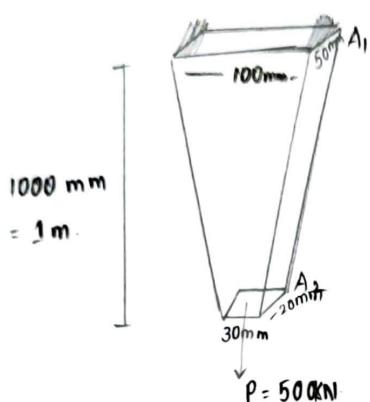


1) Varying cross-section

2) Composite section.



On a varying cross-section of a bar, point average stress in the bar,

Find the,

- average stress in the bar
- elongation.

Assume, Steel bar,

$$\text{Modulus of elasticity } E = 200 \text{ GPa}$$

$$= 200 \times 10^3 \text{ MPa}$$

$$= 200000 \text{ N/mm}^2$$

$$(i) \text{ Average stress} = \frac{P}{A}$$

$$= \frac{500 \times 10^3 \text{ N}}{(A_1 + A_2)/2}$$

$$= \frac{500 \times 10^3}{(100 \times 50 + 30 \times 20)/2}$$

$$= \frac{500 \times 10^3}{2800}$$

$$= 178.5 \text{ N/mm}^2$$

$$\text{Ans} = 178.5 \text{ MPa}$$

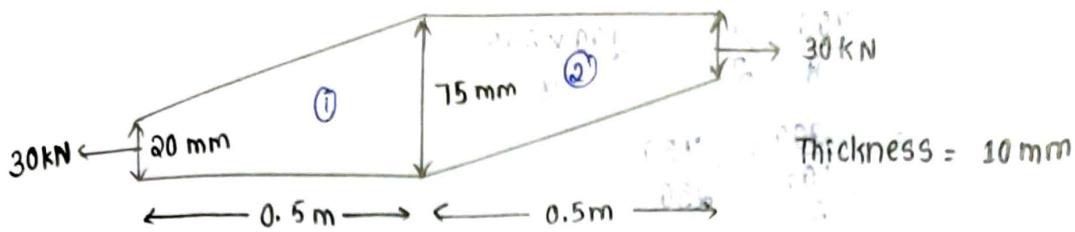
$$(ii) \text{ Total elongation, } \Delta L = \frac{PL}{AE} = \frac{Pl}{E}$$

$$= \frac{178.5 \times 1000}{200 \times 10^3}$$

$$= \frac{178.5}{200}$$

$$= 0.8925$$

$$\approx 0.89 \text{ mm}$$



Determine the elongation of a steel member when it is subjected to an axial force of 30 kN. The member is 10 mm thick.

$$\text{Elongation, } \Delta L = \frac{PL_1}{A_1 E} + \frac{PL_2}{A_2 E}$$

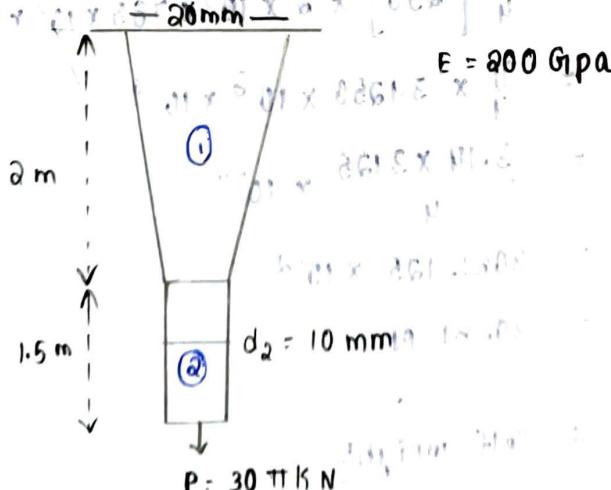
$$= \left[\frac{30 \times 10^3 \times 500}{20 \times 10 + 75 \times 10} + \frac{30 \times 10^3 \times 500}{20 \times 10 + 75 \times 10} \right] \frac{1}{200 \times 10^3}$$

$$= \left[\frac{15 \times 10^6}{200 + 750} \times 2 \right] \times \frac{1}{200 \times 10^3}$$

$$= \frac{15 \times 10^6}{1475} \times \frac{1}{100 \times 10^3}$$

$$= \frac{150 \times 10^6}{1475} = \frac{150}{1475} = 0.31 \text{ mm}$$

3)



$$\text{Elongation, } \Delta L = \frac{PL_1}{A_1 E} + \frac{PL_2}{A_2 E}$$

$$= \frac{30 \times 2000 \times 10^3}{\frac{\pi}{4} (20)^2 \times 200 \times 10^3} + \frac{30 \times 1500 \times 10^3}{\frac{\pi}{4} (10)^2 \times 200 \times 10^3}$$

$$SL = \frac{300}{400} + \frac{30 \times 15}{900}$$

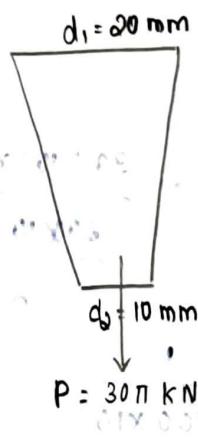
13.8 mm
12 mm

$$= \frac{300}{100} + \frac{450}{50}$$

$$= 3 + 9$$

$$= 12 \text{ mm}$$

In the above question, if the self weight of rod is included what will be the total elongation



