Eigenvalue Placement

George Higgins Hutchinson, Parth Nobel, et al.

April 12, 2019

Disclaimer

EIGENVALUE PLACEMENT

This is an unofficial review session and HKN is not affiliated with this course. All of the topics we're reviewing will reflect the material you have covered, our experiences in EE16B, and past exams. We make no promise that what we cover will necessarily reflect the content of this midterm. While some course staff members may be among the presenters, this review session is still not official.

This is licensed under the Creative Commons CC BY-SA: feel free to share and edit, as long as you credit us and keep the license. For more information, visit

https://creativecommons.org/licenses/by-sa/4.0/deed.en_US

Overview

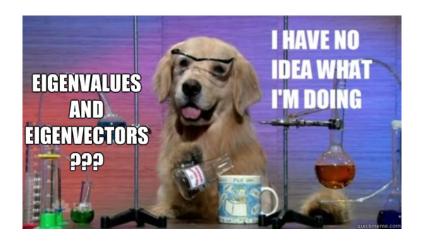
Eigenvalue Placement

Linearization

Singular Value Decomposition

Principle Component Analysis

Discretization



Why?

- ► Recall that we are always interested in determining if a given system is BIBO (bounded input bounded output) stable.
- More precisely, if we have a system described by $\vec{x}(t+1) = A\vec{x}(t) + Bu(t) + \vec{\omega}(t)$ we would like the eigenvalues of $A \in \mathbb{R}^{n \times n}$, to satisfy the following property : $|\lambda_i| < 1$.
- \blacktriangleright So what if we have a λ that does not satisfy this property?
- ► This is where eigenvalue placement comes into play!
- Assuming the system is controllable, we will use closed loop controls to change the eigenvalues such that they satisfy this property.

How?

- \blacktriangleright Assume e.g. a DT system. Input: u[t] If the system is controllable then we can use feedback, which means that we can let the input depend on the output, $\vec{x}[t]$.
- \blacktriangleright We would like to change the matrix multiplying $\vec{x}[t]$ such that $|\lambda_i| < 1$, so let's see what happens when we let $u[t] = K\vec{x}[t]$, where $K \in \mathbb{R}^{1 \times n}$
- Using this input we have:

$$\vec{x}[t+1] = A\vec{x}[t] + Bu[t] + \vec{\omega}[t]$$
$$= A\vec{x}[t] + BK\vec{x}[t] + \vec{\omega}[t]$$
$$= (A + BK)\vec{x}[t] + \vec{\omega}[t]$$

- \triangleright Strategically choosing K allows us to have specific λ 's for A + BK (Good!).
- ► This process is called coefficient matching.

► Suppose we are given a controllable system defined by:

$$\vec{x}[t+1] = \begin{bmatrix} 2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} u[t]$$

- ▶ Is the system stable? No! $\lambda = 2, 1$
- ▶ What if we let

$$u[t] = \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

$$\vec{x}(t+1) = \begin{bmatrix} -2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

- ► Solve for the values of f_1 and f_2 such that $\lambda_1 = -0.25$ and
- ► The answer is $f_1 = -1.50$ and $f_2 = 0.25$

► Suppose we are given a controllable system defined by:

$$\vec{x}[t+1] = \begin{bmatrix} 2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} u[t]$$

- ▶ Is the system stable? No! $\lambda = 2, 1$
- ► What if we let

$$u[t] = \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

Then we have:

$$\vec{x}(t+1) = \begin{bmatrix} -2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

- ▶ Solve for the values of f_1 and f_2 such that $\lambda_1 = -0.25$ and $\lambda_2 = 0$
- ▶ The answer is $f_1 = -1.50$ and $f_2 = 0.25$
- Although the process is very messy hopefully you see why eigenvalue placement is very important to stabilize systems

► Suppose we are given a controllable system defined by:

$$\vec{x}[t+1] = \begin{bmatrix} 2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} u[t]$$

- ▶ Is the system stable? No! $\lambda = 2, 1$
- ► What if we let

$$u[t] = \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

Then we have:

$$\vec{x}(t+1) = \begin{bmatrix} -2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

- ▶ Solve for the values of f_1 and f_2 such that $\lambda_1 = -0.25$ and $\lambda_2 = 0$
- ▶ The answer is $f_1 = -1.50$ and $f_2 = 0.25$
- Although the process is very messy hopefully you see why eigenvalue placement is very important to stabilize systems.

 What about his rear matrices?

► Suppose we are given a controllable system defined by:

$$\vec{x}[t+1] = \begin{bmatrix} 2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} u[t]$$

- ls the system stable? No! $\lambda = 2, 1$
- ▶ What if we let.

$$u[t] = \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

Then we have:

$$\vec{x}(t+1) = \begin{bmatrix} -2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

- ▶ Solve for the values of f_1 and f_2 such that $\lambda_1 = -0.25$ and $\lambda_2 = 0$
- ▶ The answer is $f_1 = -1.50$ and $f_2 = 0.25$
- ► Although the process is very messy hopefully you see why eigenvalue placement is very important to stabilize systems. What about bigger matrices?

> Controllable Canonical Form (CCF) for any controllable system is a special form that allows us to simplify the process of eigenvalue placement. It takes on the following form:

$$A^* = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \dots & \dots & 0 \\ 0 & \dots & \dots & 1 \\ \alpha_0 & \alpha_1 & \dots & \alpha_{n-1} \end{bmatrix} \qquad B^* = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

$$B^* = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

- ▶ The characteristic polynomial of A^* is $\lambda_n \sum_{i=1}^n \alpha_i \lambda^i = 0$.
- ► So how does it help with eigenvalue placement? The last row

► Controllable Canonical Form (CCF) for any controllable system is a special form that allows us to simplify the process of eigenvalue placement. It takes on the following form:

$$A^* = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \dots & \dots & 0 \\ 0 & \dots & \dots & 1 \\ \alpha_0 & \alpha_1 & \dots & \alpha_{n-1} \end{bmatrix} \qquad B^* = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

- ▶ The characteristic polynomial of A^* is $\lambda_n \sum_{i=0}^{n-1} \alpha_i \lambda^i = 0$.
- So how does it help with eigenvalue placement? The last row of this matrix determines the eigenvalues of A^* so modifying the last row will allow us to (easily) modify the eigenvalues.

Controllable Canonical Form

EIGENVALUE PLACEMENT 00000000000

> Controllable Canonical Form (CCF) for any controllable system is a special form that allows us to simplify the process of eigenvalue placement. It takes on the following form:

$$A^* = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \dots & \dots & 0 \\ 0 & \dots & \dots & 1 \\ \alpha_0 & \alpha_1 & \dots & \alpha_{n-1} \end{bmatrix} \qquad B^* = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

- ▶ The characteristic polynomial of A^* is $\lambda_n \sum_{i=0}^{n-1} \alpha_i \lambda^i = 0$.
- ► So how does it help with eigenvalue placement? The last row of this matrix determines the eigenvalues of A^* so modifying the last row will allow us to (easily) modify the eigenvalues.

