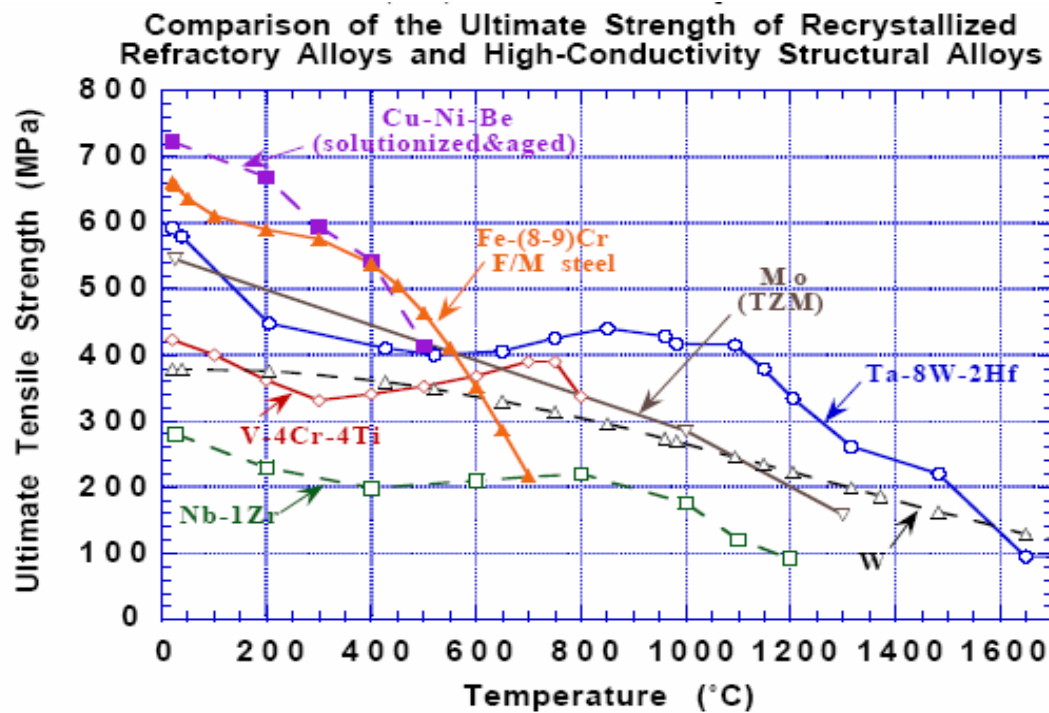


Material: Refractory Alloys and High-Conductivity Structural Alloys
Property: Ultimate Tensile Strength vs. Temperature
Condition: Un-Irradiated
Data: Experimental



Source:

