

- For the UFSS system studied in Part 4, use Simulink to compute the unit step open-loop response of the transfer function between the elevator deflection input and the pitch angle output. Using the plot, compute the percentage overshoot, rise time, peak time, settling time and compare them with the theoretical predictions. Show these values on the plot as well.

Using MATLAB

```
sys = tf(-0.125*[1 0.435],conv([1 1.23],[1 0.226 0.0169]))
step(sys,100);
stepinfo(sys)
```

```
sys =
 
      -0.125 s - 0.05437
      -----
      s^3 + 1.456 s^2 + 0.2949 s + 0.02079
```

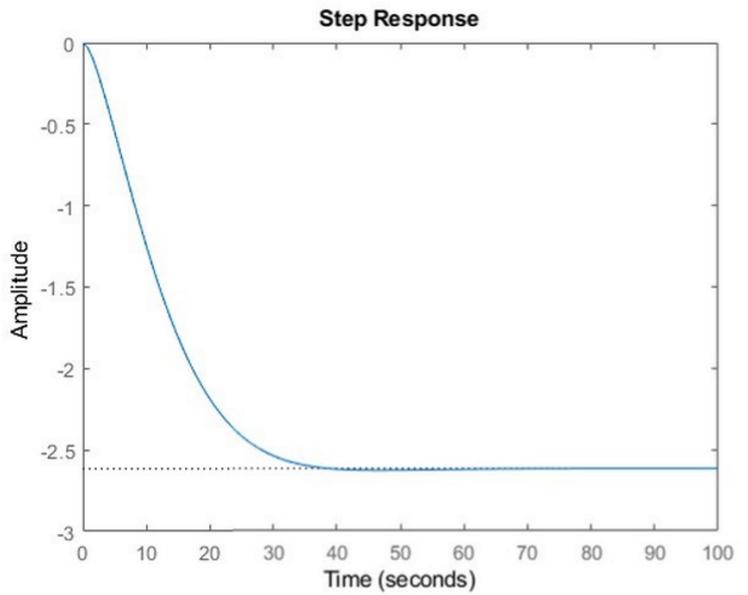
Continuous-time transfer function.



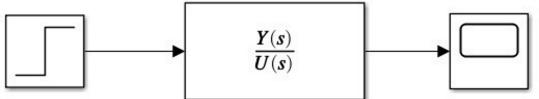
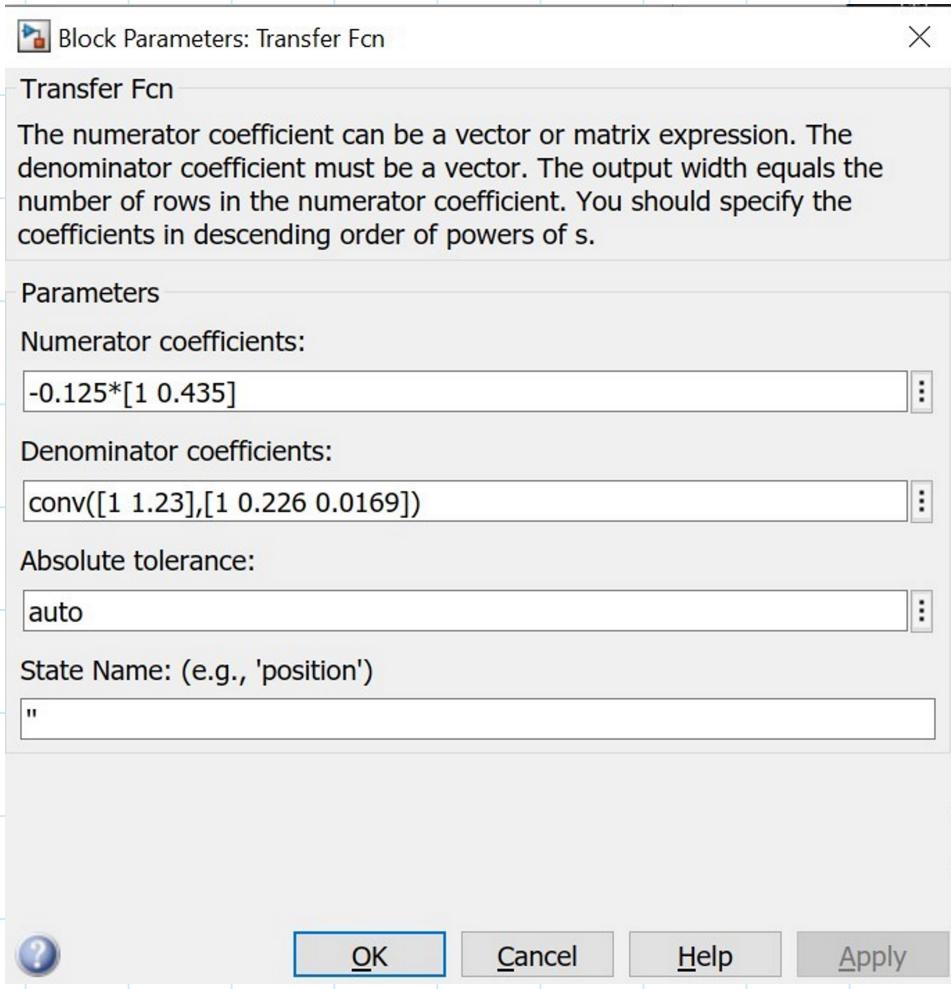
```
ans =
```