How to convert to CCF

- ▶ Let A, B be the matrices in standard form and let A^*, B^* be the matrices in CCF.
- ▶ Recall the matrix we used to check controllability?

$$C = \begin{bmatrix} B & AB & \dots & A^{n-1}B \end{bmatrix}$$

$$C^* = \begin{bmatrix} B^* & A^*B^* & \dots & A^{*n-1}B^* \end{bmatrix}$$

- ▶ We then have $T := C^*C^{-1}$, such that $A^* = TAT^{-1}$ and $B^* = TB$.
- ▶ Remember, all controllable matrices with single input can be transformed into CCF!

- ▶ Let A, B be the matrices in standard form and let A^*, B^* be the matrices in CCF.
- ► Recall the matrix we used to check controllability?

$$C = \begin{bmatrix} B & AB & \dots & A^{n-1}B \end{bmatrix}$$

$$C^* = \begin{bmatrix} B^* & A^*B^* & \dots & A^{*n-1}B^* \end{bmatrix}$$

- ▶ We then have $T := C^*C^{-1}$, such that $A^* = TAT^{-1}$ and $B^* = TB$.
- ▶ Remember, all controllable matrices with single input can be transformed into CCF!

- ▶ Let A, B be the matrices in standard form and let A^*, B^* be the matrices in CCF.
- ▶ Recall the matrix we used to check controllability?

$$C = \begin{bmatrix} B & AB & \dots & A^{n-1}B \end{bmatrix}$$

$$C^* = \begin{bmatrix} B^* & A^*B^* & \dots & A^{*n-1}B^* \end{bmatrix}$$

- ▶ We then have $T:=C^*C^{-1}$, such that $A^*=TAT^{-1}$ and $B^*=TB$.
- ► Remember, all controllable matrices with single input can be transformed into CCF!

Example

EIGENVALUE PLACEMENT

Consider the following discrete time system:

$$\vec{x}[t+1] = \begin{bmatrix} -2 & 2 & 0 \\ 2 & -4 & 2 \\ 0 & 1 & -1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} u[t]$$

- (a) Is the system stable? Is it controllable?
- (b) Using an appropriate transformation ($\vec{z}[t] = T\vec{x}[t]$), bring the system to controllable canonical form.
- (c) Using the state feedback u[t] =

$$\begin{bmatrix} f_1 & f_2 & f_3 \end{bmatrix}$$

 $\vec{z}[t]$ bring the eigenvalues of the system to 0, 0.75, -0.25.

Solutions to Example

EIGENVALUE PLACEMENT

(a) The characteristic polynomial is: $\lambda^3+7\lambda^2+8\lambda=\lambda(\lambda^2+7\lambda+8)=0, \text{ therefore the eigenvalues of A are } \{0,-5.56,-1.44\}. \text{ As we can see there are } |\lambda_i|>1 \text{ therefore the system is not stable.}$

The controllability matrix C =

$$\begin{bmatrix} 1 & -2 & 8 \\ 0 & 2 & -12 \\ 0 & 0 & 2 \end{bmatrix}$$

 ${\cal C}$ has full rank so the system is controllable

(b) As we previously mentioned the coefficients of the characteristic polynomial are closely related to the last row of the A^{\ast} matrix. Therefore, the CCF of the system is:

$$\vec{z}[t+1] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -8 & -7 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u[t]$$

Example Solutions Continued

(c) Our system then becomes:

$$\vec{z}[t+1] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ f_1 & f_2 - 8 & f_3 - 7 \end{bmatrix} \vec{x}[t]$$

Which means its characteristic polynomial is :

$$\lambda^3 - (f_3 - 7)\lambda^2 - (f_2 - 8)\lambda - f_1 = 0.$$

Now, we know the characteristic polynomial should be $\lambda(\lambda-\frac{3}{4})(\lambda+\frac{1}{4})$, so we can equate the two and solve for the feedback vector $\vec{f}^{T}=\begin{bmatrix}0&\frac{1}{2}&\frac{3}{16}\end{bmatrix}$.

Overview

Eigenvalue Placement

Eigenvalue Placemen

Linearization

Singular Value Decomposition

Principle Component Analysis

Discretization

Linearization

EIGENVALUE PLACEMENT

▶ Recall that if we have $\frac{dx}{dt} = \lambda x(t) + bu(t)$ we know a solution to this is:

$$x(t) = x(0)e^{\lambda t} + \int_0^t e^{\lambda(t-\tau)} u(\tau) \ d\tau$$

- ▶ What if we had $\frac{dx}{dt} = f(x(t)) + bu(t)$, where f is nonlinear (e.g sin)?
- ▶ Big Picture: linearize *f* around an operating point and then treat it as a linear function in a small neighborhood of that point.
- ► Why linearization?
 It allows you to treat the system as a linear one, which is very helpful as linear ODE are (usually) much easier to solve!

▶ Recall that if we have $\frac{dx}{dt} = \lambda x(t) + bu(t)$ we know a solution to this is:

$$x(t) = x(0)e^{\lambda t} + \int_0^t e^{\lambda(t-\tau)}u(\tau) \ d\tau$$

- ▶ What if we had $\frac{dx}{dt} = f(x(t)) + bu(t)$, where f is nonlinear (e.g sin)?
- ▶ Big Picture: linearize *f* around an operating point and then treat it as a linear function in a small neighborhood of that point.
- ► Why linearization?

It allows you to treat the system as a linear one, which is very helpful as linear ODE are (usually) much easier to solve!

Linearization

EIGENVALUE PLACEMENT

▶ Recall that if we have $\frac{dx}{dt} = \lambda x(t) + bu(t)$ we know a solution to this is:

$$x(t) = x(0)e^{\lambda t} + \int_0^t e^{\lambda(t-\tau)}u(\tau) \ d\tau$$

- ▶ What if we had $\frac{dx}{dt} = f(x(t)) + bu(t)$, where f is nonlinear (e.g sin)?
- ▶ Big Picture: linearize *f* around an operating point and then treat it as a linear function in a small neighborhood of that point.
- ► Why linearization? It allows you to treat the system as a linear one, which is very helpful as linear ODE are (usually) much easier to solve!

