



# 軸計算（手算）

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參考料來源：中央大學 機械設計實驗室 自編講義

# 設計問題

圖為減速機之中間軸，請根據所附的軸承與負載數據，求出軸承C與D之受力。

1. y座標正方向為自紙面朝向觀者。

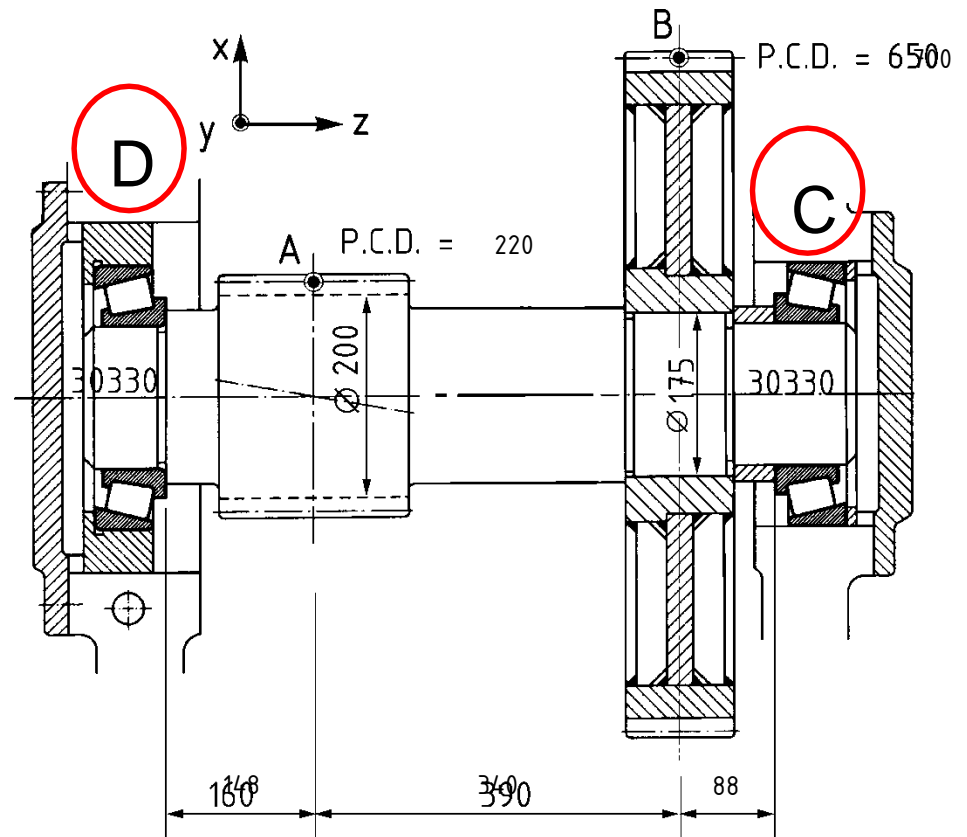
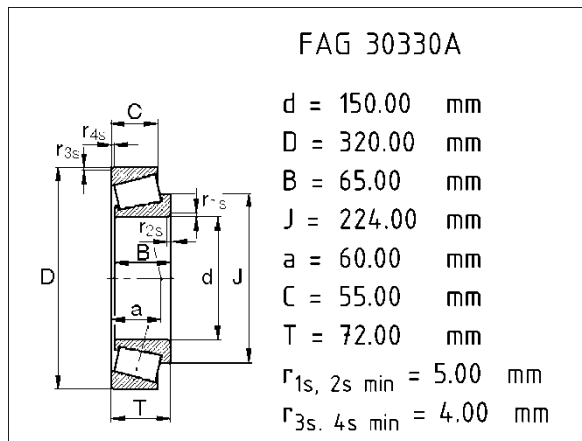
2.  表示齒輪負載施加位置

