

EE16B — Midterm 2 Review

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How?

- ▶ Assume e.g. a DT system. Input: $u[t]$ If the system is controllable then we can use feedback, which means that we can let the input depend on the output, $\vec{x}[t]$.
- ▶ We would like to change the matrix multiplying $\vec{x}[t]$ such that $|\lambda_i| < 1$, so let's see what happens when we let $u[t] = K\vec{x}[t]$, where $K \in \mathbb{R}^{1 \times n}$.
- ▶ Using this input we have:

$$\begin{aligned}\vec{x}[t+1] &= A\vec{x}[t] + Bu[t] + \vec{\omega}[t] \\ &= A\vec{x}[t] + BK\vec{x}[t] + \vec{\omega}[t] \\ &= (A + BK)\vec{x}[t] + \vec{\omega}[t]\end{aligned}$$

- ▶ Strategically choosing K allows us to have specific λ 's for $A + BK$ (Good!).
- ▶ This process is called coefficient matching.

Example

- Suppose we are given a controllable system defined by:

$$\vec{x}[t+1] = \begin{bmatrix} 2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} u[t]$$

- Is the system stable? No! $\lambda = 2, 1$
- What if we let

$$u[t] = \begin{bmatrix} f_1 & f_2 \end{bmatrix} \vec{x}[t]$$

Then we have:

$$\vec{x}(t+1) = \begin{bmatrix} -2 & -1 \\ 0 & 1 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 2 \\ -1 \end{bmatrix} [f_1 \quad f_2] \vec{x}[t]$$

- Solve for the values of f_1 and f_2 such that $\lambda_1 = -0.25$ and $\lambda_2 = 0$
- The answer is $f_1 = -1.50$ and $f_2 = 0.25$
- Although the process is very messy hopefully you see why eigenvalue placement is very important to stabilize systems. What about bigger matrices?

Controllable Canonical Form

- ▶ Controllable Canonical Form (CCF) for any controllable system is a special form that allows us to simplify the process of eigenvalue placement. It takes on the following form:

$$A^* = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \dots & \dots & \dots & 0 \\ 0 & \dots & \dots & \dots & 1 \\ \alpha_0 & \alpha_1 & \dots & \dots & \alpha_{n-1} \end{bmatrix} \quad B^* = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

- ▶ The characteristic polynomial of A^* is $\lambda_n - \sum_{i=0}^{n-1} \alpha_i \lambda^i = 0$.
- ▶ So how does it help with eigenvalue placement? The last row of this matrix determines the eigenvalues of A^* so modifying the last row will allow us to (easily) modify the eigenvalues.

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► Let A, B be the matrices

$$B^* = TB$$

How to convert to CCF

- ▶ Let A, B be the matrices in standard form and let A^*, B^* be the matrices in CCF.
- ▶ Recall the matrix we used to check controllability?

$$C = [B \quad AB \quad \dots \quad A^{n-1}B]$$

$$C^* = [B^* \quad A^*B^* \quad \dots \quad A^{*n-1}B^*]$$

- ▶ We then have $T := C^*C^{-1}$, such that $A^* = TAT^{-1}$ and $B^* = TB$.
- ▶ Remember, all controllable matrices with single input can be transformed into CCF!

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Solutions to Example

- (a) The characteristic polynomial is:

$\lambda^3 + 7\lambda^2 + 8\lambda = \lambda(\lambda^2 + 7\lambda + 8) = 0$, therefore the eigenvalues of A are $\{0, -5.56, -1.44\}$. As we can see there are $|\lambda_i| > 1$ therefore the system is not stable.

