

Chapter 14: Sedimentation Velocity

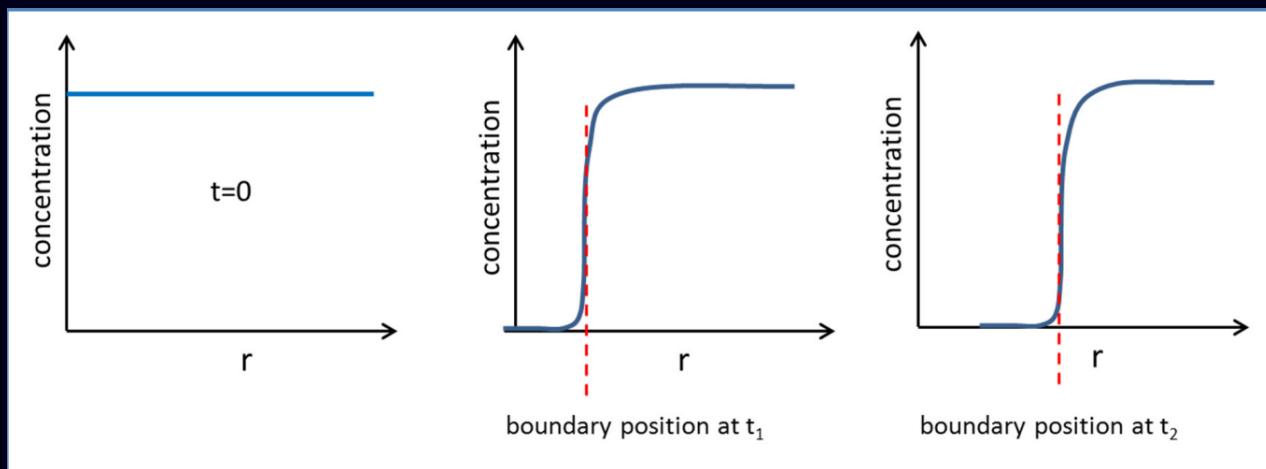
The external force (on a per molecule basis) due to centrifugation is $m\phi\omega^2r$, where ϕ is the **density increment**, ω is the **angular velocity**, m is the **mass**, and r is the **radius**. The **opposing frictional force** is $-fv$. When setting the sum of these forces to zero (terminal velocity), the equation yields:

$$V = \frac{m\phi\omega^2r}{f} \quad (1)$$

or, on a per mole basis:

$$V = \frac{M\phi\omega^2r}{N_A f} \quad (2)$$

How do you visualize velocity v in a velocity sedimentation experiment? If the sample begins with the macromolecule uniformly distributed (concentration is equal everywhere in tube), then when centrifugation begins, the **top region** (low r) of the sample will lose its macromolecules.



The sedimentation velocity v is the speed of the boundary: $\frac{\Delta r}{\Delta t}$

Meaning and Measurement of Sedimentation Coefficient, s

How does the sedimentation velocity v relate to molecular properties? From the equation $V = \frac{M\phi\omega^2 r}{N_A f}$, v is affected by both molecular properties (M) and experimental parameters (ω). We want to separate the two kinds of variables on different sides of the equation:

$$\frac{v}{\omega^2 r} = \frac{m\phi}{f} \quad (3)$$

Now, introduce **sedimentation coefficient** s to be equal to those quantities. s is obtained experimentally using $s = \frac{v}{\omega^2 r}$ s is obtained using molecular properties through:

$$s = \frac{M\phi}{N_A f} \quad \text{or} \quad s = \frac{m\phi}{f} \quad (4)$$

If angular velocity $\omega \uparrow$, then the sedimentation velocity $v \uparrow$ from eq. (1). But the sedimentation coefficient s is unaffected. We know this is true because from **equation 4**, we can relate s to molecular properties without reference to experimental parameters.

Since v is defined as $\frac{dr}{dt}$ we can determine that:

$$s = \frac{\frac{dr}{dt}}{\omega^2 r} = \frac{\frac{d \ln(r)}{dt}}{\omega^2} \quad (5)$$

Measuring the position r of the boundary at a series of time points during the experiment and plotting them as **$\ln(\text{boundary position})$ vs. t** should give a straight line with slope $s\omega^2$, which can be used to find s .

A special unit is used to express the value of the sedimentation coefficient (natural units are seconds). The **Svedberg**, S is defined as 10^{-13} sec.