Density of steel,

$$\rho_{\text{Steel}} = 7850 \text{ kg/m}^3$$

$$= 7850 \times 10 \text{ N/m}^2$$

$$= \frac{78500}{10^9} = 78500 \times 10^{-9} \text{ N/mm}^2$$

$$\text{Self weight} = \text{volume} \times \text{density} (\rho)$$

Average area $\times l \times \rho$

$$= \frac{\pi}{4} \left(\frac{20^2 + 10^2}{2} \right) \times 2000 \times 7850 \times 10^{-9}$$

$$= \frac{\pi}{4} [250] \times 2 \times 10^3 \times 785 \times 10^3 \times 10^{-9}$$

$$= \frac{\pi}{4} \times 39250 \times 10^6 \times 10^{-9}$$

$$= \frac{3.14 \times 3925}{4} \times 10^{-2}$$

$$= 3081.125 \times 10^{-2}$$

$$= 30.81 \text{ N}$$

$$\therefore P_1 = P + \text{self weight}$$

$$= 90\pi \text{ KN} + 30.81 \text{ N}$$

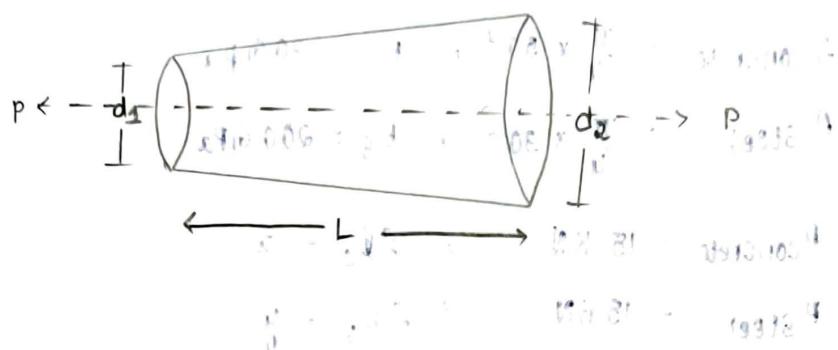
$$= 30 \times 3.14 \times 10^3 + 30.81 \text{ N}$$

$$= 94230.8 \text{ N}$$

$$= 94,230.8 \text{ KN}$$

$$= 94.2 \text{ KN}$$

A round bar of length L tapers uniformly from small diameter d_1 at one end to bigger diameter d_2 at other end. Show that the extension produced by the tensile force ' P ' is $S = \frac{4PL}{\pi d_1 d_2}$ if $d_2 = 2d_1$, compare this extension with that of a uniform cylindrical bar having a diameter equal to the mean diameter of the taper bar.

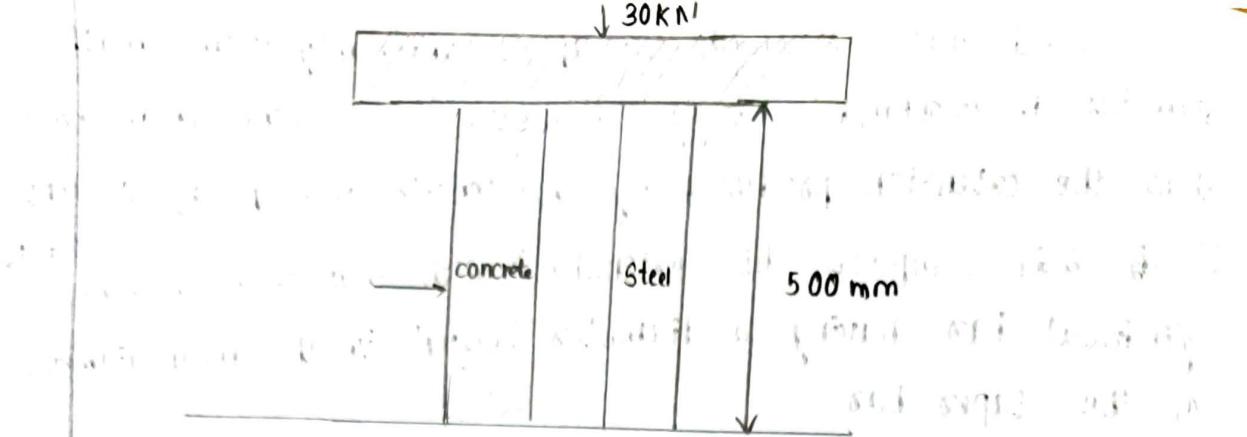


$$\text{Area} = \frac{\pi}{4} d^2 = \frac{\pi}{4} (d_1 + d_2)^2 = \frac{\pi}{4} (2d_1)^2 = 4\pi d_1^2$$

$$\text{Stress} = \frac{P}{A} = \frac{P}{4\pi d_1^2}$$

$$\text{Strain} = \frac{\Delta L}{L} = \frac{P}{E} \cdot \frac{4L}{\pi d_1^2} = \frac{4PL}{\pi E d_1^2}$$

$$\text{Strain} = \frac{\Delta L}{L} = \frac{P}{E} \cdot \frac{4L}{\pi (d_1 + d_2)^2} = \frac{4PL}{\pi E (d_1 + d_2)^2}$$



$$A_{\text{concrete}} = \frac{\pi}{4} \times 50^2, E_c = 30 \text{ GPa}$$

$$A_{\text{steel}} = \frac{\pi}{4} \times 30^2, E_s = 200 \text{ GPa}$$

$$P_{\text{concrete}} = 15 \text{ KN}, Sl_c = x$$

$$P_{\text{steel}} = 15 \text{ KN}, Sl_s = y$$

$x = y$
compatibility condition

$$Sl_c = \frac{P_c l_c}{A_c E_c}$$

$$Sl_s = \frac{P_s l_s}{A_s E_s}$$

$$\frac{P_c l_c}{A_c E_c} = \frac{P_s l_s}{A_s E_s}$$

$$P_c = P_s$$

$$l_c = l_s$$

$$\sigma_{\text{concrete}} = \frac{P_1}{A_1}$$

$$= \frac{15 \times 10^3}{\frac{\pi}{4} \times 50^2} = \underline{\underline{15000}}$$

* Method and Analyse a composite bar

i) Displacement

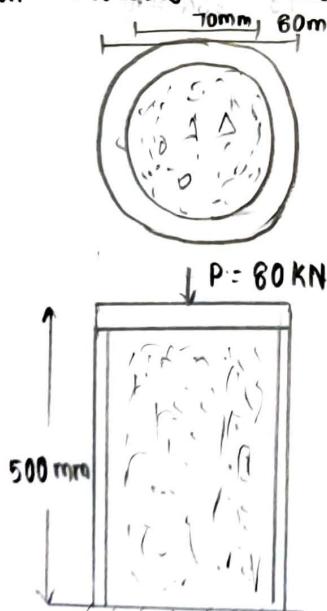
ii) Force method

- i) A steel pipe filled with a concrete having external diameter has 80 mm and internal diameter has 70 mm. It is subjected to a axial compressive force of 80 kN.