The controllability matrix $C =$

$$\begin{bmatrix} 1 & -2 & 8 \\ 0 & 2 & -12 \\ 0 & 0 & 2 \end{bmatrix}$$

C has full rank so the system is controllable

- (b) As we previously mentioned the coefficients of the characteristic polynomial are closely related to the last row of the A^* matrix. Therefore, the CCF of the system is:

$$\vec{z}[t+1] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -8 & -7 \end{bmatrix} \vec{x}[t] + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u[t]$$

Example Solutions Continued

(c) Our system then becomes:

$$\vec{z}[t+1] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ f_1 & f_2 - 8 & f_3 - 7 \end{bmatrix} \vec{x}[t]$$

Which means its characteristic polynomial is :

$$\lambda^3 - (f_3 - 7)\lambda^2 - (f_2 - 8)\lambda - f_1 = 0.$$

Now, we know the characteristic polynomial should be

$\lambda(\lambda - \frac{3}{4})(\lambda + \frac{1}{4})$, so we can equate the two and solve for the feedback vector $\vec{f}^T = [0 \quad \frac{1}{2} \quad \frac{3}{16}]$.

Overview

Eigenvalue Placement

Linearization

Singular Value Decomposition

Principle Component Analysis

Discretization

Linearization

- Recall that if we have $\frac{dx}{dt} = \lambda x(t) + bu(t)$ we know a solution to this is:

$$x(t) = x(0)e^{\lambda t} + \int_0^t e^{\lambda(t-\tau)} u(\tau) d\tau$$

- What if we had $\frac{dx}{dt} = f(x(t)) + bu(t)$, where f is nonlinear (e.g *sin*)?
- Big Picture: linearize f around an operating point and then treat it as a linear function in a small neighborhood of that point.
- Why linearization?
It allows you to treat the system as a linear one, which is very helpful as linear ODE are (usually) much easier to solve!

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Linearizing a Single-Variable Function

- ▶ Suppose we have $f(x)$ that is a non linear function. We can use a first order Taylor polynomial to linearize the function, this is equivalent to finding the slope of the tangent line of $f(x)$ at a particular point.
- ▶ From calculus: $f(x) \approx f(x^*) + f'(x^*)(x - x^*)$.
- ▶ As long as we are within some (very small) δ neighborhood of x^* the linearization is valid.
- ▶ Example: Linearize $f(x) = 3e^{x^2+2}$ around x^*
- ▶ Solution:

$$f(x^*) = 3e^{x^{*2}+2}$$

$$f'(x) = 3e^{x^2+2}(2x) = 6xe^{x^2+2}$$

$$f'(x^*) = 6x^*e^{x^{*2}+2}$$

$$\text{Therefore : } f(x) \approx 3e^{x^{*2}+2} + 6x^*e^{x^{*2}+2}(x - x^*)$$

Linearizing Steps for $\frac{dx(t)}{dt} = f(x(t)) + bu(t)$

- (i) Choose, or you may be given, a DC input point. That is, a point $u^* \equiv u(t)$ that is constant with time.
- (ii) Find a DC operating point, $x^* \equiv x(t)$. That is, solve $\frac{dx^*}{dt} = f(x^*) + bu^*$. Notice that this boils down to finding an x^* such that $f(x^*) + bu^* = 0$.
- (iii) Define $x_l(t) = x(t) - x^*$ and $u_l(t) = u(t) - u^*$, and re-write the ODE in terms of $x_l(t)$ and $u_l(t)$. By plugging in you get: $\frac{dx_l(t)}{dt} = f(x_l(t) + x^*) + b(u_l(t) + u^*)$
- (iv) It is ok to assume at this point that $u_l(t)$ is small, that means that the $u(t)$ in step 1 does not deviate too much from u^* .
- (v) Linearize the ODE: $f(x_l(t) + x^*) \approx f(x^*) + f'(x^*)x_l(t)$. Here we assume that $x_l(t)$ is also small. This is something that we will need to verify in the next step!

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Linearizing Steps for $\frac{dx(t)}{dt} = f(x(t)) + bu(t)$ (Continued)

(vi) Plug (vi) back into (iii) and we obtain :

$$\frac{dx_l(t)}{dt} \approx f'(x^*)f(x_l(t)) + \cancel{f(x^*)} + bu_l(t) + \cancel{bx^*} = f'(x^*)f(x_l(t)) + bu_l(t)$$

(vii) Verify the linearization!

