Development of detumbling prototype for a 1U CubeSat

## 1. Introduction

Add intro here

### 2. Cubesat simulation

Before developing flight ready CubeSat, it is necessary to simulate the CubeSat in a virtual environment. Initially we had to develop an open source simulation script in Matlab for determining the global position, angular dynamics, detumbling effects etc which is catered to meet our requirements and specifications. The script was created based on "Space flight Mechanics" written by Dr. Carlos Jos´e Montalvo, University of South Alabama as well as his Matlab scripts from his official repository. The entire code is available on github at https://github.com/NEONGASHMEN/arduinodemo1U

### 2.0.1 Assumptions and reference values for the CubeSat

Orbital inclination =  $98^{\circ}$ Mass of CubSat = 2kg

Mass moment of inertia, 
$$M_{3\times3} = \begin{bmatrix} 0.006 & 0 & 0 \\ 0 & 0.006 & 0 \\ 0 & 0 & 0.006 \end{bmatrix}$$

Maximum magnetic moment from Magnetorquer =  $0.2Am^2$ Resolution of the Magnetorquer = 256 (8bit)

The magnetic field model chosen was IGRF. General gravitational model is formulated where the gravitational perturbations from celestial bodies other than earth is neglected. Atmospheric drag as well as solar pressure is neglected.

### 2.0.2 The control algorithm for the simulation

The first step in our workflow was to define an arbitary earth centered, non - rotating reference frame. CubeSat parameters shall be defined with respect to this reference frame. On this reference frame the Z-axis points towards the north pole and the X-axis points towards the equator through the Prime Meridian. The conversion between the aforementioned reference frame to the real world latitude and longitudes the equations given in 6.1 and 6.2 can be used.

The next step is to derive initial conditions for the CubeSat, referenced as initial state. Initial state is an array constituting of 13 elements.

 $X_i, Y_i, Z_i$  are position coordinates given by (500,0,0) for 500km altitude at prime meridian

 $V_{xi}, V_{yi}, V_{zi}$  are velocity components with respect to body frame given by 6.3  $q_{0i}, q_{1i}, q_{2i}, q_{3i}$  are initial quarternions of CubeSat with respect to its body frame, initially taken as zero.

 $w_{xi}, w_{yi}, w_{zi}$  are initial angular velocities of CubeSat, initially taken as  $10 \deg/s$ .

Runge Kutta 4 method of iteration 6.5 is used to find out consecutive states during the satellte's orbit. A partial differential eqution which yields the state parameters are fed to the RK-4 algorithm and iterated for consecutive timesteps to obtain the state parameters at consecutive timesteps. The PDE is of the form;

$$\frac{d[S]}{dt} = f([S], t) \quad \& \quad [S]_{t=0} = [S]_0$$

and f() is given by,

$$\left(\frac{dX}{dt}, \frac{dY}{dt}, \frac{dZ}{dt}\right)_{t_i} = V_{t_{i-1}}$$

$$\left(\frac{d^2X}{dt^2}, \frac{d^2Y}{dt^2}, \frac{d^2Z}{dt^2}\right)_{t_i} = -\left(\frac{GM}{r^2}\right)\hat{r}$$

$$\left(\frac{dQ_0}{dt}, \frac{dQ_1}{dt}, \frac{dQ_2}{dt}, \frac{dQ_3}{dt}\right)_{t_i} = \omega_{t_{i-1}}$$

(Obtained from Euler angles to quarternions conversion 6.6)

$$\left(\frac{d^2\omega}{dt^2}\right) = I^{-1}(T_m)$$

(From rotational inertial equation 6.4)

