1. The equation for a FM wave is  $S(t) = 10 \cos[5.7 \times 10^8 t + 5 \sin(12 \times 10^3) t]$ . Calculate. i. Carrier frequency ii. Modulating frequency iii. Modulation index iv. Frequency deviation v. Power dissipated in a  $100\Omega$  resistor load.

S(±) = 10 Get [5.7×108± + 5 Sin (12×103) ±] 
$$\rightarrow$$
 0

Compare eq (1) with Standard equation for FM

S(±) = Ac (or [  $w_c$  ± +  $\beta$  Sin  $w_m$  ±]  $\rightarrow$  ②

Ac = 10 V,  $w_c$  = 5.7×108,  $\beta$  = 5 &  $w_m$  = 18×103

Castiley Pregreency  $\beta$  -  $w_c$  -  $\delta$ .7×108

i) Cassies frequency 
$$f_c = \frac{W_c}{3\pi} = \frac{5.7 \times 10^8}{3\pi}$$

ii) Modulating frequency 
$$f_m = \frac{w_m}{a\pi} = \frac{12x10^3}{a\pi}$$

iii) Modulation Index

iv Frequency deviation  $\Delta f = \beta f_m = 5 \times 1.909 \text{ kHz}$ 

1) power dissipated in a 1002 Tresister Load

$$p = \frac{A_c^2}{3R} = \frac{10^2}{3\times100}$$

2. A FM signal has sinusoidal modulation with  $f_m$ =15KHz and modulation index  $\beta$ =2. Using carson's rule, find the transmission bandwidth and deviation ratio. Assume  $\Delta f$  =75 KHz.

Given:-
$$f_m = 15 \text{ KHz}, B = 2, \Delta F = 75 \text{ KHz}$$
 $BW = ?$  & Dereiation Fratio  $D' = ?$ 

$$* D = \frac{\Delta F}{P_m} = \frac{75 \text{ KH3}}{15 \text{ KH3}} = 5$$

3. A sinusoidal modulating voltage of amplitude 5V and frequency 1 KHz is applied to frequency modulator. The frequency sensitivity of modulator is 40 Hz/V. The carrier frequency is 100KHz. Calculate

i. Frequency deviator

ii. Modulation index

Given: - 
$$A_m = 5v$$
,  $f_m = 1KH3$ ,  $K_F = 40H3/v$  &  $f_c = 100KH3$ .

Frequency derivation  $\Delta f = K_F A_m = 40 \times 5 = \frac{300H3}{1000}$ 

ii) Modulation Index  $B' = \frac{\Delta F}{F_m} = \frac{300}{1000} = 0.2$ 

A carrier wave of 100 MHz is frequency modulated by a 100 KHz sinewave of amplitude 20V, the sensitivity of the modulator is 25 KHz/V.

- Determine the frequency deviation and bandwidth of the modulated signal using Carson's rule.
- ii. Repeat your calculation for PM wave, assume  $k_p = k_f$

$$βW = a[ΔF + Fm]$$

$$ΔF = K_F A_m = 25 KH3 × 20 = 500 KH3$$

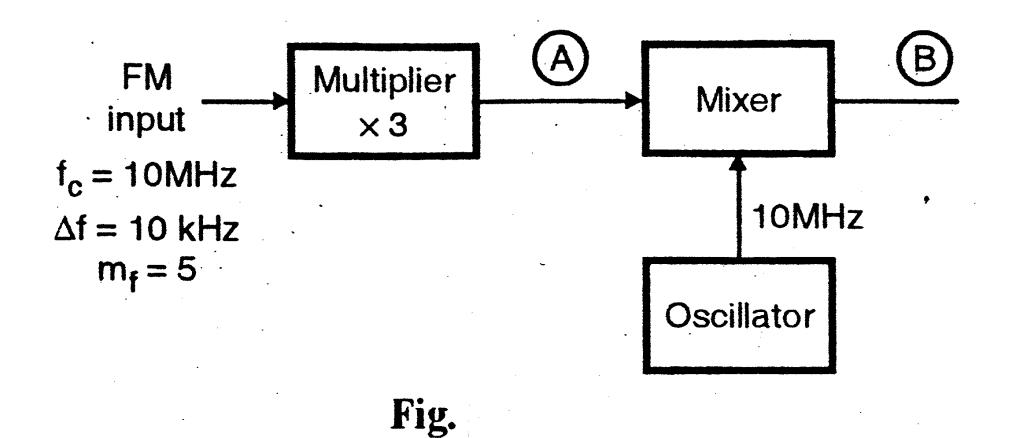
$$BW = a[500 KH3 + 100 KH3]$$

$$BW = 2F_m(1+B)$$

$$BW = \frac{500 \text{ kH}_3}{100 \text{ kH}_3} = \frac{5}{1}$$

$$BW = 2 \times 100 \text{ kH}_3(1+5)$$

In the block diagram shown in Fig. find out the carrier frequency, frequency deviation and modulation index at the points A and B. Assume that at the output of the mixer, the additive frequency component is being selected.



