

① For a physical dipole with $-q$ at \vec{r} and $+q$ at $\vec{r} + \vec{d}$

$$U = qV(\vec{r} + \vec{d}) - V(\vec{r})$$

$$= q \left[- \int_{\vec{r}}^{\vec{r} + \vec{d}} \vec{E} \cdot d\vec{r} \right]$$

$$= -q \vec{E} \cdot \vec{d}$$

$$\boxed{U = -\vec{p} \cdot \vec{E}}$$

$$U = -\vec{p}_1 \cdot \vec{E}_2$$

$$\text{Bwl } \vec{E}_2 = \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} [3(\vec{p}_2 \cdot \hat{r})\hat{r} - \vec{p}_2]$$

$$\therefore U = \frac{1}{4\pi\epsilon_0} \frac{1}{r^3} [(\vec{p}_1 \cdot \vec{p}_2) - 3(\vec{p}_1 \cdot \hat{r})(\vec{p}_2 \cdot \hat{r})]$$

②

$$\rho_v = \begin{cases} \rho_0 & , 0 < r < a \\ 0 & , r > a \end{cases}$$

For $r < a$, $\epsilon E (4\pi r^2) = \rho_0 \frac{4}{3} \pi r^3$

$$\Rightarrow E = \frac{\rho_0 r}{3\epsilon}$$

$$\begin{aligned} \therefore V &= - \int \vec{E} \cdot d\vec{l} \\ &= - \int \frac{\rho_0 r}{3\epsilon} dr \\ &= - \frac{\rho_0}{3\epsilon} \left[\frac{r^2}{2} \right]_{\infty}^{\frac{r}{2}} + C_1 \\ &= - \frac{\rho_0 r^2}{6\epsilon} + C_1 \end{aligned}$$

For $r > a$, $\epsilon_0 E (4\pi r^2) = \rho_0 \frac{4}{3} \pi a^3$

$$\Rightarrow E = \frac{\rho_0 a^3}{3\epsilon_0 r^2}$$

$$\begin{aligned} \therefore V &= - \int \vec{E} \cdot d\vec{l} \\ &= - \int \frac{\rho_0 a^3}{3\epsilon_0 r^2} dr \\ &= - \frac{\rho_0 a^3}{3\epsilon_0} \left[\frac{-1}{r} \right] + C_2 \\ &= \frac{\rho_0 a^3}{3\epsilon_0 r} + C_2 \end{aligned}$$

Boundary condition

As $r \rightarrow \infty$ $V \rightarrow 0$ $\therefore C_2 = 0$

Also at $r = a$ $V(a^+) = V(a^-)$

$$-\frac{\rho_0 a^2}{6\epsilon} + C_1 = \frac{\rho_0 a^3}{3\epsilon_0 a}$$

$$\Rightarrow -\frac{\rho_0 a^2}{6\epsilon} + C_1 = \frac{\rho_0 a^2}{3\epsilon_0}$$

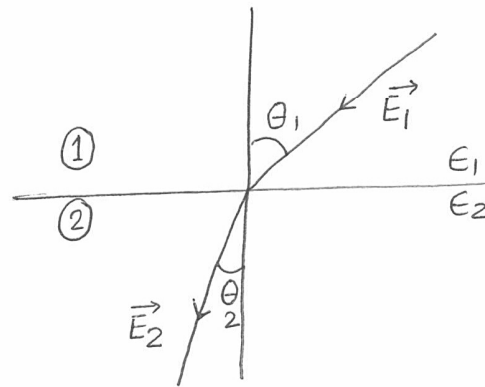
$$\begin{aligned}\Rightarrow C_1 &= \frac{\rho_0 a^2}{6\epsilon} \left[1 + \frac{2\epsilon}{\epsilon_0} \right] \\ &= \frac{\rho_0 a^2}{6\epsilon_0 \epsilon_r} (1 + 2\epsilon_r)\end{aligned}$$

$$\therefore V(0) = C_1 = \frac{\rho_0 a^2}{6\epsilon_0 \epsilon_r} (1 + 2\epsilon_r)$$