Assume, $E_{\text{steel}} = 200 \text{ GPa}$

$E_{\text{conc.}} = 24 \text{ GPa}$

Find the stresses in each of the material



$$S_c = S_s$$

$$\frac{P_c l_c}{A_c E_c} = \frac{P_s l_s}{A_s E_s}$$

$$\frac{P_c \times 500}{\frac{\pi}{4} \times (70)^2 \times 200} = \frac{P_s \times 500}{\frac{\pi}{4} \times (80^2 - 70^2) \times 24}$$

$$\frac{P_s}{P_c} = \frac{\frac{4}{70^2} \times 200}{\frac{4}{(80^2 - 70^2)} \times 24} = \frac{(80^2 - 70^2) \times 200}{70^2 \times 24}$$

$$\frac{P_s}{P_c} = 0.55 \quad \text{Ans}$$

$$P_s + P_c = 80 \quad \text{Ans}$$

$$0.55 P_c + P_c = 80$$

$$P_c = \frac{80}{0.55}$$

$$P_c = 145.45 \text{ kN}$$

$$P_S = 60 - P_C$$

$$= 60 - 82.53$$

$$= 57.47 \text{ KN}$$

$$\sigma_C = \frac{P_C}{A_C} = \frac{82.53 \times 10^3}{\frac{\pi}{4} \times 70^2}$$

$$= \frac{82530}{3846.5} = 21.47 \text{ N/mm}^2 (\text{MPa})$$

$$\sigma_S = \frac{P_S}{A_S} = \frac{57.47 \times 10^3}{\frac{\pi}{4} \times (80^2 - 70^2)}$$

$$= \frac{57470}{1500} = 48.6 \text{ N/mm}^2 (\text{MPa})$$

2) Determine the required area of steel so that the force is shared equally between the steel and concrete.

$$\text{Assume, } E_{\text{conc.}} = 24 \text{ GPa}$$

$$E_{\text{Steel}} = 200 \text{ GPa}$$

The load applied on the section is 300 KN.

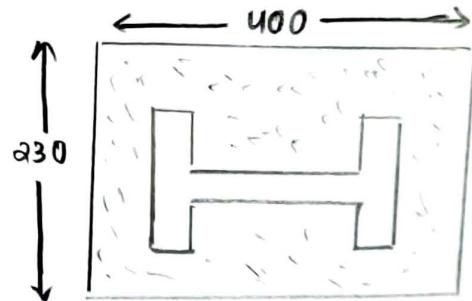
$$P = 300 \text{ KN}$$

$$A_S = ?$$

$$A_C = 400 \times 230 - A_S$$

$$\frac{P_S}{P_C} = 1$$

$$P_S + P_C = 300 \text{ KN}$$



$$\frac{P_C L_C}{A_C E_C} = \frac{P_S L_S}{A_S E_S}$$

$$A_C E_C = A_S E_S$$

$$(400 \times 230 - A_S) \times 24 = A_S \times 200$$

$$400 \times 230 \times 24 - 24 A_S = 200 A_S$$

$$224 A_S = 400 \times 230 \times 24$$

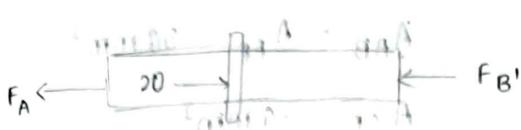
$$224 A_S = 2208000$$

$$A_S = 9857 \text{ mm}^2$$

3) A steel rod shown in figure has a diameter of 10 mm. It is fixed to wall at A and before it is loaded there is a gap of 0.2 mm between the wall B' and the rod.

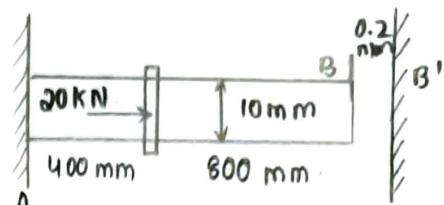
Determine the reactions at A and B' if the rod is subjected to an axial force of $P = 20 \text{ kN}$. Neglect the size of collar.

Assume, $E_{\text{steel}} = 200 \text{ GPa}$



$$-F_A - F_B' + 20 = 0$$

$$F_A + F_B' = 20 \text{ kN} \quad \text{--- (1)}$$



$$\delta_{AB} = \frac{PL_1}{AE} - \frac{F_B' L_2}{AE} = 0.2 \text{ mm}$$

$$0.2 = \frac{20 \times 10^3 \times 400}{\frac{\pi}{4} \times (10)^2 \times 200 \times 10^3} - \frac{F_B' \times 400 + 800 \times 10^3}{\frac{\pi}{4} \times (10)^2 \times 200 \times 10^3}$$

$$0.2 = \frac{8000}{0.785 \times 2 \times 10^4} - \frac{F_B' \times 1200}{0.785 \times 2 \times 10^4}$$

$$\frac{F_B' \times 1200}{0.785 \times 2 \times 10^4} = \frac{8000}{0.785 \times 2 \times 10^4} - 0.2$$