How do we know if the linearization is valid? Well, if we have $\frac{dx_l(t)}{dt} = \lambda x_l(t) + bu(t)$ we know the solution doesn't blow up if $\lambda < 0$ as we will have a term $e^{\lambda t}$.

This means that we want $m = f'(x^*) < 0$.

So what do we do if $m > 0$?

We need to go back and change our DC operating point x^*

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Practice Problem

Linearize $\frac{dx(t)}{dt} = \cos(x(t)) + bu(t)$ about $u^* = 0$.

Hint: $\cos(x^*) = 0$ has multiple solutions, which means that we can find numerous DC operating points, can you guess which one would result in a stable system ?

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Practice Problem Solution

- (i) We were given the DC input, $u^* = 0$
- (ii) $\cos(x^*) = 0$, which means that $x^* = k\frac{\pi}{2}$ for $k \in \{\dots - 2, -1, 1, 2, \dots\}$. We will choose $x^* = \frac{\pi}{2}$
- (iii) Let $x_l(t) = x(t) - \frac{\pi}{2}$ and $u_l(t) = u(t) - 0$. By plugging in we get: $\frac{dx_l(t)}{dt} = \cos(x_l(t) + \frac{\pi}{2}) + u_l(t)$
- (iv) We assume that $u_l(t)$ is small.
- (v) Linearize the ODE: $\cos(x_l(t) + \frac{\pi}{2}) \approx \cos(\frac{\pi}{2}) - \sin(\frac{\pi}{2})x_l(t)$.
- (vi) Plug (v) back into ODE: $\frac{dx_l(t)}{dt} = -x_l(t) + u_l(t)$

We see that our assumption that $x_l(t)$ is small is indeed satisfied as we will have a e^{-t} term in the solution which means that $x_l(t)$ will decay.

What if we had chosen a different DC Operating point, say $-\frac{\pi}{2}$?

When we linearize the system we see that the solution will "explode" around that particular DC operating point.

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- (vi) Plug (v) back into ODE: $\frac{dx_l(t)}{dt} = -x_l(t) + u_l(t)$

We see that our assumption that $x_l(t)$ is small is indeed satisfied as we will have a e^{-t} term in the solution which means that $x_l(t)$ will decay.

What if we had chosen a different DC Operating point, say $-\frac{\pi}{2}$?

When we linearize the system we see that the solution will "explode" around that particular DC operating point.

Practice Problem Solution

- (i) We were given the DC input, $u^* = 0$
- (ii) $\cos(x^*) = 0$, which means that $x^* = k\frac{\pi}{2}$ for $k \in \{\dots - 2, -1, 1, 2, \dots\}$. We will choose $x^* = \frac{\pi}{2}$
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Linearization of Vector Functions

What if we had $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}, \vec{u})$? We will see that the process is very similar to the scalar case we just analyzed!

First, let's see how to linearize $\vec{f}(\vec{x})$ around a DC operating point \vec{x}^* . Where $\vec{f} \in \mathbb{R}^{n \times 1}$ is a vector of scalar functions.

The idea is to linearize individually each one of the f_i around the DC operating point.

For example:

$$f_1 \approx f_1(\vec{x}^*) + \frac{\partial f_1}{\partial x_1}(\vec{x}^*)(x_1 - x_1^*) + \dots + \frac{\partial f_1}{\partial x_n}(\vec{x}^*)(x_n - x_n^*)$$

Repeating this for all n functions in \vec{f} we see we get a system of scalar, linearized, multivariate functions which makes you think, wouldn't it be nice to express it in a shorthand matrix notation?

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Jacobian Matrix

We can use the Jacobian to express everything nicely and neatly.
The Jacobian is the name given to the matrix of partial derivatives of \vec{f} , and it is denoted by $J_{\vec{x}}$ or $\nabla_{\vec{x}}\vec{f}$.