3. P.C.D為節圓直徑

4. 轉速 500 rpm

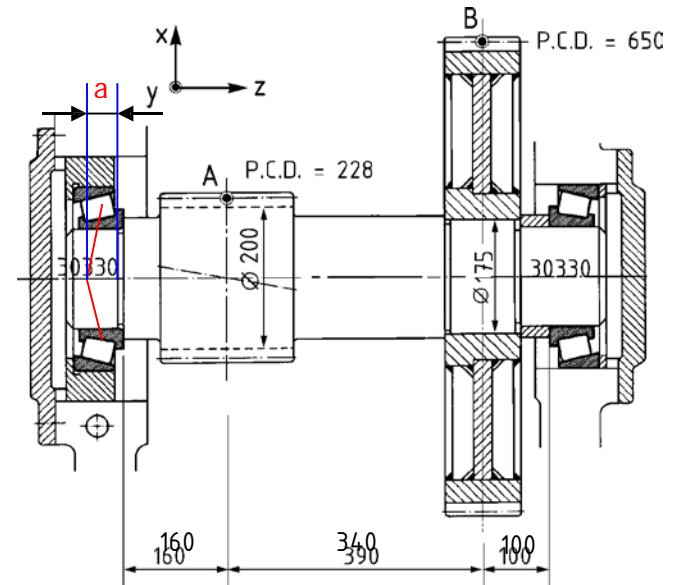
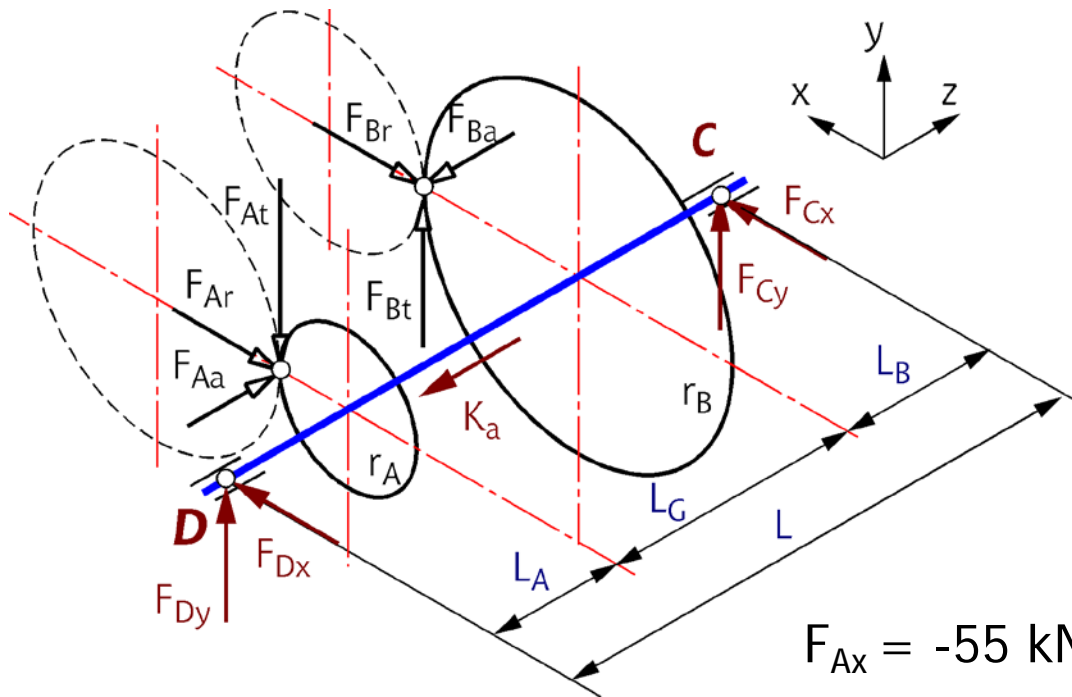
5. 齒輪齒面間作用負載如右所示

$$\begin{aligned} F_{Ax} &= -50 \text{ kN}; F_{Bx} = -20 \text{ kN}; \\ F_{Ay} &= -160 \text{ kN}; F_{By} = 50 \text{ kN}; \\ F_{Az} &= 20 \text{ kN}; F_{Bz} = -8 \text{ kN} \end{aligned}$$



# 作業檢討

- 將設計問題X型配置改成O型配置

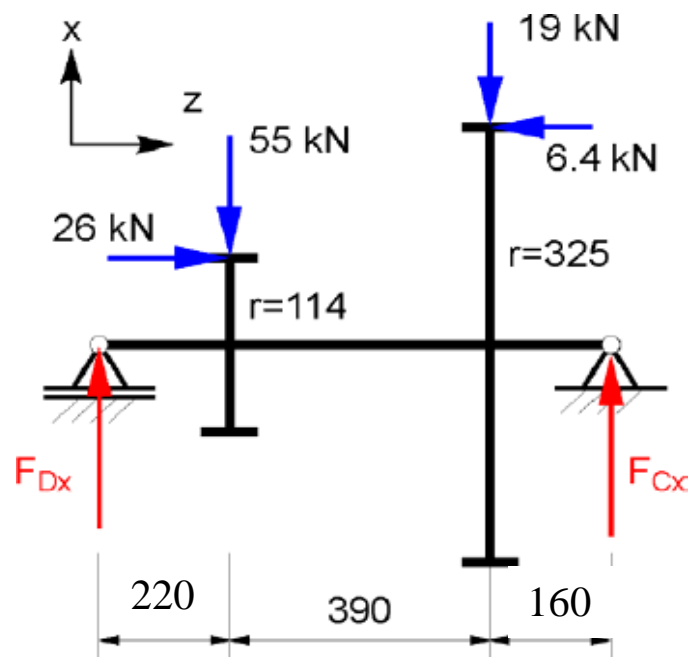


$$F_{Ax} = -55 \text{ kN}; F_{Ay} = -148 \text{ kN}; F_{Az} = 26 \text{ kN}$$

$$F_{Bx} = -19 \text{ kN}; F_{By} = 52 \text{ kN}; F_{Bz} = -6.4 \text{ kN}$$

$$L_A = 220 \text{ mm}; L_G = 340 \text{ mm}; L_B = 160 \text{ mm}$$

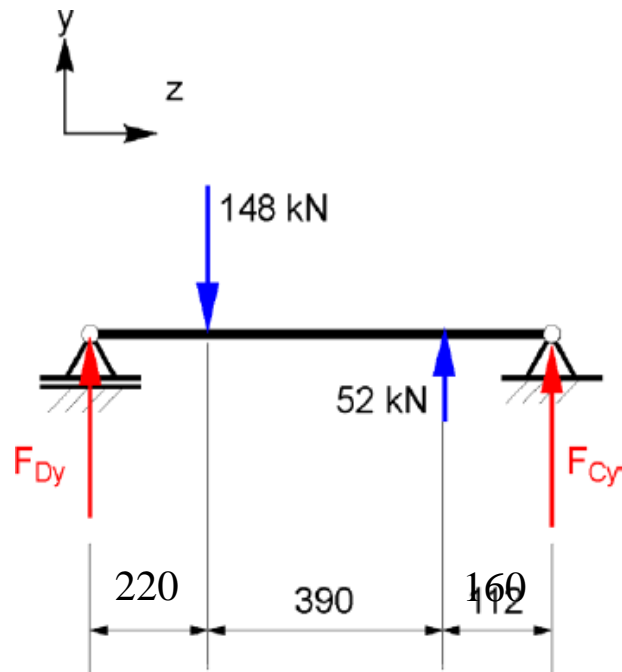
## X - Z 平面



$$L = 390 + 220 + 160 = 770$$

	$F_{Ax}$	$F_{Bx}$	$F_{Az}$	$F_{Bz}$	合力
$F_{Dx}$	$55 \cdot \frac{550}{770}$	$19 \cdot \frac{160}{770}$	$-26 \cdot \frac{114}{770}$	$6.4 \cdot \frac{325}{770}$	42.1
$F_{Cx}$	$55 \cdot \frac{220}{770}$	$19 \cdot \frac{610}{770}$	$26 \cdot \frac{114}{770}$	$-6.4 \cdot \frac{325}{770}$	31.9

