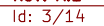
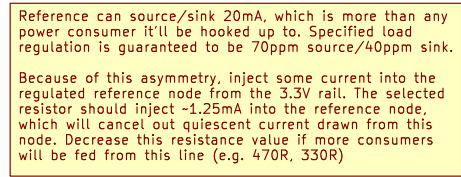
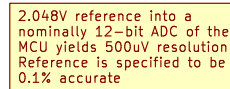
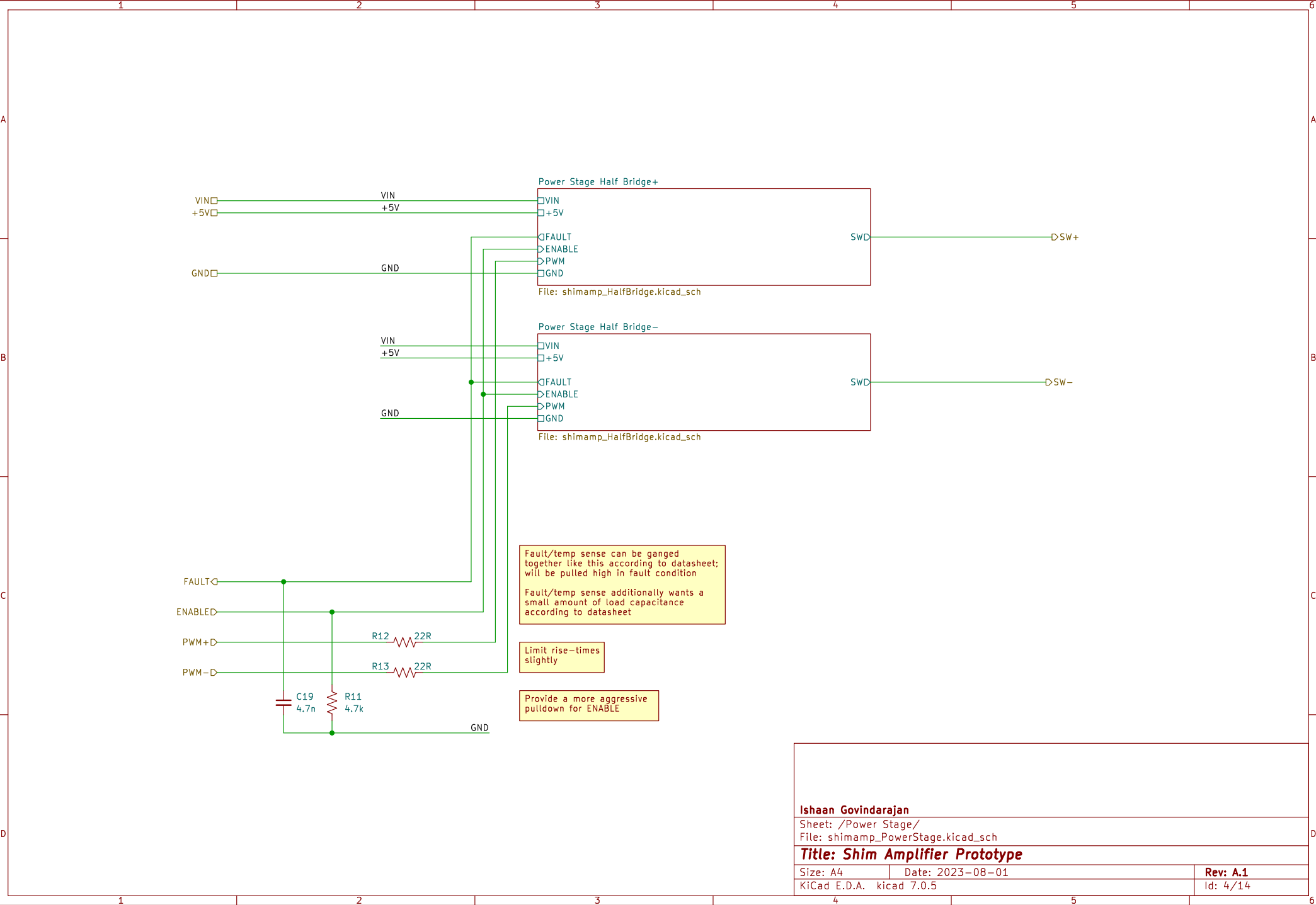


VIN\_RPP+ TP1  
VIN\_ICL+ TP2  
VIN\_RPP- TP3  
GND TP4  
VIN TP5  
GND TP6

In this configuration, power will mostly need to be dissipated in the 5V regulator. A TO-263 package was selected (in order to decrease assembly complexity compared to a TO-220 package). Datasheets suggest that this IC should safely be able to dissipate 3W of power, equating to ~425mA pulled from a 12V source.

RC filter to mitigate bootstrap charging ripple; also reduces the amount of power dissipation in the 3.3V regulator by dropping some voltage.