- ▶ Suppose we have f(x) that is a non linear function. We can use a first order Taylor polynomial to linearize the function, this is equivalent to finding the slope of the tangent line of f(x) at a particular point.
- From calculus: $f(x) \approx f(x^*) + f'(x^*)(x x^*)$.
- ▶ As long as we are within some (very small) δ neighborhood of x^* the linearization is valid.
- ► Example: Linearize $f(x) = 3e^{x^2+2}$ around x^*
- Solution:

$$\begin{split} f(x^*) &= 3e^{x^2+2} \\ f'(x) &= 3e^{x^2+2}(2x) = 6xe^{x^2+2} \\ f'(x^*) &= 6x^*e^{x^{*2}+2} \\ \text{Therefore}: \ f(x) &\approx 3e^{x^{*2}+2} + 6x^*e^{x^{*2}+2}(x-x^*) \end{split}$$

- (i) Choose, or you may be given, a DC input point. That is, a point $u^* \equiv u(t)$ that is constant with time.
- (ii) Find a DC operating point, $x^* \equiv x(t)$. That is, solve $\frac{dx^*}{dt} = f(x^*) + bu^*$. Notice that this boils down to finding an x^* such that $f(x^*) + bu^* = 0$.
- (iii) Define $x_l(t) = x(t) x^*$ and $u_l(t) = u(t) u^*$, and re-write the ODE in terms of $x_l(t)$ and $u_l(t)$. By plugging in you get: $\frac{dx_l(t)}{dt} = f(x_l(t) + x^*) + b(u_l(t) + u^*)$
- (iv) It is ok to assume at this point that $u_l(t)$ is small, that means that the u(t) in step 1 does not deviate too much from u^* .
- (v) Linearize the ODE: $f(x_l(t) + x^*) \approx f(x^*) + f'(x^*)x_l(t)$. Here we assume that $x_l(t)$ is also small. This is something that we will need to verify in the next step!

- (i) Choose, or you may be given, a DC input point. That is, a point $u^* \equiv u(t)$ that is constant with time.
- (ii) Find a DC operating point, $x^*\equiv x(t)$. That is, solve $\frac{dx^*}{dt}=f(x^*)+bu^*$. Notice that this boils down to finding an x^* such that $f(x^*)+bu^*=0$.
- (iii) Define $x_l(t)=x(t)-x^*$ and $u_l(t)=u(t)-u^*$, and re-write the ODE in terms of $x_l(t)$ and $u_l(t)$. By plugging in you get: $\frac{dx_l(t)}{dt}=f(x_l(t)+x^*)+b(u_l(t)+u^*)$
- (iv) It is ok to assume at this point that $u_l(t)$ is small, that means that the u(t) in step 1 does not deviate too much from u^* .
- (v) Linearize the ODE: $f(x_l(t)+x^*)\approx f(x^*)+f'(x^*)x_l(t)$. Here we assume that $x_l(t)$ is also small. This is something that we will need to verify in the next step!

- (i) Choose, or you may be given, a DC input point. That is, a point $u^* \equiv u(t)$ that is constant with time.
- (ii) Find a DC operating point, $x^*\equiv x(t)$. That is, solve $\frac{dx^*}{dt}=f(x^*)+bu^*$. Notice that this boils down to finding an x^* such that $f(x^*)+bu^*=0$.
- (iii) Define $x_l(t)=x(t)-x^*$ and $u_l(t)=u(t)-u^*$, and re-write the ODE in terms of $x_l(t)$ and $u_l(t)$. By plugging in you get: $\frac{dx_l(t)}{dt}=f(x_l(t)+x^*)+b(u_l(t)+u^*)$
- (iv) It is ok to assume at this point that $u_l(t)$ is small, that means that the u(t) in step 1 does not deviate too much from u^* .
- (v) Linearize the ODE: $f(x_l(t) + x^*) \approx f(x^*) + f'(x^*)x_l(t)$. Here we assume that $x_l(t)$ is also small. This is something that we will need to verify in the next step!

- (i) Choose, or you may be given, a DC input point. That is, a point $u^* \equiv u(t)$ that is constant with time.
- (ii) Find a DC operating point, $x^*\equiv x(t)$. That is, solve $\frac{dx^*}{dt}=f(x^*)+bu^*$. Notice that this boils down to finding an x^* such that $f(x^*)+bu^*=0$.
- (iii) Define $x_l(t)=x(t)-x^*$ and $u_l(t)=u(t)-u^*$, and re-write the ODE in terms of $x_l(t)$ and $u_l(t)$. By plugging in you get: $\frac{dx_l(t)}{dt}=f(x_l(t)+x^*)+b(u_l(t)+u^*)$
- (iv) It is ok to assume at this point that $u_l(t)$ is small, that means that the u(t) in step 1 does not deviate too much from u^* .
- (v) Linearize the ODE: $f(x_l(t)+x^*)\approx f(x^*)+f'(x^*)x_l(t)$. Here we assume that $x_l(t)$ is also small. This is something that we will need to verify in the next step!

- (i) Choose, or you may be given, a DC input point. That is, a point $u^* \equiv u(t)$ that is constant with time.
- (ii) Find a DC operating point, $x^*\equiv x(t)$. That is, solve $\frac{dx^*}{dt}=f(x^*)+bu^*$. Notice that this boils down to finding an x^* such that $f(x^*)+bu^*=0$.
- (iii) Define $x_l(t)=x(t)-x^*$ and $u_l(t)=u(t)-u^*$, and re-write the ODE in terms of $x_l(t)$ and $u_l(t)$. By plugging in you get: $\frac{dx_l(t)}{dt}=f(x_l(t)+x^*)+b(u_l(t)+u^*)$
- (iv) It is ok to assume at this point that $u_l(t)$ is small, that means that the u(t) in step 1 does not deviate too much from u^* .
- (v) Linearize the ODE: $f(x_l(t)+x^*)\approx f(x^*)+f'(x^*)x_l(t)$. Here we assume that $x_l(t)$ is also small. This is something that we will need to verify in the next step!

(vi) Plug (vi) back into (iii) and we obtain : $\frac{dx_l(t)}{dt} \approx f'(x^*)f(x_l(t)) + f(x^*) + bu_l(t) + bu^* = f'(x^*)f(x_l(t)) + bu_l(t)$

(vii) Verify the linearization!

How do we know if the linearization is valid? Well, if we have $\frac{dx_l(t)}{dt} = \lambda x_l(t) + bu(t)$ we know the solution doesn't blow up if $\lambda < 0$ as we will have a term $e^{\lambda t}$.

This means that we want $m = f'(x^*) < 0$

So what do we do if m > 0? We need to go back and change our DC operating point x^{2}

(vi) Plug (vi) back into (iii) and we obtain : $\frac{dx_l(t)}{dt} \approx f'(x^*)f(x_l(t)) + f(x^*) + bu_l(t) + bu^* = f'(x^*)f(x_l(t)) + bu_l(t)$

(vii) Verify the linearization!