$$\frac{F_B' \times 1200}{15700} = \frac{8000}{15700} - 0.2$$

$$\frac{F_B' \times 1200}{15700} = \frac{8000 - 3140}{15700}$$

$$F_B' = \frac{4860}{1200}$$

$$F_B' = 4.05 \text{ kN}$$

Then,

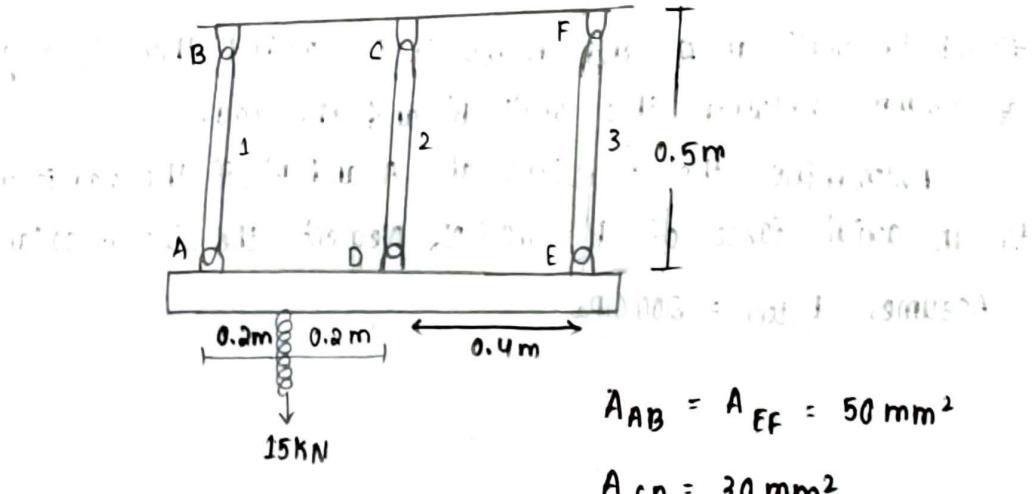
$$F_A + F_B' = 20 \text{ kN}$$

$$F_A = 20 \text{ kN} - F_B'$$

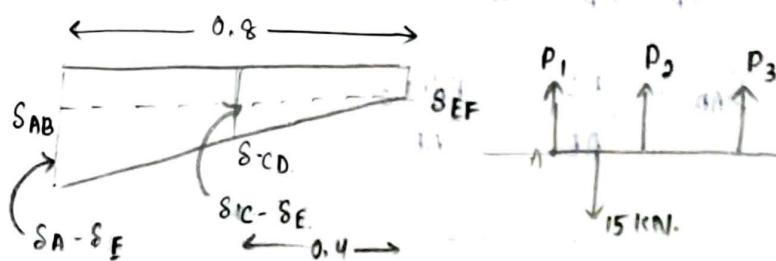
$$F_A = 20 \text{ kN} - 4.05 \text{ kN}$$

$$F_A = 15.95 \text{ kN}$$

4)



Determine the force developed in each bar



$$\delta_{AB} = \frac{P_1 L}{A_1 E}$$

$$\delta_{CD} = \frac{P_2 L}{A_2 E}$$

$$\delta_{EF} = \frac{P_3 L}{A_3 E}$$

By similar triangles,

$$\frac{\delta_C - \delta_E}{0.4} = \frac{\delta_A - \delta_E}{0.8}$$

$$2\delta_C - 2\delta_E = \delta_A - \delta_E$$

$$2\delta_C - \delta_E = \delta_A$$

$$\frac{P_2 L}{A_2 E} - \frac{P_3 L}{A_3 E} = \frac{P_1 L}{A_1 E}$$

$$\frac{2P_2}{A_2} - \frac{P_3}{A_3} = \frac{P_1}{A_1}$$

$$\frac{2P_2}{30} - \frac{P_3}{50} = \frac{P_1}{50}$$

$$A_1 = A_3 = 50 \text{ mm}^2$$

$$\Sigma F_y = 0 \Rightarrow P_1 + P_2 + P_3 = 15 \quad \text{--- (A)}$$

$$\Sigma M_A = 0 \Rightarrow P_2 \times 0.4 + P_3 \times 0.8 - 15 \times 0.2 = 0$$

$$P_2 + 2P_3 = 7.5 \quad \text{--- (1)}$$

$$\frac{\partial P_1}{30} - \frac{P_3}{50} = \frac{P_1}{50}$$

$$\frac{\partial P_2}{3} - \frac{P_3}{5} = \frac{P_1}{50}$$

$$\frac{\partial P_2}{3} = \frac{P_1 + P_3}{5}$$

$$10P_2 = 3P_1 + 3P_3 \quad \text{--- (2)}$$

$$3P_1 + 10P_2 + 3P_3 = 0 \quad \text{--- (2)}$$

$$3(A) \Rightarrow 3P_1 + 3P_2 + 3P_3 = 45 \quad \text{--- (3)}$$

$$(2) - (3) \Rightarrow 3P_1 + 10P_2 + 3P_3 = 0$$

$$3P_1 + 3P_2 + 3P_3 = 45$$

$$\underline{-13P_2 = -45}$$

$$P_2 = 3.46 \text{ KN}$$

$$(1) \Rightarrow 3.46 + 2P_3 = 7.5$$

$$2P_3 = 4.04$$

$$P_3 = 2.04 \text{ KN}$$

$$(A) \Rightarrow P_1 + 3.46 + 2.04 = 15$$

$$P_1 + 5.5 = 15$$

$$P_1 = 15 - 5.5$$

$$P_1 = 9.5 \text{ KN}$$

$$\therefore P_1 = 9.5 \text{ KN}$$

$$P_2 = 3.46 \text{ KN}$$

$$P_3 = 2.04 \text{ KN}$$

* Thermal stresses - occurs only when restrain the member

~~28/11/19~~

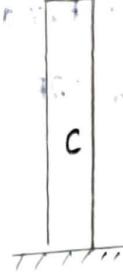
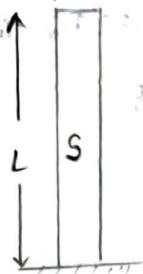
$$T_2 = 45^\circ\text{C}$$

$$T_1 = 25^\circ\text{C}$$

Steel

Concrete

Wood



$$\Delta L = \alpha \Delta T L$$

α linear coefficient of thermal expansion

$$\alpha_{\text{steel}} = 6.6 \times 10^{-6} /^\circ\text{C}$$

$$\text{strain} = \frac{\Delta L}{L} = \epsilon = \alpha \Delta T$$

- i) A steel bar shown in figure is constrained to just fix between two supports.