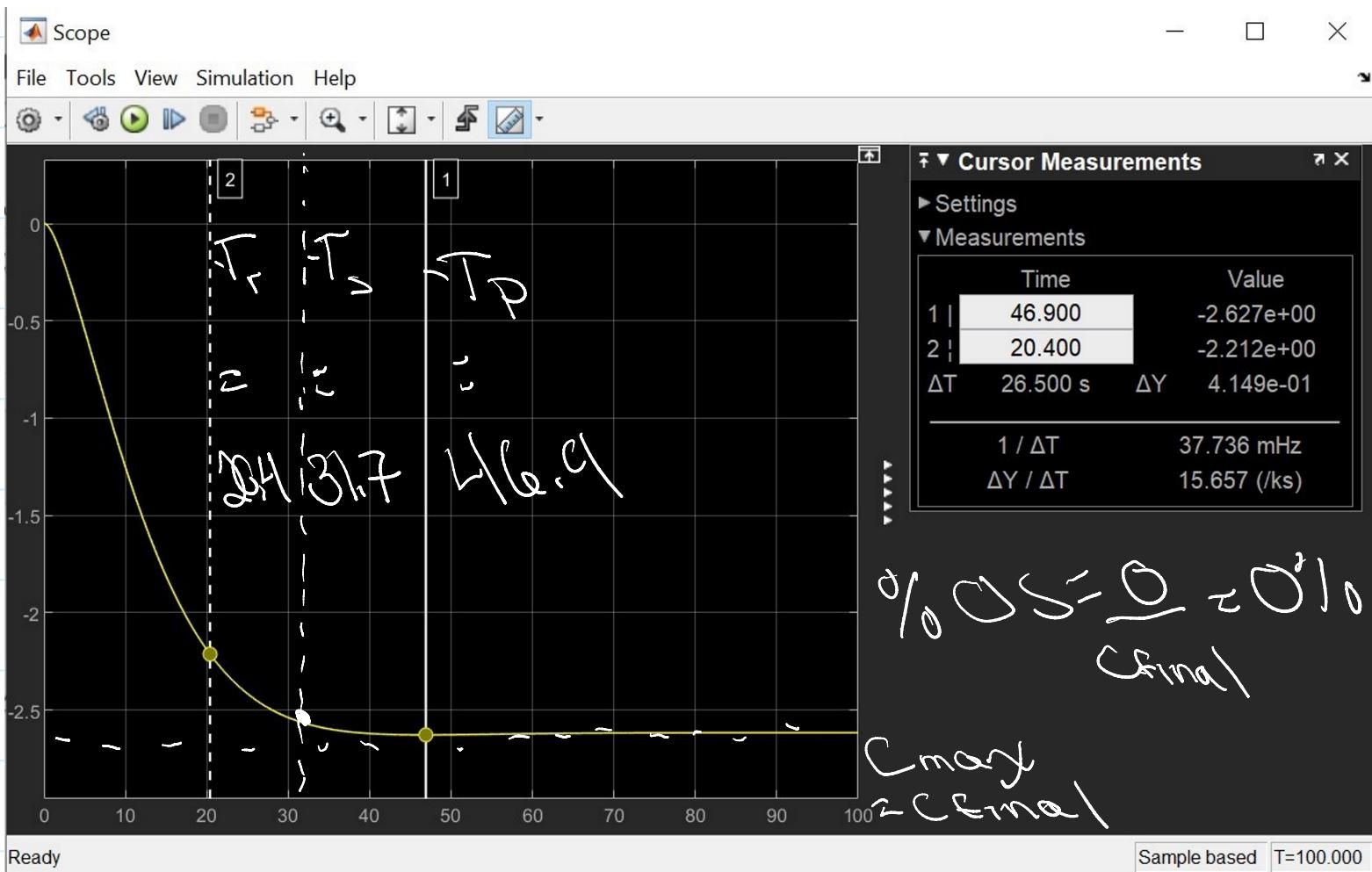
```
struct with fields:
```

```
RiseTime: 20.3983  
SettlingTime: 31.7417  
SettlingMin: -2.6269  
SettlingMax: -2.3660  
Overshoot: 0.4233  
Undershoot: 0  
Peak: 2.6269  
PeakTime: 46.8668
```