## Y - Z 平面



	$F_{Ay}$	$F_{By}$	合力
$F_{Dy}$	$148 \cdot \frac{550}{770}$	$-52 \cdot \frac{160}{770}$	94.9
$F_{Cy}$	$148 \cdot \frac{220}{770}$	$-55 \cdot \frac{610}{770}$	-1.3

# 軸承受力分析

- 合成受力

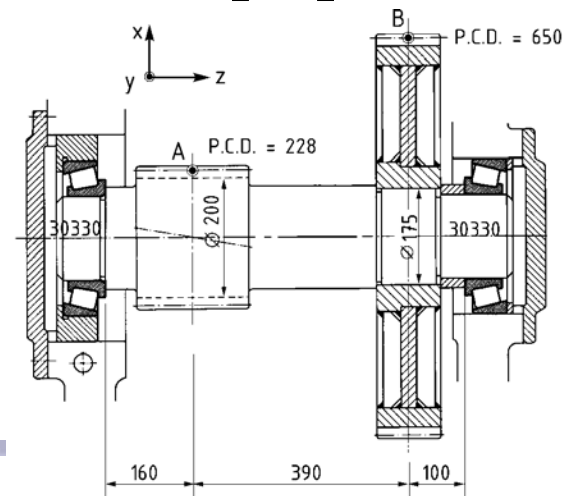
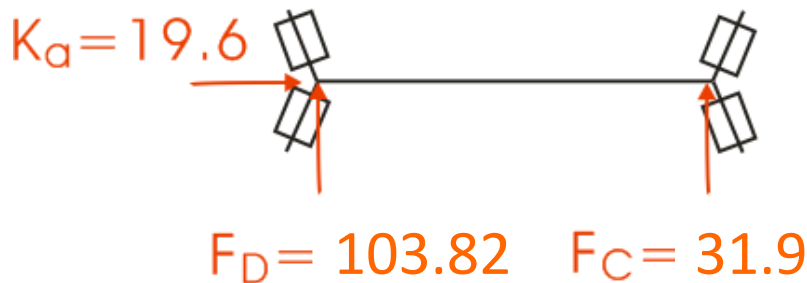
$$F_D = \sqrt{F_{Dx}^2 + F_{Dy}^2} = \sqrt{(42.1)^2 + (94.9)^2} = 103.82 \text{ [kN]}$$

$$F_C = \sqrt{F_{Cx}^2 + F_{Cy}^2} = \sqrt{(31.9)^2 + (-1.3)^2} = 31.9 \text{ [kN]}$$

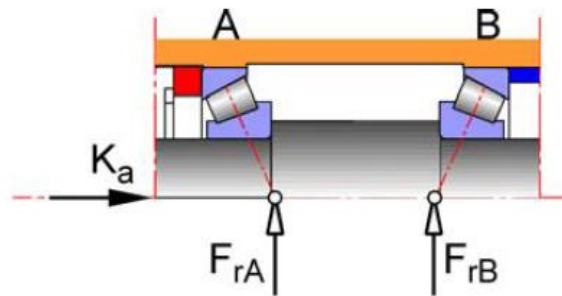
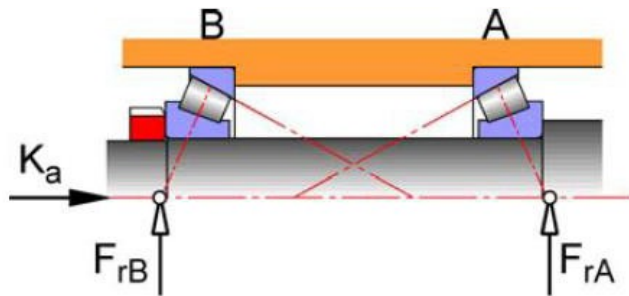
- 軸向受力Ka

$$Z\text{方向為正} = 26 - 6.4 = 19.6 \text{ [kN]}$$

∴Ka為由左至右作用在軸上的力19.6[kN]



# 錐形滾柱軸承組合之軸向負荷



$$F_a = 1.26 \cdot F_r \cdot \tan \alpha$$

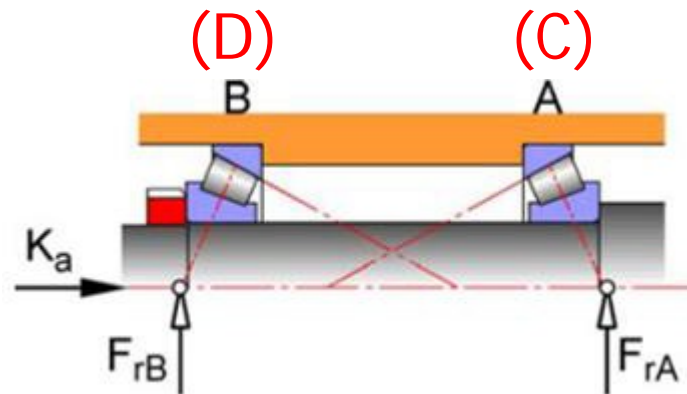
Load Condition		Axial Load for equivalent dynamic load	
		Bearing A	Bearing B
$\frac{F_{rA}}{Y_A} \geq \frac{F_{rB}}{Y_B}$	$K_a \geq 0$	$F_{aA} = \frac{F_{rA}}{2 Y_A}$	$F_{aB} = \frac{F_{rA}}{2 Y_A} + K_a$
$\frac{F_{rA}}{Y_A} < \frac{F_{rB}}{Y_B}$	$K_a \geq 0.5 \left( \frac{F_{rB}}{Y_B} - \frac{F_{rA}}{Y_A} \right)$	$F_{aA} = \frac{F_{rA}}{2 Y_A}$	$F_{aB} = \frac{F_{rA}}{2 Y_A} + K_a$
	$K_a < 0.5 \left( \frac{F_{rB}}{Y_B} - \frac{F_{rA}}{Y_A} \right)$	$F_{aA} = \frac{F_{rB}}{2 Y_B} - K_a$	$F_{aB} = \frac{F_{rB}}{2 Y_B}$