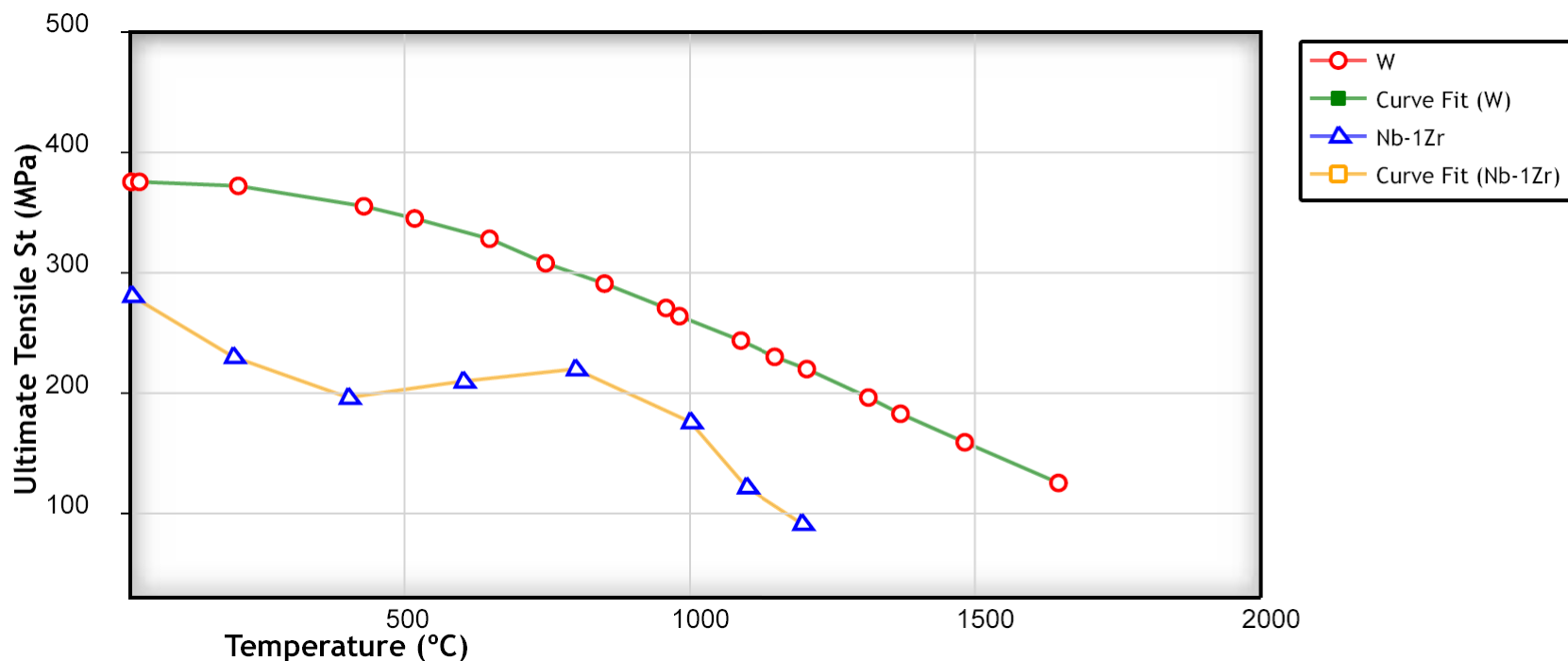
APEX Study Meeting, Sandia National Laboratory (July 27-28, 1998)

Title of paper (or report) this figure appeared in:

Status of Recent Activities by the APEX Materials Group

Author of paper or graph:

S.J. Zinkle



Comparison of the Ultimate Strength of Recrystallized Refractory Alloys and High-Conductivity Structural Alloys

Reference:

Author: S. J. Zinkle

Title: Status of Recent Activities by the APEX Materials Group

Source: APEX Study Meeting, Sandia National Laboratory (July 27-28, 1998), [\[PDF\]](#)

[View Data](#)[Author Comments](#)

Plot Format:

Y-Scale: ☒ linear ☐ log ☐ ln

X-Scale: ☒ linear ☐ log ☐ ln

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Status of Recent Activities by the APEX Materials Group

- **Physical Properties of Proposed Coolants and Structural Materials**
- **Estimated operating temperature limits**
- **Updated cost information**

**S.J. Zinkle
Oak Ridge National Laboratory**

**presented at APEX Study Meeting
Sandia National Laboratory, July 27-28, 1998**

Possible Structural Materials for High Wall Loading Concepts

- **Low-activation materials**

- Vanadium alloys

- Ferritic/martensitic (8-9%Cr) steels, ODS steels

- SiC/SiC composites

- **Refractory alloys**

- Nb-1Zr

- Nb-18W-8Hf

- T-111 (Ta-8W-2Hf)

- TZM (Mo-0.5Ti-0.1Zr-0.02C)

