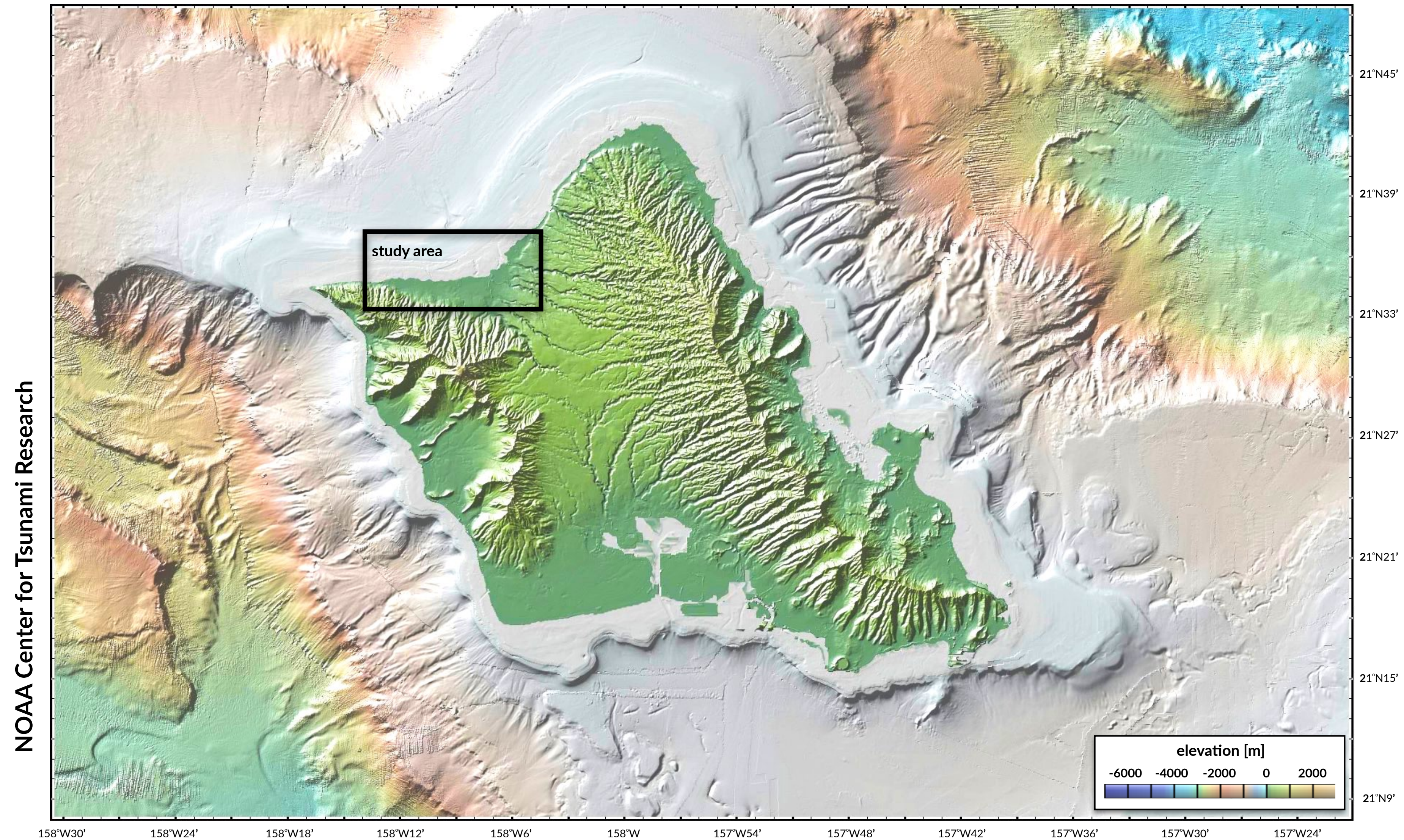


# Better physics for coastal dynamics

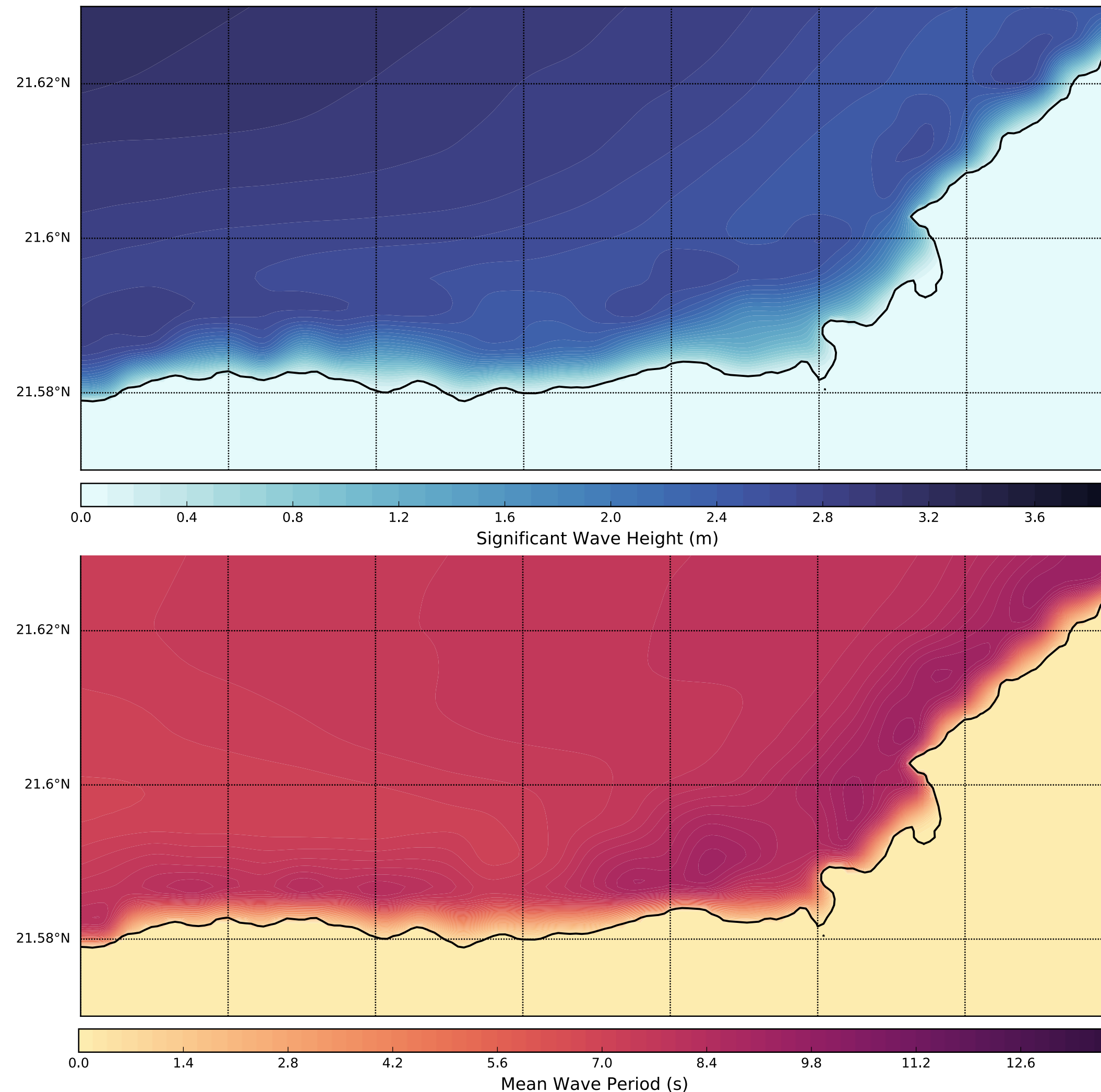
Sediment transport using open-source dataset





# Better physics for coastal dynamics

## Sediment transport



Under pure waves (*i.e.* with no superimposed current), the wave-generated bed shear stress  $\tau_w$  is typically conceived of as a quadratic bottom friction:

$$\tau_w = \frac{1}{2} \rho f_w U_{w,b}^2 \quad [2]$$

where  $\rho$  is water density,  $f_w$  is the wave friction factor, and  $U_{w,b}$  is the maximum over-the-wave-cycle horizontal wave-orbital velocity. Inserting into equation [2] the linear shallow-water approximation for  $U_{w,b}$ , given by:

$$U_{w,b} = (H_s/2) \sqrt{g/h} \quad [3]$$

where  $g$  is the acceleration due to gravity and  $h$  the water depth, yields an expression for  $\tau_w$  in terms of the wave height [Green & Coco, 2013]:

$$\tau_w = \frac{\rho g f_w}{8} \frac{H_s^2}{h} \quad [4]$$

Assuming that the wave boundary layer is hydraulically rough turbulent, the wave friction factor, by definition [Nielsen, 1992], depends solely on the bed roughness  $k_b$  relative to the wave-orbital semi excursion at the bed  $A_b$ . Following Soulsby [1997], we use:

$$f_w = 1.39 (A_b/k_b)^{-0.52} \quad [5]$$

where  $A_b = U_{w,b} T_m$  and  $k_b$  is evaluated as a grain roughness [Smith & McLean, 1977] given as  $2\pi d_{50}/12$ , where  $d_{50}$  is the median grain size of the bed sediment.

Most waves in the region reach wave base at approximately 20 m depth and convert their wave energy into shear stress across the sea floor, providing a means for mechanical abrasion of both carbonate framework and direct sediment producers. As an example figure 2 shows the derived values for horizontal wave-orbital velocity and shear stress obtained from PacIOOS dataset.