Also,

$$V(a) = \frac{\rho_0 a^2}{3\epsilon_0}$$

③



$E_{||}$ is continuous $\Rightarrow E_{1x} = E_{2x}$

D_{\perp} is continuous (with $\sigma_f = 0$)

$$\therefore D_{1y} = D_{2y}$$

$$\Rightarrow \epsilon_1 E_{1y} = \epsilon_2 E_{2y}$$

$$\begin{aligned} \frac{\tan \theta_2}{\tan \theta_1} &= \frac{E_{1x}/E_{1y}}{E_{2x}/E_{2y}} \quad \frac{E_{2x}/E_{2y}}{E_{1x}/E_{1y}} \\ &= \frac{E_{1y}}{E_{2y}} \\ &= \epsilon_2/\epsilon_1 \end{aligned}$$

(4)

Applying Ampere's law -

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{encl}}$$

$$\Rightarrow B \cdot 2\pi r = \mu_0 I \frac{\pi r^2}{\pi a^2}$$

$$\Rightarrow B \cdot 2\pi r = \mu_0 I r^2 / a^2$$

$$\Rightarrow B = \frac{\mu_0 I r}{2\pi a^2}$$

$$\boxed{\vec{B} = \frac{\mu_0 I r}{2\pi a^2} \hat{\phi}}$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

$$\Rightarrow \vec{J} = \frac{1}{\mu_0} (\vec{\nabla} \times \vec{B})$$

$$= \frac{1}{\mu_0} \frac{1}{r} \left[\frac{\partial}{\partial r} \left(r \frac{\mu_0 I r}{2\pi a^2} \right) \right] \hat{z}$$

$$= \frac{1}{\mu_0} \frac{1}{r} \frac{\mu_0 I}{2\pi a^2} 2r \hat{z}$$

$$= \frac{I}{\pi a^2} \hat{z}$$

⑤ a) $\vec{A} = x^2y \hat{i} + y^2x \hat{j} - 4xyz \hat{k} \quad \frac{\text{wb}}{\text{m}}$

$$\vec{B} = \nabla \times \vec{A}$$

$$= \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ x^2y & y^2x & -4xyz \end{vmatrix}$$

$$= \hat{i}(-4xz - 0) - \hat{j}(-4yz - 0) + \hat{k}(y^2 - x^2)$$

$$= -4xz \hat{i} + 4yz \hat{j} + (y^2 - x^2) \hat{k}$$

$$\therefore \vec{B}(-1, 2, 5) = -4(-5) \hat{i} + 4 \times 10 \hat{j} + (4 - 1) \hat{k}$$

$$= 20 \hat{i} + 40 \hat{j} + 3 \hat{k} \quad \frac{\text{wb}}{\text{m}}$$

⑥ Flux through the area is given by

$$\oint_S \vec{B} \cdot d\vec{s}$$

$$= \oint_L \vec{A} \cdot d\vec{l} = \phi_1 + \phi_2 + \phi_3 + \phi_4$$

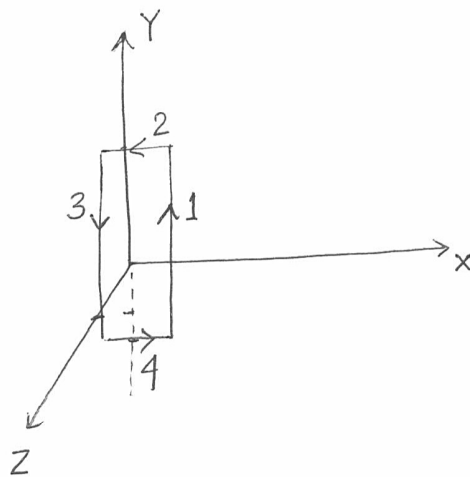
Now $\phi_1 = \left[\int_{y=-1}^4 (x^2y \hat{i} + y^2x \hat{j} - 4xyz \hat{k}) \cdot dy \hat{j} \right]$

