factor of 2 (i.e  $2g \to g$ ). Historically, this type of hamiltonian refers to the Tavis-Cummings (TC) model as it only includes a co-rotating term by the RWA (which is the actual interaction part of the TC-hamiltonian) then the TC-model keep the U(1) symmetry. However, R.H. Dicke proposes another hamiltonian involving a counter-rotating term of  $\hat{S}_{-}\hat{a} + \hat{S}_{+}\hat{a}^{\dagger}$  (without unitary transformation) which breaks the U(1) symmetry: we shall not utilize the Dicke model here because a posteriori (by simulation), the additional term is unnecessary.

This model may represent a group of N atom where each atom can be in its ground state or excited state, interacting with a radiation field. For practical reason, this system of two-level system is often called a *gain medium* as models involving such systems can be utilized for LASER simulation where the the lasing beam is enhanced by population inversion.

By construction, if one choose a unique atom with N=1, the spin structure is quantized as:

$$s = \frac{1}{2} \quad ; \quad m = \pm \frac{1}{2}$$
 (1.62)

which allows two pure states, similar to  $|\uparrow\rangle$  and  $|\downarrow\rangle$ . Morevover, if one increases the number of atom to N=2, one get three pure states:

$$\begin{array}{lll} s=1\,;\,m=-1 & \sim & |\downarrow,\downarrow\rangle \\ s=1\,;\,m=1 & \sim & |\uparrow,\uparrow\rangle \\ s=1\,;\,m=0 & \sim & |\downarrow,\uparrow\rangle & \text{or} & |\uparrow,\downarrow\rangle \end{array}$$

<sup>&</sup>lt;sup>17</sup>The second harmonic oscillator defined in (1.19) could make sense but as the original argument in the JC-model, this bosonic structure doesn't allow a closed set of energies (i.e the atom group excitation could tend to infinity).

where the last case involves two well different states of the two distinguishable systems. However, our atoms are represented as a collective spin structure which means that they are indistinguishable leading to considerate those two different states as identical from an energy point of view. In that way, our system of collective spin system scales as  $2 \times \frac{N}{2} + 1 = N + 1$  for N two-level systems and the global system involving the field scales now as  $(N + 1) \times N_{Fock}$  which looses the exponential behavior from the distinguishable case: this is a great advantage from a simulation point of view.

In other words, one can create a global excitation state  $|s=N/2, m=N/2\rangle$  where all the atoms are excited and, at the opposite, a global ground state  $|s=N/2, m=-N/2\rangle$ . However, for other values of m, one cannot say or predict which atom or sub-group of atoms are excited: this leads to degeneracies determined by the binomial coefficient,

Number of "equivalent state" = 
$$\frac{N!}{N_{excited}!(N - N_{excited}!)} = \binom{N}{N_{excited}}$$
(1.63)

where  $N_{excited}$  is the number of excited two-level syste, and the *equivalent* term holds for a collective spin system point of view. It is well known that the maximum of the binomial coefficient is reached for  $N_{excited} = \frac{N}{2}$  meaning that the maximum amount of degeneracies is reached when the gain medium is half-populated of excited entities.

Finally, we obtained a hamiltonian which looks very close to the JC-model and the natural question which now arises is: "How does one populate the gain medium of excitation? How the photons may leak outside of the cavity?". For the first case, one may start with a state of the desired excited population. However, it exists another approach where our quantum system is included into a quantum *bath*, allowing energy to leak in and out.<sup>18</sup>

# 1.4 Open quantum systems and the master equation

Firstly, we introduce the density operator in order to also treat probabilistic mixtures:

$$\rho \stackrel{\text{def}}{=} \sum_{i} p_{i} |\psi_{i}\rangle\langle\psi_{i}| \tag{1.64}$$

where  $\{|\psi\rangle, p_i\}$  is a set of pure state associated to a probability. Equivalently, if we fix an arbitrary basis  $\{|i\rangle\}$  of the Hilbert space, we can write:

$$\rho = \sum_{i,j} \rho_{i,j} |i\rangle\langle j| \tag{1.65}$$

where  $\rho_{i,j}$  are the matrix coefficient of  $\rho$  in the given basis. It can be shown that a density matrix fulfill three essential conditions which are equivalent in regard of (1.64):

- $\rho$  is positive semi-definite:  $\langle v|\rho|v\rangle \geqslant 0$ ,  $\forall |v\rangle$
- $\rho$  is hermitian:  $\rho = \rho^{\dagger}$
- $\rho$  is trace one:  $\sum_{i} p_i = \sum_{i} \rho_{i,i} = 1$

<sup>&</sup>lt;sup>18</sup>We do not go further into the spectrum caracterisation of  $\hat{H}_{TC}$ , even if it may be done, because the master equation shall complexify the exact solution at a point that we use another approach for the numerical simulation.

As a ket state obeys to Schrodinger's equation, one can derive a similar equation of evolution for a density matrix, called *Liouville - von Neumann* equation. Indeed, one may consider the two following equations:

$$i\hbar\partial_t|\phi\rangle = \hat{H}|\phi\rangle \Leftrightarrow -i\hbar\partial_t\langle\phi| = \langle\phi|\hat{H}$$
 (1.66)

where  $|\phi\rangle$  is any solution to the Schrodinger equation. Then coupling those to (1.64) one shall find:

$$i\hbar\dot{\rho} = \left[\hat{H}, \rho\right] \Leftrightarrow \dot{\rho} = -\frac{i}{\hbar} \left[\hat{H}, \rho\right]$$
 (1.67)

One can notice that this equation relies on the Schrodinger point of view, where the states evolves in time whereas the operators are static. At the opposite, the Heinsenberg picture gives:

$$\dot{\hat{X}} = \frac{i}{\hbar} \left[ \hat{H}, \hat{X} \right] \tag{1.68}$$

where  $\hat{X}$  is any operator (not necessecarily an observable or hermitian).<sup>19</sup>

At this point, we are able to simulate the evolution of the closed quantum TC-model for any initial state. It turns out that our experiment involves several *leaks* (in and out) in term of global energy: they are three in number:

- Cavity leak: as mentionned in section 1.1, the cavity purpose is to release a part of the electric field (at the cost of the linewidth broadened) in order to actually collect the radiation. In other words, some photons are transmitted through one of the mirror: this is a global energy loss in our TC system.
- Gain medium leak: counter-intuitively, the atoms (or dipole systems) may incoherently release a photon with frequency very different to the actual cavity resonances. Those photons does not couple to the surrounding electric field and are lost: this effect is another global energy loss and is called *spontaneous decay into free space*.
- Gain medium repump: as the expriments works on a *quasi*-continous radiation, even starting with excited atoms (which is not the case), we need to add some energy in order to compensate the phase coherent decay of our atoms which produce the actual radiation (through the cavity leak). This is a global energy gain in the system.

Therefore, we introduce a quantum bath system which represent the environment of our TC quantum system. The total hamiltonian reads<sup>20</sup>

$$\hat{H}_{total} = \hat{H}_{TC} + \hat{H}_{bath} + \hat{H}_{TC-bath} \tag{1.69}$$

Then, one chooses the interaction picture where the evolution is set by the interaction hamiltonian  $\hat{H}_{TC-bath}$  between the bath and our system. One starts with a bath and our system without cross correlation. Afterward, the time evolution of the density matrix of the total system can be written in term of an infinite iterative equation: one uses the *Born* approximation stating that the bath-TC interaction coupling is weak compared to the size of the bath, allowing to *cut* the infinite serie as the bath evolution is independent of the system evolution. Then, one makes a last assomption that the

This brutal change of picture shall be crucial for the section introducing  $g^1$  and  $g^2$  simulation with the cumulant expansion technique.

<sup>&</sup>lt;sup>20</sup>For simplicity, we drop the tensor product but it is important to keep in mind that the total hamiltonian lives into an Hilbert space with higher dimension than the TC system.

bath has a *short memory* meaning that the correlations are not significant for long time intervals if the bath is subject to fast dynamics: this is the *Markov* approximation.

At the end of the day, one obtains the open quantum system equation, often called the *master equation*:

$$\dot{\rho} = -\frac{i}{\hbar} \left[ \hat{H}, \rho \right] + \sum_{j} \gamma_{j} \left( \hat{L}_{j} \rho \hat{L}_{j}^{\dagger} - \frac{1}{2} \left\{ \hat{L}_{j}^{\dagger} \hat{L}_{j}, \rho \right\} \right)$$

$$(1.70)$$

where j indexes the different leak operators  $\hat{L}_j$ , often called jump operators or more simply lindblad operators. Also,  $\gamma_j$  are the associated damping rate (even if the operator's purpose may be to add energy) and the curly brackets are the anti-commutator relation. Equivalently for the Heisenberg picture, on finds:

$$\dot{\hat{X}} = \frac{i}{\hbar} \left[ \hat{H}, \hat{X} \right] + \sum_{j} \gamma_{j} \left( \hat{L}_{j}^{\dagger} \hat{X} \hat{L}_{j} - \frac{1}{2} \left\{ \hat{L}_{j}^{\dagger} \hat{L}_{j}, \hat{X} \right\} \right)$$
(1.71)

where one may notice the sign difference in front of the commutator and the opposite dagger symbol on the lindblad operator of the first term of the sum. In our case, we get three lindblad operators, representing the various *leaks* of the TC quantum system:

- The cavity leak or cavity decay operates at a rate  $\kappa$ . The associated lindblad operator is the destruction operator of the cavity field  $\hat{a}$ : this ladder operator removes energy from the harmonic oscillator.
- The spontaneous decay into free space operates at a rate  $\gamma$ . The associated lind-blad operator is the collective spin ladder operator  $\hat{S}_{-}$  which collectively removes energy from the atomic system.
- The repump operates at a rate  $\nu$  and is associated to the lindblad operator  $\hat{S}_+$ : we assume that an external laser *feeds* collectively the ensemble of two-level system, which has for effect to add energy into the TC quantum system.

