

# Techniques for Mesh Movement and Curved Mesh Generation for Computational Fluid Dynamics

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# Why mesh movement?

## Mesh movement is useful in several areas of CFD

- aeroelasticity, and fluid-structure interaction in general
- shape optimization
- generation of curved meshes for spatially high-order discretizations
- others

# Fluid-Structure Interaction

- For a body-fitted grid, robust mesh-movement is required to maintain validity and quality of the mesh after imposing motion of the structural domain<sup>1</sup>.
- Immersed boundary methods can also be used; both have advantages and disadvantages<sup>2</sup>.

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<sup>1</sup>C. Farhat and M. Lesoinne. “Two efficient staggered algorithms for the serial and parallel solution of three-dimensional nonlinear transient aeroelastic problems”. In: *Comput. Methods Appl. Mech. Engrg.* 182 (2000), pp. 499–515.

<sup>2</sup>G. Hou, J. Wang, and A. Layton. “Numerical methods for fluid-structure interaction - a review”. In: *Commun. Comput. Phys.* 12.2 (2012), pp. 337–377.

# Shape optimization

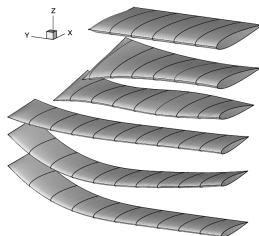


Figure : Convergence history of lift-constrained drag minimization


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<sup>3</sup>J.E. Hicken and D.W. Zingg. “Aerodynamic optimization algorithm with integrated geometry parameterization and mesh movement”. In: *AIAA Journal* 48.2 (2010), pp. 400–413.

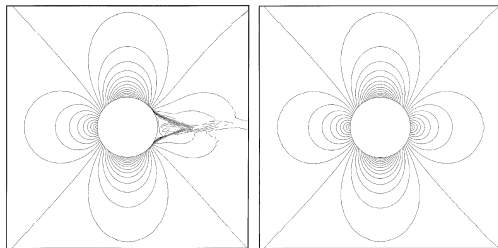
# High-order methods

- According to Wang, Fidkowski *et. al.*<sup>4</sup>, spatially high-order methods perform better than prevailing second order methods for some kinds of simulations considering CPU time taken to achieve a given error level.
- One area of challenge they mention is generation of high-order meshes.

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<sup>4</sup>Z.J. Wang et al. “High-order CFD methods: current status and perspective”. In: *Intl. J. Numer. Meth. Fluids* 72 (2013), pp. 811–845. 

# The need for curved meshes



**Figure :** Inviscid subsonic flow over a cylinder; left: DGP1 solution with regular linear mesh, right: DGP1 solution with quadratic ('Q2') mesh<sup>5</sup>

<sup>5</sup>F. Bassi and S. Rebay. "High-order accurate discontinuous finite element solution of the 2D Euler equations". In: *J. Comput. Phys.* 128 (1997), pp. 251–285.

# The need for curved meshes

Even in less extreme cases, curved meshes are required to obtain design  $(p+1)$  order of accuracy for high-order methods such as discontinuous Galerkin methods<sup>6</sup>.

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<sup>6</sup>X. Luo, M.S. Shephard, and J.-F. Remacle. “The influence of geometric approximation on the accuracy of high order methods”. In: *Rensselaer SCOREC report 1* (2001).



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# Introduction

The problem is to move the interior nodes of a mesh when a given displacement is imposed on the boundary.

- At the very least: mesh elements should not get invalidated.
- Mesh elements should not suffer much deterioration in quality.
- The technique should be computationally inexpensive.

Many mesh-movement methods for unstructured meshes can be found in literature. They can be broadly classified into two types.

- Elasticity-based methods
- Interpolation methods

Combination of these with each other and with other techniques such as topological (connectivity) smoothing are also used<sup>7</sup>.

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<sup>7</sup>F. Alauzet. “A changing-topology moving mesh technique for large displacements”. In: *Engrg. Comput.* 30 (2014), pp. 175–200.