Relating s to molecular properties

The sedimentation coefficient relates to molecular properties in two ways:

- dependence on mass
- frictional coefficient f (which depends on size \rightarrow mass)

Starting with $s = \frac{m\phi}{f}$, where $f = 6\pi\eta R \rightarrow s = \frac{m\phi}{6\pi\eta R}$

But R relates to volume and mass according to $V = \frac{4}{3}\pi R^3 \rightarrow R = \left(\frac{3V}{4\pi}\right)^{\frac{1}{3}}$

Relate volume V to mass m by the density $\rightarrow m = V\rho$ and substitute V for $\frac{m}{\rho}$

$$s = \frac{m\phi}{6\pi\eta\left(\frac{3m}{4\pi\rho}\right)^{\frac{1}{3}}}$$

$$s = m^{\frac{2}{3}}\left(\frac{\phi}{6\pi\eta}\right)\left(\frac{4\pi\rho}{3}\right)^{\frac{1}{3}} \text{ or } s = \left(\frac{M}{N_A}\right)^{\frac{2}{3}}\left(\frac{\phi}{6\pi\eta}\right)\left(\frac{4\pi\rho}{3}\right)^{\frac{1}{3}}$$

Do larger molecules sediment move faster or slower than small molecules of equal density and similar shape? Centrifugal force on an object is proportional to mass, but opposing force is only $\frac{1}{3}$ power of the mass.

So larger molecules move faster, according to $\frac{2}{3}$ power of their mass.

This assumes that the protein or molecule is nearly spherical since we used Stoke's Equation. If the molecule of interest is **non-spherical**, then it will have the same centrifugal force but \uparrow frictional force $\rightarrow \downarrow$ sedimentation coefficient s . This will result in a lower estimation for molecular weight.

Combining s and D (diffusion coefficient) to get molecular weight without a spherical assumption

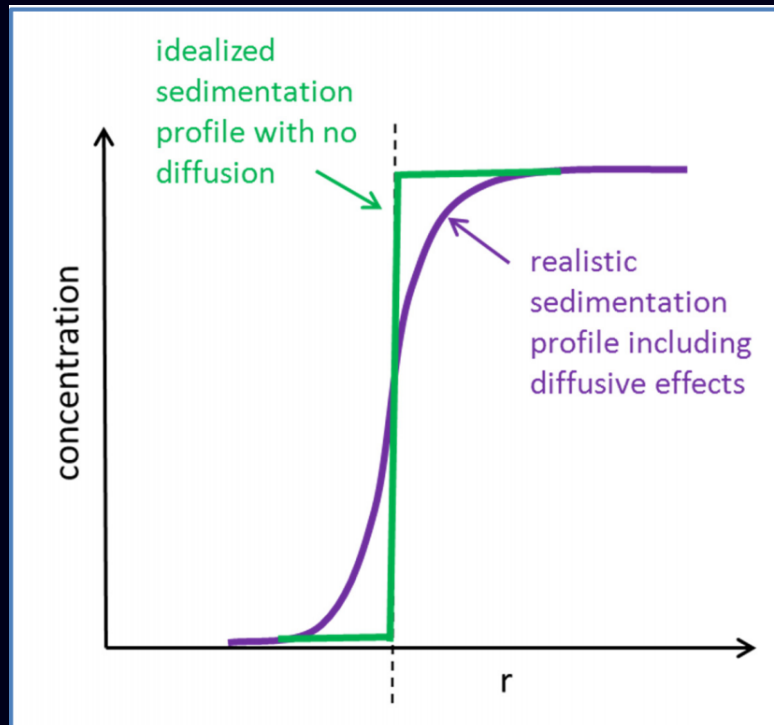
We can eliminate the assumption of spherical shape if we have measured values for s and D together. Having both values cancels frictional coefficient out. We know that $f = \frac{K_B T}{D}$ and from equation (4), $f = \frac{M\phi}{N_A s}$ If we equate the two together:

$$f = \frac{K_B T}{D} = \frac{M\phi}{N_A s}$$

$$M = \left(\frac{RT}{\phi}\right)\left(\frac{s}{D}\right)$$

Molecular weight relates only to the ratio of s to D , shape is no longer considered (frictional coefficient).

The diffusion coefficient D can be obtained from the sedimentation experiment itself. Under ideal conditions without diffusion, the concentration profile at the boundary would be perfectly steep. At a position just before the boundary layer, there will be no macromolecules. Right at the boundary layer, there will be a concentration of macromolecules that is the same all throughout the tube after that layer.



Chapter 15: Chemical Reaction Kinetics

Reaction Velocity, v

If we consider a reaction to be reactants \rightarrow products, then reaction velocity v is the frequency ($\#/\text{time}$) with which the event is occurring per unit volume. The units of v are $\frac{\#}{\text{volume} \times \text{time}}$ or M/sec. There is only one velocity associated with the reaction, even though multiple reactants and products may be involved.

The reaction velocity is indicated equally by the rate of change of **any** of the species involved:



$$\begin{aligned} \frac{-d[A]}{dt} &= \alpha v \\ \frac{-d[B]}{dt} &= \beta v \\ \frac{-d[C]}{dt} &= \gamma v \\ \frac{-d[D]}{dt} &= \delta v \end{aligned}$$

Rearranging to isolate velocity v gives

$$v = -\left(\frac{1}{\alpha}\right)\left(\frac{d[A]}{dt}\right) = \left(\frac{1}{\beta}\right)\left(\frac{d[B]}{dt}\right) = \left(\frac{1}{\gamma}\right)\left(\frac{d[C]}{dt}\right) = \left(\frac{1}{\delta}\right)\left(\frac{d[D]}{dt}\right) = \cdots$$

Evidently, if we measure the rate of change of concentration of some species, then we measured reaction velocity v .