To summarize, the density matrix evolution responds to the following first order differential equation:

$$\dot{\rho} = \left[ \rho, i\Delta\omega \,\hat{n} + \frac{i}{\hbar}g \left( \hat{S}_{+}\hat{a} + \hat{S}_{-}\hat{a}^{\dagger} \right) \right]$$

$$+ \kappa \left( \hat{a}\rho\hat{a}^{\dagger} - \frac{1}{2} \left\{ \hat{a}^{\dagger}\hat{a}, \rho \right\} \right)$$

$$+ \gamma \left( \hat{S}_{-}\rho\hat{S}_{+} - \frac{1}{2} \left\{ \hat{S}_{+}\hat{S}_{-}, \rho \right\} \right)$$

$$+ \nu \left( \hat{S}_{+}\rho\hat{S}_{-} - \frac{1}{2} \left\{ \hat{S}_{-}\hat{S}_{+}, \rho \right\} \right)$$

$$(1.72)$$

where with have taken  $\hat{H}_{TC}$  as the hamiltonian. There is a similar equation (close to a sign and dagger operators) for any operator  $\hat{X}$ . This differential equation is a system of linear differential equation in a sense that each time derivated term of the density matrix is dependent of linear terms of the density matrix. In other words:

$$\rho_{i,j} = \sum_{k,l} \alpha_{k,l} \rho_{k,l} \tag{1.73}$$

where  $\rho_{i,j}$  are the density matrix components with indices (i,j)  $\alpha_{k,l}$  are fixed complex coefficient dependent on operator values and constants.

Thereby, this system is numerically solvable with standard integration methods as the Runge-Kutta approach.<sup>21</sup> As one could think, if the system is linear, it should be diagonalizable hence exactly solvable by exponentiation. However, this approach is not possible in the form of (1.72) as the equation is treating the density operator as, obsviously, a matrix.

Nevertheless, one may introduce a new concept called the *linearization* of the density operator. In fact, the density matrix lies in the Hilbert space  $\mathcal{H}_{TC} = \mathcal{H}_{cav} \otimes \mathcal{H}_{atoms}$  and one may transform this matrix into a vector lying in the new space  $\mathcal{H}_{TC} \otimes \mathcal{H}_{TC}$ , which is often called the *Fock-Liouville space*. In this way, (1.65) becomes:

$$\rho = \sum_{i,j} \rho_{i,j} |i\rangle\langle j| \to \sum_{i,j} \rho_{i,j} |i\rangle \otimes |j\rangle = \begin{pmatrix} \rho_{0,0} \\ \rho_{0,1} \\ \vdots \\ \rho_{n-1,n-1} \end{pmatrix} \stackrel{\text{def}}{=} |\rho\rangle\rangle$$
 (1.74)

where n is the dimension of  $\mathcal{H}_{TC}$ . Then, the von-Neumann equation (1.67) transforms as:

$$\dot{\rho} = -\frac{i}{\hbar} \left( \hat{H} \rho - \rho \hat{H} \right) \to |\dot{\rho}\rangle\rangle = -\frac{i}{\hbar} \mathcal{H} |\rho\rangle\rangle \tag{1.75}$$

where  $\mathcal{H}$  is a superoperator defined as  $\mathcal{H}|\cdot\rangle\rangle \to \left[\hat{H},\cdot\right]$ .<sup>22</sup> Similarly, one may define the lindblad superoperator:

$$\mathcal{D}[\hat{L}_j]|\rho\rangle\rangle \to \hat{L}_j\rho\hat{L}_j^{\dagger} - \frac{1}{2}\left\{\hat{L}_j^{\dagger}\hat{L}_j, \rho\right\}$$
(1.76)

and the master equation becomes:

$$|\dot{\rho}\rangle\rangle = -\frac{i}{\hbar}\mathcal{H}|\rho\rangle\rangle + \kappa\mathcal{D}[\hat{a}]|\rho\rangle\rangle + \gamma\mathcal{D}[\hat{S}_{-}]|\rho\rangle\rangle + \nu\mathcal{D}[\hat{S}_{+}]|\rho\rangle\rangle$$

$$= \left(-\frac{i}{\hbar}\mathcal{H} + \kappa\mathcal{D}[\hat{a}] + \gamma\mathcal{D}[\hat{S}_{-}] + \nu\mathcal{D}[\hat{S}_{+}]\right)|\rho\rangle\rangle$$

$$= \mathcal{L}|\rho\rangle\rangle$$
(1.77)

where we defined the Liouvillian superoperator  $\mathcal{L}$  from the second line of the equation. From that, it is possible to calculate the eigenvalues and eigenvectors in order to find the exact values of  $|\rho\rangle\rangle$  at any time t.<sup>23</sup>

However, the first limitation of this method is the size of the system. Indeed, as  $\mathcal{H}_{TC}$  scales according to  $(N+1) \times N_{Fock}$  then the Fock-Liouville space scales as the square:

$$\dim \left( \mathscr{H}_{TC} \otimes \mathscr{H}_{TC} \right) = \left( (N+1) \times N_{Fock} \right)^2 \tag{1.78}$$

In order to hold the decay of the atoms, the Fock space associated to the cavity field must be at least the same dimension as the number of two-level systems.<sup>24</sup> Then, for

<sup>&</sup>lt;sup>21</sup>Note that the Runge-Kutta method is not restricted to linear systems as, by definition, this approach treats any function f where  $\dot{y}=f(y,t)$  and y can be any variable of any vector space:  $y \in \mathbb{R}, \mathbb{R}^2, \mathbb{R}^3, ..., \mathbb{C}, \mathbb{C}^2, \mathbb{C}^3, ...$  for examples.

<sup>&</sup>lt;sup>22</sup>This is not a definition symbol because the left side does not lie in the same space as the right side:  $\mathcal{H}$  belongs to the *superspace*  $\mathscr{H}_{TC} \otimes \mathscr{H}_{TC}$  whereas the commutator lies in  $\mathscr{H}_{TC}$  only.

<sup>&</sup>lt;sup>23</sup>Note that as the Liouvillian superoperator is not hermitian by construction, the right and left eigenvectors are associated to different eigenvalues. See [??] for more details.

<sup>&</sup>lt;sup>24</sup>In practice, we take twice the size for *security* and a double check of the photon number, after computation, asserts that we are not overflowing the Fock space.

N dipoles as a gain medium:

$$\dim \left( \mathcal{H}_{TC} \otimes \mathcal{H}_{TC} \right) \sim N^4 \tag{1.79}$$

Thereby, the number of components for the vector  $|\rho\rangle$  scales according to the same rule. Moreover, the number of components inside the *super*-matrix representing the Liouville superoperator scales as the square of it, namely as  $N^8$ . For instance, let's say that we want to numerically simulate our model with one hundred atoms: the supermatrix owns  $10^{16}$  components. As each component is a complex number represented by two floats of 32-bit each (in the low precision case): 8 byte per component. At the end of the day, we need approximately 80,000 TB only to store the Liouvilian superoperator<sup>25</sup>. Ideally, we would like to simulate a couple of millions of atoms.

Unfortunately, the first method of solving, involving the RK intergation, suffers the same problem for many particles: as we stay in the original Hilbert space  $\mathscr{H}_{TC}$ , the power scale is less important but many atoms simulation is still unreachable for more than a few hundreds of atoms. Even worse, this solution is not exact, in a sense that we get the solution for a finite time interval where the computation time is dependent on it!

This case is a good example of the classical computer limitation and this sort of problem is part of the reason of building a quantum computer/simulator. Indeed, one could make use of the parallelism behavior of the qubit in order to simulate many cross interaction at the same time. However, those kind of projects are not yet achieved and we have to find a *smart* solution, in a sense that we are ready to lose a bit of precision in exchange of computation power and memory space. In fact, all the crossed terms essentially represent the multiple interaction holded by each atom. Secondly, the question we have to ask is: "what mesure do we want from the simulation?". As we shall see in later section, our interested correlation function are, roughly, the expectation values of operators across the time. In other words, we absolutely do not care about the behavior of individual terms. So, what happens if one plugs directly the exceptation value on the "Heisenberg version" of the master equation (1.71)? This is the subject of the next section.

### 1.5 Cumulant expansion method

Firstly, even if we go into more details in chapter ?? about their signification, we have to recall what are the first and second order correlation function in term of quantum operators in order to visualize which sort of values we need to extract from the master equation.

Thereby, in the case of a non-stationary electric field, one can define the first order correlation function as:

$$g^{1}(t_{1}, t_{2}) \stackrel{\text{def}}{=} \frac{\langle E^{*}(t_{1})E(t_{2})\rangle}{\sqrt{\langle |E(t_{1})|^{2}\rangle \langle |E(t_{2})|^{2}\rangle}}$$
(1.80)

where  $E(t) \in \mathbb{C}$  is the phasor representation of the electric field and the mean symbol  $\langle \cdot \rangle$  is an ensemble average over a set of electric signal. Note that we also make the assumption that the correlation measurement is done at  $r_1 = r_2 = 0$  for both detectors of the electric field.

 $<sup>^{25}1</sup>TB = 1000 \text{ GB}$  which is somehow a common hard-drive capacity for the family computers on the current tech-market (2024).

In turns out that any eletric field can be quantized with the help of an artificial  $quantization \ box$  of volume V and the associated formulas are:

$$\hat{E}^{+} = i \sum_{\vec{k},\lambda} \sqrt{\frac{\hbar \omega_{k}}{2\epsilon_{0} V}} \hat{a}_{\vec{k},\lambda} e^{i\vec{k}\cdot\vec{r}} \vec{e}_{\vec{k},\lambda} \qquad \hat{E}^{-} = -i \sum_{\vec{k},\lambda} \sqrt{\frac{\hbar \omega_{k}}{2\epsilon_{0} V}} \hat{a}_{\vec{k},\lambda}^{\dagger} e^{-i\vec{k}\cdot\vec{r}} \vec{e}_{\vec{k},\lambda}^{*} \qquad (1.81)$$

where  $\omega_k$  is the mode frequency associated to the polarization vector  $\overrightarrow{k}$ ,  $\overrightarrow{e}_{\overrightarrow{k},\lambda} \in \mathbb{C}^3$  is the unit vector perpendicular to  $\overrightarrow{k}$ , with  $\lambda$  signifying one of the two vectors that are perpendicular to the polarization vector. Now, making the assumption that the electric field is composed of one frequency (i.e a unique mode of the *fake*-cavity) and replacing the electric field phasor components by their quantum operator counterparts, one finds the quantum equivalent of the first order correlation function:

$$g^{1}(t_{1}, t_{2}) = \frac{\langle \hat{a}^{\dagger}(t_{1})\hat{a}(t_{2})\rangle}{\sqrt{\langle \hat{a}^{\dagger}(t_{1})\hat{a}(t_{1})\rangle \langle \hat{a}^{\dagger}(t_{2})\hat{a}(t_{2})\rangle}}$$
(1.82)

where we may notice that the denominator terms are function of the mean photon number  $\hat{n}$  at time  $t_1$  and  $t_2$ . Moreover, we considered the time evolution of the electric field as the time evolution of the operators, in other words, the Heisenberg picture. This consideration comes from the fact that the numerator is a mean value of two operators evaluated at a different time each. Indeed, we define the mean value of any operator  $\hat{X}$  as the quantum measurement of  $\hat{X}$  over a pure state  $|\psi\rangle$  or a density matrix  $\rho$ :<sup>26</sup>

$$\left\langle \hat{X} \right\rangle_{\psi \, or \, \rho} = \left\langle \psi | \hat{X} | \psi \right\rangle \quad or \quad \text{Tr} \left[ \rho \hat{X} \right]$$
 (1.83)