Type of Bearing		e	Single Row				Double Row			
			$F_a / F_r > e$		$F_a / F_r \leq e$		$F_a / F_r > e$		$F_a / F_r \leq e$	
			X	Y	X	Y	X	Y	X	Y
Deep groove ball bearing										
$F_a / C_0 = 0.025$		0.22		2.0				2.0		
$= 0.04$		0.24		1.8				1.8		
$= 0.07$		0.27	0.56	1.6	1.00	0	0.56	1.6	1.00	0
$= 0.13$		0.31		1.4				1.4		
$= 0.25$		0.37		1.2				1.2		
$= 0.5$		0.44		1.0				1.0		
Angular contact ball bearing	$\alpha = 40^\circ$	1.14	0.35	0.57	1.00	0				
	$\alpha = 32^\circ$	0.86					0.62	1.17	1.00	0.73
Self-aligning ball bearing		$1.5 \tan \alpha$					0.65	$0.975/e$	1	$0.63/e$
Spherical roller bearing		$1.5 \tan \alpha$					0.67	$1/e$	1	$0.675/e$
Taper roller bearing		$1.5 \tan \alpha$	0.4	$0.6/e$	1	0				



# 計算軸承軸向受力

$K_a = 19.6$   
 $F_D = 103.82$   $F_C = 31.9$



Y:軸承止推係數=1.74

$$\frac{F_{rB}}{Y_B} \frac{F_{rB}}{Y_B} = \frac{F_D}{Y} = \frac{103.82}{1.74} = 60$$

$$\frac{F_{rA}}{Y_A} \frac{F_{rA}}{Y_A} = \frac{F_C}{Y} = \frac{31.9}{1.74} = 18.33$$

$$\because \frac{F_D}{Y} > \frac{F_C}{Y} \quad \frac{F_{rA}}{Y_A} < \frac{F_{rB}}{Y_B} \Rightarrow K_a < 0.5 \left( \frac{F_{rB}}{Y_B} - \frac{F_{rA}}{Y_A} \right) \Rightarrow$$

$$K_a = 19.6 < 0.5(60 - 18.33) = 20.835$$

$$F_{aA} = \frac{F_{rB}}{2 Y_B} - K_a$$

$$F_{aB} = \frac{F_{rB}}{2 Y_B}$$

# 計算軸承軸向受力

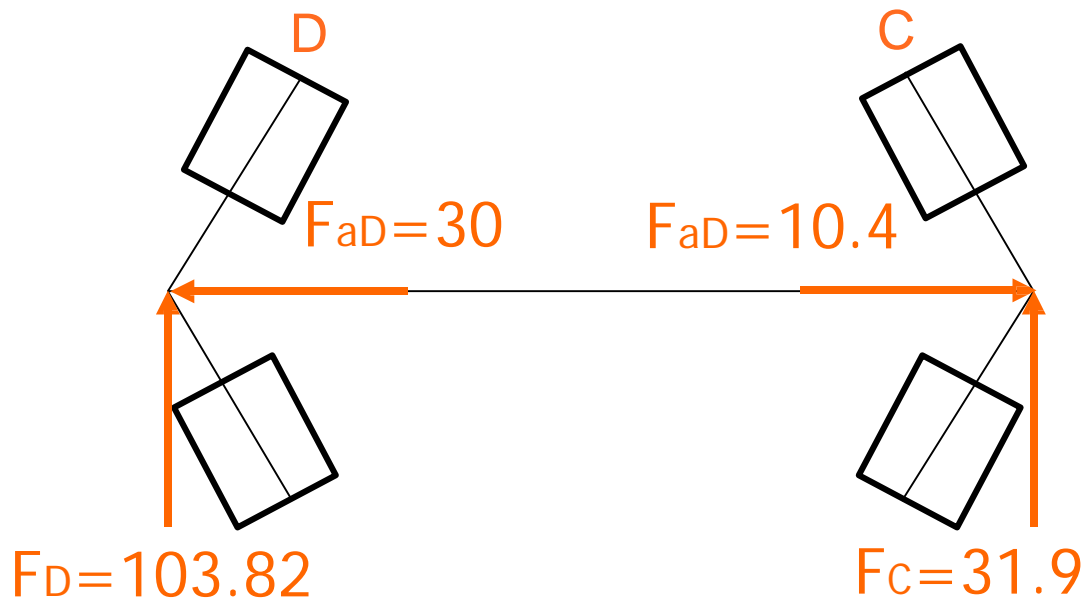
## ■ 軸承軸向受力

$$F_{aB} = \frac{F_{rB}}{2 Y_B}$$

$$\therefore F_{aD} = \frac{F_D}{2Y} = 30 \quad [kN]$$

$$F_{aA} = \frac{F_{rB}}{2 Y_B} - K_a$$

$$F_{aC} = \frac{F_D}{2Y} - K_a = 10.4 \quad [kN]$$



# 計算軸承D的壽命

## • Bearing(D)

$$\frac{F_{aD}}{F_D} = \frac{30}{103.82} = 0.289 < e = 0.35$$

$$\therefore X = 1, Y = 0$$

$$\begin{aligned} P &= X \cdot F_D + Y \cdot F_{aD} \\ &= 1 \cdot 103.82 + 0 \cdot 30 \\ &= 103.82 \text{ [kN]} \end{aligned}$$

$$\begin{aligned} \therefore L_{10h} &= \frac{10^6}{60 \cdot 500} \left( \frac{800}{103.82} \right)^{10/3} \\ &= 30123.72 \text{ [hr]} \end{aligned}$$