Ceramic bypassing for low ESR and ESL, these capacitors still work at  $f_{sw}$  of 1.25MHz (but barely). I'm including other, smaller capacitors to provide bypassing at higher frequencies to filter switching harmonics

Expecting ripple voltage amplitude <100mV at full load; input power supply filter should further reduce this

Worst-case combined power stage dissipation is ~7.68W when:

- Outputting near the supply voltage rail (i.e. high duty cycles)
- Outputting 20A load current

Nominal dissipation expected to be ~2-3W combined when driving 100-200mR shim coils

VDD also needs good bypassing - bootstrap capacitor is charged from the VDD pin

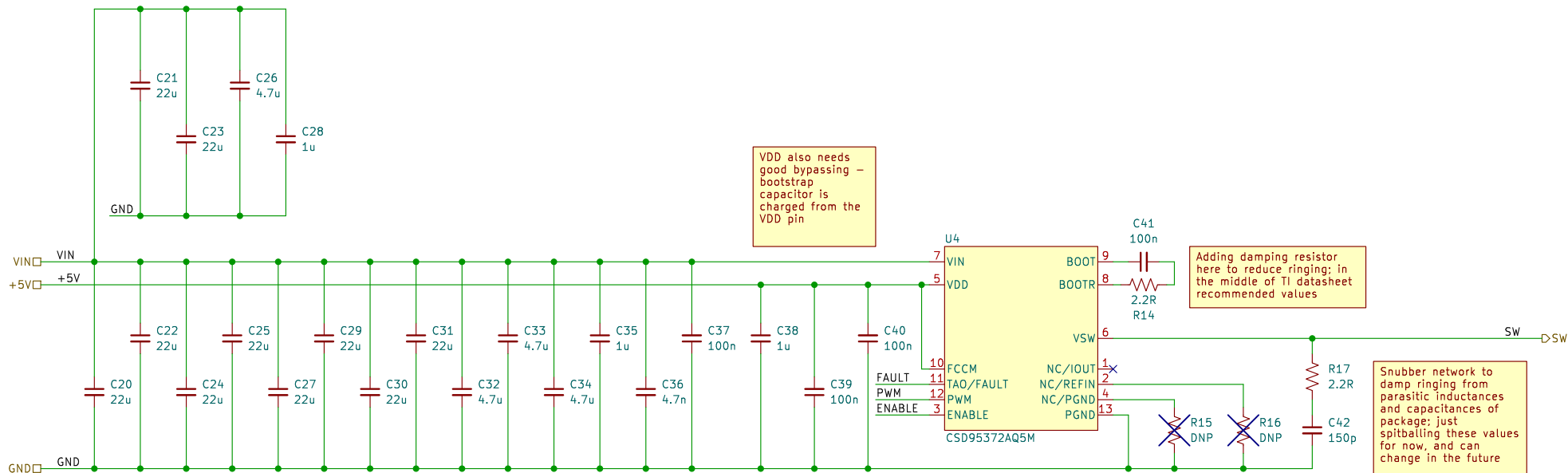
Adding damping resistor here to reduce ringing; in the middle of TI datasheet recommended values

Snubber network to damp ringing from parasitic inductances and capacitances of package; just spitballing these values for now, and can change in the future

Rate for 1/4W for a 20V bridge voltage, 1.25MHz  $f_{sw}$

Force CCM in order to have predictable frequency spectrum

DNP for pin-compatibility with other parts in family (CSD95372Bxxx)



PWM  $\rightarrow$  PWM  
FAULT  $\rightarrow$  FAULT  
ENABLE  $\rightarrow$  ENABLE

VIN  $\rightarrow$  TP13  
GND  $\rightarrow$  TP14

Ishaan Govindarajan

Sheet: /Power Stage/Power Stage Half Bridge+/  
File: shimamp\_HalfBridge.kicad\_sch

**Title: Shim Amplifier Prototype**

Size: A4 Date: 2023-08-01  
KiCad E.D.A. kicad 7.0.5

Rev: A.1  
Id: 5/14

Ceramic bypassing for low ESR and ESL, these capacitors still work at  $f_{sw}$  of 1.25MHz (but barely). I'm including other, smaller capacitors to provide bypassing at higher frequencies to filter switching harmonics

Expecting ripple voltage amplitude <100mV at full load; input power supply filter should further reduce this

Worst-case combined power stage dissipation is ~7.68W when:

- Outputting near the supply voltage rail (i.e. high duty cycles)
- Outputting 20A load current

Nominal dissipation expected to be ~2-3W combined when driving 100-200mR shim coils