- Mo-Re

- W-25Re

- **Intermetallics**

- TiAl

- Fe₃Al

- **Composites**

- C/C

- metal matrix composites

- Cu-graphite

- Ti₃SiC₂ composites

- **Ni-based superalloys**

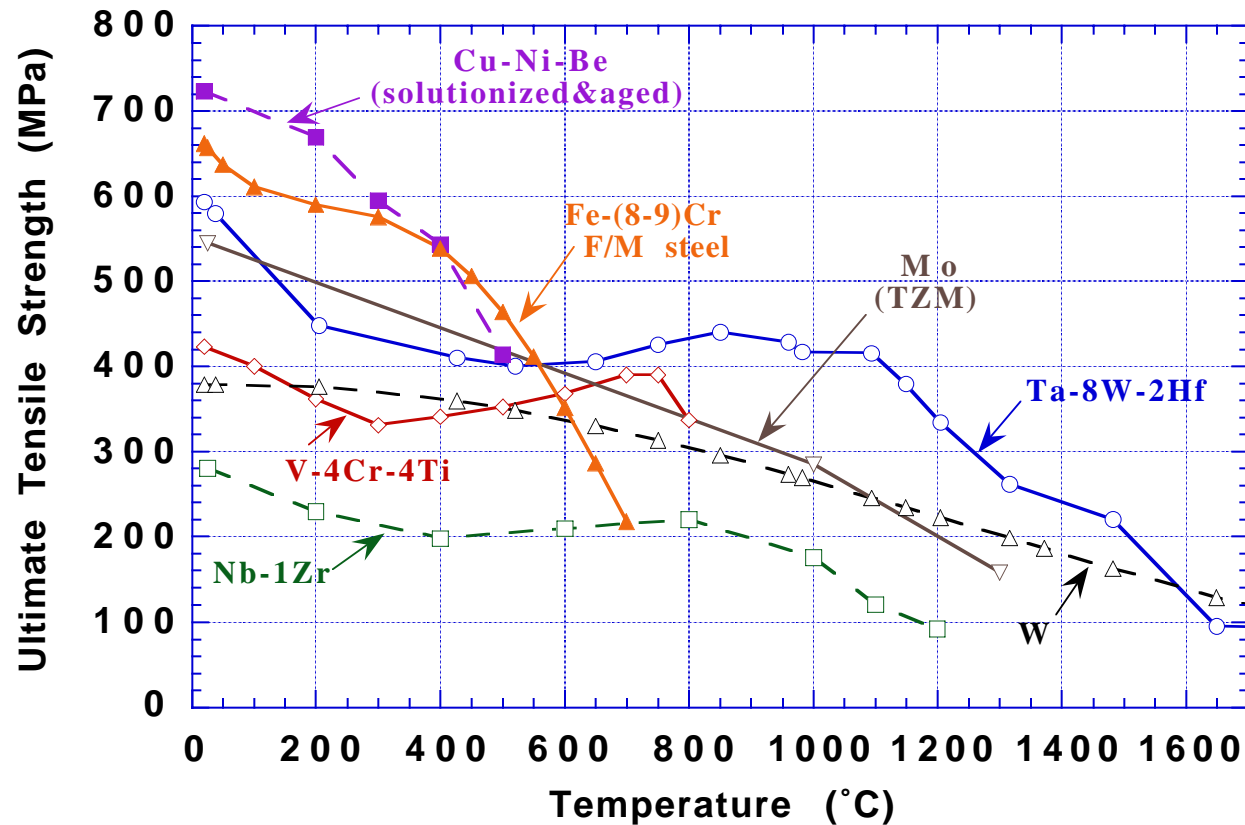
- **Porous-matrix metals and ceramics**

Factors Affecting Selection of Structural Materials

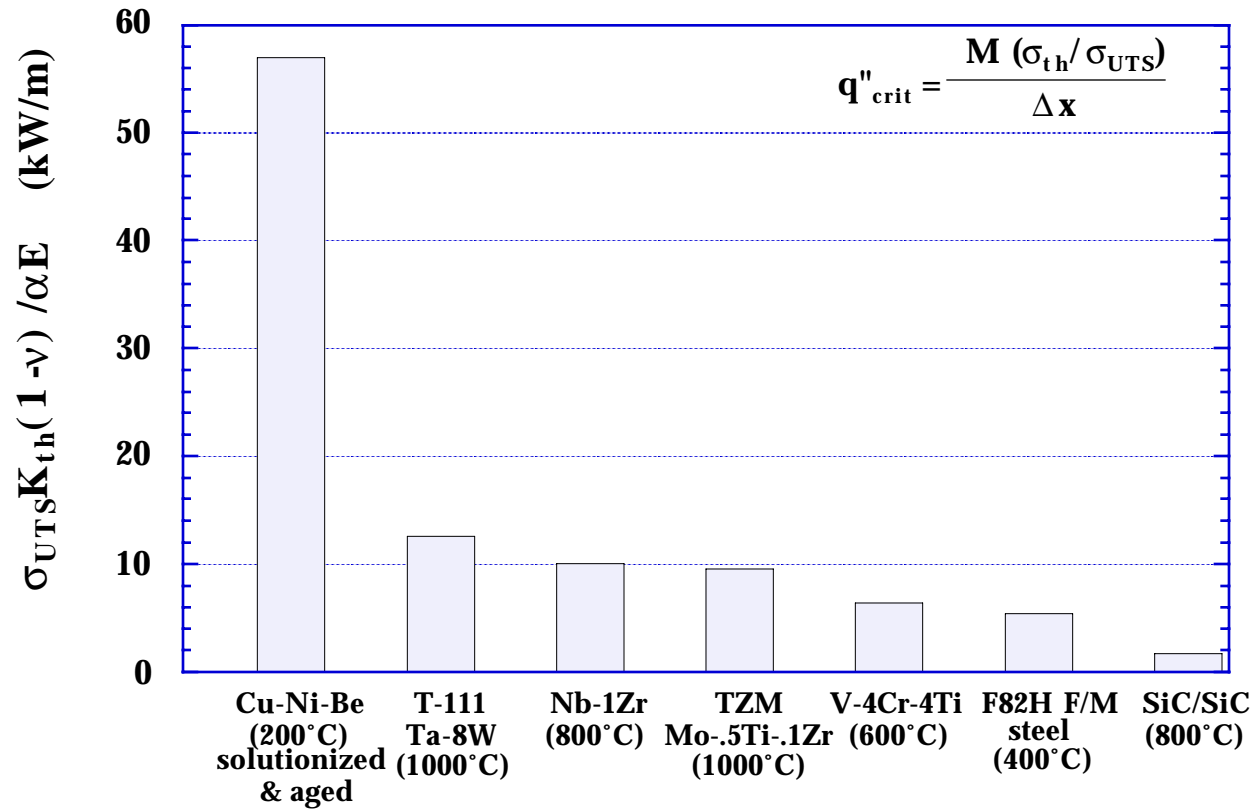
- **Unirradiated mechanical and thermophysical properties**
- **Chemical compatibility/corrosion effects**
- **Materials availability / fabricability / joining technology**
- **Radiation effects**
- **Safety aspects (decay heat, induced radioactivity, etc.)**