When temperature $T_1 = 20^\circ\text{C}$ if the temperature is raised to 60°C , determine the average normal thermal stress developed in the bar.

$$\text{Assume, } \alpha_{\text{steel}} = 6.6 \times 10^{-6} /^\circ\text{C}.$$

$$T_1 = 20^\circ\text{C} \quad T_2 = 60^\circ\text{C}$$

$$\Delta T = 40^\circ\text{C}$$

$$\text{If not constrained, } \Delta L = \alpha \Delta T \times L$$

$$= 6.6 \times 10^{-6} \times 40 \times 600 \\ = 0.15 \text{ mm}$$

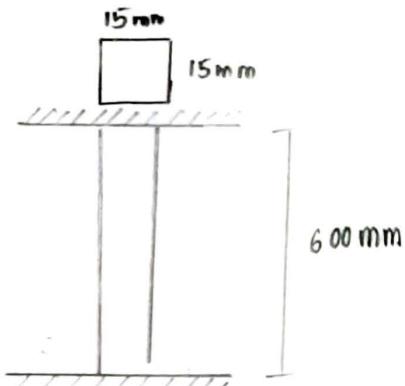
The bar is constrained.

$$S_{A/B} = 0$$

$$\alpha \Delta T L - \frac{F_{AL}}{AE} = 0$$

$$\frac{F_{AL}}{AE} = \alpha \Delta T L$$

$$F_A = \frac{0.15 \times AE}{L}$$



$$\begin{aligned}
 F_A &= \frac{0.15 \times 200 \times 10^3 \times 15 \times 15}{600} \\
 &= \frac{6750000}{600} \\
 &= 11250 \text{ KN} \\
 &\Rightarrow 11.25 \text{ KN}
 \end{aligned}$$

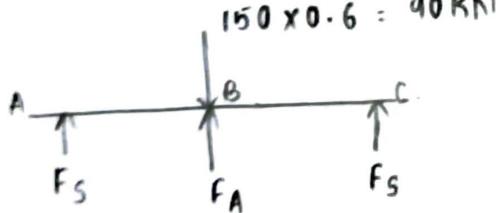
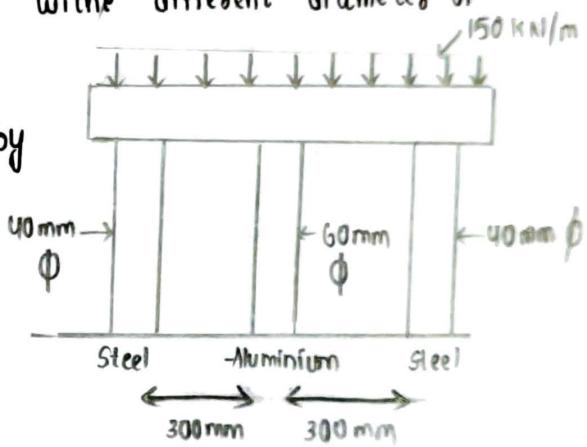
$$F = \alpha \Delta T E$$

$$\frac{F}{A} = \sigma = \alpha \Delta T E$$

$$\begin{aligned}
 \sigma &= 6.6 \times 10^{-6} \times 40 \times 200 \times 10^3 \\
 &= 52.8 \text{ N/mm}^2
 \end{aligned}$$

Three pillars on Bridge stand with different diameter of cross section.

Determine the force supported by each pillar and the initial temperature $T_1 = 20^\circ\text{C}$, final temperature $T_2 = 80^\circ\text{C}$.



$$\sum F_y = 0 \Rightarrow F_S + F_A + F_S = 90 \text{ KN}$$

$$\sum M_A = 0 \Rightarrow F_A \times 300 + F_S \times 600 = 90 \text{ KN} \quad \text{--- (1)}$$

$$F_A \times 10 + F_S \times 20 = 3 \text{ KN}$$

$$\alpha_{\text{Steel}} = 12 \times 10^{-6}/^\circ\text{C}$$

$$\alpha_{\text{Aluminium}} = 23 \times 10^{-6}/^\circ\text{C}$$

$$S_{\text{Al}} = \delta_{\text{St}} \Rightarrow [\delta_{\text{at load}} - \delta_{\text{at temp.}}] = [S_{\text{at load}} - S_{\text{at temp.}}]$$

$$\frac{F_A L}{A_a E_a} = \frac{F_S L}{A_s E_s}$$

$$\frac{\pi}{4} (60)^2 \times 70 \times 10^3 = \frac{F_S}{\pi/4 (40)^2 \times 200 \times 10^3}$$

$$\frac{F_A}{852000} = \frac{2F_S + F_A}{320000}$$

$$80F_A - 63F_S = 0 \quad \text{--- (2)}$$

$$① \times 80 \Rightarrow 80(2F_S + F_A) = 90 \times 80 \quad \text{--- (1)}$$

$$160F_S + 80F_A = 7200 \quad \text{--- (3)}$$

$$③ - ② \Rightarrow 80F_A - 63F_S = 0$$

$$80F_A + 160F_S = 7200$$

$$\hline$$

$$223F_S = 7200$$

$$F_S = 32.08 \text{ kN}$$

$$① \Rightarrow F_A + 2F_S = 90 \text{ kN}$$

$$F_A + 64.16 = 90$$

$$F_A = 25.84 \text{ kN}$$

$$F_A - S_{A\Delta T} - \alpha_A \Delta T l = S_{St\Delta T} + \alpha_{St} \Delta T l$$

$$F_A - 19.75 - 30 \cdot 10^{-6} \cdot 10^3 \cdot 10 = 26.28 + 10 \cdot 10^{-6} \cdot 10^3 \cdot 10$$

$$F_A - 19.75 - 30 \cdot 10^{-6} \cdot 10^3 \cdot 10 = 26.28 + 10 \cdot 10^{-6} \cdot 10^3 \cdot 10$$

$$F_A - 19.75 - 30 \cdot 10^{-6} \cdot 10^3 \cdot 10 = 26.28 + 10 \cdot 10^{-6} \cdot 10^3 \cdot 10$$