VDD also needs good bypassing - bootstrap capacitor is charged from the VDD pin

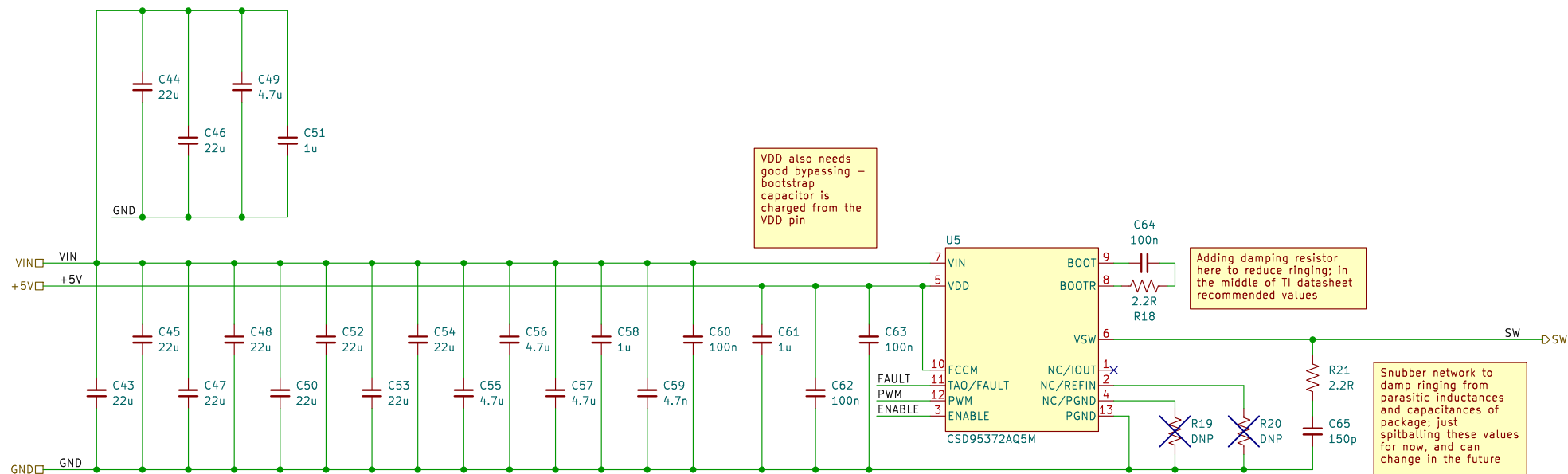
Adding damping resistor here to reduce ringing; in the middle of TI datasheet recommended values

Snubber network to damp ringing from parasitic inductances and capacitances of package; just spitballing these values for now, and can change in the future

Rate for 1/4W for a 20V bridge voltage, 1.25MHz  $f_{sw}$

Force CCM in order to have predictable frequency spectrum

DNP for pin-compatibility with other parts in family (CSD95372Bxxx)



Ishaan Govindarajan

Sheet: /Power Stage/Power Stage Half Bridge-/  
File: shimamp\_HalfBridge.kicad\_sch

**Title: Shim Amplifier Prototype**

Size: A4 Date: 2023-08-01  
KiCad E.D.A. kicad 7.0.5

Rev: A.1  
Id: 6/14

VIN TP15  
GND TP16

Calculations for this filter (and control design) can be found under the 'simulations' folder in my Dropbox



Output filter is implemented as two common-mode filters (which have a byproduct of also attenuating differential mode). Each sheet contains one half of the filter.

**Ishaan Govindarajan**

Sheet: /Output Filter/

File: shimamp\_OutputFilter.kicad\_sch

**Title: Shim Amplifier Prototype**

Size: A4 Date: 2023-08-01

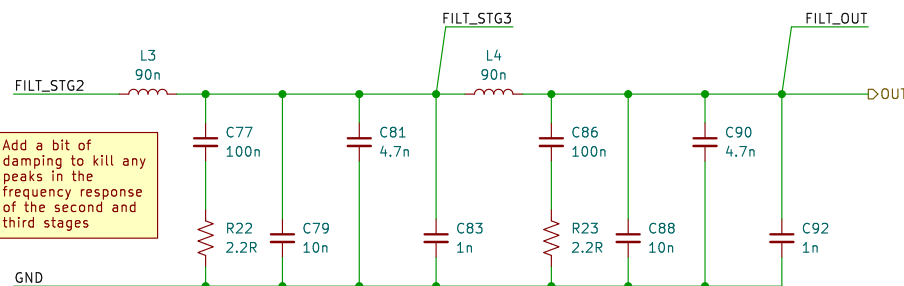
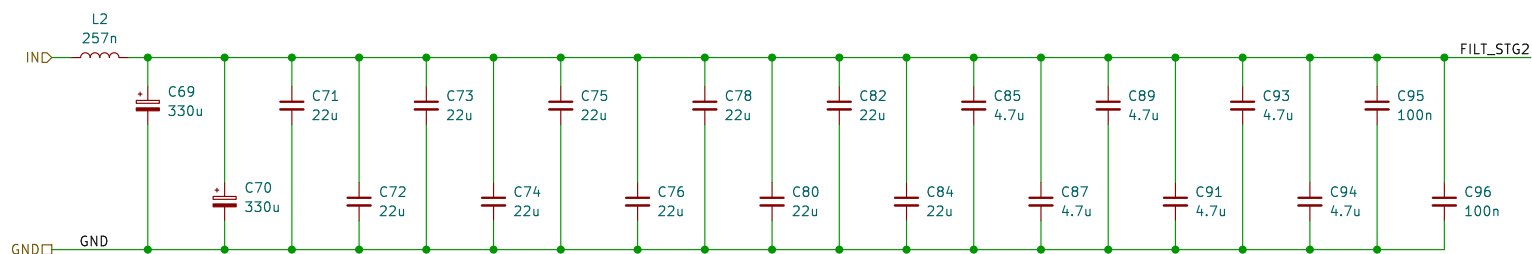
KiCad E.D.A. kicad 7.0.5

**Rev: A.1**

Id: 7/14

This is one half of a 3-stage, 6th-order filter that provides both differential and common-mode filtering. Since the control loop bandwidth is greater than the resonant frequency of the first filter stage, it can remain undamped. However, this is not the case with the second and third stages, requiring the inclusion of a damping leg. These were applied across the shunt elements in order to not compromise the filtering efficacy. Not a ton of design optimization went into the selection of damping components, so design may be suboptimal. Rough simulations check out, however, and no resonant peaks are present in an unloaded output.