# Soln.:

#### (i) At point (A):

The carrier  $f_c = 3 \times 10 \text{ MHz} = 30 \text{ MHz}$ .

The frequency deviation  $\delta = 3 \times 10 \text{ kHz} = 30 \text{ kHz}$  and modulation index  $m_f = 3 \times 5 = 15$ .

The minimum frequency  $f_{min} = 30 \text{ MHz} - 30 \text{ kHz} = 29.970 \text{ MHz}$ 

The maximum frequency  $f_{max} = 30 \text{ MHz} + 30 \text{ kHz} = 30.030 \text{ MHz}.$ 

## (ii) At point (B):

Carrier frequency  $f_c = 30 \text{ MHz} + 10 \text{ MHz} = 40 \text{ MHz}$ .

Maximum frequency  $f_{max} = 30.03 + 10 = 40.03 \text{ MHz}$ 

Minimum frequency  $f_{min} = 29.970 + 10 = 39.970 \text{ MHz}.$ 

As there is no change in deviation due to mixing, the modulation index will remain same i.e.  $m_f = 15$ .

A Carrier wave of amplitude 50 & Preguency 90MHZ is frequency modulated by a Sinusoidal rollage of amplitude 50 & frequency - 15kHZ. The Preguency devoiation constant is 1kHZ/V. Skotch—the Specthum of the modulated FM wave.

From the table of Bessel functions, for B=0.333 use approximate values for Jo, J. & J2.

- i) F81 Cossiver: Jo = 0.96
- ii) 1st Side frequency: J= 0.18
- iii) and Side Prequency: J2=0.02

Sol:- Given: Ac=5V, fc=90MHZ, Am=5V, fm=15KHZ. Kp=1KHZ/V.

\* Frequency deviation  $\Delta F = K_F A_m = 1KH3/y × 5× = 5KH3.$ 

$$\frac{AP}{AP} = \frac{AP}{Pm} = \frac{5KH3}{15KH3} = 0.333$$

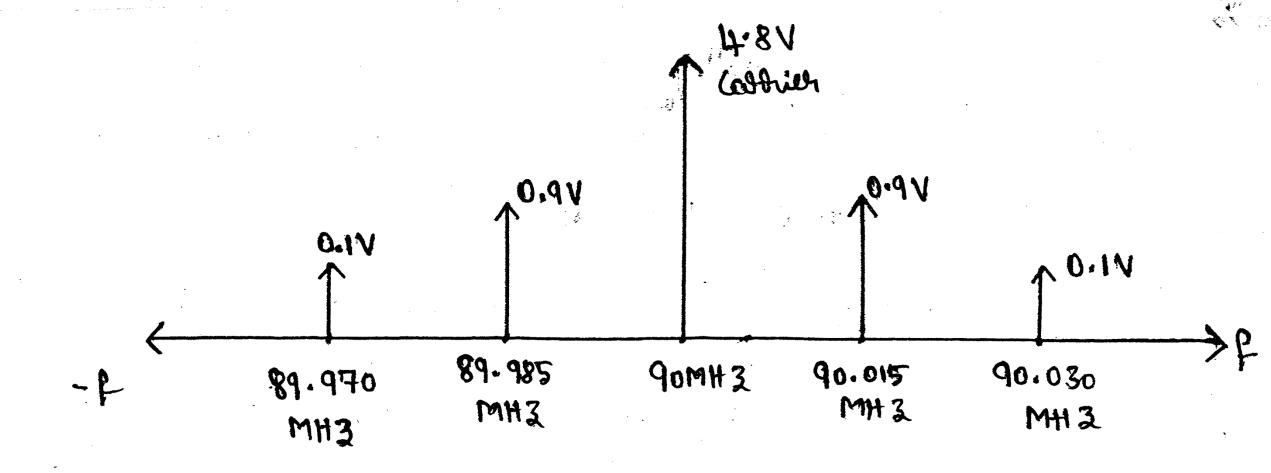
From the table of Bessel functions, for B=0.333 Use approximate values pt Jo, J, & Jg.