Which leads, for the time evolution of the mean value, to the two famous pictures (considering a density matrix as the measured state):

Schrödinger picture: 
$$\left\langle \hat{X} \right\rangle_{\rho}(t) = \text{Tr}\left[\rho(t) \cdot \hat{X}\right]$$
Heisenberg picture:  $\left\langle \hat{X} \right\rangle_{\rho}(t) = \text{Tr}\left[\rho \cdot \hat{X}(t)\right]$  (1.84)

If we set  $\hat{X}(t_1, t_2) = \hat{Y}(t_1)\hat{Z}(t_2)$ , it becomes obvious that the Heinsberg picture is appropriate:

$$\left\langle \hat{X} \right\rangle_{\rho} (t_1, t_2) = \text{Tr} \left[ \rho \cdot \hat{Y}(t_1) \cdot \hat{Z}(t_2) \right]$$
 (1.85)

In other words, we are looking for the time evolution of  $\hat{a}^{\dagger}$  and  $\hat{a}$  but not the time evolution of the initial state. By the way, those previous equations shows that the quantum  $q^1$  is dependent on the choice of the initial state.

It is important to note that  $g^1$  is by definition a 2D map<sup>27</sup>. As we are going to run numerical simulations through it, we can consider  $t_2$  as a fixed value and compute the time evolution of  $g^1$  according to  $t_1$ :

$$g^{1}(t_{1})_{t_{2}} = \frac{\langle \hat{a}^{\dagger}(t_{1})\hat{a}_{t_{2}}\rangle}{\sqrt{\langle \hat{n}(t_{1})\rangle \langle \hat{n}_{t_{2}}\rangle}}$$

$$(1.86)$$

which is a 1D map (i.e a function), then repeat the process for every  $t_2$  of the targeted time interval.

 $<sup>^{26}</sup>$ Equation (1.83) is directly derivated from the second postulate (measurement postulate) of the Quantum Mechanic Theory.

<sup>&</sup>lt;sup>27</sup>Only in its non-stationary form.

Moreover, in the stationary case, the distribution of the electric signal is independent of time and one may find that  $g^1$  is only dependent on the time difference  $t_1 - t_2 \stackrel{\text{def}}{=} \tau$ :

$$g^{1}(\tau)_{stationary} = \frac{\langle \hat{a}^{\dagger}(t_{2} + \tau)\hat{a}(t_{2})\rangle}{\sqrt{\langle \hat{n}(t_{2} + \tau)\rangle \langle \hat{n}(t_{2})\rangle}} = \frac{\langle \hat{a}^{\dagger}(\tau)\hat{a}(0)\rangle}{\sqrt{\langle \hat{n}(\tau)\rangle \langle \hat{n}(0)\rangle}}$$
(1.87)

where we set  $t_2 = 0$  as the process is considered as stationary, hence, independent on the reference time. Note the similarities with the non-stationary case (1.86) from a computational point of view: the reference time  $t_2$  is just a question of initial value of the operators  $\hat{a}$  and  $\hat{n}$ .

Similarly, for the classical second order correlation function, one defines:

$$g^{2}(t_{1}, t_{2}) \stackrel{\text{def}}{=} \frac{\langle E^{*}(t_{2})E^{*}(t_{1})E(t_{1})E(t_{2})\rangle}{\langle |E(t_{1})|^{2}\rangle \langle |E(t_{2})|^{2}\rangle}$$
(1.88)

Then, the quantum equivalent reads as:

$$g^{2}(t_{1}, t_{2}) = \frac{\left\langle \hat{a}^{\dagger}(t_{2})\hat{a}^{\dagger}(t_{1})\hat{a}(t_{1})\hat{a}(t_{2})\right\rangle}{\left\langle \hat{n}(t_{1})\right\rangle \left\langle \hat{n}(t_{2})\right\rangle}$$
(1.89)

As before, the stationary assumption allows us to write<sup>28</sup>:

$$g^{2}(\tau) = \frac{\left\langle \hat{a}^{\dagger}(0)\hat{a}^{\dagger}(\tau)\hat{a}(\tau)\hat{a}(0)\right\rangle}{\left\langle \hat{n}(\tau)\right\rangle \left\langle \hat{n}(0)\right\rangle}$$
(1.90)

At the end of day, the desired quantities are complex values dependent on operator evolution. That is to say, we actually want the quantum measurement of the ladder and photon number operators. Then, let's start with the value  $\langle \hat{a}^{\dagger} \rangle$  from the differential equation:

$$\frac{d}{dt}\hat{a}^{\dagger} = \frac{i}{\hbar} \left[ \hat{a}^{\dagger}, \hat{H}_{TC} \right] 
+ \kappa \left( \hat{a}\hat{a}^{\dagger}\hat{a}^{\dagger} - \frac{1}{2}\hat{a}^{\dagger}\hat{a}\hat{a}^{\dagger} - \frac{1}{2}\hat{a}^{\dagger}\hat{a}^{\dagger}\hat{a} \right) 
+ \gamma \left( \hat{S}_{-}\hat{a}^{\dagger}\hat{S}_{+} - \frac{1}{2}\hat{S}_{+}\hat{S}_{-}\hat{a}^{\dagger} - \frac{1}{2}\hat{a}^{\dagger}\hat{S}_{+}\hat{S}_{-} \right) 
+ \nu \left( \hat{S}_{+}\hat{a}^{\dagger}\hat{S}_{-} - \frac{1}{2}\hat{S}_{-}\hat{S}_{+}\hat{a}^{\dagger} - \frac{1}{2}\hat{a}^{\dagger}\hat{S}_{-}\hat{S}_{+} \right)$$
(1.91)

which is the *Heisenberg* equivalent of (1.72).<sup>29</sup> One uses the standard commutation relations, remembering that the collective spin operator does not lie into the same space as the cavity ladder operators then one obtains<sup>30</sup>:

$$\frac{d}{dt}\hat{a}^{\dagger} = \left(i\Delta\omega - \frac{\kappa}{2}\right)\hat{a}^{\dagger} + \frac{ig}{\hbar}\hat{S}_{+} \tag{1.92}$$

<sup>&</sup>lt;sup>28</sup>It is possible to define  $t_2 - t_1 \stackrel{\text{def}}{=} \tau$ . This time reverse step does not affect the function itself as  $g^2(\tau) = g^2(-\tau)$  for a stationary process. The same property hold for  $g^1$ .

<sup>&</sup>lt;sup>29</sup>We intentionally omit the artificial order of the operators that we made earlier for the implicit representation of the tensor structure: no ordering allows us to highlight the lindblad operators.

<sup>&</sup>lt;sup>30</sup>See details in Annexe??

Making measurement according to a state  $\rho$  and knowing that a projection is a linear operation on a time derivative, one gets:

$$\frac{d}{dt} \left\langle \hat{a}^{\dagger} \right\rangle = \left( i\Delta\omega - \frac{\kappa}{2} \right) \left\langle \hat{a}^{\dagger} \right\rangle + \frac{ig}{\hbar} \left\langle \hat{S}_{+} \right\rangle \tag{1.93}$$

which is again a differential equation involving but involving only complex (or real) numbers: we have lost all the cross interaction information contained inside the operator and reduced it to the mean value of the operators. However, this first order differential equation is of two variable instead of one as the master equation with the variable  $\rho$ . Indeed,  $\langle \hat{S}_{+} \rangle$  is also time dependent and one needs its time evolution in order to solve the equation: in fact, we are actually treating a system of equations and are now looking for the second member. Then, we can reengage the process with the operator  $\hat{S}_{+}$  instead and the differential equation is this time:

$$\frac{d}{dt} \left\langle \hat{S}_{+} \right\rangle = -2ig \left\langle \hat{S}_{+} \hat{a}^{\dagger} \right\rangle + \hbar(\nu - \gamma) \left\langle \hat{S}_{z} \hat{S}_{+} \right\rangle - \nu \hbar^{2} \left\langle \hat{S}_{+} \right\rangle \tag{1.94}$$

Unfortunately, this new equation leads to new variables, namely:  $\langle \hat{S}_{+} \hat{a}^{\dagger} \rangle$  and  $\langle \hat{S}_{z} \hat{S}_{+} \rangle$ . Moreover, the mean value or cross-correlation between two operators (or even for two random variable from a classical point of view) is not equal to the multiplication of the individual correlations:

$$\langle \hat{X}\hat{Y} \rangle \neq \langle \hat{X} \rangle \langle \hat{Y} \rangle$$
 (1.95)

Therefore, it makes sense to write:

$$\left\langle \hat{X}\hat{Y}\right\rangle = \left\langle \hat{X}\right\rangle \left\langle \hat{Y}\right\rangle \tag{1.96}$$

only if we assume that  $\hat{X}$  and  $\hat{Y}$  are independent in term of probability representation. In that case, one loses all the quantum interaction happening in the correlated variables: this approximation is named mean field approximation.