Calculations for this filter (and control design) can be found under the 'simulations' folder in my Dropbox



Paralleled aluminum polymer capacitors for lower ESR and higher ripple rating; good for 100's of kHz;  
Inductor Ripple current ~4.75A worst case (50% duty cycle) with 12V supply, 1.25MHz switching; should result in <40mV ripple at the end of the first stage

- Aluminum Poly caps are good up to about ~2-300kHz
- 22u ceramics are good to ~1MHz
- 4.7u, 1u ceramics are good to ~8MHz
- 100n ceramics are good to ~20MHz
- 10n ceramics resonate at ~80MHz
- 4.7n ceramics resonate at ~120MHz
- 1n ceramics resonate at ~280MHz

Ceramics will derate about 75% (i.e. 25% of their value) at 12V DC Bias  
Except for the 1u caps those only derate by 15% for whatever reason--it's not even like a tolerance reason; +/-10% 10u caps still aggressively derate at those levels of DC bias. I'll investigate if it's a capacitor family reason.

FILT\_STG2 TP17  
FILT\_STG3 TP18  
FILT\_OUT TP19  
GND TP20  
GND TP21  
GND TP22

In the board design, give the smallest capacitors the tightest loops; this will minimize parasitic inductance for those components where it matters most.

Ishaan Govindarajan

Sheet: /Output Filter/Output Filter+/  
File: shimamp\_OutputFilterHalf.kicad\_sch

**Title: Shim Amplifier Prototype**

Size: A4 Date: 2023-08-01

KiCad E.D.A. kicad 7.0.5

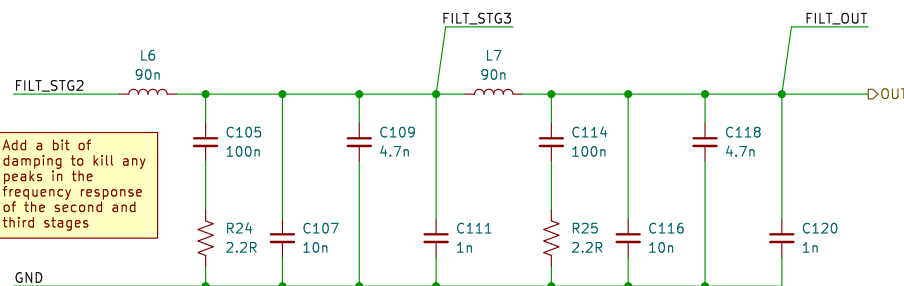
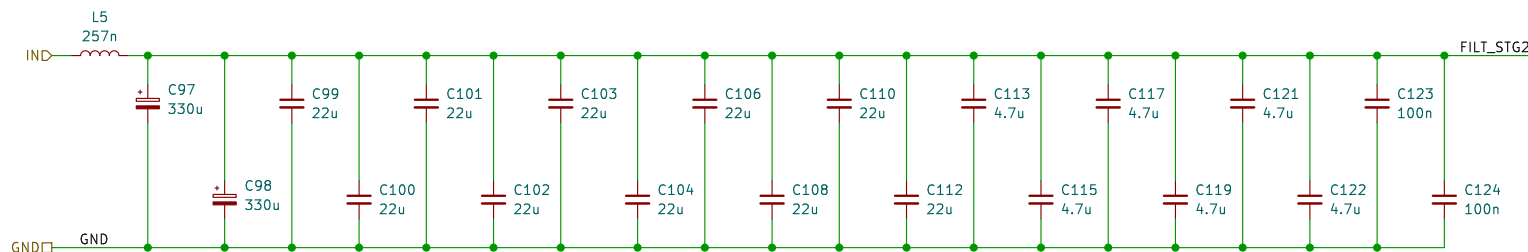
Rev: A.1

Id: 8/14



This is one half of a 3-stage, 6th-order filter that provides both differential and common-mode filtering. Since the control loop bandwidth is greater than the resonant frequency of the first filter stage, it can remain undamped. However, this is not the case with the second and third stages, requiring the inclusion of a damping leg. These were applied across the shunt elements in order to not compromise the filtering efficacy. Not a ton of design optimization went into the selection of damping components, so design may be suboptimal. Rough simulations check out, however, and no resonant peaks are present in an unloaded output.

Calculations for this filter (and control design) can be found under the 'simulations' folder in my Dropbox



Add a bit of damping to kill any peaks in the frequency response of the second and third stages

In the board design, give the smallest capacitors the tightest loops; this will minimize parasitic inductance for those components where it matters most.