How do we know if the linearization is valid? Well, if we have $\frac{dx_l(t)}{dt} = \lambda x_l(t) + bu(t)$ we know the solution doesn't blow up if $\lambda < 0$ as we will have a term $e^{\lambda t}$.

This means that we want $m = f'(x^*) < 0$.

So what do we do if m > 0? We need to go back and change our DC operating point x?

- (vi) Plug (vi) back into (iii) and we obtain : $\frac{dx_l(t)}{dt} \approx f'(x^*)f(x_l(t)) + f(x^*) + bu_l(t) + bu^* = f'(x^*)f(x_l(t)) + bu_l(t)$
- (vii) Verify the linearization!

How do we know if the linearization is valid? Well, if we have $\frac{dx_l(t)}{dt} = \lambda x_l(t) + bu(t)$ we know the solution doesn't blow up if $\lambda < 0$ as we will have a term $e^{\lambda t}$.

This means that we want $m = f'(x^*) < 0$.

So what do we do if m > 0?

We need to go back and change our DC operating point x^*

(vi) Plug (vi) back into (iii) and we obtain : $\frac{dx_l(t)}{dt} \approx f'(x^*)f(x_l(t)) + f(x^*) + bu_l(t) + bu^* = f'(x^*)f(x_l(t)) + bu_l(t)$

(vii) Verify the linearization!

How do we know if the linearization is valid? Well, if we have $\frac{dx_l(t)}{dt} = \lambda x_l(t) + bu(t)$ we know the solution doesn't blow up if $\lambda < 0$ as we will have a term $e^{\lambda t}$.

This means that we want $m = f'(x^*) < 0$.

So what do we do if m > 0?

We need to go back and change our DC operating point x^*

Practice Problem

EIGENVALUE PLACEMENT

Linearize $\frac{dx(t)}{dt} = \cos(x(t)) + bu(t)$ about $u^* = 0$.

Practice Problem

EIGENVALUE PLACEMENT

Linearize $\frac{dx(t)}{dt} = \cos(x(t)) + bu(t)$ about $u^* = 0$. $\textit{Hint:} \ \cos(x^*) = 0$ has multiple solutions, which means that we can find numerous DC operating points, can you guess which one would result in a stable system ?

- (i) We were given the DC input, $u^* = 0$

- - (i) We were given the DC input, $u^* = 0$
 - (ii) $\cos(x^*) = 0$, which means that $x^* = k\frac{\pi}{2}$ for $k \in \{...-2,-1,1,2,...\}$. We will choose $x^* = \frac{\pi}{2}$

- (i) We were given the DC input, $u^* = 0$
- (ii) $\cos(x^*) = 0$, which means that $x^* = k\frac{\pi}{2}$ for $k \in \{...-2,-1,1,2,...\}$. We will choose $x^* = \frac{\pi}{2}$
- (iii) Let $x_l(t) = x(t) \frac{\pi}{2}$ and $u_l(t) = u(t) 0$. By plugging in we get: $\frac{dx_l(t)}{dt} = \cos(x_l(t) + \frac{\pi}{2}) + u_l(t)$

- (i) We were given the DC input, $u^* = 0$
- (ii) $\cos(x^*)=0$, which means that $x^*=k\frac{\pi}{2}$ for $k\in\{\ldots-2,-1,1,2,\ldots\}$. We will choose $x^*=\frac{\pi}{2}$
- (iii) Let $x_l(t)=x(t)-\frac{\pi}{2}$ and $u_l(t)=u(t)-0$. By plugging in we get: $\frac{dx_l(t)}{dt}=\cos(x_l(t)+\frac{\pi}{2})+u_l(t)$
- (iv) We assume that $u_l(t)$ is small.
- (v) Linearize the ODE: $\cos(x_l(t) + \frac{\pi}{2}) \approx \cos(\frac{\pi}{2}) \sin(\frac{\pi}{2})x_l(t)$.
- (vi) Plug (v) back into ODE: $\frac{dx_l(t)}{dt} = -x_l(t) + u_l(t)$

We see that our assumption that $x_l(t)$ is small is indeed satisfied as we will have a e^{-t} term in the solution which means that $x_l(t)$ will decay.

What if we had chosen a different DC Operating point, say $-\frac{\pi}{2}$? When we linearize the system we see that the solution will "explode" around that particular DC operating point.

- (i) We were given the DC input, $u^* = 0$
- (i) we were given the DC input, $u' \equiv 0$

(ii) $\cos(x^*)=0$, which means that $x^*=k\frac{\pi}{2}$ for $k\in\{\ldots-2,-1,1,2,\ldots\}$. We will choose $x^*=\frac{\pi}{2}$

- (iii) Let $x_l(t)=x(t)-\frac{\pi}{2}$ and $u_l(t)=u(t)-0$. By plugging in we get: $\frac{dx_l(t)}{dt}=\cos(x_l(t)+\frac{\pi}{2})+u_l(t)$
- (iv) We assume that $u_l(t)$ is small.
- (v) Linearize the ODE: $\cos(x_l(t) + \frac{\pi}{2}) \approx \cos(\frac{\pi}{2}) \sin(\frac{\pi}{2})x_l(t)$.
- (vi) Plug (v) back into ODE: $\frac{dx_l(t)}{dt} = -x_l(t) + u_l(t)$

We see that our assumption that $x_l(t)$ is small is indeed satisfied as we will have a e^{-t} term in the solution which means that $x_l(t)$ will decay.

What if we had chosen a different DC Operating point, say $-\frac{\pi}{2}$? When we linearize the system we see that the solution will "explode" around that particular DC operating point.

- (i) We were given the DC input, $u^* = 0$
- (ii) $\cos(x^*) = 0$, which means that $x^* = k\frac{\pi}{2}$ for $k \in \{...-2,-1,1,2,...\}$. We will choose $x^* = \frac{\pi}{2}$
- (iii) Let $x_l(t) = x(t) \frac{\pi}{2}$ and $u_l(t) = u(t) 0$. By plugging in we get: $\frac{dx_l(t)}{dt} = \cos(x_l(t) + \frac{\pi}{2}) + u_l(t)$
- (iv) We assume that $u_l(t)$ is small.
- (v) Linearize the ODE: $\cos(x_l(t) + \frac{\pi}{2}) \approx \cos(\frac{\pi}{2}) \sin(\frac{\pi}{2})x_l(t)$.
- (vi) Plug (v) back into ODE: $\frac{dx_l(t)}{dt} = -x_l(t) + u_l(t)$

- (i) We were given the DC input, $u^* = 0$
- (ii) $\cos(x^*)=0$, which means that $x^*=k\frac{\pi}{2}$ for $k\in\{\ldots-2,-1,1,2,\ldots\}$. We will choose $x^*=\frac{\pi}{2}$
- (iii) Let $x_l(t)=x(t)-\frac{\pi}{2}$ and $u_l(t)=u(t)-0$. By plugging in we get: $\frac{dx_l(t)}{dt}=\cos(x_l(t)+\frac{\pi}{2})+u_l(t)$
- (iv) We assume that $u_l(t)$ is small.
- (v) Linearize the ODE: $\cos(x_l(t) + \frac{\pi}{2}) \approx \cos(\frac{\pi}{2}) \sin(\frac{\pi}{2})x_l(t)$.
- (vi) Plug (v) back into ODE: $\frac{dx_l(t)}{dt} = -x_l(t) + u_l(t)$

We see that our assumption that $x_l(t)$ is small is indeed satisfied as we will have a e^{-t} term in the solution which means that $x_l(t)$ will decay.