Data from Tietz & Wilson (1965), Conway (1984), Buckman (1994),
Zinkle et al (1998), ITER MPH, and Aerospace Structural Metals Handbook (1969)

Comparison of the Ultimate Strength of Recrystallized Refractory Alloys and High-Conductivity Structural Alloys



COMPARISON OF THERMAL STRESS PARAMETERS FOR ANNEALED ALLOYS
 (recrystallized Ta, Nb, Mo, V alloys; aged Cu alloy; tempered martensitic steel)



Resources for Structural Materials Database

- **Fusion Materials Properties Handbook / ITER Materials Properties Handbook, ed. J.W. Davis (Boeing/St Louis)**
 - V alloy chapter has NOT been updated in latest versions of IMPH (pubs. 4, 5)
 - limited or no information for F/M steels, SiC/SiC
- **Aerospace Structural Metals Handbook (1963-1988), ed. W.F. Brown, Jr.**
 - mechanical and thermophysical properties of refractory alloys vs. temperature
- **Proc. Conf. on Refractory Alloys for Space Nuclear Power Applications, eds. R.H. Cooper, Jr. and E.E. Hoffman, CONF-8308130 (1984)**
- **ITER Materials Assessment Report G A1 DDD 01 97-08-13 W01.1 (Chapter 2.2, W alloys)**
- **Original research publications**

Summary of V-4Cr-4Ti Properties

Ultimate Tensile Strength (unirradiated)

$$\sigma_{\text{UTS}}(\text{MPa}) = 446 - 0.806 * T + 0.00221 * T^2 - 1.79\text{e-}06 * T^3 + 1.82\text{e-}10 * T^4 \quad (T \text{ in } ^\circ\text{C})$$

Yield Strength (Unirradiated)

$$\sigma_Y(\text{MPa}) = 377 - 0.704 * T + 0.00090 * T^2 - 1.23\text{e-}07 * T^3 - 1.98\text{e-}10 * T^4 \quad (T \text{ in } ^\circ\text{C})$$

Elongation

e_{tot} , RA are high in unirradiated and irradiated conditions

e_u is high in unirradiated conditions, moderate (>2%) after irradiation at $T > 430^\circ\text{C}$ and low (<1%) for irradiation at $T < 400^\circ\text{C}$

Elastic constants

$$E_Y (\text{GPa}) = 128 - 0.00961 * T \quad (T \text{ in Kelvin})$$

$$G (\text{GPa}) = 48.8 - 0.00843 * T \quad (T \text{ in Kelvin}) \quad \nu = (E_Y / 2G) - 1$$