If one applies this approximation, one shall obtain:

$$\frac{d}{dt} \left\langle \hat{S}_{+} \right\rangle = -2ig \left\langle \hat{S}_{+} \right\rangle \left\langle \hat{a}^{\dagger} \right\rangle + \hbar(\nu - \gamma) \left\langle \hat{S}_{z} \right\rangle \left\langle \hat{S}_{+} \right\rangle - \nu \hbar^{2} \left\langle \hat{S}_{+} \right\rangle \tag{1.97}$$

Now the only missing variable equation evolution is  $\langle \hat{S}_z \rangle$ . Then we repeat the process again and we find two more equations.

$$\frac{d}{dt} \left\langle \hat{S}_z \right\rangle = -ig \left\langle \hat{S}_+ \right\rangle \left\langle \hat{a} \right\rangle + ig \left\langle \hat{S}_- \right\rangle \left\langle \hat{a}^{\dagger} \right\rangle + \hbar(\gamma - \nu) \left\langle \hat{S}_- \right\rangle \left\langle \hat{S}_+ \right\rangle - 2\nu \hbar^2 \left\langle \hat{S}_z \right\rangle \quad (1.98)$$

One can be tented to develop two more variables which would be  $\langle \hat{S}_{-} \rangle$  and  $\langle \hat{a} \rangle$ . However, those two operators are the conjugate transpose of  $\hat{S}_{+}$  and  $\hat{a}^{\dagger}$  respectively and their quantum measurement is just complex conjugate:

$$\left\langle \hat{S}_{-} \right\rangle = \left\langle \hat{S}_{+} \right\rangle^{*} \qquad \left\langle \hat{a} \right\rangle = \left\langle \hat{a}^{\dagger} \right\rangle^{*}$$
 (1.99)

Therefore, the three differential equations (1.93), (1.97) and (1.98) form a complete system of equation, hence, can be solved taking the initial values as:

$$\langle \hat{a}^{\dagger} \rangle (t=0) = \text{Tr} \left[ \rho \hat{a}_0^{\dagger} \right]$$
 (1.100)

where  $\rho$  is the initial density matrix of the system and  $\hat{a}_0^{\dagger}$  is the common constructor operator<sup>31</sup>. One may say that this system of equation is a *closed* form in a sense that, with the mean field approximation, if one chooses any of the five operators  $\hat{a}^{\dagger}, \hat{a}, \hat{S}_+, \hat{S}_-$  or  $\hat{S}_z$  at the start, then the final set of differential would be exactly the same as (1.93), (1.97) and (1.98) (taking into account the complex conjugated equations).

Now, we have to remember that, in addition of retrieving the quantum correlation lost with the mean field approximation (i.e a first order approximation), our goal is to get the evolution of correlation functions involving several operators. In fact, it is clear that if we develop a differential equation with  $\langle \hat{S}_{+} \hat{a}^{\dagger} \rangle$  for example, we shall get correlation variables involving three or more operators. Repeating the process will certainly give an infinity amount of differential equations. In other words, we have to break the loop with a certain order of approximation. In this way, one may invoke the definition of the joint cumulant:

$$\left\langle \hat{X}_1 \hat{X}_2 ... \hat{X}_n \right\rangle_c \stackrel{\text{def}}{=} \sum_{p \in P(\mathcal{I})} (|p| - 1)! (-1)^{|p| - 1} \prod_{B \in p} \left\langle \prod_{i \in B} \hat{X}_i \right\rangle$$
 (1.101)

where  $\mathcal{I} = \{1, 2, ..., n\}$ ,  $P(\mathcal{I})$  is the set of all partition of  $\mathcal{I}$ , |p| is the length of the partition and B is successively each element of the partition. It is possible to prove (ref??) that the joint cumulant is null if any operator  $\hat{X}_i$  is independent of all the others (in term of probabilities). Then, the main approximation is to assume that, at a certain number of operator m inside the cumulant, at least one of the operator among them is independent of the others. This implies  $\langle \hat{X}_1 \hat{X}_2 ... \hat{X}_m \rangle_c = 0$  and one may write:

$$\left\langle \hat{X}_1 \hat{X}_2 ... \hat{X}_m \right\rangle = \sum_{p \in P(\mathcal{I})/\mathcal{I}} (|p| - 1)! (-1)^{|p|-1} \prod_{B \in p} \left\langle \prod_{i \in B} \hat{X}_i \right\rangle$$
 (1.102)

where  $\mathcal{I} = \{1, 2, ..., n\}$  and  $P(\mathcal{I})/\mathcal{I}$  is the set of all the partitions of  $\mathcal{I}$  without  $\mathcal{I}$  itself. From that, it is obvious that the mean field approximation is condidering this formula with m = 2. Then, for m = 3:

$$\left\langle \hat{X}_{1}\hat{X}_{2}\hat{X}_{3}\right\rangle = \left\langle \hat{X}_{1}\hat{X}_{2}\right\rangle \left\langle \hat{X}_{3}\right\rangle + \left\langle \hat{X}_{1}\hat{X}_{3}\right\rangle \left\langle \hat{X}_{2}\right\rangle + \left\langle \hat{X}_{2}\hat{X}_{3}\right\rangle \left\langle \hat{X}_{1}\right\rangle - 2\left\langle \hat{X}_{1}\right\rangle \left\langle \hat{X}_{2}\right\rangle \left\langle \hat{X}_{3}\right\rangle \tag{1.103}$$

and so on for m > 3. This approximation is named the *cumulant expansion method*.

At the end of day, the algorithmic approach is choosing an order m where, if one finds a correlation variable with m or more operators inside of the correlation brackets when developing the set of equations, one applies the cumulant expansion in order to transform a correlation variable of m operators into several correlation variables of m-1 operators. In other words, m is the amount of operators where one breaks the loop. Finally, one may choose any order of approximation knowing that greater is the order (i.e, more operator we have inside the correlation brackets), more quantum correlations one takes into account (i.e more precision in the simulation) but more equations one has to treat and more computational power is needed. The question is then to find a good compromise.

Nevertheless, at any order of the expansion one can go, the time evolution of the correlation variable involve the time evolution of all the operators inside of it at the

 $<sup>^{31}</sup>$ Note that a t=0, quantum measurements according to the Schrödinger or Heisenberg picture are equivalent.

same time reference. That is to say:

$$\langle \hat{X}_1 \hat{X}_2 \rangle (t) = \langle \hat{X}_1(t) \hat{X}_2(t) \rangle$$
 (1.104)

for instance. In other words, one cannot access the  $g^1$  and  $g^2$  values directly from this method as those two correlation involve different time evolution of the operators. However, one may see from (1.86) that the desired differential equation needed for  $g^1$  before making the quantum measurement (i.e before applying  $\langle \cdot \rangle$ ) reads:

$$\frac{d}{dt_1} \left( \hat{a}^{\dagger}(t_1) \hat{a}_{t_2} \right) = \frac{d}{dt_1} \left( \hat{a}^{\dagger}(t_1) \right) \hat{a}_{t_2} \tag{1.105}$$

where  $\hat{a}_{t_2}$  is treated as a constant compared to  $t_1$ . We can see that the right term of the previous equation calls the already derivated formula (1.92) of  $\hat{a}^{\dagger}$ , which is of the form:

$$\frac{d}{dt_1}\hat{a}^{\dagger}(t_1) = f(\hat{a}^{\dagger}(t_1)) \tag{1.106}$$

where f is basically the heisenberg version of the master equation. Then multiplying by a tre constant operator (compared to  $t_1$ ), namely  $\hat{a}_{t_2}$  <sup>32</sup>, one obtains:

$$\frac{d}{dt_1} \left( \hat{a}^{\dagger}(t_1) \right) \hat{a}_{t_2} = f(\hat{a}^{\dagger}(t_1)) \hat{a}_{t_2} \tag{1.107}$$

which, in the case of (1.92), reads as:

$$\frac{d}{dt_1} \left( \hat{a}^{\dagger}(t_1) \right) \hat{a}_{t_2} = \left( i\Delta\omega - \frac{\kappa}{2} \right) \hat{a}^{\dagger}(t_1) \hat{a}_{t_2} + \frac{ig}{\hbar} \hat{S}_{+}(t_1) \hat{a}_{t_2}$$
 (1.108)

Now, one can make a quantum measurement and gets:

$$\frac{d}{dt_1} \left\langle \hat{a}^{\dagger}(t_1)\hat{a}_{t_2} \right\rangle = \left( i\Delta\omega - \frac{\kappa}{2} \right) \left\langle \hat{a}^{\dagger}(t_1)\hat{a}_{t_2} \right\rangle + \frac{ig}{\hbar} \left\langle \hat{S}_+(t_1)\hat{a}_{t_2} \right\rangle \tag{1.109}$$

Of course, this multiplication followed by quantum measurement must be applied to the whole set of differential equation in order to update all the correlation variables: before obtaining (1.109), one derived the closed system of equation containing  $\langle \hat{S}_{+}(t_1) \rangle$  but not  $\langle \hat{S}_{+}(t_1) \hat{a}_{t_2} \rangle^{33}$ .

The initial value of (1.109) is expressed as:

$$\left\langle \hat{a}^{\dagger}(t_1)\hat{a}_{t_2}\right\rangle(t_1=0) = \left\langle \hat{a}_0^{\dagger}\hat{a}_{t_2}\right\rangle \tag{1.110}$$

However, we do not dispose to this information as we only know the initial operator values  $\hat{a}_0^{\dagger}$  and  $\hat{a}_0$  but not the time evolution of  $\hat{a}_{t_2}$ . Nevertheless, if we derive a set of equation to a certain order allowing the access to the correlation variable  $\langle \hat{a}^{\dagger}(t)\hat{a}(t)\rangle$ , then we can get any initial value of (1.109) for  $t_1 = t_2$ : solving the system of differential equation leads to solution with  $t_1 \geq t_2$  which represents the lower-half of the 2D map according to the diagonal  $t_1 = t_2$  as on Fig ??.

This initial value problem only stands for non-stationary processes. Indeed, for a stationary process, we firstly have to numerically compute a time interval long enough

 $<sup>^{32}</sup>$ We make this choice of  $\hat{a}_{t_2}$  in order to fit the  $g^1$  notation but it is important to keep in mind that it could be any constant operator.

<sup>&</sup>lt;sup>33</sup>Algorithmically speaking, the set is first derived without applying the brackets (i.e quantum measurement), then the multiplication and brackets are applied.

to reach the steady-state of the correlation variables. Then, as stated in the begining of this section,  $g^1$  for a stationary process is dependent on the time difference  $\tau$ , that is to say, once  $\langle \hat{a}^{\dagger}(t)\hat{a}(t)\rangle$  is stable after a certain amount of time, let's say at  $t=t_{stable}$ , we have the following relation:

$$\langle \hat{a}^{\dagger}(t_1 + t_{stable}) \hat{a}_{t_2 + t_{stable}} \rangle = \langle \hat{a}^{\dagger}(t_1) \hat{a}_{t_2} \rangle \tag{1.111}$$

hence,  $\langle \hat{a}^{\dagger}(t_{stable})\hat{a}_{t_{stable}}\rangle$  becomes the initial value of (1.109). Obviously, the same argmuent applies for the whole system of differential equations.