Taper roller bearing →

$F_a / F_r \leq e$	
X	Y
1.00	0

**P**

軸承等效動負載  
 $= X \cdot F_r + Y \cdot F_a$

X: 軸承徑向係數  
Y: 軸承止推係數  
 $F_r$ : 徑向負荷  
 $F_a$ : 軸向負荷

基本額定壽命

$$L_{10h} = \frac{10^6}{60 \cdot n} \left( \frac{C}{P} \right)^p \text{ [hr]}$$

$L_{10h}$  基本額定壽命 (小時)

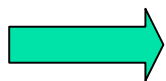
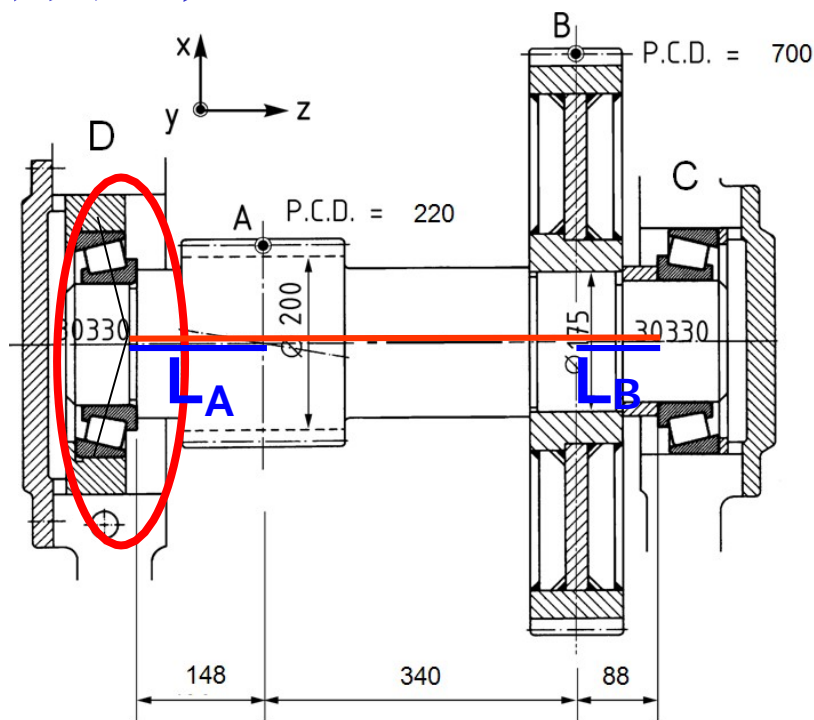
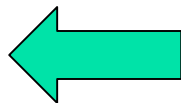
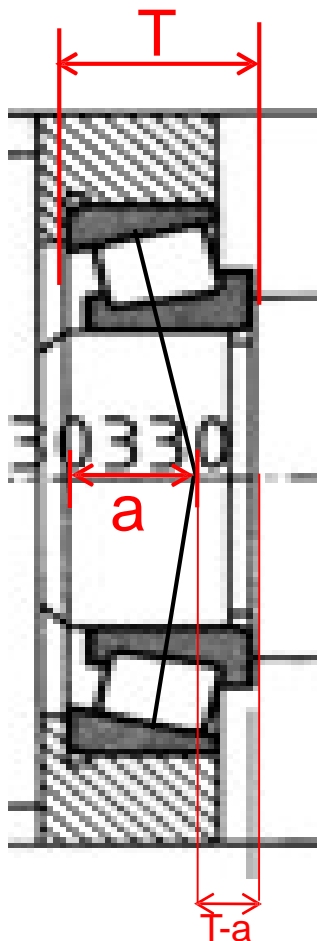
$C$  基本額定負動負荷

$n$  軸承轉速 (rpm)