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$$F_A - 19.75 - 30 \cdot 10^{-6} \cdot 10^3 \cdot 10 = 26.28 + 10 \cdot 10^{-6} \cdot 10^3 \cdot 10$$

$$F_A - 19.75 - 30 \cdot 10^{-6} \cdot 10^3 \cdot 10 = 26.28 + 10 \cdot 10^{-6} \cdot 10^3 \cdot 10$$

$$F_A = 25.84 \text{ kN}$$

$$F_A = 25.84 \text{ kN}$$

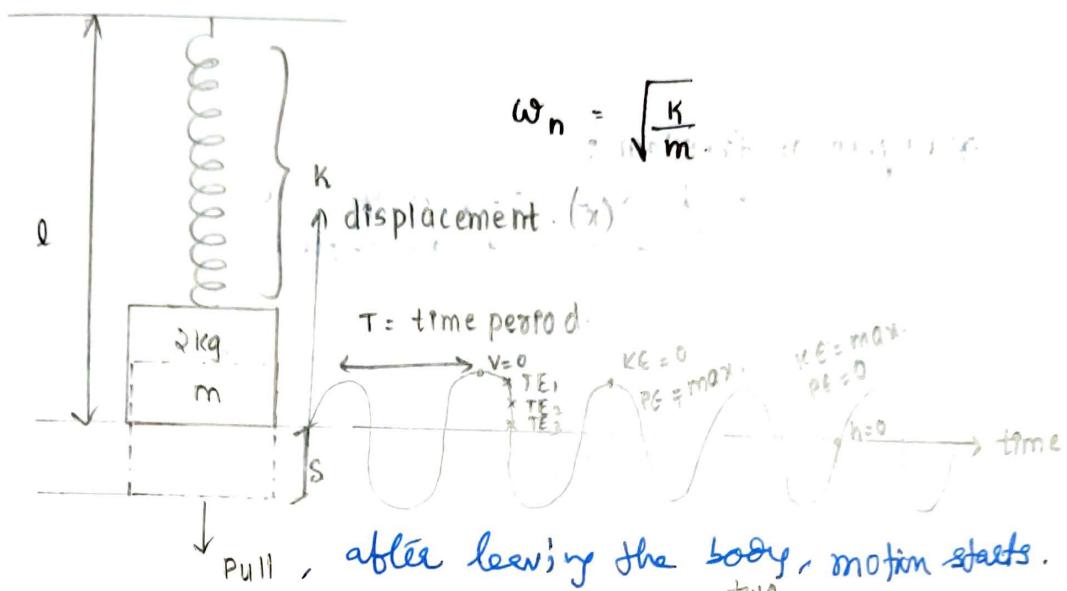
$$F_A = 25.84 \text{ kN}$$

Natural frequency of spring mass system

$$\text{Stiffness} = \frac{\text{Load}}{\text{static displacement}}$$

$$K = \frac{W}{S} \quad (\text{Newton})$$

S (meter)



Time period : The distance between any two crests or troughs.

$$T = \frac{2\pi}{\omega_n}$$

subscription

ω_n is measured in radians/sec or cycles/sec = Hertz (Hz)

$$KE = \frac{1}{2}mv^2 \quad PE = mgh$$

$$\begin{aligned} \text{Total energy} &= KE + PE \\ &= \text{constant} \quad (\text{for perfectly elastic spring}) \end{aligned}$$

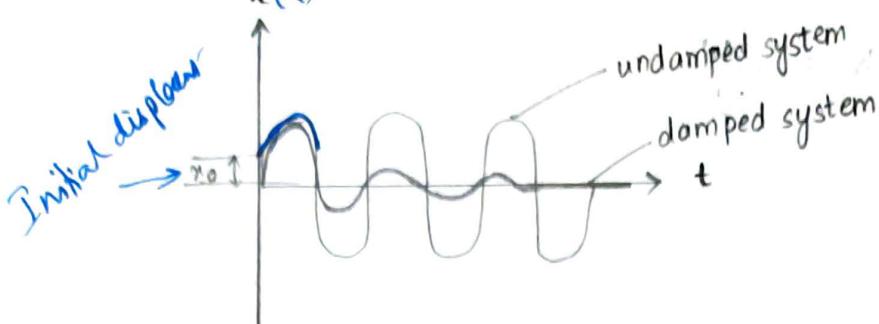
This is only possible for perfectly elastic spring only
then, system is continuous oscillating.

$$\frac{1}{2}mv^2 + mgh = \text{Constant}$$

Free vibration : A spring-mass system given an initial displacement (stretched) and left free the mass to oscillate. This is called free vibration.

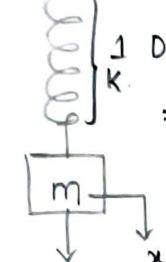
* Undamped system :

When oscillation amplitude remains constant forever in the life time of system, that system is called undamped system.



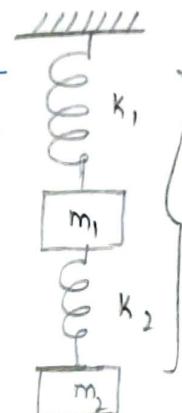
* Degree of freedom :

Defined as no. of independent ways a mass can displace.