Similarly, equivalent steps allow us to compute  $g^2$ . Indeed, this time the desired differential equation reads:

$$\frac{d}{dt_1} \left( \hat{a}_{t_2}^{\dagger} \hat{a}^{\dagger}(t_1) \hat{a}(t_1) \hat{a}_{t_2} \right) = \hat{a}_{t_2}^{\dagger} \left( \frac{d}{dt_1} \hat{a}^{\dagger}(t_1) \hat{a}(t_1) \right) \hat{a}_{t_2}$$
(1.112)

which leads to calulate the differential equation (hence, the complete set of differential equation) for:

$$\frac{d}{dt} \left( \hat{a}^{\dagger}(t)\hat{a}(t) \right) \tag{1.113}$$

then multiplying the full set on the left by  $\hat{a}_{t_2}^{\dagger}$  and on the right by  $\hat{a}_{t_2}$  before doing the quantum measurement (i.e applying the brackets). The initial values are computed from a complete set of equation involving:

$$\langle \hat{a}^{\dagger}(t)\hat{a}^{\dagger}(t)\hat{a}(t)\hat{a}(t)\rangle$$
 (1.114)

Again, this allows time evolution only when  $t_1 \ge t_2$  for non-stationary process whereas we need to reach the steady-state of the set of differential equation involving (1.114) in order to get the stable values hence a stationary process for  $q^2(\tau)$ .

In general, if one wants to numerically simulate the behavior of  $g^1$  and  $g^2$  of the quantum system (stationary or not), it is necessary to generate a complete set of equation at a minimum order of m=5 (i.e maximum four operators inside the correlation variables). From this set of equation, one must generate another set by multiplying the first set with  $\hat{a}_{t_2}$  by the right. Finally, the last set is generated from the second one by multiplying it with  $\hat{a}_{t_2}^{\dagger}$  by the left. At the end of the day, one gets three independent complete set of differential equation of order, at least, m=5, m=6 and m=7. <sup>34</sup>

<sup>&</sup>lt;sup>34</sup>The variable m is artificially incremented by one each time as the correlation variables get an additional operator constant: we do not derive explicitly a set with m = 6 and m = 7.

# Chapter 2

# Heterodyne experiment

### 2.1 Standard setup for $g^1$ and its limitations

In this section, we shall describe a standard method of measuring the frist order correlation function of a given classical electric field. This is meant to introduce some concepts of wave mixing, intensity detection and noise limit. Some detection properties are limited in the present case and this give a justification of the setup used in the actual experiment for measuring  $g^1$ .

Firstly, let's consider a linearly poilarized electric field  $E_1(x,t)$  in its phasor representation as in equation (1.2) where we droped the vector sign as the field can be described only by its amplitude. Note that at this point, we do not make any hypothesis about the frequencies bearing by this field except that the field is quasi-monochromatic (i.e the linewidth of the emited light is not null around the main frequency beat). This field is our field of interest, that is to say, we want to extract coherence information from it. Thereby, we mix it with another field  $E_2(x,t)$  which trivially gives a total field of:

$$E_{total} = E_1 + E_2 \tag{2.1}$$

Now, we place a detector at x=0 relatively to the total field. However, to highlight the phase difference from a field to another at the detector, we write the second electric field with a time delay  $\tau$ . In the classical view, the role of the detector is to transform a mean light intensity (i.e an amount of photon) into an electric intensity (i.e an amount of electron). With certain hypothesis <sup>1</sup> one may approximate the intensity as:

$$I_{total}(t,\tau) \simeq |\overline{E}_{total}(t)|^2 = (\overline{E}_1(t) + \overline{E}_2(t+\tau))(\overline{E}_1^*(t) + \overline{E}_2^*(t+\tau))$$
$$= |\overline{E}_1(t)|^2 + |\overline{E}_2(t+\tau)|^2 + 2\Re\left\{\overline{E}_1(t)\overline{E}_2^*(t+\tau)\right\}$$
(2.2)

that we may rewrite for simplicity:

$$I_{total}(t,\tau) = I_1(t) + I_2(t+\tau) + 2\Re\left\{\overline{E}_1(t)\overline{E}_2^*(t+\tau)\right\}$$
(2.3)

where the approximation sign is implicit.

Then, we assume that the decrector transfer exactly 100% of the received light into the eletric wire (i.e quantum efficiency  $\eta = 1$ ) and that the collected intensity is the mean value of the total intensity for an interval of time T:

$$I_{detected}(\tau) \stackrel{\text{def}}{=} \langle I_{total}(t) \rangle_T = \langle I_1(t) \rangle_T + \langle I_2(t+\tau) \rangle_T + 2 \left\langle \Re \left\{ \overline{E}_1(t) \overline{E}_2^*(t+\tau) \right\} \right\rangle_T \quad (2.4)$$

<sup>&</sup>lt;sup>1</sup>See section ?? (Data analysis)

with:

$$\langle \cdot \rangle_T = \int_T \cdot dt \tag{2.5}$$

We introduce the correlation variable:

$$\gamma_{1,2}(\tau) \stackrel{\text{def}}{=} \frac{\langle E_1(t)E_2^*(t+\tau)\rangle_T}{\sqrt{\langle I_1(t)\rangle_T \langle I_2(t+\tau)\rangle_T}} \in \mathbb{C}$$
(2.6)

This previous definition transforms  $I_{detected}$  as:

$$I_{detected} = I_1 + I_2 + 2\sqrt{I_1 I_2} \Re \{\gamma_{1,2}\}$$
 (2.7)

where we interchanged  $\Re\{\cdot\}$  with  $\langle\cdot\rangle^2$  and where we dropped the time dependences of the intensity terms (from integration, those terms becomes constant according to the time t). By its normalization factor (i.e the denominator in (2.6)), one may say that the norm of gamma is included between 0 and 1 where 0 holds for complete incoherence whereas 1 holds for full coherence. This means that we can write two extrema:

$$I_{detected,max} = I_1 + I_2 + 2\sqrt{I_1I_2}|\gamma_{1,2}|$$
 (2.8)

$$I_{detected,min} = I_1 + I_2 - 2\sqrt{I_1 I_2} |\gamma_{1,2}|$$
 (2.9)

Moreover, we define a last variable  $\nu$  called the *visibility*<sup>3</sup>:

$$\nu \stackrel{\text{def}}{=} \frac{I_{max} - I_{min}}{I_{max} + I_{min}} \tag{2.10}$$

which represents the maximal contrast that one may observe for an intensity signal. From the decrector point of view, that is to say, the visibility of the electric signal after the wire reads:

$$\nu = \frac{I_{detected,max} - I_{detected,min}}{I_{detected,max} + I_{detected,min}} = \frac{2\sqrt{I_1 I_2}|\gamma_{1,2}|}{I_1 + I_2}$$
(2.11)

In other words, the visibility two mixed electric field is proportional to the coherence term  $\langle E_1(t)E_2^*(t+\tau)\rangle_T$ .

Now, we make two final hypothesis:

- The second electric field is coming from the same source as the first one:  $E_1 = E_2 = E$ . However, the two field are still delayed from each other by a time  $\tau$ . Experimentally, this may be reproduced with a simple Michelson interferometer which allows to vary the delay thanks to the difference of the optic path length of the two arms.
- The mean value of the total intensity  $I_{total}$  is constant over the time. This assumption is not necessarily obvious in a sense that our previous development could involve pulses of light, gaussian envelopes, etc. However this hypothesis lets us write that the detected intensity does not vary with time, hence the mean of interval lengths T taken at different origins give the same value:  $\langle I(t) \rangle_T = \langle I(t+\tau) \rangle_T$ .

<sup>&</sup>lt;sup>2</sup>In other words, the mean value of the real part is equivalent to the real part of the mean value, by linearity.

<sup>&</sup>lt;sup>3</sup>Sometimes,  $\nu$  is named the *fringes visibility* in order to recall the periodicity involved in interference experiments.

At the end of the day, we obtain:

$$\nu = |\gamma_{1,2}| = \frac{|\langle E(t)E^*(t+\tau)\rangle_T|}{|I|} = |g^1(\tau)|$$
 (2.12)

that is to say, for a quasi-monochromatic input field, the detection of the output field of a Michelson interferometer produces a detected intensity through the connected oscilloscope which, after maths done, gives the norm of the first order correlation function. Then, varying the path length difference allows to sketch the norm of  $g^1$  according to the time delay  $\tau$ . It is important to notice that if we set:

$$I_{detected}(\tau) \stackrel{\text{def}}{=} \eta \langle I_{total}(t) \rangle_T$$
 (2.13)

Then, when defining the visbility in (2.10), the quantum efficiency vanishes equally through the division. In other words, measuring  $g^1$  in this way is not dependent on the dectector efficiency: loosing photons at the arrival does not change the statistics with the visibility approach.

However, although the Michelson interferometer is a simple setup which gives nicely  $g^1$ , this method suffer from three major incovenients:

- The detector must follow the frequency of the input field: as we are overlapping the same field (i.e the same frequency), the resulting field gives only component of null, same or twice the original frequency. In other words, as the actual experiment works with lasers involving a few hundreds of THz, our detector must follow those frequencies. No real decretor can achieve it in those days.<sup>4</sup>
- As the theory is facing experiment, it is worth to notice that the detector *always* has a specific range of possible power inputs. In other words, for to low or to high laser power, the detector does not send any electric signal, which is critical for the first case as the cavity output gives superadiant lasing of a few nano watts.
- This configuration is highly sensitive to the noise. Indeed, any variation in the detected intensity is concidered as a variation from the electric field, thus, a variation for  $g^1$ . However, those variations are not necessarily only representative of the output field generated by the quantum system but also by other external perturbations called *noise* which can be classical (electric current noise for example) or quantum<sup>5</sup>.

At the end of the day, this setup turns out to not be optimal for rigorous and/or advanced measurements. Therefore, the next section shall present another approach as well as the basic concept involved in order to solve the three previous inconvenients.