$p$  運轉壽命乘幂係數 = 3 滾珠  
= 10/3 滾柱

## 軸承支撐點的位置

- 注意軸承作用力線與軸線相交，兩交點之間跨距才為軸承在軸上的跨距(P.C.D為齒輪節圓直徑)。

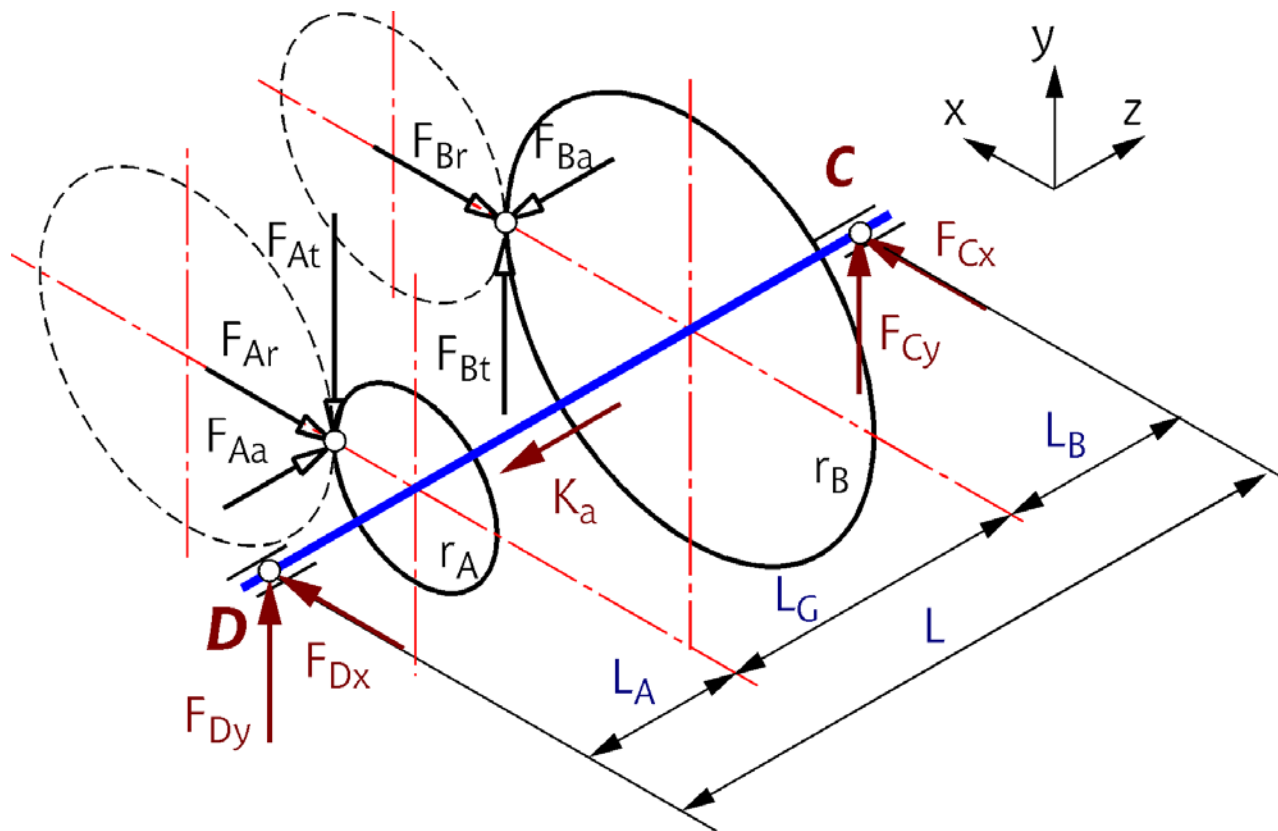


$$L_A = 148 + (T - a) = 148 + 12 = 160 \text{ (mm)}$$

$$L_B = 88 + (T - a) = 88 + 12 = 100 \text{ (mm)}$$

$$L = 160 + 100 + 340 = 600 \text{ (mm)}$$

## 列出所有受力情形



$$F_{Ax} = -50 \text{ kN}; F_{Ay} = -160 \text{ kN}; F_{Az} = 20 \text{ kN}$$