Here the torque from magnetorquers  $T_m$  is computed from B-dot control algorithm. The algorithm takes in the current angular velocity of the CubeSat and the magnetic field around the satellite to determine the required magnetic moment that is to be produced by the Magnetorquer, inorder to achieve efficient detumbling. The B-dot algorithm states that the magnetic moment that is to be produced should be mututally perpendicular to the angular velocity vector  $(\vec{\omega})$  and the Earth's magnetic field  $(\vec{B})$ . To emulate real world noissy sensors, a random noise generation is also hard coded in the script. This gives magnetic field (magnetometer sensor) with an error of few microteslas as well as angular velocity (gyro-error) with an error of few milli radians. This gave us the opportunity to implement a filtering algorithm which minimises the error. A modified Kalman filter is employed 6.7 - combining the current sensor data and previous sensor value, thereby smoothening any steep variations in the measured value. This corrected data is fed to the B-dot algorithm.

$$\vec{\mu} = k. \left( \vec{B} \times \vec{\omega} \right)$$

Here the control variable k can be adjusted as per the mission's requirements to fine tune the rate of detumbling. In our case k is adjusted to generate magnetic moments between -0.2 to  $0.2Am^2$ . In the script, the IGRF model is used to obtain the magnetic field at current location. The torque produced, in the magnetometer is given by,

$$\vec{T_m} = \vec{\mu} \times \vec{B}$$

Each consecutive states are stored in each iteration of timestep. For post processing, the numerical values are exported as excel and for visualisation, plotted in a graph.

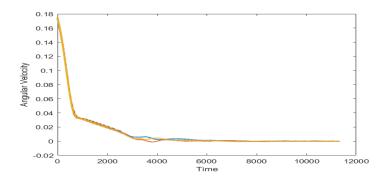
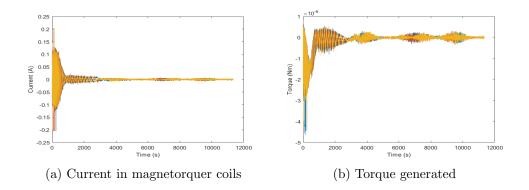


Figure 2.1: Decrease in Cubesat's angular velocity



From these results, the duration for detumbling from  $\vec{\omega}=10\hat{i}+10\hat{j}+10\hat{k}$  (in degrees) to  $\vec{\omega}=0.01\hat{i}+0.013\hat{j}+0.01\hat{k}$  was found to be 106.7667 mins (1.132 orbits) 2.1. Plot between Angular velocity of the CubeSat, Current in each magnetorquers and Torque produced from each torquers V/S time in seconds is given above 2.2a2.2b.

### 3. Miniature model of helmholtz

add a small description

### 3.0.1 Aim

To build a miniature model of helmholtz coil inorder to check whether the theoretical value of the magnetic field at the centre of helmholtz coil is equal to the practical value.

### 3.0.2 Procedure

First we made a miniature structure of helmholtz by 3D printing it with ABS(Acrylonitrile Butadiene Styrene) with diameter 10cm with 28 AWG copper wire.

We tested it and proved that the theoretical value of the magnetic field at the centre of the two coils is equal to the practical value of magnetic field measured using EMF detector.

The formula used to calculate the theoretical value of magnetic field at the centre of two coils is given below

$$B\left(\frac{R}{2}\right) = 2B_1\left(\frac{R}{2}\right)$$

$$= \frac{2\mu_0 n I R^2}{2\left(R^2 + \left(\frac{R}{2}\right)^2\right)^{\frac{3}{2}}} = \frac{\mu_0 n I R^2}{\left(R^2 + \left(\frac{R}{2}\right)^2\right)^{\frac{3}{2}}}$$

$$= \frac{\mu_0 n I R^2}{\left(R^2 + \frac{1}{4}R^2\right)^{\frac{3}{2}}} = \frac{\mu_0 n I R^2}{\left(\frac{5}{4}R^2\right)^{\frac{3}{2}}}$$

$$= \left(\frac{4}{5}\right)^{\frac{3}{2}} \frac{\mu_0 N I}{R}$$

$$= \frac{8}{5\sqrt{5}} \frac{\mu_0 N I}{R}$$

Where n=number of turns I= current (measured using multi meter) R=radius of the Helmholtz coil.

### 3.0.3 Result

We proved that the theoretical and practical values of magnetic field are the same.

# 4. Designing and testing the magnetorquer using iron core

In this design we used iron as the core with diameter 5.5mm and number of turns 1088 and gauge 28SWG.