### 2.2 Balanced heterodyne setup

An heterodyne setup is, as stated by its name, an experiment involving two mixed electric fields of different frequencies<sup>6</sup> which are collected by two detectors. The electric current produced by both detected intensity, that we call *photocurrent*, is then

<sup>&</sup>lt;sup>4</sup>Actually, the detector is able to show the mean intensity value, that is to say a DC signal, in the presence of *any* light (depending on the specification). However, because of the *dead time* and other technical reasons, modern detectors are not able to follow the high frequency variations of orders of THz

<sup>&</sup>lt;sup>5</sup>The quantum noise is not directly related to the quantum system in itlsef but by the fundamental photon statistics generated from the system.

<sup>&</sup>lt;sup>6</sup>"Hetero" is the Greek prefix meaning "irregularity" and "dyne" suffix for "dynamic" in contrary to "homo" (= "same") for a homodyne setup with equal frequencies.

substracted and the resulting electric signal can be recorded on an oscilloscope for example.

The heterodyne setup used in the actual experiment is summarysed on Fig??.

- $\vec{E}_{cav}$  is the electric field generated at the outure of the cavity.
- $\vec{E}_{LO}$  stands for the electric field named the *local oscillator* and sometimes abbreviated as the *reference* laser. Its frequency diverges from the cavity field frequency. It is in general emited from a laser and hence is concidered as  $nearly^7$  perfectly coherent source.
- The beam splitter essentially mix the input fields in a way described in section ?? (Data analysis) which roughly gives, as outputs, the added or substracted input fields.

The experiement is configured as the input electric fields being linearly and parallely polarized: so we consider  $\overrightarrow{E}_{cav}$  and  $\overrightarrow{E}_{LO}$  as such. This simplifies the equation by only taking into account the amplitude of the fields instdead of their vector components. Also, as the intensity calculation involve a scalar product of the electric vector fields, the linear polarization allows to maximise the light power when mixing two E-fields.

In order to show the different frequency components involved into the detected intensity, we mix the two E-fields as in (2.1) with the following definitions:

$$E_{cav}(t) = \frac{E_{cav}}{2}e^{i\omega_c t} + \frac{E_{cav}}{2}e^{-i\omega_c t}$$

$$E_{LO}(t) = \frac{E_{LO}}{2}e^{i\omega_{LO}t} + \frac{E_{LO}}{2}e^{-i\omega_{LO}t}$$
(2.14)

that is to say, we consider  $E_{cav}(t)$  as perfectly coherent (i.e monochromatic) and we omit the phase difference, the whole for the sake of simplicity as the excepted result effects would be similar in case of phase unmatch and quasi-monochromatic cavity field. Note that  $E_{cav/LO}$  without the time dependence t is the amplitude of the respective field.

Now appling the exact formula  $I_{total}(t) = E_{total}(t)^2$ , one gets four different terms<sup>8</sup>:

$$I_{total,a}(t) = E_{cav}^2 \cos^2(\omega_{cav}t)$$
(2.15)

$$I_{total,b}(t) = E_{LO}^2 \cos^2(\omega_{LO}t) \tag{2.16}$$

$$I_{total,c}(t) = E_{cav} E_{LO} \cos \left( (\omega_{cav} - \omega_{LO})t \right)$$
 (2.17)

$$I_{total,d}(t) = E_{cav} E_{LO} \cos \left( (\omega_{cav} + \omega_{LO})t \right)$$
 (2.18)

where  $I_{total}(t) = I_{total,a}(t) + I_{total,b}(t) + I_{total,c}(t)$ . In other words, the detected intensity, which is proportional to the total intensity, has four beat mode as one would see on a spectrum analyzer:  $\omega_{cav}$ ,  $\omega_{LO}$ ,  $\omega_{cav} - \omega_{LO}$  and  $\omega_{cav} + \omega_{LO}$ . As stated in the previous section, the cavity frequency is in order of THz, which is undetectable for a realistic detector. Now, if we set the frequency of the local oscillator of the same order of magnitude as  $\omega_{cav}$  but slightly shifted with  $\omega_{LO} = \omega_{cav} + \delta \omega$  and  $\delta \omega$  is a frequency belonging to the bandwidth of the detector, then we get again four beats:

$$\omega_{cav}, \qquad \omega_{cav} + \delta\omega, \qquad \delta\omega, \qquad 2\omega_{cav} + \delta\omega \tag{2.19}$$

 $<sup>{}^{7}\</sup>vec{E}_{LO}$  cannot be perfectly coherent from an experimental point of view but we consider it as such in the theoretical development.

<sup>&</sup>lt;sup>8</sup>See annexe??

The only detected beat is  $\delta\omega$  as all the others are of order of  $\omega_{cav}$  (i.e in few hundreds of Thz). Thereby, the detector is sensitive to the frequency variations of  $I_{total,c}(t)$  only. Moreover, this is not the only advantage of adding a local oscillator. Indeed, one may notice that the intensity term (2.17) is dependent to the amplitude of the cavity field and the amplitude of the local oscillator. In that way, we are able to tune the total light intensity observed and face the problem of low power from the cavity field: the local oscillator is a well controlled laser and if, for example, the  $E_{cav}$ -field power is in order of picowatts (i.e well below the range of detected power), it is enough to power up the reference laser in order to detect the expected beat again.

Finally, the principle of photocurrent substraction is called a balanced detection. As we substract the two photocurrent, the resulting electric signal should be null in the case where both fields are equal. In that way, a very samll variation in one arm should give a non-null signal: this setup is extremely sensitive to small variations. However, even with the exact same field hitting both diodes of the dectector, some noise still resides. We distinguish two types of noise:

- The shot noise: it reflects the statistical randomness of the light and is only dependent on the quantum uncertainties of the photons. That is why, it is often called equivalently quantum noise. For Poissonian distribution of the photons (i.e for classical light) the photocurrent noise is also amplified and is linearly dependent to the mean intensity light<sup>9</sup>.. For sub-Poissonian lights, where the photons are anti-bunched, it is possible to detect light below the shot noise limit (which is defined by the classical limit of detection for Poissonian light)<sup>10</sup>.
- The eletrical noise: all the electric component induces a white noise into the resulting signal which is inner to the way the detector is manufactured.

Those two types of noises are uncorrellated and just add together while the amplification through the circuit, naturally increases those two noises.

Thus, the idea behind balanced detection is to cancel the classical noise which can randomly appear on both diodes of the detector at the same time. Indeed, if any correlated variation of the signal appears in both emited photocurrent, the substraction erases this correlated variation (i.e noise) in a sense that the resulting signal then owns the quantum noise, the uncorrelated photocurrent noise (which may be amplified) as well as the electric noise (which is a white noise, hence uncorrelated). Nevertheless, the remaining noise may be considered as very small for our purpose and the detector is made in order to reduce the electrical and amplified power noise in the bandwidth of interest. This reduction of noise by electronic design is the subject of the next section.

### 2.3 Balanced low-noise detector

In theory, the electronic circuit does not produce any additional noise. That is to say, if there is any variation of the photocurrent at the entry of the circuit, thus after the diodes, the output noise corresponds to this variation (except the amplification of the noise which is a side effect from the purpose of the circuit). In a real world however, without any photocurrent input, the exit cable of the detector shows a random ouput voltage. Of course, the detector must be under voltage, otherwise, no ouput can be generated as some essential components need an external source of electric power.

<sup>&</sup>lt;sup>9</sup>See section 2.5

 $<sup>^{10}</sup>$ See Fox ??

Moreover, this electrical noise being evaluated in term of power (dBm), is a critical parameter. Indeed, if the shot noise limit is lower than the electrical noise, it is possible to lose some part of the data, especially the very weak quantum correlations. Therefore, it is essential to reduce the electrical noise generated by the internal components as much as possible.

Firstly, we introduce a basic diagram on the working principle of the detector in Fig ??. It is mainly composed of two diodes (block (1)), which are also called *photodiodes* as they react to the incoming light, plus an essential circuit called *transimpedance* amplifier (block (2)) connected in between of the diodes.

Fig

The photodiodes are placed in the so called *photoconductive mode* where the region of reverse bias on the following diagram ?? defines the relation bewteen the voltage and the current.

Diag

In fact a basic diode, by principle, allows the current to flow through it only if the voltage is positive on the cathode and negative on the anode (i.e forward bias). Otherwise, when reverse biased, the current does not flow<sup>11</sup>. For a photodiode, the same idea applies except that when reverse biased, the current can flow through it only if the diode is illuminated. Note that even if the current flows, the difference of voltage between the anode and cathode stays the same: in other words, the photodiode does not act as a switch where the the voltage is homogeneous through the component when the current flow (i.e when the circuit is closed). Thereby, if we isolate the block (1), the current flow through the positive voltage (+) above the first diode (D1) to the negative voltage (-) under the second diode (D2) when both photodiodes are illuminated. In that case, by Kirchhoff's current law, no current can flow through (A) to (B). Otherwise, we can distinguish two cases:

- D1 is illuminated but not D2: as A is considered grounded, D1 is in reverse bias with a relative voltage of -5V (from cathode to anode) and the current flow from (+) to (A) and (B).
- D2 is illuminated but not D1: as A is considered grounded, D1 is in reverse bias with a relative voltage of -5V (from cathode to anode) and the current flow from (B) to (A) and (-).

Therefore, both photodiodes makes the current flow in opposite direction. As the current quantity I is proportional to the illumination, the direction of the current flux is leaded by the diode being the most illuminated. When the illumination is balanced, no current flows. In that way, we reproduce electronically a substraction over the photocurrent.

Before, we considered (A) as grounded (zero voltage in theory) as well as (B) because the principle of the transimpedance amplifier is to transform the current into a voltage (with amplification of the signal) while while keeping its inputs grounded. In fact, block (2) owns a central component called *operational amplifier* with two inputs:

- Non-inverting input (+)
- Inverting input (-)

<sup>&</sup>lt;sup>11</sup>In practice, there exists a a certain voltage called <sup>12</sup> where the current suddenly flow exponentially from the anode to the cathode.

and an ouput<sup>13</sup>. To understand how the op-amp works in our case, we apply the golden rules:

- The op-amp's output attempts to do whatever it is necessary to make the voltage difference between the inputs zero until a saturation output voltage
- The op-amp's inputs draw no current.

As showed on Fig??, the inverting input is grounded which involve (B) to be grounded. Now, let's say that the output saturation voltage of the op-amp is 10V (i.e the max ouput is 10V and min is -10V), if a current flows through B, by second golden rule, then the current flows through the resistance R and generate a voltage.