Using Simulink





Theoretical Approximate as Second Order

$$G(s) = \frac{-0.125(s + 0.425)}{(s + 1.23)(s^2 + 0.226s + 0.0164)}$$

Poles $s = -1.23$

Zeros $s_4 = -6433$

$$s_{1,2} = -6 \pm \sqrt{162 - 400}$$

$$= 0.226 \pm \sqrt{-0.0165}$$

$$= 0.112 + 0.120i$$

Approximate as
 $G(s) = \frac{-0.125}{(s_2 + 0.2265 + 0.0164)}$

since $s_{1,2}$ dominates

closer to origin than $s_{2,3}$

$$2\omega_n = 0.226 \quad \omega_n^2 = 0.0164$$

$$\zeta = 0.869$$

$$\omega_n = 0.13$$

$$T_p = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}} = 48.4$$

$$T_s = \frac{1}{\zeta \omega_n} = 35.4 \quad T = \frac{\text{Peak}_1}{\text{Peak}_2}$$

$$\eta_{OS} = 100 \times \left(\frac{s_1}{s_2} \right)^2 = 0.389\%$$

$$\omega_n T_p = 2.75 \quad \text{From Plot } T_p = 21.2$$

$$\text{Peak}_2 = f(\infty) = \lim_{S \rightarrow 0} SF(S) =$$

$$\lim_{S \rightarrow 0} \frac{10}{S} \left(\frac{-0.125}{s_2 + 0.2265 + 0.0164} \right) = \frac{-0.125}{0.0164}$$

$$5500 S \left(s^2 + 0.226s + 0.0169 \right) 0.0169 \\ = -7.11$$

$$K = \frac{\text{Peak}_1}{\text{Peak}_2} = \frac{-2.6269}{-7.1124} = 0.354$$

$$G(s) = \frac{0.0442}{(s^2 + 0.226s + 0.0169)}$$

MATLAB

```
K = 0.354
sys = tf(K*[-0.125], [1 0.226 0.0169])
step(sys, 100);
stepinfo(sys)
```

K =

0.3540

sys =

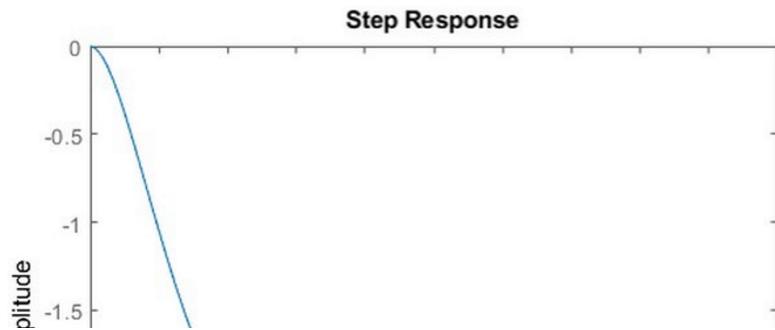
$$\frac{-0.04425}{s^2 + 0.226 s + 0.0169}$$

Continuous-time transfer function.

ans =

struct with fields:

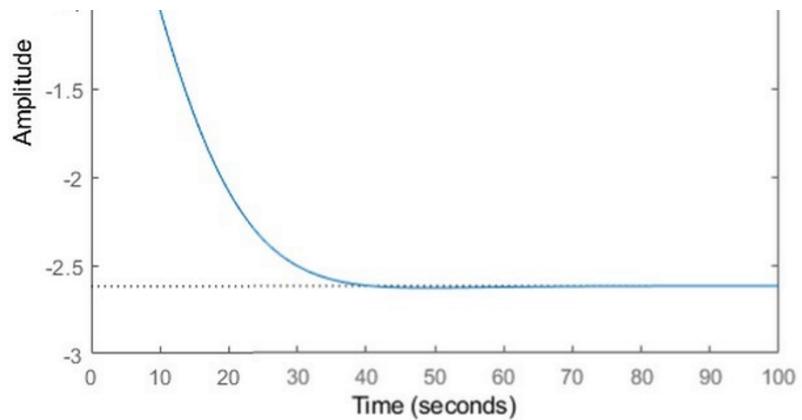
RiseTime:	21.1397
SettlingTime:	33.6748
SettlingMin:	-2.6288



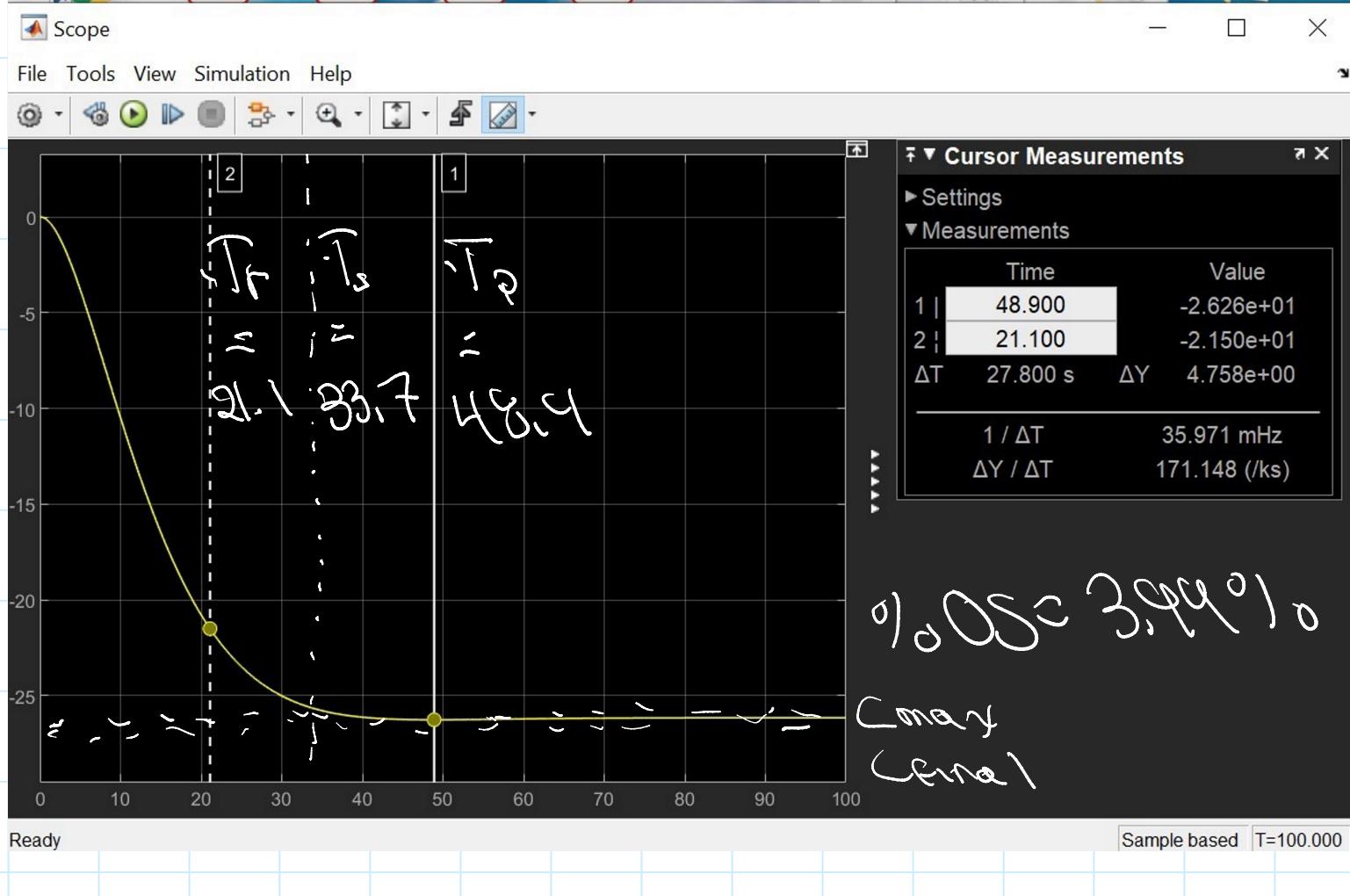
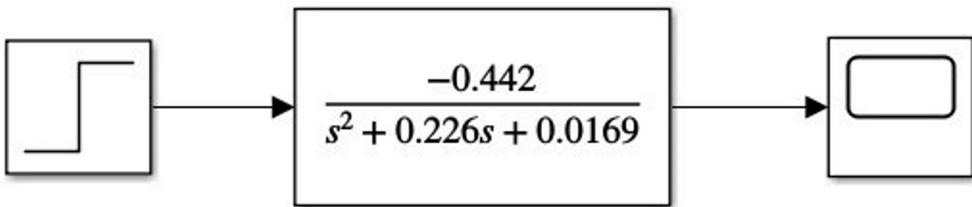
```

RiseTime: 21.1551
SettlingTime: 33.6748
SettlingMin: -2.6288
SettlingMax: -2.3618
Overshoot: 0.3993
Undershoot: 0
Peak: 2.6288
PeakTime: 48.9045