Higher Erder Side Arequencies dre negligible Since B is Small.

i) Amplitude Specthum of the Carrier: Ac To(B) = 5v x 0.96 = 4:8V Corrier Prequency Pc = 90MHZ ii) Amplitude Spectisum of the 1st Side Phegruency: AcT, (B) = 5x0.18 v=0.9 v 1st Side frequency: fetfm = 90MHz+15KHz=90.015
MHZ

Amplitude Specthum of the and Side Pheguency: Acta(B) = 5K0.002V = 0.1V

and Side Pheguency: fc+2fm = 90MH3+2(15KH3) = 90.030MH3



$$F_{c}-F_{m} = 90MH_{3}-15KH_{3}= 89.985MH_{3}$$
  
 $F_{c}-aF_{m} = 90MH_{3}-2(15KH_{3})=89.940MH_{3}$ 

A Corrier wave of amplitude 10V & frequency 10019472 is frequency modulated by a Sinubidal voltage. The modulating. voltage has an amplitude of 5V & frequency Rm = 20KH3. The Frequency devoiation Constant is 2KH3/V. Draw the frequency Spectourn of FM wave.

## NOTE:-

- > Castion Signal -> AcTo(B) Cos attet
- 3) 1st pain of Side Prequencies → Ac J, (3) Cosaπ (fc ± fm) ±
- 3) and pain of Side Phegruencies AcJa(B) Cosam(Pc+2Fm)+
- n) nth pair of Side frequencies -> Actn(B) Cosam(fc+nfm)+

\* From the table of Beyel functions, for B = 0.5 Use approximate values of J-coefficients one:

$$J_0 = 0.94$$
,  $J_1 = 0.24$ ,  $J_2 = 0.03$ 

Sol:- Given: 
$$A_c = 10V$$
,  $F_c = 100MHZ$ ,  $K_F = 2KHZ/V$ .  
 $A_m = 5V$ ,  $F_m = 20KHZ$ .

$$\frac{A}{A} = \frac{\Delta P}{Pm} = \frac{10 \text{ kHz}}{20 \text{ kHz}} = 0.5$$

\* From the table of Bessel functions, for B = 0.5Use approximate values of J-coefficients one:

$$J_0 = 0.94$$
,  $J_1 = 0.24$ ,  $J_2 = 0.03$ 

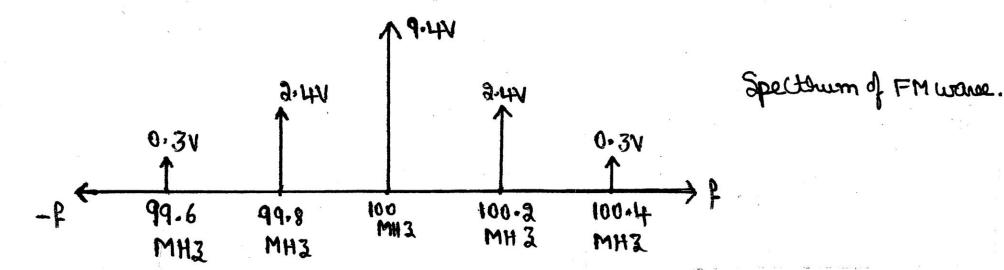
- \* The amplitude, Prequencier of the Costier & Sidebands are as
- Costies amplitude -> AcJ(B) = 10 VX 0.94 = 9.44 V Costies frequency -> 100 MHZ

ii) Farequency of 1st Sideband  $\rightarrow$  fc + fm = 100. 2mHz fc - fm = 99.8 mHz Amplitude of 1st Sideband  $\rightarrow$  AcJ<sub>1</sub>(B) = 10V x 0.24 = 2.44V

iii) Frequency of grd Sideband -> fc+2fm = 100.4MHZ

fc-2fm = 99.6MHZ

Amplitude of 3rd Sideband -> Ac Ja(B) = 10V × 0.03 = 0.3 V.



#### Problem 1

Consider the frequency multiplier of Fig. 4-4 and an NBFM signal

$$x_{\text{NBFM}}(t) = A \cos (\omega_c t + \beta \sin \omega_m t)$$

with  $\beta < 0.5$  and  $f_c = 200$  kHz. Let  $f_m$  range from 50 Hz to 15 kHz, and let the maximum frequency deviation  $\Delta f$  at the output be 75 kHz. Find the required frequency multiplication n and the maximum allowed frequency deviation at the input.