What if we had chosen a different DC Operating point, say $-\frac{\pi}{2}$? When we linearize the system we see that the solution will "explode" around that particular DC operating point.

- (i) We were given the DC input, $u^* = 0$
- (ii) $\cos(x^*)=0$, which means that $x^*=k\frac{\pi}{2}$ for $k\in\{\ldots-2,-1,1,2,\ldots\}$. We will choose $x^*=\frac{\pi}{2}$
- (iii) Let $x_l(t)=x(t)-\frac{\pi}{2}$ and $u_l(t)=u(t)-0$. By plugging in we get: $\frac{dx_l(t)}{dt}=\cos(x_l(t)+\frac{\pi}{2})+u_l(t)$
- (iv) We assume that $u_l(t)$ is small.
- (v) Linearize the ODE: $\cos(x_l(t) + \frac{\pi}{2}) \approx \cos(\frac{\pi}{2}) \sin(\frac{\pi}{2})x_l(t)$.
- (vi) Plug (v) back into ODE: $\frac{dx_l(t)}{dt} = -x_l(t) + u_l(t)$

We see that our assumption that $x_l(t)$ is small is indeed satisfied as we will have a e^{-t} term in the solution which means that $x_l(t)$ will decay.

What if we had chosen a different DC Operating point, say $-\frac{\pi}{2}$? When we linearize the system we see that the solution will "explode" around that particular DC operating point.

What if we had $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}, \vec{u})$? We will see that the process is very similar to the scalar case we just analyzed!

First, let's see how to linearize $\vec{f}(\vec{x})$ around a DC operating point \vec{x}^* . Where $\vec{f} \in \mathbb{R}^{n \times 1}$ is a vector of scalar functions.

The idea is to linearize individually each one of the f_i around the DC operating point.

For example

EIGENVALUE PLACEMENT

$$f_1 \approx f_1(\vec{x}^*) + \frac{\partial f_1}{\partial x_1}(\vec{x}^*)(x_1 - x_1^*) + \dots + \frac{\partial f_n}{\partial x_1}(\vec{x}^*)(x_n - x_n^*)$$

Repeating this for all n functions in \vec{f} we see we get a system of scalar, linearized, multivariate functions which makes you think, wouldn't it be nice to express it in a shorthand matrix notation?

What if we had $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}, \vec{u})$? We will see that the process is very similar to the scalar case we just analyzed!

First, let's see how to linearize $\vec{f}(\vec{x})$ around a DC operating point \vec{x}^* . Where $\vec{f} \in \mathbb{R}^{n \times 1}$ is a vector of scalar functions.

The idea is to linearize individually each one of the f_i around the DC operating point.

For example

EIGENVALUE PLACEMENT

$$f_1 \approx f_1(\vec{x}^*) + \frac{\partial f_1}{\partial x_1}(\vec{x}^*)(x_1 - x_1^*) + \dots + \frac{\partial f_n}{\partial x_1}(\vec{x}^*)(x_n - x_n^*)$$

Repeating this for all n functions in \vec{f} we see we get a system of scalar, linearized, multivariate functions which makes you think, wouldn't it be nice to express it in a shorthand matrix notation?

What if we had $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}, \vec{u})$? We will see that the process is very similar to the scalar case we just analyzed!

First, let's see how to linearize $\vec{f}(\vec{x})$ around a DC operating point \vec{x}^* . Where $\vec{f} \in \mathbb{R}^{n \times 1}$ is a vector of scalar functions.

The idea is to linearize individually each one of the f_i around the DC operating point.

EIGENVALUE PLACEMENT

$$f_1 \approx f_1(\vec{x}^*) + \frac{\partial f_1}{\partial x_1}(\vec{x}^*)(x_1 - x_1^*) + \dots + \frac{\partial f_n}{\partial x_1}(\vec{x}^*)(x_n - x_n^*)$$

What if we had $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}, \vec{u})$? We will see that the process is very similar to the scalar case we just analyzed!

First, let's see how to linearize $\vec{f}(\vec{x})$ around a DC operating point \vec{x}^* . Where $\vec{f} \in \mathbb{R}^{n \times 1}$ is a vector of scalar functions.

The idea is to linearize individually each one of the f_i around the DC operating point.

For example:

EIGENVALUE PLACEMENT

$$f_1 \approx f_1(\vec{x}^*) + \frac{\partial f_1}{\partial x_1}(\vec{x}^*)(x_1 - x_1^*) + \dots + \frac{\partial f_n}{\partial x_1}(\vec{x}^*)(x_n - x_n^*)$$

Repeating this for all n functions in \tilde{f} we see we get a system of scalar, linearized, multivariate functions which makes you think, wouldn't it be nice to express it in a shorthand matrix notation?

What if we had $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}, \vec{u})$? We will see that the process is very similar to the scalar case we just analyzed!

First, let's see how to linearize $\vec{f}(\vec{x})$ around a DC operating point \vec{x}^* . Where $\vec{f} \in \mathbb{R}^{n \times 1}$ is a vector of scalar functions.

The idea is to linearize individually each one of the f_i around the DC operating point.

For example:

EIGENVALUE PLACEMENT

$$f_1 \approx f_1(\vec{x}^*) + \frac{\partial f_1}{\partial x_1}(\vec{x}^*)(x_1 - x_1^*) + \dots + \frac{\partial f_n}{\partial x_1}(\vec{x}^*)(x_n - x_n^*)$$

Repeating this for all n functions in \vec{f} we see we get a system of scalar, linearized, multivariate functions which makes you think, wouldn't it be nice to express it in a shorthand matrix notation?