```



Simulating



Comparison
True Response

$$\%OS = 0\%$$

$$T_r = 20.5 \text{ s}$$

$$T_p = 46.4 \text{ s}$$

$$T_f = 31.7 \text{ s}$$

Approximate Response

$$\%OS \approx 3.00\%$$

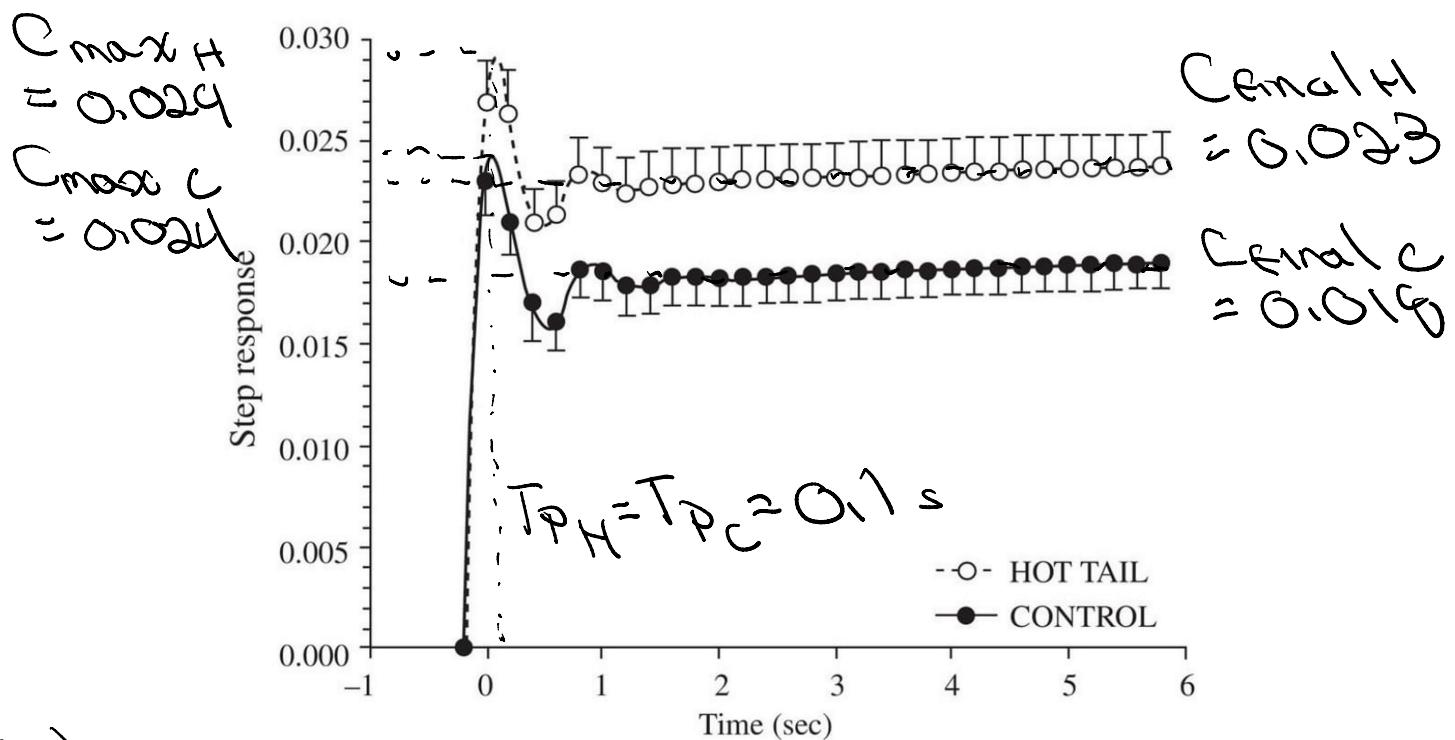
$$T_r \approx 21.1 \text{ s}$$

$$T_p \approx 46.9 \text{ s}$$

$$T_f \approx 33.7 \text{ s}$$

2. (Nise, 7th Edition) Several factors affect the working of the kidneys. The figure below shows how a step change in arterial flow pressure affects renal blood flow in rats. In the "hot tail" part of the experiment, peripheral thermal receptor stimulation is achieved by inserting the rat's tail in heated water. The vertical lines indicate the variations between different test subjects. It has been argued in the literature that the "control" and "hot-tail" responses are identical except their steady state values.

- Using the figure below, obtain the normalized ($c_{final} = 1$) transfer function for both responses.
- Use MATLAB to prove or disprove the assertion about the control and hot-tail responses.



(a)

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$\zeta_0 OS_T = \frac{C_{max\ H} - C_{final\ H}}{C_{final\ H}}$$

$$\zeta_0 OS_T = \frac{0.029 - 0.023}{0.023} = 0.261$$

$$\% OS_C = \frac{C_{max\ C} - C_{final\ C}}{C_{max\ C}} = \frac{0.024 - 0.018}{0.024} = 0.25$$

$$\%OS_C = \frac{C_{max} - C_{min}}{C_{max}} = \frac{0.024 - 0.018}{0.018}$$