Paralleled aluminum polymer capacitors for lower ESR and higher ripple rating; good for 100's of kHz;  
Inductor Ripple current ~4.75A worst case (50% duty cycle) with 12V supply, 1.25MHz switching; should result in <40mV ripple at the end of the first stage

- Aluminum Poly caps are good up to about ~2-300kHz
- 22u ceramics are good to ~1MHz
- 4.7u, 1u ceramics are good to ~8MHz
- 100n ceramics are good to ~20MHz
- 10n ceramics resonate at ~80MHz
- 4.7n ceramics resonate at ~120MHz
- 1n ceramics resonate at ~280MHz

Ceramics will derate about 75% (i.e. 25% of their value) at 12V DC Bias  
Except for the 1u caps those only derate by 15% for whatever reason--it's not even like a tolerance reason; +/-10% 10u caps still aggressively derate at those levels of DC bias. I'll investigate if it's a capacitor family reason.

FILT\_STG2 TP23  
FILT\_STG3 TP24  
FILT\_OUT TP25  
GND TP26  
GND TP27  
GND TP28

Ishaan Govindarajan

Sheet: /Output Filter/Output Filter-/  
File: shimamp\_OutputFilterHalf.kicad\_sch

Title: Shim Amplifier Prototype

Size: A4 Date: 2023-08-01

KiCad E.D.A. kicad 7.0.5

Rev: A.1

Id: 9/14

This schematic page captures the output voltage and current sensing circuitry. A feedback loop will be closed around both voltage and current, allowing for the stabilization of plants with slightly different dynamics. These sensors must provide minimal distortion up to the controllers' unity gain frequency while maximally attenuating energy at frequencies beyond. Additionally, sensing circuit must have good common-mode rejection (CMR) to minimize sensitivity to power stage switching.

To achieve these objectives, a fully-differential amplifier topology was chosen for voltage sensing. The fully-differential topology maximizes CMR (>75dB from the amplifier, more from the MCU, ADC), and allows for the implementation of a high-order active filter. The cutoff frequency of this filter was chosen such that it has near-zero phase up to the voltage controller crossover frequency (~40-50kHz). This improves stability and phase margin.

For current sensing, an INA241x series amplifier was chosen for its low offset, noise, and high CMR (~80dB @ 1MHz). Due to its higher CMR, current measurements will be made with a simpler single-ended sensing technique, filtered with a simpler first-order RC filter. The zero-current reference is selected to place a reading of 0A in the middle of the MCU ADC range.

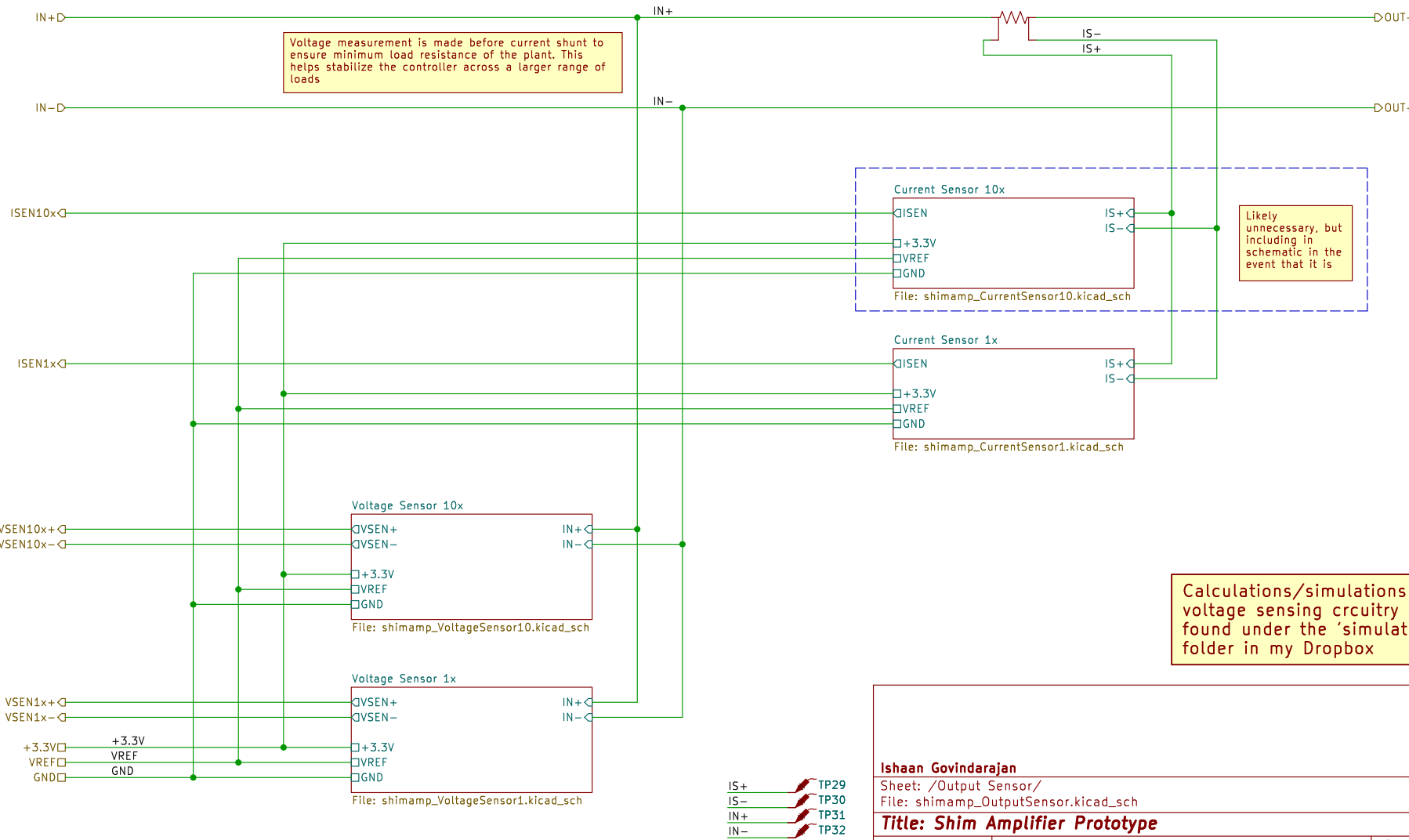
Additionally, both of these measurements benefit from a large dynamic range, and may run into resolution limits with the MCU's 12-bit ADC. As such, ADC channels may be "stacked"—one ADC channel will handle the full voltage/current range, and the other will handle measurements close to zero with a 10x greater resolution (at a cost of 10x reduced dynamic range). This measurement strategy is likely needed for voltage sensing, but may not be needed for current sensing.