$x=1$
 $z=1$

$$= \left. \int_{y=-1}^4 y^2x dy \right|_{x=1, z=1}$$

$$= \left. \frac{y^3}{3} \right|_{-1}^4$$

$$= \frac{64}{3} + \frac{1}{3} = \frac{65}{3}$$



$$\Phi_2 = \left[\int_{x=1}^0 (x^2 y \hat{i} + y^2 x \hat{j} - 4xyz \hat{k}) \cdot (-dx \hat{i}) \right]_{\substack{y=4 \\ z=1}}$$

$$= - \int_{x=1}^0 x^2 y dx \Big|_{\substack{y=4 \\ z=1}}$$

$$= -4 \left[\frac{x^3}{3} \right]_1^0$$

$$= +4 \times \frac{1}{3}$$

$$= +\frac{4}{3}$$

$$\Phi_3 = \left[\int_4^{-1} (x^2 y \hat{i} + y^2 x \hat{j} - 4xyz \hat{k}) \cdot (-dy \hat{j}) \right]_{\substack{x=0, z=1 \\ y=4}}$$

$$= 0$$

$$\Phi_4 = \left[\int_{x=0}^{x=1} (x^2 y \hat{i} + y^2 x \hat{j} - 4xyz \hat{k}) \cdot (+dx \hat{i}) \right]_{\substack{y=-1 \\ z=1}}$$

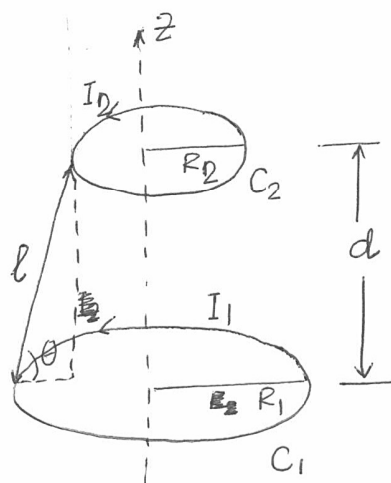
$$= \int_0^1 x^2 y dx \Big|_{\substack{y=-1 \\ z=1}}$$

$$= - \left[\frac{x^3}{3} \right]_0^1$$

$$= -\frac{1}{3}$$

$$\begin{aligned} \therefore \text{Flux through the surface} = \Phi &= \frac{65}{3} + \frac{4}{3} + 0 - \frac{1}{3} \\ &= \frac{68}{3} \text{ Wb.} \end{aligned}$$

⑥



We consider two coils \$C_1\$ and \$C_2\$ of radii \$R_1\$ and \$R_2\$ respectively, carrying currents \$I_1\$ and \$I_2\$ respectively. Let \$d\$ be the separation between the centers of the coils.

Force per unit length on either coil is

$$F_0 = \frac{\mu_0 I_1 I_2}{2\pi l}$$

By symmetry, the component of \$F_0\$ perpendicular to the \$z\$-axis will cancel.

\$\therefore\$ The total force along \$z\$-axis

$$F = \frac{\mu_0 I_1 I_2}{2\pi l} \sin\theta \times 2\pi R_2 \quad R_1 \simeq R_2$$

$$= 2\pi R_2 \times \frac{\mu_0 I_1 I_2}{2\pi l} \times \frac{d}{l}$$

$$F = \mu_0 I_1 I_2 R_2 \frac{d}{d^2 + (R_1 - R_2)^2}$$

Force is maximum when,

$$\frac{dF}{dd} = 0$$

$$\Rightarrow \frac{d^2 + (R_1 - R_2)^2 - d \cdot 2d}{(d^2 + (R_1 - R_2)^2)^2} = 0$$

$$\Rightarrow (R_1 - R_2)^2 = d^2$$

$$\Rightarrow d = R_1 - R_2$$