Thermophysical properties

$$\alpha_{\text{th}} = 9.03767 + 0.00301422 * T + 4.95937 \times 10^{-7} * T^2 \quad \text{ppm}/^\circ\text{C} \quad (T \text{ in } ^\circ\text{C})$$

$$C_p = 0.5755 - 21.1 / T \quad \text{J/g-K} \quad (T \text{ in Kelvin})$$

$$k_{\text{th}} = 27.8 + 0.0086 T \quad \text{W/m-K} \quad (T \text{ in Kelvin})$$

Recommended operating temperature limits (structural applications)

$T_{\text{min}} = 400^\circ\text{C}$ (due to rad.-induced increase in DBTT at low T_{irr})

$T_{\text{max}} = 700^\circ\text{C}$ (corrosion/chemical compatibility and thermal creep)

Summary of Recrystallized Ta-8W-2Hf (T-111) Properties

Ultimate Tensile Strength (unirradiated)

$$\sigma_{\text{UTS}}(\text{MPa}) = 630 - 1.532 * T + 0.003388 * T^2 - 2.807 \text{e-}06 * T^3 + 7.338 \text{e-}10 * T^4 \quad (T \text{ in } ^\circ\text{C})$$

Yield Strength (Unirradiated)

$$\sigma_Y(\text{MPa}) = 612 - 1.743 * T + 0.003585 * T^2 - 3.076 \text{e-}06 * T^3 + 8.819 \text{e-}10 * T^4 \quad (T \text{ in } ^\circ\text{C})$$

Elongation

e_{tot} , RA are high in unirradiated and irradiated conditions

e_u is high in unirradiated conditions, moderate (>2%) after irradiation at $T > 650^\circ\text{C}$ and low (<1%) for irradiation at $T < 600^\circ\text{C}$

Elastic constants (pure Ta)

$$E_Y (\text{GPa}) = 169 - 0.00822 * T - 1.66 \times 10^{-6} T^2 \quad (T \text{ in Kelvin})$$

$$G (\text{GPa}) = 77.4 - 0.0173 * T \quad (T \text{ in Kelvin})$$

$$\nu = (E_Y / 2G) - 1$$

$$\nu = 0.35 \text{ (300 K)}$$

Thermophysical properties

$$\alpha_{\text{th}} = 5.9 \text{ ppm}/^\circ\text{C} \text{ (20}^\circ\text{C)} \text{ and } 7.6 \text{ ppm}/^\circ\text{C} \text{ (1650}^\circ\text{C)}$$

$$C_p = 150 \text{ J/kg-K} \quad (20^\circ\text{C})$$

$$K_{\text{th}} (\text{W/m-K}) = 41.0 + 0.020 T - 6.32 \times 10^{-6} T^2 \quad (T \text{ in } ^\circ\text{C})$$

Recommended operating temperature limits (structural applications)

$T_{\text{min}} = 650^\circ\text{C}$ (due to rad.-induced increase in DBTT at low T_{irr})

$T_{\text{max}} = 1200^\circ\text{C}$ (thermal creep)

Summary of 8-9Cr Ferritic/Martensitic Steel Properties

Ultimate Tensile Strength (unirradiated)

$$\sigma_{\text{UTS}}(\text{MPa}) = 683 - 1.162 * T + 0.00547 * T^2 - 1.17 \text{e-}05 * T^3 + 6.24 \text{e-}09 * T^4 \quad (T \text{ in } ^\circ\text{C})$$

Yield Strength (Unirradiated)

$$\sigma_Y(\text{MPa}) = 531 - 0.388 * T + 0.00148 * T^2 - 2.40 \text{e-}06 * T^3 - 1.45 \text{e-}10 * T^4 \quad (T \text{ in } ^\circ\text{C})$$

Elongation

e_{tot} , RA are moderate to high in unirradiated and irradiated conditions ($e_{\text{tot}} \sim 8\text{-}10\%$ for $T_{\text{irr}} < 400^\circ\text{C}$)
 e_u is low in unirradiated (0.2-7%) and irradiated (<3%) conditions

Elastic constants

$$E_Y(\text{GPa}) = 233 - 0.0558 * T \quad 20\text{-}450^\circ\text{C} \quad (T \text{ in Kelvin})$$

$$G(\text{GPa}) = 90.1 - 0.0209 * T \quad 20\text{-}450^\circ\text{C} \quad (T \text{ in Kelvin}) \quad \nu = (E_Y / 2G) - 1$$

