

Sheet: /  
File: PWM Ramp Gen Prototype.kicad\_sch

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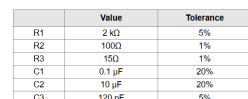
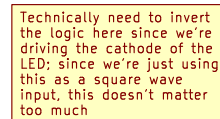
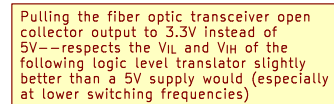
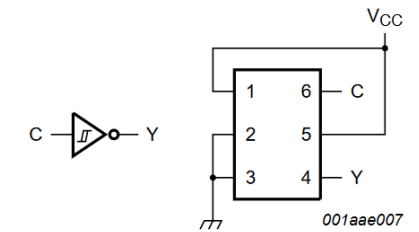
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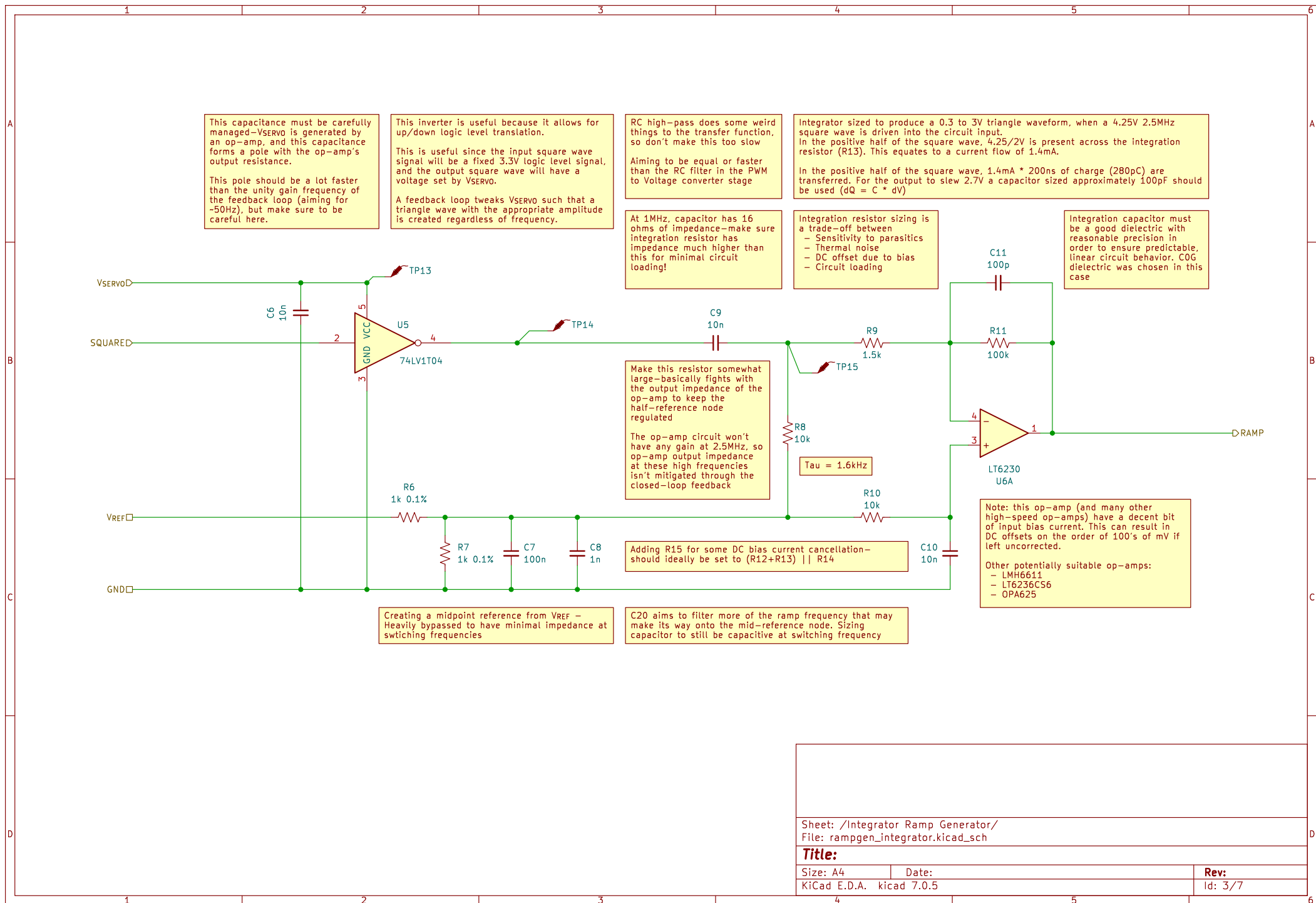
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There's a couple different part numbers that may be relevant (e.g. AFBR-15x8) but it's so difficult to parse their differences so I did.