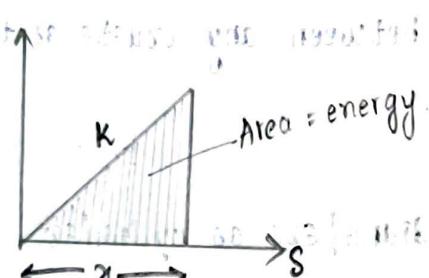


1 Degree of freedom (DOF)

= single degree of freedom
(SDOF)



2 DOF



$$P \propto S$$

$$P = K S$$

$$\frac{P}{S} = K \text{ - spring constant}$$

$$TE = KE + PE$$

$$= \frac{1}{2} mv^2 + mgh$$

$$PE = \frac{1}{2} Kx^2$$

$$KE = \frac{1}{2} \times mv^2$$

$$= \frac{1}{2} \times \frac{w}{g} \left(\frac{dx}{dt} \right)^2$$

$$TE = \frac{1}{2} \frac{w}{g} \left(\frac{dx}{dt} \right)^2 + \frac{1}{2} Kx^2$$

Differentiating w.r.t. dt.

$$\frac{1}{2} \frac{w}{g} \cdot 2 \frac{dx}{dt} \frac{d^2x}{dt^2} + \frac{1}{2} K \cdot 2x \cdot \frac{dx}{dt} = 0$$

$$\frac{w}{g} \frac{d^2x}{dt^2} + kx = 0$$

$$m \frac{d^2x}{dt^2} + kx = 0$$

$m \frac{d^2x}{dt^2} + kx = 0$ is equation of motion for single degree freedom system i.e., undamped system

* Equivalent stiffness

$$\frac{1}{K_{eq}} = \frac{1}{K_1} + \frac{1}{K_2}$$

Springs in series,

$$K_{eq} = \frac{K_1 K_2}{K_1 + K_2}$$

$$\text{Springs in parallel, } \frac{1}{K_{eq}} = \frac{1}{K_1} + \frac{1}{K_2}$$

$$K_{eq} = K_1 + K_2$$

Equation of motion

$$m \frac{d^2x}{dt^2} + kx = 0$$

$$m \ddot{x} + kx = 0$$

x is a function in terms of time

$$m\ddot{x}(t) + kx(t) = 0$$

where, $x(t)$ = Response of system

↳ At what time function first displacement

frequency

Derive the response for undamped single degree of freedom (SDOF) free vibration

Equation of motion

$$m \frac{d^2x}{dt^2} + kx = 0$$

$$m \ddot{x} + kx = 0$$

Assume a solution,

$$x(t) = A \sin \omega_n t \quad \text{--- (1)}$$

where, A = Amplitude of Sine

$$\ddot{x}(t) = Aw_n \cos \omega_n t$$

$$\ddot{x}(t) = -Aw_n^2 \sin \omega_n t \quad \text{--- (2)}$$

Now,

$$m(-Aw_n^2 \sin \omega_n t) + kA \sin \omega_n t = 0$$

$$A \sin \omega_n t [-m\omega_n^2 + k] = 0$$

$A \sin \omega_n t \neq 0$ since, there is some amplitude for a vibrational body.

$$-m\omega_n^2 + k = 0$$

$$m\omega_n^2 = k$$

$$\omega_n^2 = \frac{k}{m}$$

$$\boxed{\omega_n = \sqrt{\frac{k}{m}}} \quad \text{following eqn}$$

where, ω_n = natural frequency

* Units : radian/second | $k \rightarrow \text{N/m}$

Derive the response for SDOF for undamped system
Assume a solution

$$x(t) = A \sin \omega_n t + B \cos \omega_n t$$

where, A, B are constants obtained from initial conditions

$$x(t) \text{ at time } t=0 \text{ is } x_0$$

$$\dot{x}(t) \text{ at time } t=0 \text{ is } u_0 \quad \text{--- initial velocity}$$

$$x(t) \text{ at } t=0 \text{ is } x_0 = A \sin \omega_n \cdot 0 + B \cos \omega_n \cdot 0$$

$$x_0 = B \cdot 1 = B$$

$$\ddot{x}(t) = Aw_n \cos \omega_n t - B\omega_n \sin \omega_n t$$

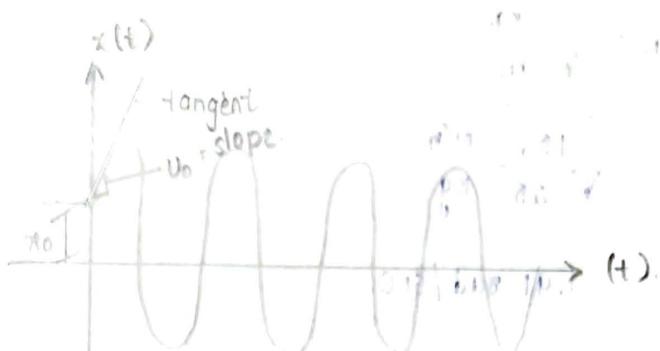
$$u_0 = Aw_n \cos \omega_n \cdot 0 - B\omega_n \sin \omega_n \cdot 0$$

$$u_0 = Aw_n$$

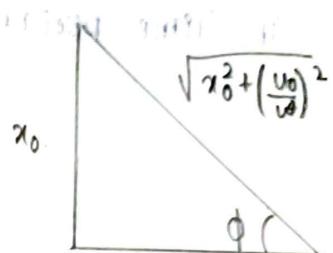
$$A = \frac{u_0}{\omega_n}$$

$$\therefore x(t) = A \sin \omega t + B \cos \omega t$$

$$x(t) = \frac{U_0}{\omega} \sin \omega t + \frac{x_0}{\omega} \cos \omega t$$



$$x(t) = \sqrt{x_0^2 + \left(\frac{U_0}{\omega}\right)^2} \frac{\frac{U_0}{\omega}}{\sqrt{x_0^2 + \left(\frac{U_0}{\omega}\right)^2}} \sin \omega t + \frac{x_0}{\sqrt{x_0^2 + \left(\frac{U_0}{\omega}\right)^2}}$$



$$\frac{x_0}{\sqrt{x_0^2 + \left(\frac{U_0}{\omega}\right)^2}} \cos \omega t$$

$$x(t) = \sqrt{x_0^2 + \left(\frac{U_0}{\omega}\right)^2} \left[\cos \phi \sin \omega t + \sin \phi \cos \omega t \right]$$

$$x(t) = \sqrt{x_0^2 + \left(\frac{U_0}{\omega}\right)^2} \sin(\omega t + \phi)$$

$$x(t) = R \sin(\omega t + \phi)$$

where, R = maximum amplitude

Determine the nature & frequency of a system shown in figure. A weight of 250 N is connected to a cantilever beam of stiffness $K_1 = 72.34 \text{ N/cm}$ through a spring stiffness of 20 N/cm