Thermophysical properties

$$\alpha_{\text{th}} = 10.4 \text{ ppm}/^\circ\text{C} (20^\circ\text{C}) \text{ to } 12.4 \text{ ppm}/^\circ\text{C} (700^\circ\text{C})$$

$$C_p = 0.47 \text{ J/g-K} (20^\circ\text{C}) \text{ to } 0.81 \text{ J/g-K} (700^\circ\text{C})$$

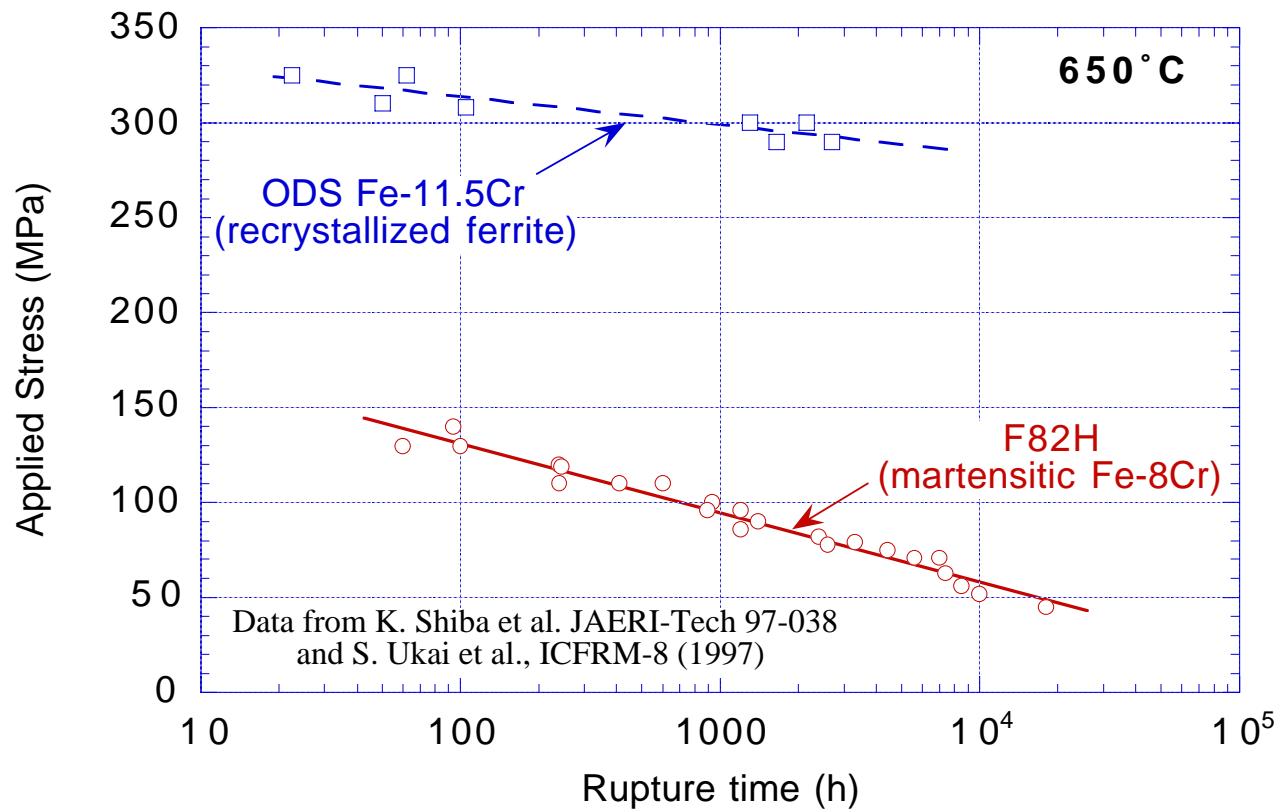
$$k_{\text{th}} = 33 \text{ W/m-K} \quad (20\text{-}700^\circ\text{C})$$

Recommended operating temperature limits (structural applications)

$T_{\text{min}} = 250^\circ\text{C}$ (due to rad.-induced increase in DBTT at low T_{irr})

$T_{\text{max}} = 550^\circ\text{C}$ (thermal creep); $T_{\text{max}} \sim 700^\circ\text{C}$ for ODS steels?