Jacobian Matrix

EIGENVALUE PLACEMENT

We can use the Jacobian to express everything nicely and neatly. The Jacobian is the name given to the matrix of partial derivatives of \vec{f} , and it is denoted by $J_{\vec{x}}$ or $\nabla_{\vec{x}}\vec{f}$.

$$\begin{bmatrix} f_1(\vec{x}) \\ \vdots \\ f_n(\vec{x}) \end{bmatrix} \approx \begin{bmatrix} f_1(\vec{x}^*) \\ \vdots \\ f_n(\vec{x}^*) \end{bmatrix} + \begin{bmatrix} \frac{\partial f_1}{\partial x_1}(\vec{x}^*) & \dots & \frac{\partial f_1}{\partial x_n}(\vec{x}^*) \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1}(\vec{x}^*) & \dots & \frac{\partial f_n}{\partial x_n}(\vec{x}^*) \end{bmatrix} (\vec{x} - \vec{x}^*)$$

We can use the Jacobian to express everything nicely and neatly. The Jacobian is the name given to the matrix of partial derivatives of \vec{f} , and it is denoted by $J_{\vec{x}}$ or $\nabla_{\vec{x}} \vec{f}$.

Continuing from the previous slide we have:

$$\begin{bmatrix} f_1(\vec{x}) \\ \vdots \\ f_n(\vec{x}) \end{bmatrix} \approx \begin{bmatrix} f_1(\vec{x}^*) \\ \vdots \\ f_n(\vec{x}^*) \end{bmatrix} + \begin{bmatrix} \frac{\partial f_1}{\partial x_1}(\vec{x}^*) & \dots & \frac{\partial f_1}{\partial x_n}(\vec{x}^*) \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1}(\vec{x}^*) & \dots & \frac{\partial f_n}{\partial x_n}(\vec{x}^*) \end{bmatrix} (\vec{x} - \vec{x}^*)$$

22/50

Find the Jacobian

Find the Jacobian:

$$\begin{bmatrix} x_2(t)\cos(x_1(t)*x_2(t)) + 2x_3^2(t) & x_1(t)\cos(x_1(t)*x_2(t)) & 4x_1(t)x_3(t) \\ \frac{1}{x_3(t)} & -x_3(t)\sin(x_2(t)) & \cos(x_2(t)) - \frac{x_1(t)}{x_3^2(t)} \\ 1 & 6x_3(t)x_2^2(t) & 2x_2^3(t) \end{bmatrix}$$

Evaluate the Jacobian about \vec{x}^* :

$$\begin{bmatrix} 5\pi & 0 & 0 \\ \frac{2\pi}{3} & 0 & 1 \\ 1 & 36\pi^3 & 16\pi^3 \end{bmatrix}$$

Linearize:

$$\vec{f}(\vec{x}(t)) \approx \begin{bmatrix} 0 \\ \frac{3\pi}{4} \\ 24\pi^4 \end{bmatrix} + \begin{bmatrix} 5\pi & 0 & 0 \\ \frac{2\pi}{3} & 0 & 1 \\ 1 & 36\pi^3 & 16\pi^3 \end{bmatrix} \begin{bmatrix} x_1(t) - 0 \\ x_2(t) - \frac{3\pi}{4} \\ x_3(t) - 24\pi^4 \end{bmatrix}$$

- (i) Solve $\vec{f}(\vec{x}^*, \vec{u}^*) = \vec{0}$ to determine the equilibrium point.
- (ii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}^*$
- (iii) Linearize $\vec{f}(\vec{x}, \vec{u})$ about (\vec{x}^*, \vec{u}^*) . That is: $\vec{f}(\vec{x}(t), \vec{u}(t)) \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$
- (iv) Plug (iv) back into the ODE: $\frac{d\vec{x}}{dt} \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$

Steps to Linearize Vector ODE Systems

EIGENVALUE PLACEMENT

- (i) Solve $\vec{f}(\vec{x}^*, \vec{u}^*) = \vec{0}$ to determine the equilibrium point.
- (ii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}^*$
- (iii) Linearize $\vec{f}(\vec{x}, \vec{u})$ about (\vec{x}^*, \vec{u}^*) . That is: $\vec{f}(\vec{x}(t), \vec{u}(t)) \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$
- (iv) Plug (iv) back into the ODE: $\frac{d\vec{x}}{dt} \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$

- (i) Solve $\vec{f}(\vec{x}^*, \vec{u}^*) = \vec{0}$ to determine the equilibrium point.
- (ii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}^*$
- (iii) Linearize $\vec{f}(\vec{x}, \vec{u})$ about (\vec{x}^*, \vec{u}^*) . That is: $\vec{f}(\vec{x}(t), \vec{u}(t)) \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$
- (iv) Plug (iv) back into the ODE: $\frac{d\vec{x}}{dt} \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$

- (i) Solve $\vec{f}(\vec{x}^*, \vec{u}^*) = \vec{0}$ to determine the equilibrium point.
- (ii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}^*$
- (iii) Linearize $\vec{f}(\vec{x}, \vec{u})$ about (\vec{x}^*, \vec{u}^*) . That is: $\vec{f}(\vec{x}(t), \vec{u}(t)) \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$
- (iv) Plug (iv) back into the ODE: $\frac{d\vec{x}}{dt} \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$

- (i) Solve $\vec{f}(\vec{x}^*, \vec{u}^*) = \vec{0}$ to determine the equilibrium point.
- (ii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}^*$
- (iii) Linearize $\vec{f}(\vec{x}, \vec{u})$ about (\vec{x}^*, \vec{u}^*) . That is: $\vec{f}(\vec{x}(t), \vec{u}(t)) \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$
- (iv) Plug (iv) back into the ODE: $\frac{d\vec{x}}{dt} \approx \vec{f}(\vec{x}^*, \vec{u}^*) + J_{\vec{x}}\vec{x}_l(t) + J_{\vec{u}}\vec{u}_l(t)$

Linearizing Vector ODE Systems Example

Given a DC input $u^* = 1$, linearize:

EIGENVALUE PLACEMENT

$$\frac{d\vec{x}(t)}{dt} = \begin{bmatrix} x_1^2(t) - x_2(t)u(t) \\ x_2^2(t)(1 + x_1(t)) + \sin(\pi x_1(t)u(t)) \end{bmatrix}$$

Again, we will do this in steps:

- (i) We are given $u^* = 1$
- (ii) We need to find a DC operating point, this means solving the following system of equations:

$$x_1^{*2} - x_2^* u^* = 0 (1)$$

$$x_2^{*2}(x_1^* + 1) + \sin(\pi x_1^* u^*) = 0 \tag{2}$$

The solution is $x_1^* = -1$ and $x_2^* = 1$

- (iii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}$
- (iv) Linearize

$$\vec{f}(\vec{x}(t), u(t)) \approx \vec{f}(\vec{x}^*, 1) + \begin{bmatrix} -2 & -1 \\ 1 - \pi & 0 \end{bmatrix} \vec{x}_l(t) + \begin{bmatrix} -1 \\ \pi \end{bmatrix} u_l(t)$$

Again, we will do this in steps:

- (i) We are given $u^* = 1$
- (ii) We need to find a DC operating point, this means solving the following system of equations:

$$x_1^{*2} - x_2^* u^* = 0 (1)$$

$$x_2^{*2}(x_1^*+1) + \sin(\pi x_1^* u^*) = 0 \tag{2}$$

The solution is $x_1^* = -1$ and $x_2^* = 1$.