Current shunt resistor sized for +/-10A; will dissipate ~1W, so power rating is derated for extra stability and general headroom  
Resistor specified at 1%, 20ppm/C

Voltage measurement is made before current shunt to ensure minimum load resistance of the plant. This helps stabilize the controller across a larger range of loads

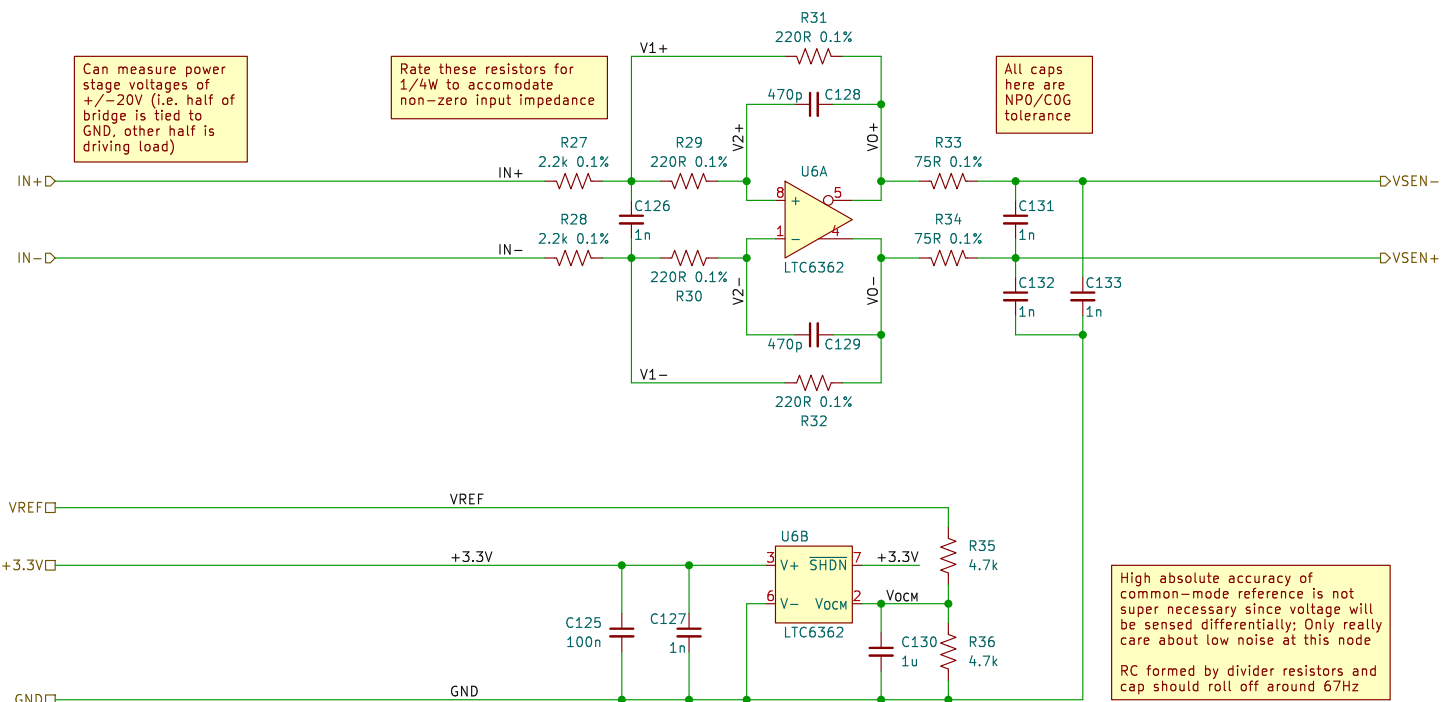
Likely unnecessary, but including in schematic in the event that it is