Continuing from the previous slide we have:

$$\begin{bmatrix} f_1(\vec{x}) \\ \vdots \\ f_n(\vec{x}) \end{bmatrix} \approx \begin{bmatrix} f_1(\vec{x}^*) \\ \vdots \\ f_n(\vec{x}^*) \end{bmatrix} + \begin{bmatrix} \frac{\partial f_1}{\partial x_1}(\vec{x}^*) & \dots & \frac{\partial f_1}{\partial x_n}(\vec{x}^*) \\ \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1}(\vec{x}^*) & \dots & \frac{\partial f_n}{\partial x_n}(\vec{x}^*) \end{bmatrix} (\vec{x} - \vec{x}^*)$$

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Linearization with Jacobians Example

$$\text{Linearize } \vec{f}(\vec{x}(t)) = \begin{bmatrix} \sin(x_1(t) * x_2(t)) + 2x_1(t)x_3^2(t) \\ x_3(t) \cos(x_2(t)) + \frac{x_1(t)}{x_3(t)} \\ x_1(t) + 2x_3(t)x_2^3(t) \end{bmatrix} \text{ about } \vec{x}^* = \begin{bmatrix} 0 \\ 2\pi \\ \frac{2\pi}{3} \end{bmatrix}$$

Solutions

Find the Jacobian:

$$\begin{bmatrix} x_2(t) \cos(x_1(t) * x_2(t)) + 2x_3^2(t) & x_1(t) \cos(x_1(t) * x_2(t)) & 4x_1(t)x_3(t) \\ \frac{1}{x_3(t)} & -x_3(t) \sin(x_2(t)) & \cos(x_2(t)) - \frac{x_1(t)}{x_3^2(t)} \\ 1 & 6x_3(t)x_2^2(t) & 2x_2^3(t) \end{bmatrix}$$

Evaluate the Jacobian about \vec{x}^* :

$$\begin{bmatrix} 5\pi & 0 & 0 \\ \frac{2\pi}{3} & 0 & 1 \\ 1 & 36\pi^3 & 16\pi^3 \end{bmatrix}$$

Linearize:

$$\vec{f}(\vec{x}(t)) \approx \begin{bmatrix} 0 \\ \frac{3\pi}{4} \\ 24\pi^4 \end{bmatrix} + \begin{bmatrix} 5\pi & 0 & 0 \\ \frac{2\pi}{3} & 0 & 1 \\ 1 & 36\pi^3 & 16\pi^3 \end{bmatrix} \begin{bmatrix} x_1(t) - 0 \\ x_2(t) - \frac{3\pi}{4} \\ x_3(t) - 24\pi^4 \end{bmatrix}$$

Steps to Linearize Vector ODE Systems

To linearize $\frac{d\vec{x}}{dt} = \vec{f}(\vec{x}(t), \vec{u}(t))$ we use a similar procedure as we did for the scalar case.

- (i) Solve $\vec{f}(\vec{x}^*, \vec{u}^*) = \vec{0}$ to determine the equilibrium point.
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Linearizing Vector ODE Systems Example

Given a DC input $u^* = 1$, linearize:

$$\frac{d\vec{x}(t)}{dt} = \begin{bmatrix} x_1^2(t) - x_2(t)u(t) \\ x_2^2(t)(1 + x_1(t)) + \sin(\pi x_1(t)u(t)) \end{bmatrix}$$

Solutions

Again, we will do this in steps:

- (i) We are given $u^* = 1$
- (ii) We need to find a DC operating point, this means solving the following system of equations:

$$x_1^{*2} - x_2^* u^* = 0 \quad (1)$$

$$x_2^{*2} (x_1^* + 1) + \sin(\pi x_1^* u^*) = 0 \quad (2)$$

The solution is $x_1^* = -1$ and $x_2^* = 1$.