Comparison of Creep Strength of F82H and ODS Fe-11.5Cr steels



Summary of SiC/SiC Properties

Ultimate Tensile Strength (unirradiated)

$\sigma_{\text{UTS}} \sim 220\text{-}240 \text{ MPa}$ (20-1000°C)

Proportional Limit Strength (Unirradiated)

$\sigma_Y(\text{MPa}) \sim 70 \text{ MPa}$ (20-1000°C)

Elongation

e_{tot} , e_u , RA are very low in unirradiated and irradiated conditions

Elastic constants

$E_Y \text{ (GPa)} \sim 400 \text{ GPa}$ 20- 1000°C (Sylramic or Hi-Nicalon type S fibers, 10% matrix porosity)

$G \text{ (GPa)} \sim 165 \text{ GPa}$ 20- 1000°C

$\nu = 0.16$ 20- 1000°C

Thermophysical properties

$\alpha_{\text{th}} \sim 2.5 \text{ ppm/}^\circ\text{C}$ (20°C) to $4.5 \text{ ppm/}^\circ\text{C}$ (1000°C)

$C_p = 1110 + 0.15 T - 425 e^{-0.003T} \text{ J/kg-K}$ (1000°C)

$k_{\text{th}} = 10\text{-}15 \text{ W/m-K}$ (400-1000°C, after irradiation)

Recommended operating temperature limits (structural applications)

$T_{\text{min}} \sim 400^\circ\text{C}$ (due to rad.-induced decrease in thermal conductivity)

$T_{\text{max}} = 1000^\circ\text{C?}$ (due to cavity swelling)

Summary of Recrystallized Tungsten Properties (from IMPH)

Ultimate Tensile Strength (unirradiated)

$$\sigma_{\text{UTS}}(\text{MPa}) = 377.9 + 0.03207 * T - 1.955 \times 10^{-4} * T^2 + 5.129 \times 10^{-8} * T^3 \quad (T \text{ in } ^\circ\text{C})$$

Yield Strength (Unirradiated)

$$\sigma_Y(\text{MPa}) = 94.2 - 0.0214 * T - 2.12 \times 10^{-4} * T^2 - 7.48 \times 10^{-10} * T^3 \quad (T \text{ in } ^\circ\text{C})$$

Elongation

$$e_{\text{tot}}(\%) = 20.8 + 0.053 * T - 2.18 \times 10^{-5} * T^2 \quad (T > 500^\circ\text{C})$$

Elastic constants

$$E_Y(\text{GPa}) = 398 - 0.00231 * T - 2.72 \times 10^{-5} T^2 \quad (T \text{ in } ^\circ\text{C})$$

$$\nu = 0.279 + 1.09 \times 10^{-5} T \quad (T \text{ in } ^\circ\text{C})$$

Thermophysical properties

$$\alpha_m (10^{-6}/^\circ\text{C}) = 3.922 + 5.835 \times 10^{-5} * T + 5.705 \times 10^{-11} * T^2 - 2.046 \times 10^{-14} * T^3 \quad (T \text{ in } ^\circ\text{C})$$

$$C_P (\text{J/kg-K}) = 128.3 + 0.0328 * T - 3.41 \times 10^{-6} * T^2 \quad (T \text{ in } ^\circ\text{C})$$

$$K_{\text{th}} (\text{W/m-K}) = 174.9 - 0.107 T + 5.01 \times 10^{-5} T^2 - 7.835 \times 10^{-9} * T^3 \quad (T \text{ in } ^\circ\text{C})$$

Recommended operating temperature limits (structural applications)

$T_{\text{min}} = 800^\circ\text{C}$ (due to rad.-induced increase in DBTT at low T_{irr})

$T_{\text{max}} = 1400^\circ\text{C}$ (corrosion/chemical compatibility and thermal creep)

Chemical Compatibility of High Temperature Refractory Alloys with Liquid Metals and FLiBe

- In general, the refractory alloys have very good compatibility with the liquid metals and salts of interest for fusion applications
 - impurity pickup is the key engineering issue
- Li chemical compatibility data base (to be discussed by Nasr Ghoniem):
 - T-111 (Ta-8W-2Hf) data up to 1370°C (good compatibility; static and circulating loops)
 - Nb-1Zr data up to 1000°C (good compatibility; static and circulating loops)
 - W alloys up to 1370°C (attack observed at $\geq 1540^\circ\text{C}$)
 - Mo alloys (TZM) up to 1370°C (attack observed at $\geq 1540^\circ\text{C}$)
- Chemical compatibility data base for FLiBe will be presented by Dai-Kai Sze (generally good compatibility with proposed structural metals)