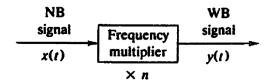


Fig. 4-4 Frequency multiplier

Solution: From Eq. (4.22),  $\beta = \Delta f/f_m$ . Thus,

$$\beta_{\min} = \frac{75(10^3)}{15(10^3)} = 5$$
  $\beta_{\max} = \frac{75(10^3)}{50} = 1500$ 

If  $\beta_1 = 0.5$ , where  $\beta_1$  is the input  $\beta$ , then the required frequency multiplication is

$$n = \frac{\beta_{\text{max}}}{\beta_1} = \frac{1500}{0.5} = 3000$$

The maximum allowed frequency deviation at the input, denoted  $\Delta f_1$ , is

$$\Delta f_1 = \frac{\Delta f}{n} = \frac{75(10^3)}{3000} = 25 \,\text{Hz}$$

# Problem 2

A block diagram of an indirect (Armstrong) FM transmitter is shown in Fig. 4-9. Compute the maximum frequency deviation  $\Delta f$  of the output of the FM transmitter and the carrier frequency  $f_c$  if  $f_1 = 200$  kHz,  $f_{LO} = 10.8$  MHz,  $\Delta f_1 = 25$  Hz,  $n_1 = 64$ , and  $n_2 = 48$ .

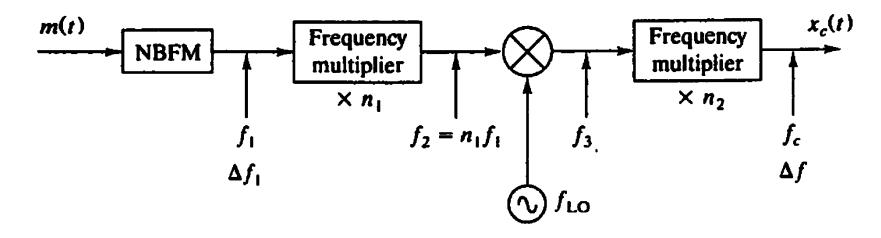


Fig. 4-9 Block diagram of an indirect FM transmitter

## Solution

$$\Delta f = (\Delta f_1)(n_1)(n_2) = (25)(64)(48) \text{Hz} = 76.8 \text{ kHz}$$

$$f_2 = n_1 f_1 = (64)(200)(10^3) = 12.8(10^6) \text{Hz} = 12.8 \text{ MHz}$$

$$f_3 = f_2 \pm f_{LO} = (12.8 \pm 10.8)(10^6) \text{Hz} = \begin{cases} 23.6 & \text{MHz} \\ 2.0 & \text{MHz} \end{cases}$$

Thus, when  $f_3 = 23.6 \,\mathrm{MHz}$ , then

$$f_c = n_2 f_3 = (48)(23.6) = 1132.8 \,\mathrm{MHz}$$

When  $f_3 = 2 \text{ MHz}$ , then

$$f_c = n_2 f_3 = (48)(2) = 96 \,\mathrm{MHz}$$

## Problem 3

In an Armstrong-type FM generator of Fig. 4-9 (Prob. 4.16), the crystal oscillator frequency is 200 kHz. The maximum phase deviation is limited to 0.2 to avoid distortion. Let  $f_m$  range from 50 Hz to 15 kHz. The carrier frequency at the output is 108 MHz, and the maximum frequency deviation is 75 kHz. Select multiplier and mixer oscillator frequencies.

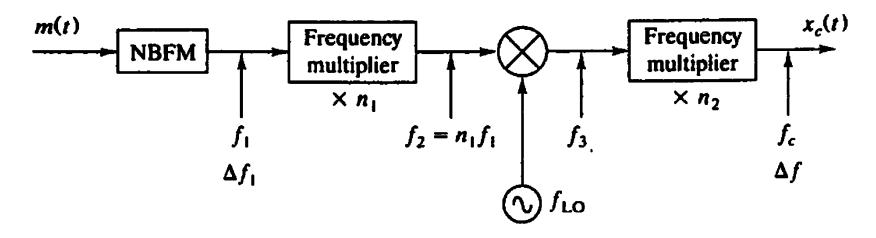


Fig. 4-9 Block diagram of an indirect FM transmitter

# Solution

$$\Delta f_1 = \beta f_m = (0.2) (50) = 10 \text{ Hz}$$

$$\frac{\Delta f}{\Delta f_1} = \frac{75(10^3)}{10} = 7500 = n_1 n_2$$

$$f_2 = n_1 f_1 = n_1 (2) (10^5) \text{ Hz}$$

Assuming down conversion, we have

$$f_2 - f_{LO} = \frac{f_c}{n_2}$$

Thus,

$$f_{LO} = n_1 f_1 - \frac{f_c}{n_2} = \frac{7500(2)(10^5) - 108(10^6)}{n_2} = \frac{1392}{n_2} (10^6) \text{ Hz}$$