Calculations/simulations for the voltage sensing circuitry can be found under the 'simulations' folder in my Dropbox



3rd-order butterworth mutiple feedback filter with ~750kHz cutoff frequency (slight mismatch to the 10x amplifier), \*10x\* attenuation

Want high-accuracy resistors to ensure good matching between positive and negative branches; this ensures good CMR



Can measure power stage voltages of +/-20V (i.e. half of bridge is tied to GND, other half is driving load)

Rate these resistors for 1/4W to accomodate non-zero input impedance

All caps here are NP0/C0G tolerance

High absolute accuracy of common-mode reference is not super necessary since voltage will be sensed differentially; Only really care about low noise at this node

RC formed by divider resistors and cap should roll off around 67Hz

LTC6362 chosen for good offset/noise performance; THS453x may also be a good part candidate (similar pinout but slightly different package)

Ishaan Govindarajan

Sheet: /Output Sensor/Voltage Sensor 10x/  
File: shimamp\_VoltageSensor10.kicad\_sch

**Title: Shim Amplifier Prototype**

Size: A4 Date: 2023-08-01

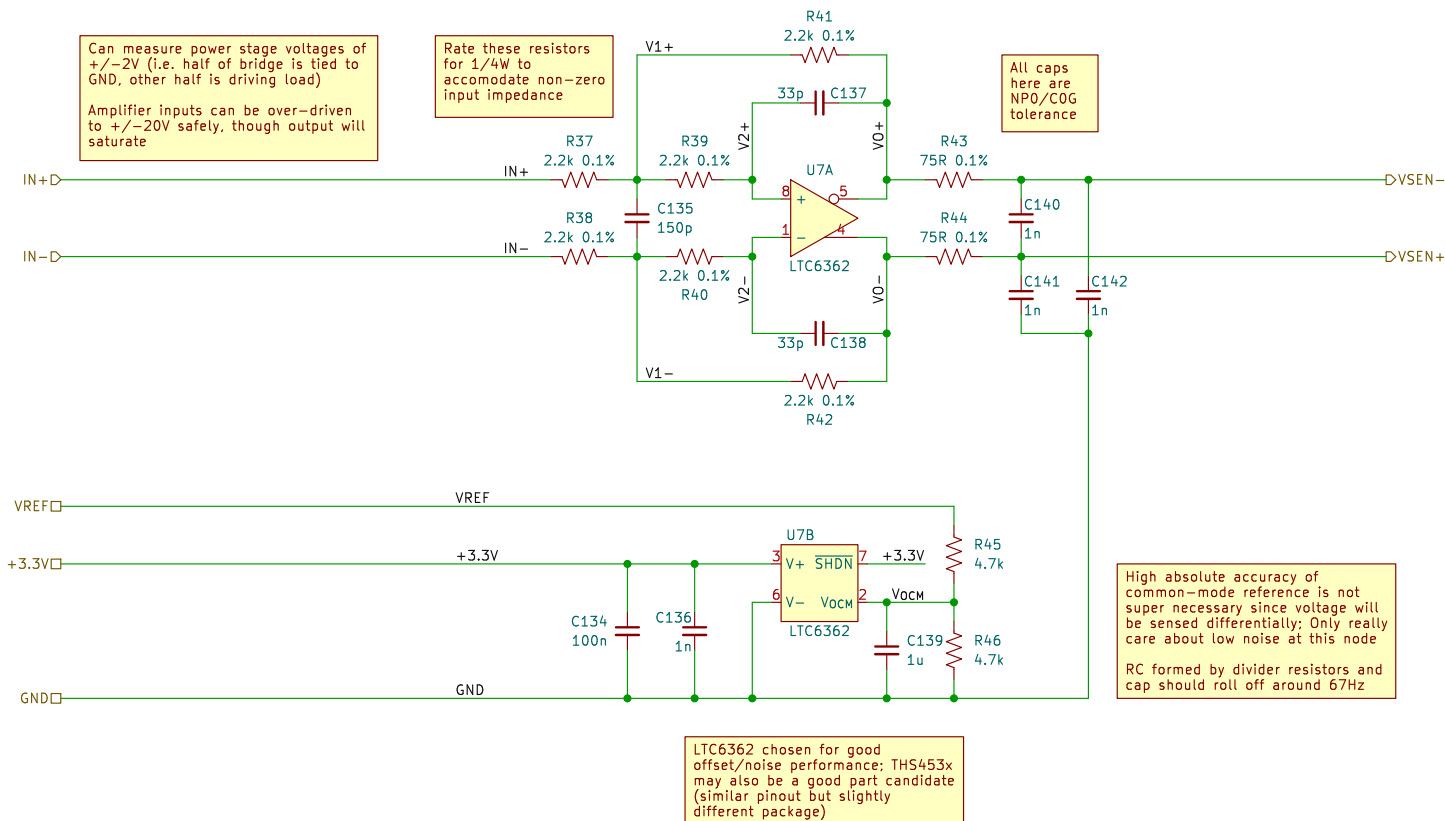
KiCad E.D.A. kicad 7.0.5

Rev: A.1

Id: 12/14

3rd-order butterworth mutple feedback filter with ~730kHz cutoff frequency (slight mismatch to the 10x amplifier), \*1x\* attenuation