Rate laws: how v depends on concentrations

Velocity of a reaction depends on how concentrated the reactants are. Besides concentration, different reactions (different chemical species) will have different v according to likelihood of underlying chemical events $\rightarrow k$

Combined dependence of v on rate constant k and concentrations \rightarrow **rate law**.

Consider the equation: $A \xrightarrow{k} B$

The rate law is $v = k[A]$, this reaction is first order in A.

Now consider $2A \xrightarrow{k} B \Rightarrow v = k[A]^2$, and the reaction is second order in A.

If the equation is now $A + B \xrightarrow{k} C$, the rate law is now $v = k[A][B]$.

Relationship of rate constants to equilibrium constants

What about if we had reversible processes? Velocities of forward and reverse reactions depend on the concentrations of reactants and products, respectively. When the concentrations are reached where forward and reverse reactions are equal, no **net** conversion is occurring. This is **chemical equilibrium**. Consider the reaction:



The **forward** reaction velocity is $v = k_1[A]^2$

The **reverse** reaction velocity is $v = k_{-1}[B]^2$

At **equilibrium**, $k_1[A]^2 = k_{-1}[B]^2$ and $\frac{k_1}{k_{-1}} = \frac{[B]}{[A]^2}$

The ratio of the rate constants is equal to the equilibrium constant K.

Integrating Rate Laws

For simple reactions, we can integrate the differential equations that come from rate law to describe how concentrations of reactants and products change over time

1st Order Decay



To get a differential equation in terms of $[A]$, combine two points:

- First need $v = \frac{-d[A]}{dt}$
- Also need $v = k[A]$

If we equate them together, we get the following:

$$\frac{-d[A]}{dt} = k[A]$$

$$\int \frac{d[A]}{[A]} = -k \int dt$$

$$\ln[A] \Big|_{[A]_0}^{[A]} = -kt \Big|_0^t$$

This gives us the familiar first order decay equations

$$\ln\left(\frac{[A]}{[A]_0}\right) = -kt \quad (8)$$

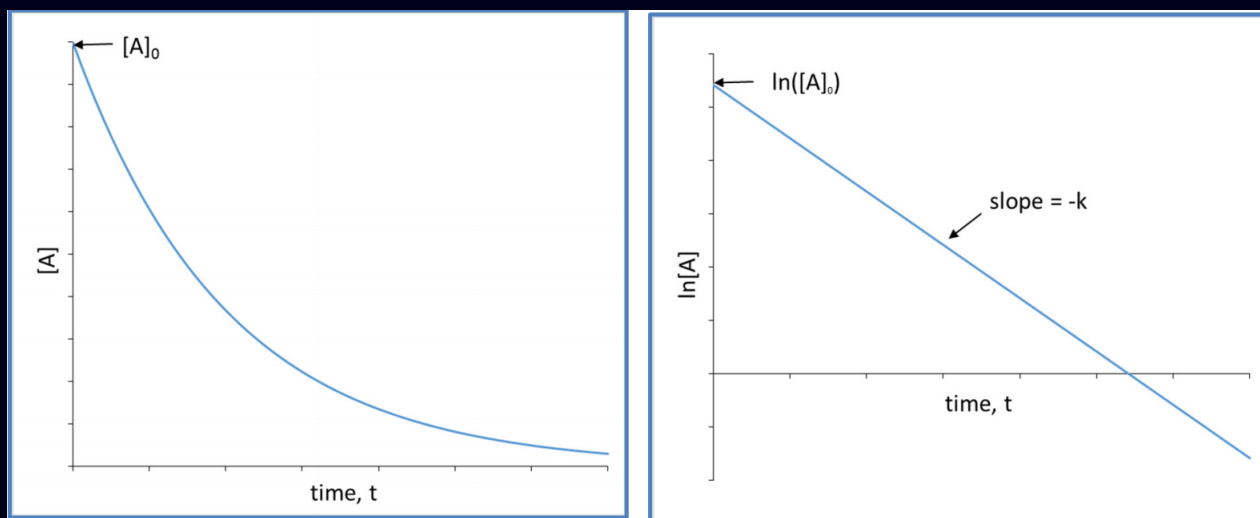


Figure 1: Behavior of $[A]$ over time is exponential, while $\ln[A]$ is linear, with slope $\rightarrow k$

Describing decay times for 1st order decay

Time scale of first order decay is described in terms of half-life, $t_{1/2}$, which is the time required for a reaction to reach 50% completion. Parameter τ is used to describe decay times. It gives the time required for a reaction to reach $\frac{1}{e}$ completion compared to initial condition: $\frac{[A]}{[A]_0} = \frac{1}{e}$