- (iii) Let $\vec{x}_l(t) = \vec{x}(t) - \vec{x}^*$ and $\vec{u}_l(t) = \vec{u}(t) - \vec{u}^*$

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Solutions Continued

(v) Substitute linear approximation back into the system,

$$\frac{d\vec{x}(t)}{dt} \approx \cancel{\vec{f}(\vec{x}^*, 1)} + \begin{bmatrix} -2 & -1 \\ 1 - \pi & 0 \end{bmatrix} \vec{x}_l(t) + \begin{bmatrix} -1 \\ \pi \end{bmatrix} u_l(t)$$

Overview

Eigenvalue Placement

Linearization

Singular Value Decomposition

Principle Component Analysis

Discretization

SVD Theorem

Any matrix $A \in \mathbb{R}^{m \times n}$ can be decomposed into the product of three matrices

$$A = U\Sigma V^T$$

$$U : m \times m$$

$$\Sigma : m \times n$$

$$V^T : n \times n$$

Such that U, V are unitary matrices and Σ only has nonnegative values along its main diagonal.

SVD: Compact Form

We can also express the SVD as

$$A = U S V^T$$

$$U : m \times r$$

$$S : r \times r$$

$$V^T : r \times n$$

where r is the rank of A . The compact form matrices maintain properties of the original matrices, but have entries removed whenever they correspond to zero singular values.

SVD: Outer Product Form

Lastly, we can express

$$A = \sum_{i=1}^r \sigma_i \vec{u}_i \vec{v}_i^T$$

where \vec{u}_i, \vec{v}_i are the columns of U, V , respectively, and σ_i are corresponding diagonal entry of the matrix Σ

Computing SVD with $A^T A$

$$\begin{aligned} A^T A &= U \Sigma V^T V \Sigma^T U^T \\ &= U \Sigma^2 U^T \end{aligned}$$

This is an eigen decomposition since Σ^2 is diagonal and $U^{-1} = U^T$. Thus solving for the eigenvalues and eigenvectors of $A^T A$ give $\lambda_i = \sigma_i^2$ with eigenvectors which correspond to the right singular vectors. We need to sort by decreasing σ_i .

Side note: $\Sigma^T \Sigma$ is not actually equal to Σ^2 , but the former product yields a matrix with singular values squared on the diagonal entries, hence we call it Σ^2

Computing SVD with $A^T A$

Given a right singular vector \vec{v}_i which we found from the previous part, we can apply it

$$\begin{aligned}
 A\vec{v}_i &= \left(\sum_{k=1}^r \sigma_k \vec{u}_k \vec{v}_k^T \right) \vec{v}_i \\
 &= \sum_{k=1}^r \sigma_k \vec{u}_k \vec{v}_k^T \vec{v}_i \\
 &= \sigma_i \vec{u}_i \\
 \vec{u}_i &= \frac{1}{\sigma_i} A\vec{v}_i
 \end{aligned}$$

Computing SVD with AA^T

Similar calculations yield $\sigma_i = \sqrt{\lambda_i}$ of AA^T with eigenvectors as left singular vectors, and $\vec{v}_i = \frac{1}{\sigma_i} A^T \vec{u}_i$

Intepretation of SVD

- ▶ Unitary matrices act as rotation in a given space. A diagonal matrix stretches in a given coordinate space.
- ▶ SVD visualization (open in browser)

Intepretation of SVD

For a product $A\vec{x}$, we can decompose every vector \vec{x} into a linear combination of right singular vectors

$$\vec{x} = \sum_{i=1}^n \alpha_i \vec{v}_i$$

Thus, we can see exactly which parts of \vec{x} affect the output.

Compression of Low-Rank Matrices

- ▶ Suppose I had a matrix $A \in \mathbb{R}^{m \times n}$ with $m, n \gg \text{rank}(A)$. How could I more efficiently store A and compute products like $A\vec{x}$?
- ▶ With the SVD, we only have to save r set of two vectors and a scalar, which saves us a lot of space if the rank is small with respect to the matrix. Also, less computation is carried out if we represent the matrix as the outer product form.