- If I = 10mA with  $R = 500\Omega$  then C = -5V.
- If I = 20mA with same resistance then C = -10V.
- If I = 40mA with same resistance then C = -10V as the op-amp is saturated but (B) is know +10V in order to satisfy the relative voltage of 20V at the resistance.

where we used the formula:

$$U = R \times I \tag{2.20}$$

with U the tension in volts, R the resistance in ohms, and I the current in ampères. Evidently, those examples are representing a DC signal. However, the photodiodes react to a beat created by the overlap of two beams as described in the previous section <sup>14</sup>: this beat is an AC signal and from the previous example, the limit of photocurrent for saturation would variate periodically (according to the shape if the signal) between +20 mA and -20 mA.

In other words, the transimpedance amplifier circuit has a limited range of input current which can be transformed into a voltage. In fact, one has to be careful on the photocurrent involved after the diodes (i.e at (A)) by testing the ouput voltage of the detector according to the light power hiting the diodes. Otherwise, if the incoming light deliver a photocurrent leading to saturation, one loses the data. Actually, as the photocurrent are substracted, the range limits must be tested with one of the two diodes disabled  $^{15}$ . The actual detector has a limited range output of  $\pm 15$ V and the saturation test of the circuit is tested in a further section.

In that configuration, one considers the electonical components as perfect or *ideal*, meaning that their behavior follows their associated physical law (for example, (2.20) is always respected). Therefore, except the amplified power noise which only increases the already existing photocurrent variance from the light, no additional noise is added. However, this concept is not real and the components add electrical noise by their own presence, especially the op-amp of the circuit<sup>16</sup>. Indeed, in reality, the non-inverting input, which is connected to the ground, may receive some nano-ampères (i.e somewhat a *ghost* current) and, as stated earlier, the golden rules allows to generate a voltage at the ouput of the dectector even without incoming light. Thereby, we add one filter between (A) and (B) like sketched on diagram ??.

Diag

<sup>&</sup>lt;sup>13</sup>This is an active component so it needs to be under tension thanks to additional entries that we do not represent here.

<sup>&</sup>lt;sup>14</sup>They react to the  $\delta\omega$  term defined earlier which is in practice around 43MHz.

<sup>&</sup>lt;sup>15</sup>In practice, we just put a piece of paper in front of one photodiode.

<sup>&</sup>lt;sup>16</sup>The op-amp is an *active component* and is suspicious to create much more noise because of its tension inputs than its passive counter part which are the resistor, the capcaitor, the inductor, etc...

This filter is commonly called a *Notch filter* or *band-stop filter* as its purpose is to block a certain range of frequency in the response of the circuit. The gain of such a circuit is dicted by the formula<sup>17</sup>:

$$\left| \frac{V_{out}}{V_{in}}(\omega) \right| = \frac{1}{\sqrt{1 + \left(\frac{R}{\omega L - \frac{1}{\omega C}}\right)}}$$
 (2.21)

where the diagram ?? (b) sketch a typical response of this RLC circuit (a).

Diag

(Note on the image)  $R = 10\Omega$ , C = 1 Farad(F) and L = 1 Henry(H). As we can see, the gain is set to 1 (i.e the output voltage has the same value than the input voltage) except for a band of frequency where the center of this gap is found to be:

$$\omega_0 = \frac{1}{\sqrt{LC}} \Leftrightarrow f_0 = \frac{1}{2\pi\sqrt{LC}} \tag{2.22}$$

which is called the *resonance* of the circuit caracterizing a null impedance of the LC component  $^{18}$ .

Moreover, the whole circuit, as depicted on diagram ?? (previous diag) has a hidden filter. Indeed, the photodiodes, when enabled and receiving light, may be theoretically replaced by an equivalent circuit as represented on diagram ??: one current source in parallele of a capacitor and a resistance.

Diag

Those two capacitors add with an internal capacitance of the op-amp for which the value may be found in its associated data sheet. Here, we deal with a THS4021 from Texas Instrument for the op-amp and two S5971 photodiodes from Hamamatsu<sup>19</sup>. In this configuration, those three capacitors are in parallele and the total capacitance reads:

$$C_{total} = C_{photodiode,1} + C_{photodiode,2} + C_{op-amp}$$
(2.23)

In theory (i.e from the data sheets) we have a total capacitance of 9pF (pico-Farads) but in practice, and with further analyses of the dectector, it turns out that  $C_{total}$  is around 14pF Note that this formula is clearly the same for resistors in series. Now, the diagram ?? shows the simplified circuit of the dectector with the Notch filter.

Diag

Indeed, this additional capacity  $C_1$  is in parallele with the inductor L of the Notch filter. This new LC component is called a tank filter and, in contrary to its counter part LC in serie, the tank filter allows only a certain range of frequency to go through the circuit:

$$\left| \frac{V_{out}}{V_{in}}(\omega) \right| = \frac{1}{\sqrt{1 + R^2 \left(\frac{1}{\omega L} - \omega C\right)^2}}$$
 (2.24)

where the diagram ?? (b) sketch a typical response of this RLC circuit (a).

Diag

(Note on the image)  $R = 10\Omega$ , C = 1 Farad(F) and L = 1 Henry(H). As we can see, the gain is set to 1 only for a very narrow frequency range (parametrized by

<sup>&</sup>lt;sup>17</sup>See Annexe ??

<sup>&</sup>lt;sup>18</sup>Of course, it does not mean that L and C are null but (2.22) is an equivalent of removing the inductor and the capacitor from the Notch filter.

<sup>&</sup>lt;sup>19</sup>Those two diodes have a high speed response of 100MHz: far more than the expected frequency of 43MHz.

the R, L and C values) which can be found to be the exact same as (2.22) which means that the impedance of LC component is null.

Finally, we sketch in diagram ?? the actual (but simplified) version of the dectector with the two filters.

Diag

As we can see, compared to the transimpedance amplifier, this circuit on diagram ?? has an additional impedance  $Z_{in}$  between the nodes (A) and (B). Considering the photodiodes as a current source, things get more complex than the transimpedance amplifier by the presence of  $Z_{in}$ . Actually, we use an *electronic design automation software*, namely LTSpice, in order to get the gain at the ouput of the actual detector. Then, from simulation, we get picture ?? which clearly shows that the filters does not affect the interesting region which consist of a narrow bandwidth arround 43MHz: the expected signal collected from the photodiodes is amplified whereas high frequencies (i.e above 100Mhz) are removed from the output signal.

Picture

However, we stated before that the noise is generated from the non-inverting input of the op-amp whereas the photodiodes does not receive light: the equivalent circuit corresponds to the simplified diagram which is given on figure ??.

Fig

This circuit (??) is called a non-inverting voltage amplifier where the gain may be formulated as<sup>20</sup>:

$$Gain = \frac{V_{out}}{V_{in}} = 1 + \frac{Z_f}{Z_{in}}$$

$$(2.25)$$

where  $Z_f$  is basically a resistor<sup>21</sup> and  $Z_{in}$  is composed of the filters (Notch plus Tank filter). Thanks to the inversion if the impedance, namely  $1/Z_{in}$ , the behavior of all the components constituing  $Z_{in}$  are inverted. In other words, the Notch filter corresponds now to a band-pass filter whereas the Tank filter corresponds to a band-cut filter for the electronical noise. Thereby, we need to match the band-cut filter resonance, that is to say where the gain of the electronic noise is minimum, to the main frequency of our incoming beam (i.e 43MHz).

Electronic scheme

From simulation of the electronic scheme??, we get the following gain graph??.

Graph simu

The peak clearly comes from the Notch filter with:

$$f_{notch} = \frac{1}{2\pi\sqrt{100 \times 10^{-6} \times 20 \times 10^{-9}}} \simeq 112kHz \tag{2.26}$$

whereas the deep *should* come from the Tank filter with:

$$f_{tank} = \frac{1}{2\pi\sqrt{100 \times 10^{-6} \times 14 \times 10^{-12}}} \simeq 4.2MHz$$
 (2.27)

Then, we can compare those values with the detector directly connect to the spectrum analyzer (detector under tension and photodiodes blocked from incoming light). We obtain both centered<sup>22</sup> experimental graphs??.

Graphs

The peak corresponds very well to the theoretical one (2.26) with an error of about  $\pm 1 \text{kHz}$ . However, the deep is clearly shifted to -400 kHz (i.e positioning at 3.8 MHz

<sup>&</sup>lt;sup>20</sup>See Annexe ??

<sup>&</sup>lt;sup>21</sup>On the real electronic scheme ??, the resistor owns an additional capacitor in parallele.

<sup>&</sup>lt;sup>22</sup>"Centered" in a sense that the graph are localized around the interesting features.

on the graph ??) from the simulated graph and is even shifted to to -700kHz (i.e positioning at 3.5MHz): it appears after further tests and modification that there is a lack of understanding in the capacitor value and the best guess would be that the surrounding of the circuit induces a non-linear behavior of the stray capacitance of 14pF, thus explaining the shift with the experimental graphs.

Nevertheless, it is obvious that the drop of electronic noise is not localized on the right spot: ideally, the minimum noise gain would be at 43MHz. In that way, we modify the inductor value to a theoretical one, namely  $0.82\mu F$  instead of  $100\mu F$ :

$$f_{tank} = \frac{1}{2\pi\sqrt{0.82 \times 10^{-6} \times 14 \times 10^{-12}}} \simeq 46MHz$$
 (2.28)

which appears to be 3MHz out of resonance. However, when simulating the full circuit with this new value for the inductor, one obtains the graph ??

Graph simu

where the deep of  $-170 \mathrm{dBm}$  clearly corresponds to the 43MHz resonance. Thus, modifying the inductor to  $0.82 \mu F$  should move the deep to the correct position of 43Mhz. Moreover, in the worst case of misunderstanding this misalignment with the theoretical resonances, the inductor would change values from several hundreds of micro-Farads, in order to reach a theoretical maximum of 60MHz: for example, taking  $L=0.5 \mu F$  would give approximately 60Mhz of resonance for the deep and considering a shift to the left, we should attain the targeted deep of 43MHz. In that way, we commanded several inductors of values ranging 100nF to  $2\mu F$  and replace the original inductor by removing and making a new soldered joint.

Picture of the detector

At the end of the day, we have an inductor of exactly  $0.8\mu F$  which allow a nice deep of the noise gain of  $-80 \text{dBm}^{23}$  as showed on the experimental graph ?? taken from the oscilloscope after replacement of the component.