$$= 0.333$$

$$f = \frac{-\ln(\%OS)}{\sqrt{s^2 + \ln(9 \%OS)^2}}$$

$$f_H = \frac{-\ln(0.1261)}{\sqrt{s^2 + \ln(0.1261)^2}} = 0.343$$

$$f_C = \frac{-\ln(0.333)}{\sqrt{s^2 + \ln(0.333)^2}} = 0.330$$

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{1-f^2}}$$

$$\omega_n = \frac{\pi}{T_p \sqrt{1-f^2}}$$

$$\omega_{nH} = \frac{\pi}{(0.1) \sqrt{1-0.3932}} = 34.2$$

$$\omega_{nC} = \frac{\pi}{(0.1) \sqrt{1-0.330^2}} = 33.3$$

$$G_H(f) = \frac{34.2^2}{s^2 + 2(0.393)(34.2f) + 34.2^2} \quad f = 1 \text{ (Normalized)}$$

$$= \frac{1167.5}{s^2 + 26.9s + 1167.5}$$

$$K = C_{final} N = 0.023$$

$$s^2 + 26.9s + 1167.5$$

$$f(\infty) = \lim_{s \gg 0} s F(s) \approx \lim_{s \gg 0} s G_H(s) = 1$$

$$G_H(s) = \frac{26.9}{s^2 + 26.9s + 1167.5} \quad (\text{Non-normalized})$$

$$G_C(s) = \frac{333^2}{s^2 + 2(0.330)(333)s + 333^2} \quad K = 1 \quad (\text{Normalized})$$

$$= \frac{1107.7}{s^2 + 21.97s + 1107.7} \quad K = C_{final} c = 0.018$$

$$f(\infty) = \lim_{s \gg 0} s F(s) \approx \lim_{s \gg 0} s G_C(s) = 1$$

$$G_C(s) = \frac{19.19}{s^2 + 21.97s + 1107.7} \quad (\text{Non-normalized})$$

(b)

```

sys_hot_tail = tf([1167.5],[1 26.9 1167.5])
sys_control = tf([1107.7],[1 21.97 1107.7])
step(sys_hot_tail,sys_control)
legend({'Hot-Tail','Control'})
hot_tail = stepinfo(sys_hot_tail)
control = stepinfo(sys_control)

sys_hot_tail =