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PCA is a linear dimensionality reduction tool. Given data $\vec{x}_i \in \mathbb{R}^d$, we can create a mapping $T : \mathbb{R}^d \rightarrow \mathbb{R}^{d'}$, $d' < d$ such that the variance in the dataset is still captured

PCA — Computation

1. Store data row-major in $A \in \mathbb{R}^{n \times d}$
2. De-mean A
3. Take SVD: $A = U\Sigma V^T$
4. Create $V_{d'} \in \mathbb{R}^{n \times d'}$ from vectors of V corresponding to d' greatest singular values
5. To project data into the representative subspace:
 $T(x) := V_{d'}^T x$

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3. Take SVD: $A = U\Sigma V^T$
4. Create $V_{d'} \in \mathbb{R}^{n \times d'}$ from vectors of V corresponding to d' greatest singular values
5. To project data into the representative subspace:
 $T(x) := V_{d'}^T x$

PCA: computation

The mapping T can then be expressed as

$$T(\vec{x}) = V_k^T \vec{x}$$

If we apply this transformation onto the entire dataset (which has row vectors), we can say

$$T(A) = B = AV_k$$

where $B \in \mathbb{R}^{n \times k}$

PCA: computation

If we were to show the projected vectors in the original space, we can multiply back with the projection vectors

$$A' = BV_k^T$$

Overview

Eigenvalue Placement

Linearization

Singular Value Decomposition

Principle Component Analysis

Discretization

Discretization: Q1

Note: this section follows hw8 q1 almost exactly. Suppose we have a scalar system

$$\frac{d}{dt}x(t) = \alpha x + \vec{\beta}^T \vec{u}(t)$$

and we apply a constant input \vec{u}_n for times $t \in [nT, (n+1)T)$ for some $T > 0$. Given $x(nT)$ solve the differential equation

Discretization: Q1 Sol

From $t = nT$ to $t = (n + 1)T$, $\vec{\beta}^T \vec{u}$ is a constant scalar. Thus, we can solve this like a normal differential equation. Let

$x = x' - \frac{\vec{\beta}^T \vec{u}}{\alpha}$. Then

$$\begin{aligned}\frac{d}{dt}x(t) &= \alpha(x' - \frac{\vec{\beta}^T \vec{u}}{\alpha}) + \vec{\beta}^T \vec{u}(t) \\ &= \alpha x'\end{aligned}$$

$$x' = Ae^{\alpha(x-nT)}$$

$$x + \frac{\vec{\beta}^T \vec{u}}{\alpha} = Ae^{\alpha(x-nT)}$$

$$x = Ae^{\alpha(x-nT)} - \frac{\vec{\beta}^T \vec{u}}{\alpha}$$

At which point we can use our initial condition to get

$$x(nT) = A - \frac{\vec{\beta}^T \vec{u}}{\alpha}$$

Discretization: Q2

Using the differential equation derived from question 1, create a discrete-time system to model the continuous time. In other words, if $x[n] = x(nT)$, $\vec{u}[n] = \vec{u}(nT)$, find a relation such that

$$x[n+1] = A_d x[n] + B_d \vec{u}[n]$$

Discretization: Q2 Sol

We can solve the previous solution for $x((n+1)T)$

$$x((n+1)T) = \left(x(nT) + \frac{\vec{\beta}^T \vec{u}(nT)}{\alpha} \right) e^{\alpha((n+1)T - nT)} - \frac{\vec{\beta}^T \vec{u}(nT)}{\alpha}$$

$$x[n+1] = e^{\alpha T} x[n] + \frac{e^{\alpha T} - 1}{\alpha} \vec{\beta}^T \vec{u}[n]$$

We see that $A_d = e^{\alpha T}$, $B_d = ((e^{\alpha T} - 1)/\alpha) \vec{\beta}^T$

Discretization: Q3

Instead of a scalar, we instead have a diagonal matrix A such that

$$\frac{d}{dt}\vec{x} = A\vec{x} + B\vec{u}$$

Discretize this system in the same way as Q2.

Discretization: Q3 Sol

Expanding the original system out line-by-line gives

$$\frac{d}{dt}x_i = a_i x_i + b_i \vec{u}_i$$

where x_i is the i th variable of \vec{x} , a_i is the diagonal entry of A , and b_i is the row of B .

Discretization: Generic Matrix

Math not shown, but we can perform a change of basis from our original space to our diagonal space, and then apply the results of the previous part.