Graphs

The graph ?? also shows the peak from the Notch filter which, by virtue of (2.22) moved to the right at, approximately, 900kHz where, from simulation, we were waiting it at 700kHz (again this shift to the left). However, the deep on graph ?? is very well localized around the expected light frequency of 43Mhz.

Finally, we succeded to modify the detector with our frequency requirements by replacing some components of the filters, in order to reduce as much as possible the electrical noise comming from the active components, namely the op-amp.

The next sections will focus on the parametrization/configuration of the detector which involve, among others, saturation test, amplification noise test and technical procedures in order to make sure that the experiment works in the parameter's range of the detector.

#### 2.4 Diodes size versus laser's cross section area

Firstly, we start to simply verify if the *final* laser beam, which is composed of the cavity beam plus the optical oscillator laser, is not oversized compared to the diode area. Inddeed, the specification sheet for those diodes (S5971) gives an explicit photosensitive diameter size of 1.2mm (the sheet specifies it as the *area size*). In other words, the laser beam after the overlap of the beam splitter must have a diameter of less than

<sup>&</sup>lt;sup>23</sup>100dBm less of reduction from the simulation but it is sufficient for our purpose.

1.2mm. Otherwise, we would *spatially saturate* the diodes and lose some part of the laser's cross section area.

Therefore, we add two lenses with a focal length of 50mm each in front of both diodes. We place them at 65mm from the diodes respectively as on Fig??.

Fig

From a geometrical optic's point of view, the laser is essentially an ensemble of parallel lines of light as one could perceive from a distant star. Thereby, from the optical rule involved for a convergent lens, the laser's parallel lines firstly converge after crossing the lens until they all reach the focal point, then diverges. With this configuration, summarized on Fig??, the diodes are exactly 15mm after the focal point of the lenses.

Fig

As the focal point to diode distance is lower than the focal length, the resulting laser's cross section area while hitting the diodes is smaller than the original one (i.e before the lens). This ratio is computed as follow:

Cross Section Area Ratio 
$$\stackrel{\text{def}}{=} r_{cs} = \frac{|d - f|}{f}$$
 (2.29)

where d is the the focal point to diode distance whereas f is the focal length. Note the absolute value which avoid the ratio (2.29) to become negative if d is smaller than f (i.e the diodes reside in the *convergent* part of the lens). Thus, we obtain in our case a  $r_{cs} = 0.3$ . In other words, the beams hitting the diodes after crossing the lenses are approximately three times smaller in area than the original beam.

In order to check if the amount  $r_{cs} = 0.3$  of cross section area reduction is sufficient, we shall move progressively the decrector perpendicularly to the optical axis. As represented on Fig ??, we block one diode while transposing lateraly the detector and recording the DC output voltage<sup>24</sup>.

Fig

According to the laser beal size compared to the photosensitive area, two cases are distinguishable:

- The laser beam size is smaller than the photodiodes: Fig??. The voltage output increases, reach a plateau of constant voltage ouput, then decreases. Fig
- The laser beam size is equivalent to the photodiodes: Fig??. The voltage output increases, reach a maximal pick of voltage, then decreases. Fig
- The laser beam size is bigger than the photodiodes: Fig??. The voltage output increases, reach a plateau of constant voltage ouput, then decreases. Fig

As we can notice, this technic shows the same behavior for bigger or smaller beam sizes. However, it is possible to evaluate the beam's diameter by measuring the distance between the beginning and the end of the slope. Indeed, this measure is literraly the position when the laser's beam starts hitting the photosensitive area (i.e this is the beginning of the slope) whereas when the laser's beam is fully included into the photodiode (i.e this is the *plateau* and the end of the slope). Moreover, if the beam is bigger than the photosensitive area, the plateau (hence the end of the slope) will be reached when the beam covers entirely the photodiode: the *slope distance* is the photodiode's

<sup>&</sup>lt;sup>24</sup>The DC component of the electric signal, when only one diode is enabled, is proportional to the intensity received (until saturation) independently of the frequencies of the light.

diameter, not the beam diameter. In other worlds, if we measure less than 1.2mm for the *slope distance* then the laser's beam is encompassed into the photosensitive area.

Fig ?? shows the results for two different powers involved in the local oscillator: using two powers ensure that we are not saturating the photodiodes in term of intensity when measuring the beam's size. As we consider the cavity laser very weak (in order of picowatts), the main power come out of the reference laser<sup>25</sup>.

Fig

As we can see, the yellow curves (low power) may be considered not saturating the diodes as those curves doesn't reach the same maximum than the red curves (high power).<sup>26</sup>. We can measure the beam's diameter as roughly 0.6mm for the red curves and 1mm for the yellow curves. Thus, the laser beam is well encompassed into the photodiodes. Secondly, those measurements mean that the power associated to the read curves are saturating the diodes: before the beam hits entirely the photosensitive area, the detector reaches its maximum/minimum of output voltage which is now determined to be  $\pm 11$  volts.

Note that the whole procedure relies on the horizontale diplacement. Naively, one could repeat the process accross different vertical positions: one should obtain a 2D map of the output voltage according to the relative beam to diode position. Nevertheless, we only check in practice that the ouput voltage cannot be maximized while moving the decrector up or down when the beam reaches the plateau region (This is done with the yellow curves power, knowing that we are not already saturating the diodes).

#### 2.5 Power to noise ratio

As we already mentioned in section 2.2 (Balanced heterodyne setup), the detection of light involves an amplification of the light's noise dependenging on the light's power. The photocurrent i(t) produced by the diodes may always be written with the sum of the mean photocurrent and a shift to the mean:

$$i(t) = \langle i \rangle + \Delta i(t) \tag{2.30}$$

where the mean is obviously a constant over time. By definition of  $\Delta i(t)$ , its variance is not null. As the electrical power is given by the well known formula  $P = U \times I$ , applying (2.20) gives naturally the noise power definition:

$$P_{noise}(t) \stackrel{\text{def}}{=} R \times (\Delta i(t))^2 \tag{2.31}$$

where R is a dummy constant dependent on the circuit design, meaning that the noise power is proportional to the variance of the photocurrent. However, the choice R is not innocent: it is the resistance/impedance load of the circuit, namely  $Z_f$  from a previous section, which transforms the current into a voltage. The current-voltage link also implies that the noise power can be equivalently defined through the voltage's variance. At this stage of the development, we do not make any assumption on the source of the variance (i.e noise) of the current: this variance may come from the quantum noise and/or the photodiode noise which may produce some randmoness from the transformation intensity to photocurrent<sup>27</sup>.

<sup>&</sup>lt;sup>25</sup>In that case, we use two very distinct powers which are tuned mechanically, with a button on the *laser box*. This is not a *clean* method because it is not very precise and we shall use a different method in the next section.

<sup>&</sup>lt;sup>26</sup>Note than this argument, alone, does not allow to decide if the red curves means the saturation of the diodes or not

<sup>&</sup>lt;sup>27</sup>We consider the photocurrent *after* the diodes but *before* the transimpedance amplifier: no electrical noise yet.

It can be shown<sup>28</sup> that the variance of the photocurrent from an incoming light is proportional to its mean value (with certain conditions on the statistics of the light, namely, having a *classical* light):

$$(\Delta i(t))^2 \propto \langle i \rangle \tag{2.32}$$

This relation explicitly says that the quantum noise of a classical light (i.e with a Poissonian distribution) is proportional to the mean photon number. Then, putting (2.32) into (2.31) gives:

$$P_{noise} \propto \langle i \rangle$$
 (2.33)

where  $P_{noise}$  is not dependent on time anymore if we consider the mean current as constant over time<sup>29</sup>. Then, we consider the photocurrent as proportional to the light intensity hitting the diodes (i.e no randomness into the photodiodes). Thus it comes<sup>30</sup>:

Noise power (in watts) 
$$\propto$$
 Light intensity (in watts) (2.34)

In other words, increasing the intensity of the incoming light also increases linearly the variance of the photocurrent, that is to say, the quantum noise.

As we collect the ouput voltage *after* the whole circuit, the electrical noise is superposed to the quantum noise: as those two are uncorrelated, they add together. This means that the noise value, or equivalently the variance of the photocurrent, when no light hits the diodes, is exactly the amount of electrical noise in the circuit. Then, adding light progressively gives a linear curve which is the power to noise ratio. Obviously, this curve is limited by the saturation of the circuit<sup>31</sup>.

In order to check experimentally this behavior and evaluate the power to noise ratio, we need a precise and efficient method to tune the local oscillator's power. To do so, we use a pair of optical devices:

• A polarizer: this device allows only light with the same polarization to cross it. For a linearly polarized electric field, things get mathematically simpler as the resulting field  $\overrightarrow{E}_{out}$  is the equivalent of the entering field  $\overrightarrow{E}_{in}$  projected along the polarizer's unitary vector  $\overrightarrow{e}_{pol}$ :

$$\vec{E}_{out} = \left(\vec{E}_{in} \cdot \vec{e}_{pol}\right) \vec{e}_{pol} \tag{2.35}$$

• A waveplate: its working principle is described in Annexe??. Here we use a lambda-half waveplate (abbreviated  $\lambda/2$ -waveplate): for a linearly polarized electric field, this device simply rotate the polarization's direction of the electric field.

Assuming that the input electric field is linearly polarized (which is the case experimentally), coupling those two devices makes a very precise power-tunable instrument. Fig ?? represents how they must be placed along the optical axis.

<sup>&</sup>lt;sup>28</sup>See Fox ??

<sup>&</sup>lt;sup>29</sup>In reality, the noise power is now dependent on the frequency of the photocurrent.

<sup>&</sup>lt;sup>30</sup>Formally we define the light intensity by its Poynting vector which is in watt per meter-squared. However, the measured power (i.e experimental) is in watts, thus normalized to the beam's cross section area

<sup>&</sup>lt;sup>31</sup>The global saturation could also be induced by the saturation of the photodiodes but it turns out experimentally that the saturation is made by the electrical components first, which cannot support a too high current/voltage level.

The waveplate rotate the electric field. The polarizer project the electric field. If the E-field is parallel to the polarizer axis, the output amplitude is the same as the input one. If the E-field is perpendicular to the polarizer axis, the ouput amplitude is null. Every E-field polarisation's direction in between shall give a reduced amplitude compared to the maximum amplitude: because of the scalar operation, the amplitude relation is not linear but *cosine* dependent, hence very sensitive for almost perpendicular E-fields.