- (iii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}$
- (iv) Linearize

$$\vec{f}(\vec{x}(t), u(t)) \approx \vec{f}(\vec{x}^*, 1) + \begin{bmatrix} -2 & -1 \\ 1 - \pi & 0 \end{bmatrix} \vec{x}_l(t) + \begin{bmatrix} -1 \\ \pi \end{bmatrix} u_l(t)$$

Again we will do this in stone

(i) We are given $u^* = 1$

- Again, we will do this in steps:
- (ii) We need to find a DC operating point, this means solving the following system of equations:

$$x_1^{*2} - x_2^* u^* = 0 (1)$$

$$x_2^{*2}(x_1^* + 1) + \sin(\pi x_1^* u^*) = 0 \tag{2}$$

The solution is $x_1^* = -1$ and $x_2^* = 1$.

(iii) Let
$$\vec{x}_l(t) = \vec{x}(t) - \vec{x}^*$$
 and $\vec{u}_l(t) = \vec{u}(t) - \vec{u}^*$

(iv) Linearize,

$$\vec{f}(\vec{x}(t), u(t)) \approx \vec{f}(\vec{x}^*, 1) + \begin{bmatrix} -2 & -1 \\ 1 - \pi & 0 \end{bmatrix} \vec{x}_l(t) + \begin{bmatrix} -1 \\ \pi \end{bmatrix} u_l(t)$$

Solutions

EIGENVALUE PLACEMENT

Again, we will do this in steps:

- (i) We are given $u^* = 1$
- (ii) We need to find a DC operating point, this means solving the following system of equations:

$$x_1^{*2} - x_2^* u^* = 0 (1)$$

$$x_2^{*2}(x_1^* + 1) + \sin(\pi x_1^* u^*) = 0 \tag{2}$$

The solution is $x_1^* = -1$ and $x_2^* = 1$.

- (iii) Let $\vec{x}_l(t) = \vec{x}(t) \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) \vec{u}^*$
- (iv) Linearize,

$$\vec{f}(\vec{x}(t), u(t)) \approx \vec{f}(\vec{x}^*, 1) + \begin{bmatrix} -2 & -1 \\ 1 - \pi & 0 \end{bmatrix} \vec{x}_l(t) + \begin{bmatrix} -1 \\ \pi \end{bmatrix} u_l(t)$$

Solutions Continued

EIGENVALUE PLACEMENT

(v) Substitute linear approximation back into the system,

$$\frac{d\vec{x}(t)}{dt} \approx \vec{f}(\vec{x}^*, 1) + \begin{bmatrix} -2 & -1 \\ 1 - \pi & 0 \end{bmatrix} \vec{x}_l(t) + \begin{bmatrix} -1 \\ \pi \end{bmatrix} u_l(t)$$

Overview

Eigenvalue Placement

Eigenvalue Placemen

Linoarization

Singular Value Decomposition

Principle Component Analysis

Discretization

SVD Theorem

Eigenvalue Placement

Any matrix $A \in \mathbb{R}^{m \times n}$ can be decomposed into the product of three matrices

$$A = U\Sigma V^{T}$$

$$U : m \times m$$

$$\Sigma : m \times n$$

$$V^{T} : n \times n$$

Such that U,V are unitary matrices and Σ only has nonnegative values along its main diagonal.

SVD: Compact Form

EIGENVALUE PLACEMENT

We can also express the SVD as

$$A = \mathcal{U}S\mathcal{V}^{T}$$

$$\mathcal{U}: m \times r$$

$$S: r \times r$$

$$\mathcal{V}^{T}: r \times n$$

where r is the rank of A. The compact form matrices maintain properties of the original matrices, but have entries removed whenever they correspond to zero singular values.

SVD: Outer Product Form

Eigenvalue Placement

Lastly, we can express

$$A = \sum_{i=1}^{r} \sigma_i \vec{u}_i \vec{v}_i^T$$

where \vec{u}_i, \vec{v}_i are the columns of U, V, respectively, and σ_i are corresponding diagonal entry of the matrix Σ

$$A^{T}A = U\Sigma V^{T}V\Sigma^{T}U^{T}$$
$$= U\Sigma^{2}U^{T}$$

This is an eigen decomposition since Σ^2 is diagonal and $U^{-1}=U^T$. Thus solving for the eigenvalues and eigenvectors of A^TA give $\lambda_i=\sigma_i^2$ with eigenvectors which correspond to the right singular vectors. We need to sort by decreasing σ_i . Side note: $\Sigma^T\Sigma$ is not actually equal to Σ^2 , but the former product yields a matrix with singular values squared on the diagonal entries, hence we call it Σ^2

Given a right singular vector \vec{v}_i which we found from the previous part, we can apply it

$$A\vec{v}_i = \left(\sum_{k=1}^r \sigma_k \vec{u}_k \vec{v}_k^T\right) \vec{v}_i$$
$$= \sum_{k=1}^r \sigma_k \vec{u}_k \vec{v}_k^T \vec{i}$$
$$= \sigma_i \vec{u}_i$$
$$\vec{u}_i = \frac{1}{\sigma_i} A \vec{v}_i$$

Computing SVD with AA^T

Eigenvalue Placement

Similar calculations yield $\sigma_i = \sqrt{\lambda_i}$ of AA^T with eigenvectors as left singular vectors, and $\vec{v}_i = \frac{1}{\sigma_i}A^T\vec{u}_i$

Intepretation of SVD

Eigenvalue Placement

- ► Unitary matrices act as rotation in a given space. A diagonal matrix stretches in a given coordinate space.
- ► SVD visualization (open in browser)

Intepretation of SVD

Eigenvalue Placement

For a product $A\vec{x}$, we can decompose every vector \vec{x} into a linear combination of right singular vectors

$$\vec{x} = \sum_{i=1}^{n} \alpha_i \vec{v}_i$$

Thus, we can see exactly which parts of \vec{x} affect the output.

Compression of Low-Rank Matrices

EIGENVALUE PLACEMENT

▶ Suppose I had a matrix $A \in \mathbb{R}^{m \times n}$ with m, n >> rank(A). How could I more efficiently store A and compute products like $A\vec{x}$?