**Maximum temperatures of structural alloys (bare walls) in contact
with high-purity liquid coolants, based on a 5 $\mu\text{m}/\text{yr}$ corrosion limit**

	Li	Pb-17 Li	Flibe
F/M steel	550-600°C [1,2,3]	450°C [1,2,9]	700°C ? 304/316 st. steel [13]
V alloy	600-700°C [1,4,5]	~650°C [1,10]	?
Nb alloy	>1300°C [6,7]	>600°C [10] (>1000°C in Pb) [11]	>800°C [14]
Ta alloy	>1370°C [6,7]	>600°C [10] (>1000°C in Pb) [11]	?
Mo	>1370°C [6,7]	>600°C [10]	>1100°C? [15,16]
W	>1370°C [6,7]	>600°C [10]	>900°C? [15]
SiC	~550°C ? [8]	>800°C ? [12]	?

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Overview of Radiation Effects in Refractory Metals

- Void swelling is not anticipated to be a lifetime-limiting issue due to the BCC structure of the high-temperature refractory alloys
 - existing fission reactor data base indicate low swelling ($<2\%$) for doses up to 50 dpa or higher
 - effects of fusion-relevant He generation on swelling is uncertain
 - swelling regimes are ~ 600 to 1000°C for all 4 classes of refractory alloys
- The Group Vb alloys (Nb, Ta) exhibit better ductility before and after irradiation
 - very limited mechanical properties data base on irradiated Nb, Ta alloys
 - extensive mechanical properties data base on irradiated Mo, W alloys
- Very limited or no fracture toughness/Charpy impact data on irradiated high temperature refractory alloys
 - “tensile DBTT” of Mo, W alloys increases to very high values even for low dose irradiations at moderate temperatures (e.g., 600°C after ~ 1 dpa irradiation at 300°C for W, W-10Re)
- Refractory alloys are generally designed for use in stress-relieved condition (rather than recrystallized) in order to achieve of higher strength
 - radiation-enhanced recrystallization and/or radiation creep effects need to be investigated (designs should use recrystallized strengths to be conservative)

Radiation Effects on Mechanical Properties of High-Temperature Refractory Alloys

Ta Alloys: T-111 (Ta-8W-2Hf)

- Significant radiation hardening at 415, 640°C (σ_y , UTS > 1000 MPa) after 1.9×10^{26} n/m², E > 0.1 MeV (2.5 dpa Ta, 10 dpa steel) -- Wiffen 1984
- Very little radiation hardening at 800°C, 2.5 dpa (Gorynin 1992)

=> estimated minimum operating temperature ~650°C, based on DBTT considerations

Mo Alloys: TZM (largest irradiated data base among high temperature refractories)

- Pronounced radiation hardening up to ~800°C, 7-34 dpa (Hasegawa et al. 1996)
- Tensile elongation ~0 for $T_{irr} < 700^\circ\text{C}$, 5-20 dpa (Chakin & Kazakov 1996, Fabritsiev & Pokrovsky 1998)

=> estimated minimum operating temperature ~750°C, based on DBTT considerations

W and W Alloys: P/M or CVD W, W-1% La₂O₃, W-Mo-Y (alloy W-13I)

- Tensile elongation ~0 for $T_{irr} = 400, 500^\circ\text{C}$, $0.5 - 1.5 \times 10^{26}$ n/m², ≤ 2 dpa (Wiffen 1984, Gorynin et al 1992); irradiations at 700°C are in progress

=> estimated minimum operating temperature ~800°C, based on DBTT considerations (scaling from Mo alloy data base)

Updated Cost Information (~1996 prices)

Material	Cost per kg
Fe-9Cr steels	\leq \$5.50 (plate form)
SiC/SiC composites	$>$ \$1000 (CVI processing) ~\$200 (CVR processing of CFCs)
V-4Cr-4Ti	\$200 (plate form--average between 1994-1996 US fusion program large heats and Wah Chang 1993 “large volume” cost estimate)
Nb-1Zr	~\$100
Ta	\$300 (sheet form)
Mo	~\$80 (3 mm sheet); ~\$100 for TZM
W	~\$200 (2.3 mm sheet); higher cost for thin sheet

Estimated Operating Temperature Limits for Refractory Alloys in Fusion Reactors