We can connect $t_{1/2}$ and τ with the following comparison:

$$\ln\left(\frac{1}{2}\right) = -kt_{\frac{1}{2}} \text{ to } \ln\left(\frac{1}{e}\right) = -1 = -k\tau \quad (9)$$

This will give:

$$t_{\frac{1}{2}} = \ln(2)\tau \quad (10)$$

For the simple first order decay reaction of [A]

$$t_{\frac{1}{2}} = \frac{\ln(2)}{k} \text{ and } \tau = \frac{1}{k}$$

Integrated rate law for a 2nd order irreversible reaction



Repeat the same process as above to get:

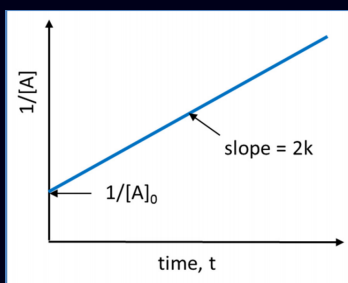
$$\frac{-d[A]}{dt} = 2k[A]^2$$

$$\int \frac{d[A]}{[A]^2} = -2k \int dt$$

$$-\frac{1}{[A]} \Big|_{[A]_0}^{[A]} = -2kt \Big|_0^t$$

$$\frac{1}{[A]} - \frac{1}{[A]_0} = 2kt$$

A plot of $\frac{1}{[A]}$ vs. time gives a straight line, where slope = k



Establishing a rate law from measured reaction velocities

A different way of experimentally examining a rate law is by evaluating the dependence of reaction velocity on concentrations.

If a reaction is **first order** in $[A]$, then v will depend linearly on $[A]$. If $[A]$ doubles, then v will also double.

If a reaction is **second order** in $[A]$, then doubling $[A]$ will quadruple the reaction velocity.

In general:

$$v = [A]^\alpha \quad (11)$$

Then for rate measurements made at two different concentrations:

$$\ln\left(\frac{v_2}{v_1}\right) = \alpha \ln\left(\frac{[A]_2}{[A]_1}\right) \quad (12)$$

Behavior of more complex reaction schemes

Now, we want to consider events that are more complex than one step reactions. Consider the following example:

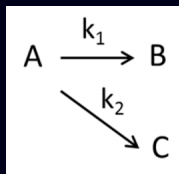
This gives the following equations:

$$\frac{d[A]}{dt} = -k_1[A]$$

$$\frac{d[B]}{dt} = k_1[A] - k_2[B]$$

$$\frac{d[C]}{dt} = k_2[B]$$

For another example:



The change in concentration as a function of time is given as:

$$\frac{d[A]}{dt} = -k_1[A] - k_2[A] = -(k_1 + k_2)[A]$$

$$\frac{d[B]}{dt} = k_1[A]$$

$$\frac{d[C]}{dt} = k_2[A]$$

Steady state assumptions for obtaining simple rate laws for complex reactions

For complex reactions, dependence of the rate of the overall reaction (rate law) can depend on concentrations of species that do not contribute to the reaction itself.

When sequential reactions are involved, simplified rate laws can be obtained by assuming steady state conditions.

Steady state is when the intermediate species (that do not contribute to overall reaction stoichiometry) concentrations have reached constant value, at least momentarily.

$$\frac{d[Intermediate]}{dt} = 0$$

Consider the following equation:



In this equation, the intermediate is B, and the overall reaction stoichiometry is $A \longrightarrow C$. Based on equation 13, we can then state that:

$$\begin{aligned}
 \frac{d[B]}{dt} &= k_1[A] - k_{-1}[B] - k_2[B] \\
 &= k_1[A] - [B](k_{-1} + k_2) = 0
 \end{aligned}$$

Now rearrange to isolate $[B]$:

$$[B] = \frac{k_1[A]}{k_2 + k_1} \quad (14)$$

Now go back to the original reaction scheme. The overall reaction velocity is $v = \frac{d[C]}{dt}$, but we know that $\frac{d[C]}{dt} = k_2[B]$. Substituting $[B]$ from equation 14 shows that:

$$v = \frac{k_1 k_2 [A]}{k_2 + k_1} \quad (15)$$

From the equation 15 above, this 2-step reaction behaves as first order in $[A]$ at steady state.

Enzyme Kinetics under a steady-state assumption

The following model is used to treat kinetics of a simple unimolecular enzyme reaction:



E is the free enzyme, S is the free/unbound substrate, ES is the enzyme-substrate complex, and P is the product. $\frac{k_1}{k_{-1}}$ describes how tightly the enzyme binds the substrate. k_{cat} describes the catalytic rate constant for formation of P .