$$F_{Bx} = -20 \text{ kN}; F_{By} = 50 \text{ kN}; F_{Bz} = -8 \text{ kN}$$

$$L_A = 160 \text{ mm}; L_G = 340 \text{ mm}; L_B = 100 \text{ mm}$$

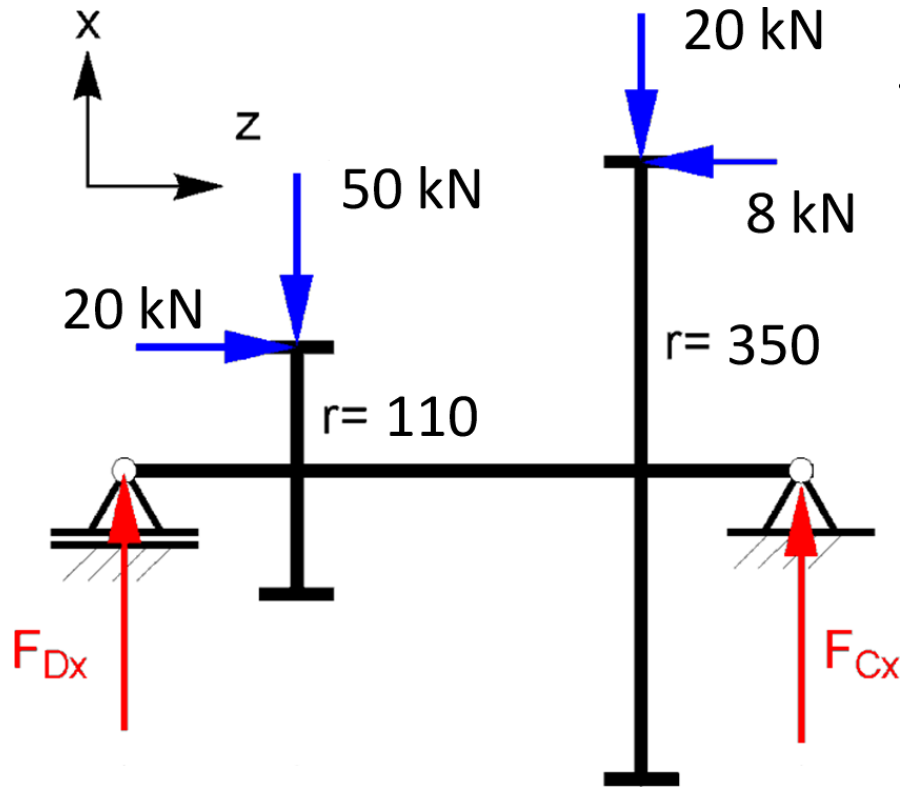
## X - Z 平面 F B D 與彎曲應力分佈

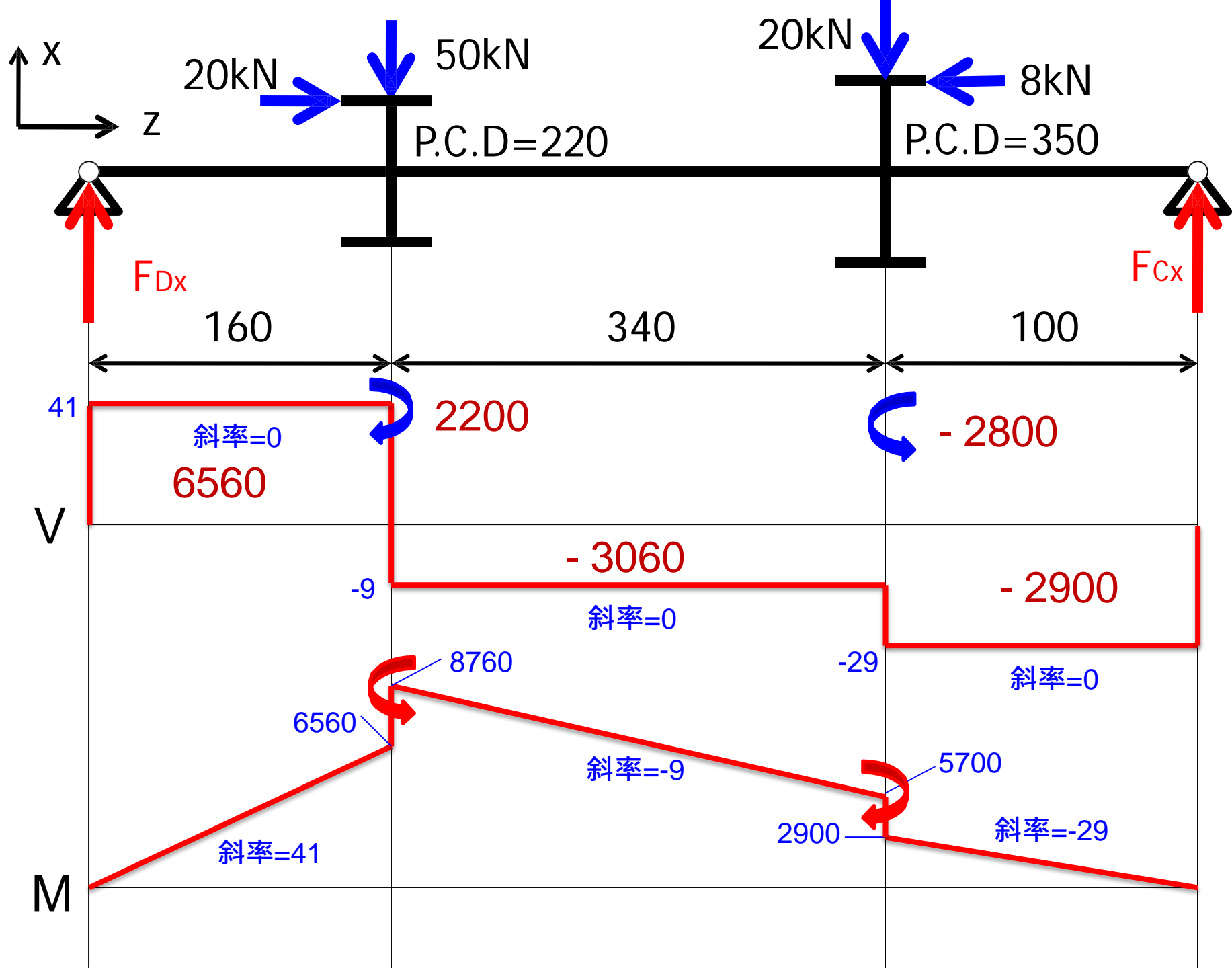
$$\sum F_X = 0 \quad F_{DX} + F_{CX} - 50 - 20 = 0 \dots (1)$$

$$\sum M_{CX} = 0 \quad 8 \times 350 + 20 \times 100 + 50 \times 440 - 20 \times 110 - F_{DX} \times 600 = 0$$