▶ With the SVD, we only have to save r set of two vectors and a scalar, which saves us a lot of space if the rank is small with respect to the matrix. Also, less computation is carried out if we represent the matrix as the outer product form.

Compression of Low-Rank Matrices

EIGENVALUE PLACEMENT

▶ Suppose I had a matrix $A \in \mathbb{R}^{m \times n}$ with m, n >> rank(A). How could I more efficiently store A and compute products like $A\vec{x}$?

ightharpoonup With the SVD, we only have to save r set of two vectors and a scalar, which saves us a lot of space if the rank is small with respect to the matrix. Also, less computation is carried out if we represent the matrix as the outer product form.

Overview

Eigenvalue Placement

Eigenvalue Placemen

Linearization

Singular Value Decomposition

Principle Component Analysis

Discretization

PCA

Eigenvalue Placement

PCA is a linear dimensionality reduction tool. Given data $\vec{x}_i \in \mathbb{R}^d$, we can create a mapping $T: \mathbb{R}^d \to \mathbb{R}^{d'}, d' < d$ such that the variance in the dataset is still captured

PCA — Computation

- 1. Store data row-major in $A \in \mathbb{R}^{n \times d}$
- 2. De-mean A
- 3. Take SVD: $A = U\Sigma V^T$
- 4. Create $V_{d'} \in \mathbb{R}^{n \times d'}$ from vectors of V corresponding to d greatest signular values
- 5. To project data into the representative subspace $T(x) := V_{d'}^T x$

- 1. Store data row-major in $A \in \mathbb{R}^{n \times d}$
- 2. De-mean A
- 3. Take SVD: $A = U\Sigma V^T$
- 4. Create $V_{d'} \in \mathbb{R}^{n \times d'}$ from vectors of V corresponding to d' greatest signular values
- 5. To project data into the representative subspace $T(x) := V_{d'}^T x$

- 1. Store data row-major in $A \in \mathbb{R}^{n \times d}$
- 2. De-mean A
- 3. Take SVD: $A = U\Sigma V^T$
- 4. Create $V_{d'} \in \mathbb{R}^{n \times d'}$ from vectors of V corresponding to d greatest signular values
- 5. To project data into the representative subspace $T(x) := V_{d'}^T x$

PCA — Computation

- 1. Store data row-major in $A \in \mathbb{R}^{n \times d}$
- 2. De-mean A
- 3. Take SVD: $A = U\Sigma V^T$
- 4. Create $V_{d'} \in \mathbb{R}^{n \times d'}$ from vectors of V corresponding to d' greatest signular values
- 5. To project data into the representative subspace: $T(x) := V_d^T x$

PCA — Computation

- 1. Store data row-major in $A \in \mathbb{R}^{n \times d}$
- 2. De-mean A
- 3. Take SVD: $A = U\Sigma V^T$
- 4. Create $V_{d'} \in \mathbb{R}^{n \times d'}$ from vectors of V corresponding to d' greatest signular values
- 5. To project data into the representative subspace: $T(x) := V_{d'}^T x$

PCA: computation

Eigenvalue Placement

The mapping T can then be expressed as

$$T(\vec{x}) = V_k^T \vec{x}$$

If we apply this transformation onto the entire dataset (which has row vectors), we can say

$$T(A) = B = AV_k$$

where $B \in \mathbb{R}^{n \times k}$

PCA: computation

Eigenvalue Placement

If we were to show the projected vectors in the original space, we can multiply back with the projection vectors

$$A' = BV_k^T$$

Eigenvalue Placement

PCA

Overview

Eigenvalue Placemen

Linearization

Singular Value Decomposition

Principle Component Analysis

Discretization

Discretization: Q1

EIGENVALUE PLACEMENT

Note: this section follows hw8 q1 almost exactly. Suppose we have a scalar system

$$\frac{d}{dt}x(t) = \alpha x + \vec{\beta}^T \vec{u}(t)$$

and we apply a constant input \vec{u}_n for times $t \in [nT, (n+1)T)$ for some T>0. Given x(nT) solve the differential equation

EIGENVALUE PLACEMENT

From t=nT to t=(n+1)T, $\vec{\beta}^T\vec{u}$ is a constant scalar. Thus, we can solve this like a normal differential equation. Let $x=x'-\frac{\vec{\beta}^T\vec{u}}{\vec{v}}$. Then

$$\begin{split} \frac{d}{dt}x(t) &= \alpha(x' - \frac{\vec{\beta}^T \vec{u}}{\alpha}) + \vec{\beta}^T \vec{u}(t) \\ &= \alpha x' \\ x' &= Ae^{\alpha(x-nT)} \\ x + \frac{\vec{\beta}^T \vec{u}}{\alpha} &= Ae^{\alpha(x-nT)} \\ x &= Ae^{\alpha(x-nT)} - \frac{\vec{\beta}^T \vec{u}}{\alpha} \end{split}$$

At which point we can use our initial condition to get

$$x(nT) = A - \frac{\vec{\beta}^T \vec{u}}{2}$$

Discretization: Q2

EIGENVALUE PLACEMENT

Using the differential equation derived from question 1, create a discrete-time system to model the continuous time. In other words, if x[n] = x(nT), $\vec{u}[n] = \vec{u}(nT)$, find a relation such that

$$x[n+1] = A_d x[n] + B_d \vec{u}[n]$$

EIGENVALUE PLACEMENT

We can solve the previous solution for x((n+1)T)

$$x((n+1)T) = \left(x(nT) + \frac{\vec{\beta}^T \vec{u}(nT)}{\alpha}\right) e^{\alpha((n+1)T - nT)} - \frac{\vec{\beta}^T \vec{u}(nT)}{\alpha}$$
$$x[n+1] = e^{\alpha T} x[n] + \frac{e^{\alpha T} - 1}{\alpha} \vec{\beta}^T \vec{u}[n]$$

We see that $A_d = e^{\alpha T}$, $B_d = ((e^{\alpha T} - 1)/\alpha)\vec{\beta}^T$

Discretization: Q3

Eigenvalue Placement

Instead of a scalar, we instead have a diagonal matrix A such that

$$\frac{d}{dt}\vec{x} = A\vec{x} + B\vec{u}$$

Discretize this system in the same was as Q2.

EIGENVALUE PLACEMENT

Expanding the original system out line-by-line gives

$$\frac{d}{dt}x_i = a_i x_i + b_i \vec{u}_i$$

where x_i is the *i*th variable of \vec{x} , a_i is the diagonal entry of A, and b_i is the row of B.

Discretization: Generic Matrix

Eigenvalue Placement

Math not shown, but we can perform a change of basis from our original space to our diagonal space, and then apply the results of the previous part.