The velocity of the overall reaction is described by $v = \frac{d[P]}{dt}$. According to the rate law, $v = k_{cat}[ES]$. $[ES]$ is an intermediate, and so we need to replace $[ES]$ by adopting steady state assumption (where $\frac{d[ES]}{dt} = 0$).

$$\frac{d[ES]}{dt} = k_1[E][S] - (k_{-1} + k_{cat})[ES] = 0$$

$$[ES] = \frac{k_1[E][S]}{k_{-1} + k_{cat}}$$

Now plug in $[ES]$ from above into $v = k_{cat}[ES]$:

$$v = \frac{k_{cat} k_1 [E][S]}{k_{-1} + k_{cat}} \quad (17)$$

This equation is a start, but it only describes the reaction velocity in terms of the free enzyme concentration. In an experiment, we usually only have control over the total enzyme concentration. We want to rewrite the equation in terms of total enzyme concentration and in terms of the ratio of the reaction velocity to the maximum possible value ($[ES] = [E]_{total}$). The maximum velocity is $k_{cat} \times \text{max value for } [ES]$, which is:

$$v_{max} = k_{cat}[E]_{total} = k_{cat}([ES] + [E]) \quad (18)$$

The ratio of reaction velocities relative to its maximum is given:

$$\frac{v}{V_{max}} = \frac{k_{cat}[ES]}{k_{cat}([E] + [ES])}$$

$$\frac{v}{V_{max}} = \frac{[ES]}{([ES] + [E])}$$

$$\frac{v}{V_{max}} = \frac{1}{1 + \frac{[E]}{[ES]}}$$

Taking the previous equation $[ES] = \frac{k_1[E][S]}{k_{-1} + k_{cat}}$ and rearranging so that it becomes $\frac{[E]}{[ES]} = \frac{k_{-1} + k_{cat}}{k_1[S]}$, substitute this equation above to give:

$$\frac{v}{V_{max}} = \frac{1}{1 + \frac{k_{-1} + k_{cat}}{k_1[S]}}$$

$$\frac{v}{V_{max}} = \frac{[S]}{[S] + \frac{k_{-1} + k_{cat}}{k_1}}$$

$$\frac{v}{V_{max}} = \frac{[S]}{[S] + K_M} \longrightarrow K_M = \frac{k_{-1} + k_{cat}}{k_1}$$

Or, we can also convert from fractional velocity to v using equation 18 for V_{max} :

$$v = \frac{k_{cat}[E]_{total}[S]}{[S] + K_M} \quad (19)$$

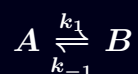
Relaxation kinetics: how systems approach equilibrium

The T-Jump Method

The temperature jump method was developed to study fast reactions and their "relaxation" back towards equilibrium. If energy is rapidly delivered to a solution containing reactant and product at equilibrium, the temperature of the system can be heated nearly instantaneously. Recalling the **van't Hoff equation**, if ΔH for the reaction is non-zero, then the equilibrium constant will be different at a new temperature. Then you can observe how fast the reaction returns to its new equilibrium.

The speed at which equilibrium is achieved depends on the forward and backward rate constants of the reaction.

Consider a simple system:



Let x be the distance of each species from equilibrium. \bar{A} will be $[A]_{equilibrium}$ at the new temperature, same for \bar{B} . The concentrations of A and B are related to the equilibrium conc. by:

$$\begin{aligned}[A] &= \bar{A} + x \\ [B] &= \bar{B} - x\end{aligned}$$

Now examine the approach to equilibrium by writing an equation for time dependence of x .

$$\frac{d[A]}{dt} = \frac{d[\bar{A} + x]}{dt} = \frac{dx}{dt}$$

$$\frac{d[A]}{dt} = -k_1[A] + k_{-1}[B]$$

$$\begin{aligned}\frac{d[A]}{dt} &= -k_1[\bar{A} + x] + k_{-1}[\bar{B} - x] \\ &= k_{-1}\bar{B} - k_{-1}\bar{A} - x(k_1 + k_{-1})\end{aligned}$$

The term $k_{-1}\bar{B} - k_{-1}\bar{A} = 0$ because $\frac{\bar{B}}{\bar{A}} = K = \frac{k_1}{k_{-1}}$

So, after setting the above to 0, the equation yields:

$$\frac{dx}{dt} = -(k_1 + k_{-1})x \quad (20)$$

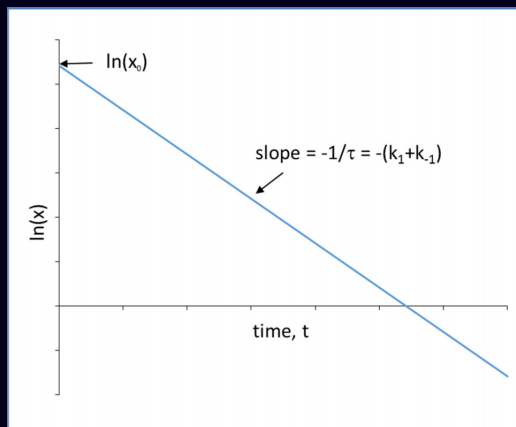
X follows first order kinetics. Skipping the familiar details for handling a first order differential equation:

$$x = x_o^{-(k_1+k_{-1})} \text{ and } \ln\left(\frac{x}{x_o}\right) = -(k_1 + k_{-1})t \quad (21)$$