Letting  $n_2 = 150$ , we obtain

$$n_1 = 50$$
 and  $f_{LO} = 9.28 \,\text{MHz}$ 

#### Problem 4

Design an Armstrong indirect FM modulator to generate an FM carrier with a carrier frequency of 96 MHz and  $\Delta f = 20$  kHz. A narrowband FM generator with  $f_c = 200$  kHz and adjustable  $\Delta f$  in the range of 9 to 10 Hz is available. We also have an oscillator with adjustable frequency in the range of 9 to 10 MHz and there is a bandpass filter with any centre frequency and only frequency doublers are available.

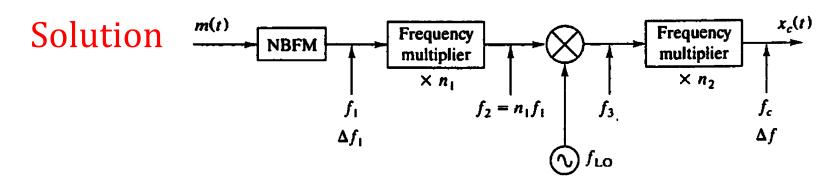


Fig. 4-9 Block diagram of an indirect FM transmitter

$$9 < \Delta f_1 < 10$$
 W. K. T  $\Delta f = n_1 n_2 \Delta f_1$   
 $9 < \frac{20000}{n_1 n_2} < 10$   $\Delta f = 20 \text{ kHz}$ 

Since only doublers are available, therefore  $n_1 n_2$  has to be power of 2.

By trail and error,  $n_1 n_2 = 2018$ 

Hence,  $n_1 = 64$ ,  $n_2 = 32$ 

The output of the first multiplier is  $64 \times 200 \text{ kHz} = 12.8 \text{ MHz}$ 

Input to the second multiplier has to be  $\frac{96 \times 10^6}{32} = 3MHz$ 

The local oscillator frequency = 12.8 - 3 = 9.8 MHz which is in the given range.

Modulation index	Sideband amplitude																
	Carrier	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
0.00	1.00																
0.25	0.98	0.12															
0.5	0.94	0.24	0.03														
1.0	0.77	0.44	0.11	0.02													
1.5	0.51	0.56	0.23	0.06	0.01												
2.0	0.22	0.58	0.35	0.13	0.03												
2.41	0	0.52	0.43	0.20	0.06	0.02											
2.5	-0.05	0.50	0.45	0.22	0.07	0.02	0.01										
3.0	-0.26	0.34	0.49	0.31	0.13	0.04	0.01										
4.0	-0.40	-0.07	0.36	0.43	0.28	0.13	0.05	0.02									
5.0	-0.18	-0.33	0.05	0.36	0.39	0.26	0.13	0.05	0.02								
5.53	0	-0.34	-0.13	0.25	0.40	0.32	0.19	0.09	0.03	0.01							
6.0	0.15	-0.28	-0.24	0.11	0.36	0.36	0.25	0.13	0.06	0.02							
7.0	0.30	0.00	-0.30	-0.17	0.16	0.35	0.34	0.23	0.13	0.06	0.02						
8.0	0.17	0.23	-0.11	-0.29	-0.10	0.19	0.34	0.32	0.22	0.13	0.06	0.03					
8.65	0	0.27	0.06	-0.24	-0.23	0.03	0.26	0.34	0.28	0.18	0.10	0.05	0.02				
9.0	-0.09	0.25	0.14	-0.18	-0.27	-0.06	0.20	0.33	0.31	0.21	0.12	0.06	0.03	0.01			
10.0	-0.25	0.04	0.25	0.06	-0.22	-0.23	-0.01	0.22	0.32	0.29	0.21	0.12	0.06	0.03	0.01		
12.0	0.05	-0.22	-0.08	0.20	0.18	-0.07	-0.24	-0.17	0.05	0.23	0.30	0.27	0.20	0.12	0.07	0.03	0.01