I've designed this interface circuit in an attempt to be as generic and part-agnostic as possible, but make sure to verify circuit functionality

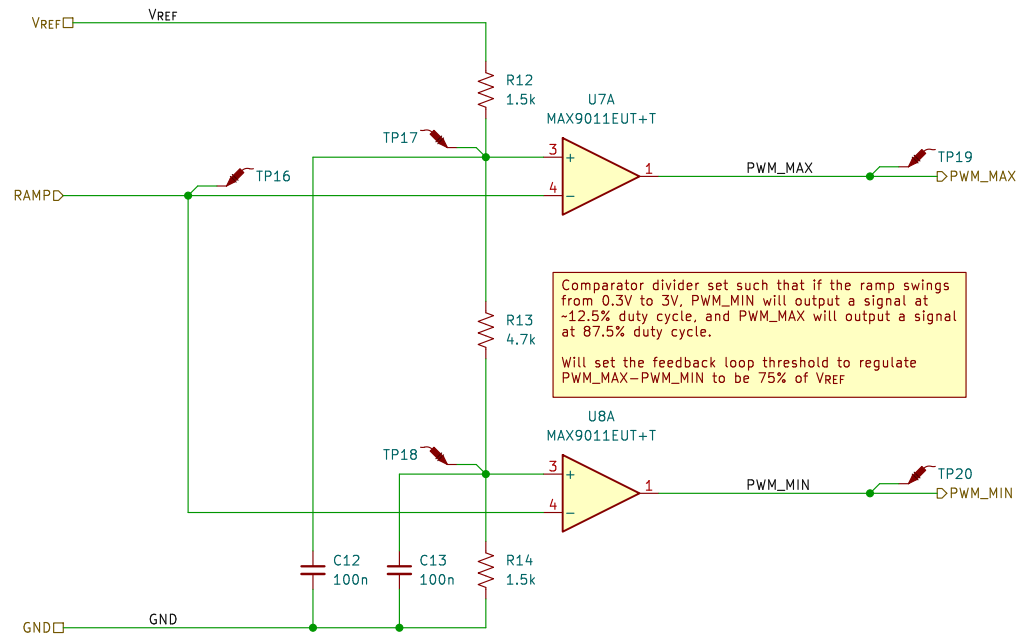


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Selecting the TLV3502 due to:

- high speed
- low propagation delay
- no weird business w.r.t. input differential mode range (I think)
- pinout compatibility with MAX9012 and MAX962
- Cost



Comparator divider set such that if the ramp swings from 0.3V to 3V, PWM\_MIN will output a signal at ~12.5% duty cycle, and PWM\_MAX will output a signal at 87.5% duty cycle.

Will set the feedback loop threshold to regulate PWM\_MAX-PWM\_MIN to be 75% of VREF

Sheet: /MinMax PWM Comparator/  
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Depending on the peak-peak ramp voltage coming out of the ramp generator, PWM\_MIN and PWM\_MAX will be set to certain duty cycles.

We want to regulate the difference between the MIN and the MAX duty cycles --> this corresponds to a particular voltage magnitude of the ramp function.

NOTE: ramp voltage --> PWM delta is a monotonic function, i.e. every ramp voltage value corresponds to a unique PWM delta.

In order to implement this analog regulator, we'll first create a waveform representing the difference between the PWM waveforms using a multi-function logic gate. We'll then take the average value of this synthesized PWM waveform using an RC lowpass filter. This will yield us a voltage representing the difference between the high and low PWM values

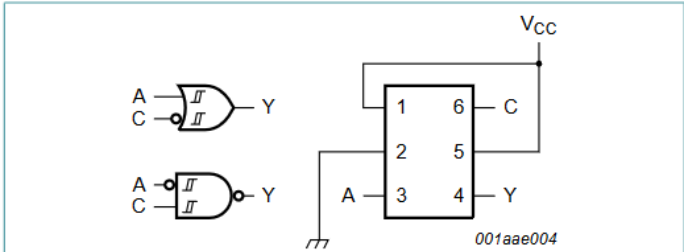
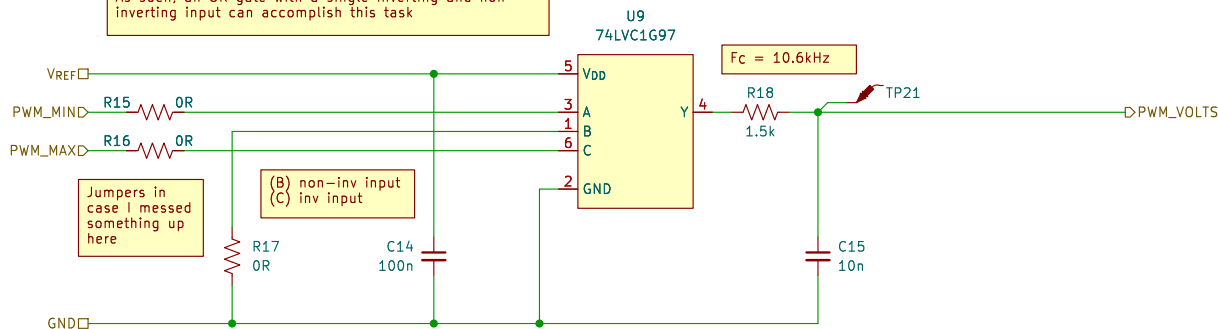
**IMPORTANT NOTE:** Instead of converting the "valid" PWM region to an analog voltage, I'm converting the "INVALID" region to an analog voltage.