Convert these to even more general forms:

$$x = x_o e^{\frac{-t}{\tau}} \text{ and } \ln\left(\frac{x}{x_o}\right) = \frac{-t}{\tau} \quad (22)$$

where $\tau = \frac{1}{k_1+k_{-1}}$



If you can find $[A]$ or $[B]$ as a function of time, then you can also find x as a function of time.

$$x = [A] - \bar{A} = \bar{B} - [B]$$

You can use this to measure τ , and thus also $k_1 + k_{-1}$

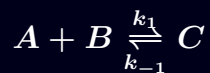
$$1/\tau = k_1 + k_{-1} \text{ and } k_1 = Kk_{-1}$$

$$1/\tau = Kk_{-1} + k_{-1} = (K + 1)k_{-1}$$

$$k_{-1} = \frac{1}{\tau(K + 1)} \text{ and } k_1 = \frac{K}{\tau(K + 1)}$$

Higher Order Reactions Approaching Equilibrium

Now consider this second order reversible reaction:



There is only one transformation, so the distance can still be described by x :

$$[A] = \bar{A} + x$$

$$[B] = \bar{B} + x$$

$$[C] = \bar{C} - x$$

We can use the same approach from the above to describe the change in concentrations:

$$\frac{d[A]}{dt} = \frac{d\bar{A} + x}{dt} = \frac{dx}{dt}$$

$$\frac{d[A]}{dt} = -k_1(\bar{A} + x)(\bar{B} + x) + k_{-1}(\bar{C} - x)$$

$$= k_{-1}\bar{C} - k_1\bar{A}\bar{B} - x(k_1(\bar{A} + \bar{B}) + k_{-1}) - k_1x^2$$

$k_{-1}\bar{C} - k_1\bar{A}\bar{B}$ cancels to 0, and if we are close enough to equilibrium then x is small, so we can neglect the x^2 term. So,

$$\frac{dx}{dt} = -(k_1(\bar{A} + \bar{B}) + k_{-1})x \quad (23)$$

So, the distance from equilibrium x shows first order behavior close to equilibrium, with $\tau = \frac{1}{k_1(\bar{A} + \bar{B}) + k_{-1}}$

Kinetics from Single Molecule Studies

For a unimolecular event, we can get a sense for the rate constant by looking at how long the molecule persists in its current state before undergoing a reaction.

Think of this as the "waiting time" before a reaction or conformational change occurs. While reactions are random, the average waiting time should be shorter for a process with a higher rate constant.

Consider $A \longrightarrow B$ with rate constant k .

How long before any molecule A turns into B? Treat the reaction in bulk:

$$\frac{A}{A_0} = e^{\frac{-t}{\tau}} \text{ where } \tau = \frac{1}{k} \quad (24)$$

$\frac{A}{A_0}$ can be considered the probability that any molecule A will **not** convert at time t .

The probability that molecule A reacts precisely at time t is $P(A)_{\text{react}} = \frac{1}{\tau} e^{\frac{-t}{\tau}}$.

To get the average time at which a molecule of A reacts (aka waiting time), we need to get the average value of t by weighting all possible values of t by probability of reaction at time t .

To do this, multiply t by the probability of reaction at time t , then integrate from $t = 0$ to infinity.

$$\text{waiting time} = \int_{t=0}^{t=\infty} \left(t \left(\frac{1}{\tau} \right) e^{\frac{-t}{\tau}} \right) dt \quad (25)$$

If we can measure how long it takes a single molecule to undergo a transition, then we have measured τ .

Chapter 16: Kinetic Theories and Enzyme Catalysis

Now we want to look at what determines the rate constant, k . What makes some reactions innately fast or slow? There are two main models that try to explain the mechanisms of chemical reactions and their rate constants.

The Arrhenius Equation

This is often used to discuss reaction rates in terms of **molecular collisions**. The rate constant k is determined by:

$$k = Ae^{-\frac{E_a}{RT}} \quad (26)$$

A is the **frequency factor** and E_a is an **activation energy**. We already know that the frequency of collisions in a reaction is dependent on concentrations. The frequency factor in the equation for k accounts for other phenomena ie. the dependence of molecular velocities and consequently collision rates on temperature, and the dependence of reaction probability on the orientation of the colliding molecules.

E_a describes a lower bound for energy that reactants must have for reaction to occur. Why does E_a enter the equation for k as an exponential term? **Boltzmann Distribution!**

If $N(E) \propto e^{-\frac{E}{RT}}$, then we can find the fraction of molecules having energy at least as high as E_a by **taking the ratio of area that falls under the curve and has $E \geq E_a$ divided by entire area under the curve.**

$$\frac{\int_{E_a}^{\infty} e^{-\frac{E}{RT}}}{\int_0^{\infty} e^{-\frac{E}{RT}}} = \frac{-RT e^{-\frac{E}{RT}} \Big|_{E_a}^{\infty}}{-RT e^{-\frac{E}{RT}} \Big|_0^{\infty}}$$

$$\frac{e^{-\frac{E_a}{RT}}}{1} = e^{-\frac{E_a}{RT}}$$

A key element of Arrhenius equation: **the rate constant depends strongly on the height of an energy barrier**. It also depends on the temperature.