$$\therefore F_{DX} = 41 \text{ [kN]} \dots \text{代入(1)中得}$$

$$F_{CX} = 29 \text{ [kN]}$$





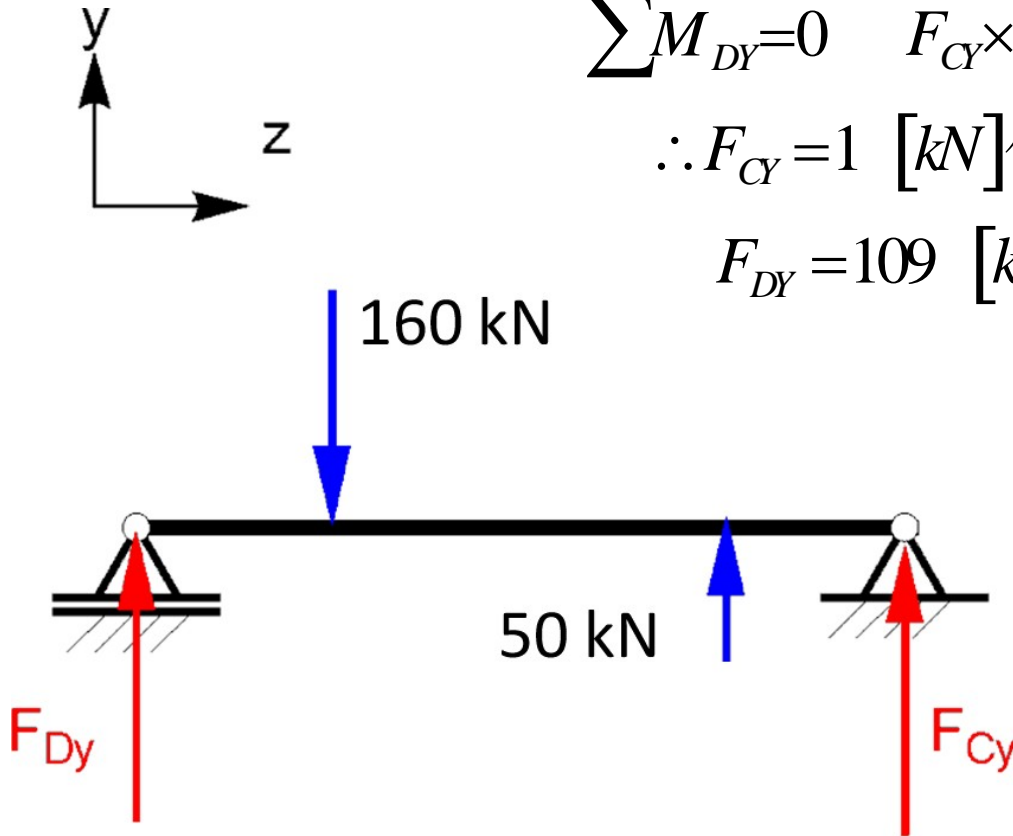
## Y - Z 平面 FBD 與彎曲應力分佈

$$\sum F_Y = 0 \quad F_{DY} - 160 + 50 + F_{CY} = 0 \dots (1)$$

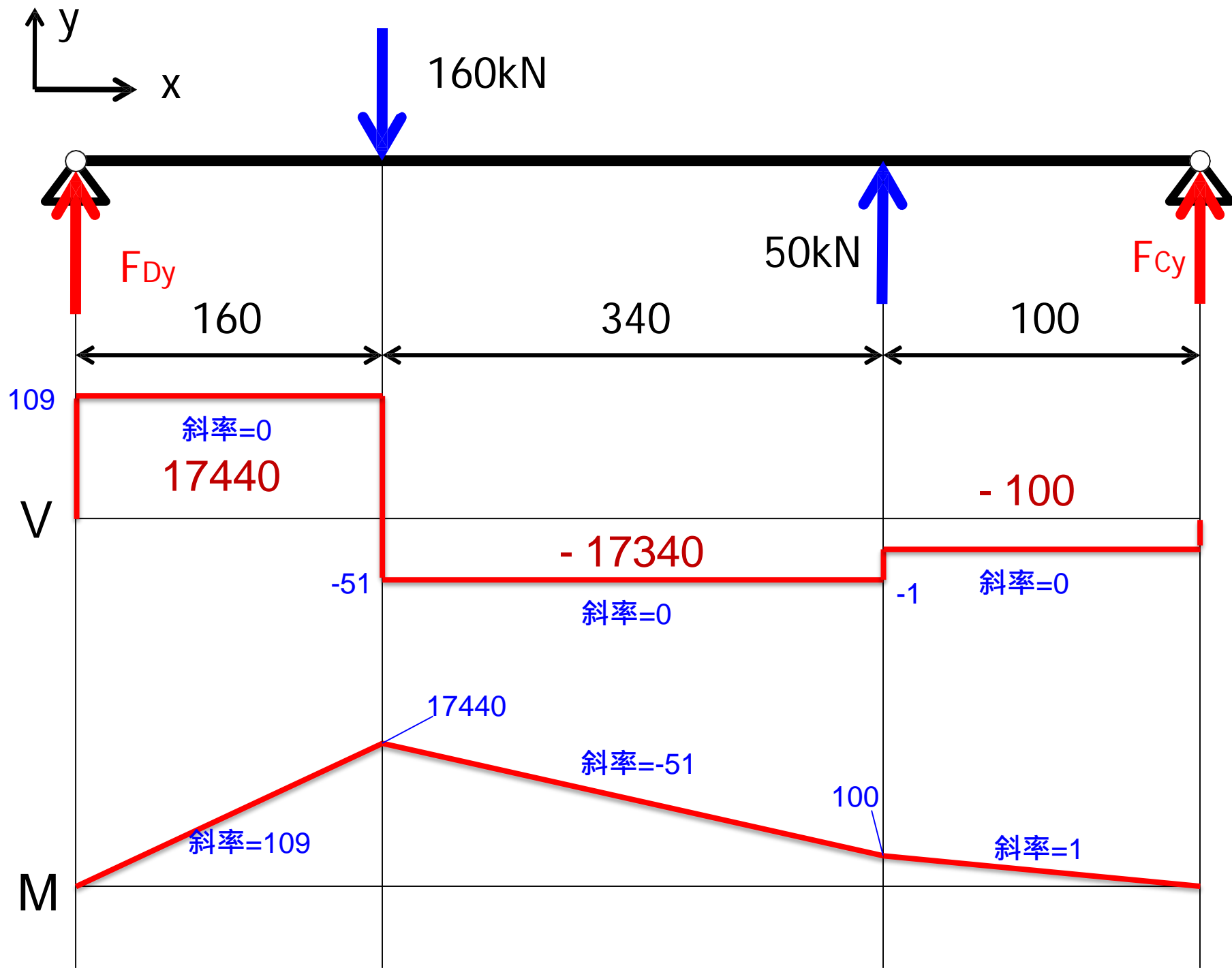
$$\sum M_{DY} = 0 \quad F_{CY} \times 600 - 160 \times 160 + 50 \times 500 = 0$$

$\therefore F_{CY} = 1 \text{ [kN]}$  代入(1)中得

$$F_{DY} = 109 \text{ [kN]}$$







- 合成受力

$$F_D = \sqrt{F_{Dx}^2 + F_{Dy}^2} = \sqrt{(41)^2 + (109)^2} = 116.456 \text{ [kN]}$$

$$F_C = \sqrt{F_{Cx}^2 + F_{Cy}^2} = \sqrt{(29)^2 + (1)^2} = 29.02 \text{ [kN]}$$