Both of these transfer functions are nonlinear (have  $V_{servo}$  in the denominator). However, the PWM\_INVALID signal has a small-signal gain that's strictly positive. This is preferable because implementing the controller in the analog domain is significantly easier for forward path transfer functions with positive gains.

In order to generate the required PWM\_INVALID waveform, we'll use a multi-function gate. The output waveform is HIGH iff:

- PWM MAX is LOW
- or -
- PWM MIN is HIGH

As such, an OR gate with a single inverting and non inverting input can accomplish this task



**Fig. 8.** 2-input NAND gate with input A inverted or 2-input OR gate with input C inverted

Part of this ramp generator systems includes a servo feedback loop to ensure the ramp amplitude is nearly identical with different frequency inputs and across device drift and operating conditions

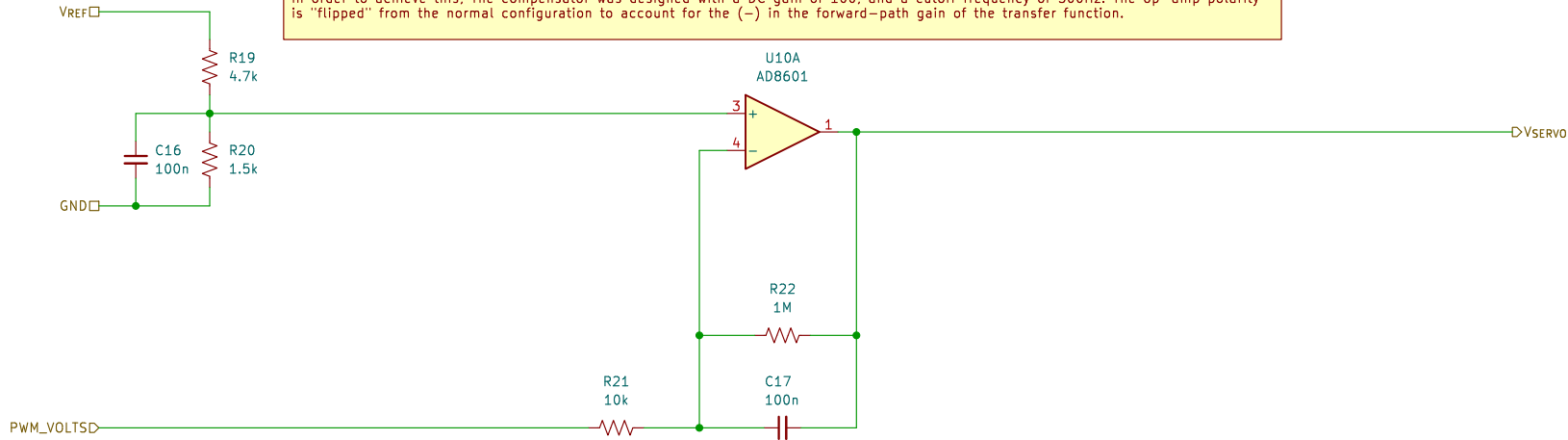
The servo system works as follows:

- Sets the drive voltage amplitude of the square wave going to the integrator circuit
- Integrator circuit generates a ramp with a corresponding amplitude
- Comparators referenced to a fractional level of the reference voltage generate min/max PWM waveforms for the power stages
- The difference between the min/max PWM waveforms is generated (max - min) via boolean operations
- The average value of this difference waveform is sent back to a compensation circuit
  - If the difference is too large, ramp voltage is too low (increase drive voltage supply)
  - If the difference is too small, ramp voltage is too high (decrease drive voltage supply)

Forward path of the plant is non-linear (transfer function is proportional to  $1/V_{DRIVE}$ ); forward path gain also varies with operating frequency (decreases at higher operating frequencies). Calculated linearized forward path gain at the desired operating point is  $-1.1389V/V$  @1.25MHz and  $-0.565V/V$  with the current operating parameters. There's a single pole in the forward path set by the frequency of the RC PWM --> Voltage conversion filter (currently 10.6kHz).

We want the crossover frequency of the open-loop transfer function to be at most one decade below this (~1kHz) to ensure minimal overshoot of the controller step response.

In order to achieve this, The compensator was designed with a DC gain of 100, and a cutoff frequency of 500Hz. The op-amp polarity is "flipped" from the normal configuration to account for the (-) in the forward-path gain of the transfer function.



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