```

$$\frac{1168}{s^2 + 26.9 s + 1168}$$

Continuous-time transfer function.

```

sys_control =

```

$$\frac{1108}{s^2 + 21.97 s + 1108}$$

Continuous-time transfer function.

```

hot_tail =

```

struct with fields:

- RiseTime: 0.0426
- SettlingTime: 0.2461
- SettlingMin: 0.9271
- SettlingMax: 1.2604
- Overshoot: 26.0395
- Undershoot: 0
- Peak: 1.2604
- PeakTime: 0.0993

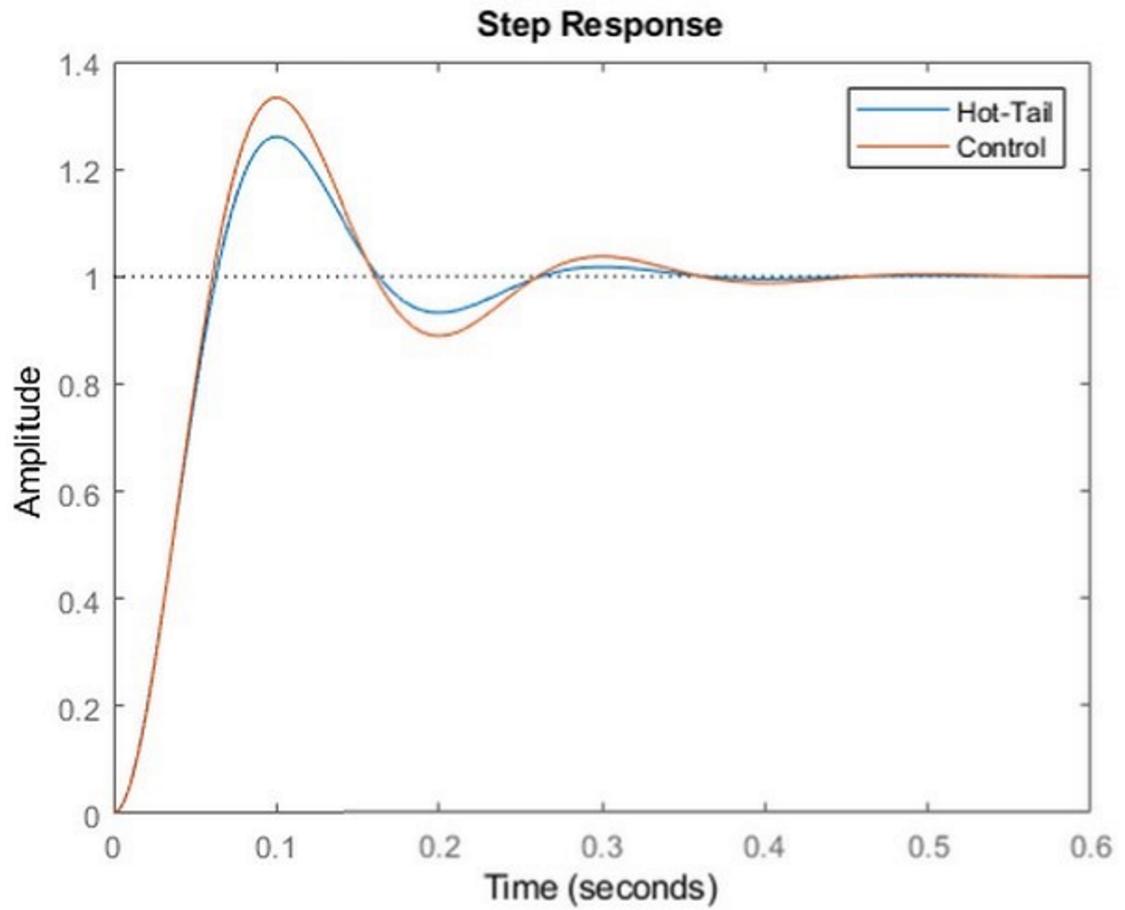
```

control =

```

struct with fields:

- RiseTime: 0.0410
- SettlingTime: 0.3341
- SettlingMin: 0.8889
- SettlingMax: 1.3333
- Overshoot: 33.3314
- Undershoot: 0
- Peak: 1.3333
- PeakTime: 0.1006



∵ From the normalized analysis
 we disprove the assertion
 "control and hot-tail response
 are 'identical' besides their
 steady state values". One
 characteristic that differs
 apparent from the graph is
 max peak. Other characteristics

main peak. Other characteristics
from the step response
can be deducted.