Want high-accuracy resistors and capacitors to ensure good matching between positive and negative branches; this ensures good CMR



**Ishaan Govindarajan**

Sheet: /Output Sensor/Voltage Sensor 1x/

File: shimamp\_VoltageSensor1.kicad\_sch

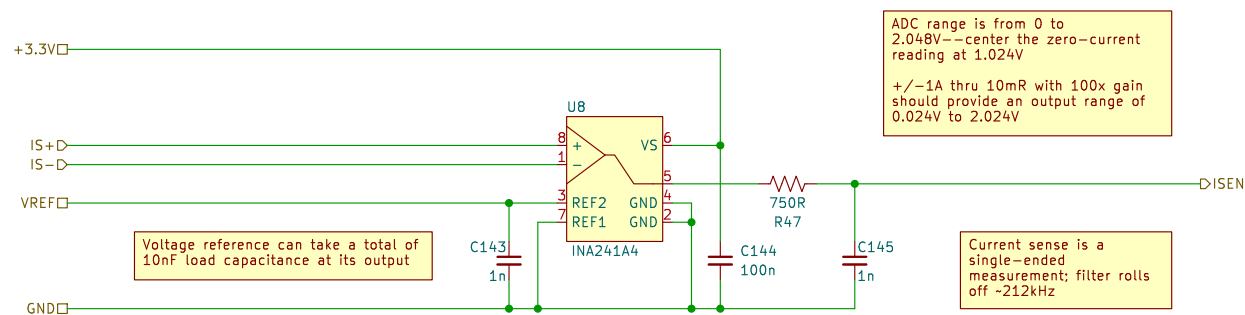
**Title: Shim Amplifier Prototype**

Size: A4 Date: 2023-08-01

KiCad E.D.A. kicad 7.0.5

**Rev: A.1**

Id: 13/14



**Ishaan Govindarajan**

Sheet: /Output Sensor/Current Sensor 10x/  
File: shimamp\_CurrentSensor10.kicad\_sch

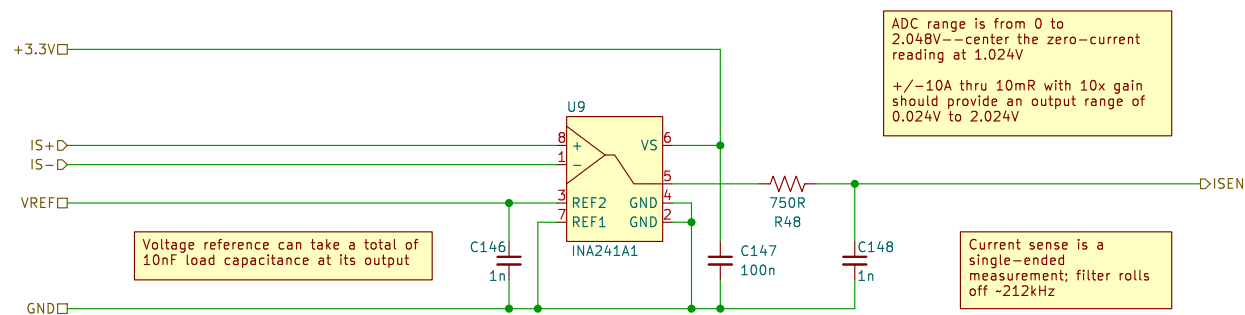
**Title: Shim Amplifier Prototype**

Size: A4 Date: 2023-08-01

KiCad E.D.A. kicad 7.0.5

**Rev: A.1**

Id: 14/14



Voltage reference can take a total of 10nF load capacitance at its output

Reference divider is like insanely (ratiometrically) accurate,  $\pm 0.005\%$  maximum for the grade of part specified in this schematic;

We'll never be able to easily generate something that accurate, so let's just leverage the chip's divider accuracy to generate the "zero-current reference voltage". This will center the amplifier output to be at half of the ADC range. It should be accurate enough that we don't even need to sense what the voltage actually is

ADC range is from 0 to 2.048V—center the zero-current reading at 1.024V

$\pm 10\text{A}$  thru  $10\text{mR}$  with  $10\times$  gain should provide an output range of 0.024V to 2.024V

Current sense is a single-ended measurement; filter rolls off  $\sim 212\text{kHz}$

Ishaan Govindarajan	
Sheet: /Output Sensor/Current Sensor 1x/	
File: shimamp_CurrentSensor1.kicad_sch	
Title: <b>Shim Amplifier Prototype</b>	
Size: A4	Date: 2023-08-01
KiCad E.D.A. kicad 7.0.5	Rev: <b>A.1</b>
	Id: 15/14