We tested it theoretically using the code written by ourself and practically using the magnetometer. Both the tests did not yield the desired result. So we decided to use Stainless steel FR430 instead of iron core and change the number of turns to 350.

- 4.0.1 Procedure
- 4.0.2 Inference
- 4.0.3 Result

# 5. Designing the actual Helmholtz Coil

description

### 5.0.1 Aim

### 5.0.2 Components used:

- Plywood frame with diameter 50cm
- 14SWG Copper wire

#### 5.0.3 Procedure

We wound the wire around the plywood frame ,150 turns per coil, which was calculated from the formula. The Helmholtz coil is designed to produce  $8\mathrm{mT}$  magnetic field and current .

### 5.0.4 Inference

#### 5.0.5 Result

## 6. Equations

$$\rho = \sqrt{x^2 + y^2 + z^2}$$

$$\theta_E = \cos^{-1}\left(\frac{z}{\rho}\right)$$

$$\psi_E = \tan^{-1}\left(\frac{y}{x}\right)$$
Cartesian to spherical coordinate conversion
$$(6.1)$$

$$\lambda_{LAT} = 90 - \theta_E \frac{180}{\pi} 
\lambda_{LON} = \psi_E \frac{180}{\pi} 
h = \rho - R_E$$
Latitude, Longitude and height (6.2)

$$v = \sqrt{\mu \left(\frac{2}{r} - \frac{1}{a}\right)}$$
 Vis-viva equation, NB: for the simulation  $a \approx r$  (6.3)

$$\dot{\vec{\omega}} = I^{-1} \left( T_{Propulsion} + T_{Magnetorquer} + T_{Reactionwheel} - \dot{\vec{\omega}} \times \vec{H} - \dot{I}\vec{\omega} \right)$$
(6.4)

If, 
$$\frac{dy}{dx} = f(t_n, y_n)$$
 and  $y(t_n) = y_n$   
 $k_1 = f(t_n, y_n)$   
 $k_2 = f\left(t_n + \frac{h}{2}, y_n + h\frac{k_1}{2}\right)$   
 $k_3 = f\left(t_n + \frac{h}{2}, y_n + h\frac{k_2}{2}\right)$   
 $k_4 = f(t_n + h, y_n + hk_3)$   
 $k = \frac{1}{6}(k_1 + 2k_2 + 2k_3 + k_4)$   
 $y(t_n + h) = y_n + hk$  (6.5)

$$\begin{bmatrix} q_0 \\ q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} \cos\left(\frac{\phi}{2}\right)\cos\left(\frac{\theta}{2}\right)\cos\left(\frac{\psi}{2}\right) + \sin\left(\frac{\phi}{2}\right)\sin\left(\frac{\theta}{2}\right)\sin\left(\frac{\psi}{2}\right) \\ \sin\left(\frac{\phi}{2}\right)\cos\left(\frac{\theta}{2}\right)\cos\left(\frac{\psi}{2}\right) - \cos\left(\frac{\phi}{2}\right)\sin\left(\frac{\theta}{2}\right)\sin\left(\frac{\psi}{2}\right) \\ \cos\left(\frac{\phi}{2}\right)\sin\left(\frac{\theta}{2}\right)\cos\left(\frac{\psi}{2}\right) + \sin\left(\frac{\phi}{2}\right)\cos\left(\frac{\theta}{2}\right)\sin\left(\frac{\psi}{2}\right) \\ \cos\left(\frac{\phi}{2}\right)\cos\left(\frac{\theta}{2}\right)\sin\left(\frac{\psi}{2}\right) - \sin\left(\frac{\phi}{2}\right)\sin\left(\frac{\theta}{2}\right)\cos\left(\frac{\psi}{2}\right) \end{bmatrix} \end{bmatrix}$$
Euler to Quarternion conversion (6.6)

$$X_{filtered} = S.X_{current} + (1 - S) X_{previous}$$
 ,  $0 < S < 1$ , S being the sensor reliability (6.7)