The dependence of k on T can be used to evaluate the activation energy in the Arrhenius model.

$$\frac{d(\ln(k))}{dt} \cong \frac{d(\frac{-E_a}{RT})}{dT} = \frac{E_a}{RT^2}$$

or

$$\begin{aligned} \frac{d(\ln(k))}{d(\frac{1}{T})} &\cong \frac{d(\frac{-E_a}{RT})}{d(\frac{1}{T})} = \frac{d(\frac{-E_a}{RT})}{-\frac{dT}{T^2}} \\ &= \frac{-E_a}{RT^2} = \frac{-E_a}{R} \end{aligned}$$

Eyring Transition State Theory

This method provides a slightly different way of looking at things that are more explicit about the occurrence of high energy species during a single reaction event. A single reaction step:



is broken down in terms of two steps.

- First step: unstable high energy species (the transition state)
- Second step: the transition breaks down to product.

The double-dagger symbol indicates the **transition state**.



The rate constant for breakdown of transition state is approximately the frequency of molecular vibrations, which is on the order of $\frac{k_B T}{h}$, where h is **Planck's Constant**

$$k_{breakdown} = \frac{k_B T}{h} \text{ and } v = \frac{d[C]}{dt} = k_{breakdown}[AB^{\ddagger}] \quad (28)$$

Then, the velocity of the reaction scheme above is:

$$v = \frac{d[C]}{dt} = \frac{k_B T}{h}[AB^{\ddagger}] \quad (29)$$

If we assume that the first step (formation of the transition state) is at equilibrium, then $\frac{k_{+‡}}{k_{-‡}} = K_{‡} = \frac{[AB‡]}{[A][B]}$, so, $[AB‡] = K_{‡} [A][B]$. If we substitute this value, then the reaction velocity would be $v = \frac{k_B T}{h} K_{‡} [A][B]$

Match this up to the simple rate law we would write for a single elementary reaction $\rightarrow v = k[A][B]$. The Eyring Model gives:

$$k = \frac{k_B T}{h} K_{‡}$$

The rate constant k is largely dependent on the equilibrium constant $K_{‡}$ for forming the transition state. We can also write $K_{‡}$ in terms of free energy for reaching the transition state:

$$K_{‡} = e^{\frac{-\Delta G}{RT}}$$

Substituting this gives us the equation:

$$k = \frac{k_B T}{h} e^{\frac{-\Delta G}{RT}} \quad (30)$$

While this is different than the **Arrhenius Equation**, it is similar in that it shows the exponential dependence on an energy barrier.

We can also look at the temperature difference of $\ln(k)$ for the Eyring equation like we did for the Arrhenius:

$$\begin{aligned} \frac{d \ln(k)}{dT} &\cong \frac{d(\frac{-\Delta G_{‡}}{RT})}{dT} \\ &= \frac{d(\frac{-\Delta H_{‡}}{RT} + \frac{\Delta S}{R})}{dT} \\ &= \frac{\Delta H_{‡}}{RT^2} \end{aligned}$$

The activation energy in the Arrhenius Equation relates closely to the transition state enthalpy in the Eyring model.

Catalysis by lowering the transition state energy

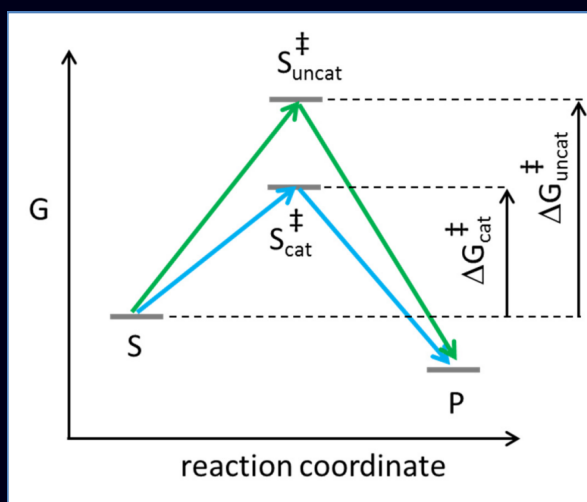
The Eyring transition state model provides a way to look at catalysis in terms of transition state energies.