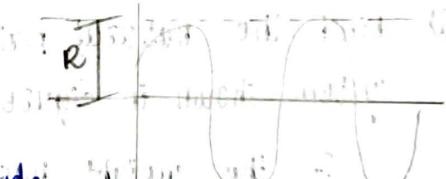
$$K_{eq} = \frac{K_1 K_2}{K_1 + K_2}$$

$$= \frac{72.34 \times 20}{72.34 + 20}$$

$$= \frac{1446.8}{92.34}$$

$$= 15.67 \text{ N/cm} = 15.67 \text{ N/10}^{-2} \text{ m}$$

$$= 1567 \text{ N/m}$$



$$K_1 = 72.34 \text{ N/cm}$$

$$K_2 = 20 \text{ N/cm}$$

$$W = 250 \text{ N}$$

$$m = \frac{w}{g}$$

$$= \frac{850}{10} = 85 \text{ kg}$$

$$\omega_n = \sqrt{\frac{k_e a}{m}}$$

$$= \sqrt{\frac{1567 \text{ N/m}}{85 \text{ kg}}}$$

$$= 7.91 \text{ rad/sec.}$$

In Time period, $T = \frac{2\pi}{\omega_n}$

$$= \frac{2 \times 3.14}{7.91}$$

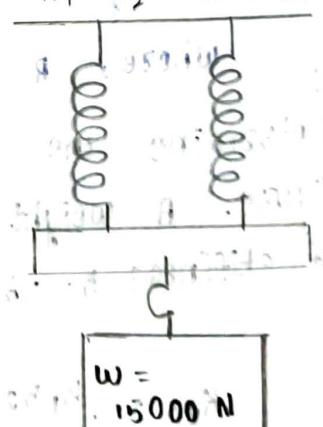
$$= 0.79 \text{ sec. or}$$

Cycles per second, $f = \frac{1}{T}$

$$= \frac{1}{0.79} \text{ cycles/sec. (Hz)}$$

- a) Find the natural period and frequency of oscillations for the system shown in figure.

If the weight has initial displacement $y_0 = 2.5 \text{ cm}$ and an initial velocity $v_0 = 50 \text{ cm/sec}$ determine the displacement and velocity after 1 second. Find Amplitude of vibration.



$$k_{eq} = k_1 + k_2$$

$$= 8000 \text{ N/cm}$$

$$= 8000 \times 10^2 \text{ N/m}$$

$$\omega_n = \sqrt{\frac{k_{eq}}{m}}$$

$$m = \frac{W}{g}$$

$$= \frac{15000}{10} = 1500 \text{ kg}$$

$$\omega_n = \sqrt{\frac{8 \times 10^5}{1500}}$$

$$\omega_n = 23.09 \text{ rad/sec.}$$

$$\begin{aligned} \text{Time period, } T &= \frac{2\pi}{\omega_n} \\ &= \frac{2 \times 3.14}{23.09} \\ &= 0.27 \text{ sec} \end{aligned}$$

$$\begin{aligned} \text{frequency, } f &= \frac{1}{T} \\ &= \frac{1}{0.27} \\ &= 3.7 \text{ cycles/sec.} \end{aligned}$$

$$\begin{aligned} x(t) &= \frac{v_0}{\omega_n} \sin \omega_n t + i x_0 \cos \omega_n t \\ x(t=1) &= \frac{50 \times 10^3}{23.09} \times \sin(23.09)(1) + 25 \times 10^3 \cos(23.09)(1) \\ &= 21.65 \times \sin(23.09) + 25 \cos(23.09) \\ &= 21.65 \times [-0.892] + 25 \times [-0.45] \\ &= -19.3118 - 11.25 \\ &= -30.56 \text{ mm} \end{aligned}$$

$$\begin{aligned} \dot{x}(t=1) &= \frac{v_0}{\omega_n} \cos \omega_n t \times \omega_n - i x_0 \sin \omega_n t \times \omega_n \\ &= 500 \cos(23.09 \times 1) - 25 \times 23.09 \times \sin(23.09 \times 1) \\ &= 500 [-0.45] - 577.25 [-0.892] \\ &= -225 + 514.907 \\ &= 286.75 \text{ mm/sec} \end{aligned}$$

Maximum amplitude,

$$R = \sqrt{x_0^2 + \left(\frac{v_0}{\omega}\right)^2}$$

$$\begin{aligned}
 R &= \sqrt{(0.25)^2 + \left(\frac{500}{23.09}\right)^2} \\
 &= \sqrt{62.5 + 468.8} \\
 &= \sqrt{531.3} \\
 &= 23.09 \text{ mm}
 \end{aligned}$$

Impact loading

$$\text{Weight} = W$$

$$\text{Height} = h$$

$$\text{Maximum deflection, } \Delta_{\max} = \Delta_{st} \left[1 + \sqrt{1 + 2\left(\frac{h}{\Delta_{st}}\right)} \right]$$

It is maximum displacement in a spring because of weight 'W' falling from height 'h'.

$$\text{Work done} = \text{PE of spring}$$

$$W(h + \Delta_{\max}) = \frac{1}{2} K \Delta_{\max}^2$$

$$\Delta_{st} = \text{static displacement} = \frac{W}{K}$$

$$K = \text{stiffness in N/m}$$

$$W = \text{Weight in N}$$