Let the rate constant for the uncatalyzed reaction = k_{uncat} , and the rate constant for catalyzed reaction = k_{cat} . Using the **Eyring equation** for the rate constant, we can write out the ratio of two rate constants:

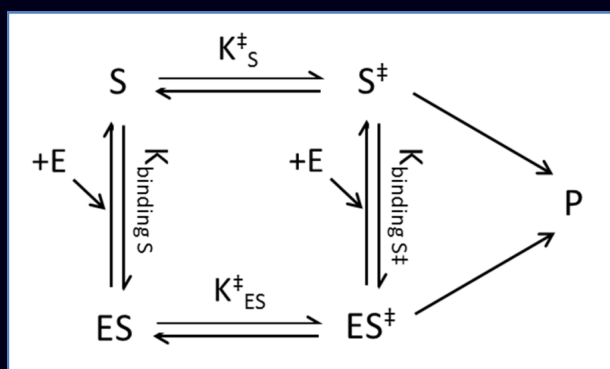
$$\begin{aligned}\frac{k_{cat}}{k_{uncat}} &= \frac{\frac{k_B T}{h} K_{\ddagger cat}^\ddagger}{\frac{k_B T}{h} K_{\ddagger uncat}^\ddagger} \\&= \frac{K_{\ddagger cat}^\ddagger}{K_{\ddagger uncat}^\ddagger} \\&= \frac{e^{-\frac{\Delta G_{\ddagger cat}^\ddagger}{RT}}}{e^{-\frac{\Delta G_{\ddagger uncat}^\ddagger}{RT}}} \\&= e^{\frac{-(\Delta G_{\ddagger cat}^\ddagger - \Delta G_{\ddagger uncat}^\ddagger)}{RT}}\end{aligned}$$

If a catalyst lowers the transition state energy for a reaction by an energy that amounts to $10RT$, then the reaction will be sped up by a factor of $e^{10} \rightarrow 22,000$.

How is it that a catalyst lowers the transition state energy of a reaction?



The surface configuration of the enzyme is complimentary to the unstable molecule with only transient existence (intermediate state), or the "activated complex" for the reaction that is catalyzed by that reaction. The enzyme would show attraction for the substrate, which would become attached to it in its active surface region. The substrate would be strained, and typically deform into the configuration of the activated complex. The activated complex then reassumes the original configuration or turns into the product.



We can relate the binding events in the presence of an enzyme to the formation of the transition state. The reactions on the **top** describe the reaction in the **absence** of the enzyme. The reactions on the bottom describe reaction with enzyme. The ratio between the rate constants with and without enzymes is:

$$\frac{k_{cat}}{k_{uncat}} = \frac{K_{ES}^{\ddagger}}{K_S^{\ddagger}}$$

By providing a binding surface that is complimentary to the transition state form for substrate, the equilibrium constant for reaching the transition state is increased by mass action → reaction is sped up.

The ratio for how much a reaction is sped up is:

$$\frac{k_{cat}}{k_{uncat}} = \frac{K_{ES}^{\ddagger}}{K_S^{\ddagger}} = \frac{K_{bindingS^{\ddagger}}}{K_{bindingS}}$$

By this equation: the enzyme speeds up its reaction by binding exceptionally tightly to the transition state form of the substrate. This is what lowers the free energy of the transition state.

Practical Consequences of Enzymes Binding Tightly to the Transition State

Transition state analogues as enzyme inhibitors

If an enzyme speeds up a reaction by a factor of 1000, then by the math above, the enzyme binds the transition state form of the substrate (S^\ddagger) more tightly than it binds the substrate.

A drug molecule that looks like the S^\ddagger will bind tightly to the enzyme and thus act as an inhibitor. The main challenge is that the transition state is unstable. The main goal is to find a compound that looks as similar to the transition state, but is still stable.

Creating new enzymes from a natural antibody repertoire

The goal was to create novel enzymes that would catalyze useful chemical types of reactions that no natural enzymes had evolved to carry out.

If you can find an antibody sequence with a high affinity for the transition state of a desirable reaction, then you have found an enzyme for that reaction.

Computational Enzyme Design

Instead of designing a novel protein from scratch, take a natural protein that has a surface cleft suitable for binding a compound of about the right size. Then modify the amino acid sequence mainly within the binding site cleft. No need to create transition state analogs, and instead only requires an accurate model for what the transition state is likely to look like. Computer programs can then design reasonable models of transition states.

The most challenging part is designing amino acid changes into a protein so that the TS is tightly bound. One issue concerns the calculation of free energies for large systems like proteins and their complexes.

Changing amino acid sequences can also cause loss of stability and aggregation, or make alternate (non-native) configurations more stable than the intended structure.

Kinetic Parameters of Natural Enzymes

Part of the complexity concerns the saturation behavior of enzyme kinetics.

$$v = \frac{[E_{total}]k_{cat}[S]}{[S] + K_M}$$

An enzyme that has a high k_{cat} may not be great if it does not bind substrate well (i.e. if K_M is high). The best conditions is to have **high** k_{cat} and **low** K_M .

The ratio of $\frac{k_{cat}}{K_M}$ is considered the general measure of efficiency of an enzyme. k_{cat} is the maximum velocity at any substrate concentration. $\frac{k_{cat}}{K_M}$ is the slope of the velocity curve in its linear region well below saturation. We are evaluating the standard Michaelis-Menten velocity equation (above) at $[S] \ll K_M$.

Typically, K_M values exhibited by natural enzymes tend to be roughly in the same range as natural cellular concentration of the substrate on which they operate.