# Lineal spring analogy

Every mesh edge is treated as a linear spring in each coordinate direction<sup>8</sup>.

$$\sum_j k_{ij}(\Delta \mathbf{r}_i - \Delta \mathbf{r}_j) = \mathbf{0} \quad \forall i \quad (1)$$

where  $i$  ranges over all nodes,  $j$  ranges over points surrounding node  $i$  and  $\Delta \mathbf{r}_i$  is the displacement of node  $i$ .  $k_{ij}$  is the stiffness of the spring between nodes  $i$  and  $j$ , which can be taken as

$$k_{ij} = \frac{1}{\|\mathbf{r}_i - \mathbf{r}_j\|}. \quad (2)$$

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<sup>8</sup>J.T. Batina. “Unsteady Euler Algorithm with Unstructured Dynamic Mesh for Complex-Aircraft Aerodynamic Analysis”. In: *AIAA Journal* 29.3 (1991), pp. 327–333.

# Lineal spring analogy

This scheme requires the solution of a linear system of size  $N_n$  (the number of mesh nodes),  $n_{dim}$  (the spatial dimension of the problem) times.

# Torsional springs

The lineal spring analogy fails for large deformations or stretched elements. Farhat *et. al.* came up with a more robust scheme, which is also a spring analogy<sup>9</sup>. They introduce two

improvements over Batina's model.

- The model is closer to a structural analogy in that the displacements in each coordinate direction are coupled.
- 'Torsional springs' are introduced at each node in each element. These are designed to prevent edges collapsing into each other due to rotational motion.

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<sup>9</sup>C. Farhat et al. "Torsional springs for two-dimensional dynamic unstructured fluid meshes". In: *Computer methods in applied mechanics and engineering* 163 (1998), pp. 231–245.

# Torsional springs

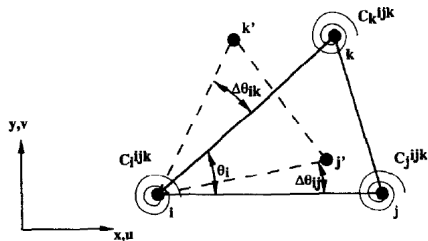


Figure : Movement of an element in torsion spring analogy

A coupled system of  $n_{dim}N_n$  equations must be solved.

# Linear elasticity

The mesh is assumed to model a deformable solid body, which is then deformed according to the equations of solid mechanics, that is, linear or non-linear elasticity.

The simplest approach is linear elasticity.

$$\nabla \cdot \sigma = \mathbf{0} \quad \text{in } \Omega \quad (3)$$

$$\sigma = 2\mu\epsilon + \lambda(\text{tr}\epsilon)\mathbf{I} \quad (4)$$

$$\epsilon = \frac{1}{2}(\nabla \mathbf{u} + \nabla \mathbf{u}^T) \quad (5)$$

$$\mathbf{u} = \mathbf{u}_b \quad \text{on } \partial\Omega \quad (6)$$



# Stiffened Linear elasticity

- The linear elasticity scheme is often modified by ‘stiffening’ the mesh appropriately.
- We attain some control over the propagation of deformation into the interior of the mesh, as done, for instance, by Stein *et. al.*<sup>10</sup>.
- The material is stiffened based on the determinant of the local Jacobian matrix of the reference-to-physical mapping; i.e., smaller elements are stiffer than larger ones.

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<sup>10</sup>K. Stein, T. Tezduyar, and R. Benney. “Mesh moving techniques for fluid-structure interactions with large displacements”. In: *J. Appl. Mech.* 70 (2003), pp. 58–63.

# Nonlinear elasticity

Claimed to be a highly robust method for mesh movement by Persson and Peraire<sup>11</sup>.

The constitutive equation (4) and strain-displacement relation (5) are replaced by the 'neo-Hookean' constitutive model

$$\boldsymbol{\sigma} = \mu((\mathbf{F}^T \mathbf{F}) \mathbf{F}^{-T} - \mathbf{F}^{-T}) + \lambda(\ln \det \mathbf{F}) \mathbf{F}^{-T} \quad (7)$$

Here,  $\mathbf{F} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}}$ ,  $\mathbf{x}$  is the physical position vector of a point with coordinate  $\boldsymbol{\xi}$  in the reference configuration.

The system is solved using Newton-GMRES iterations.

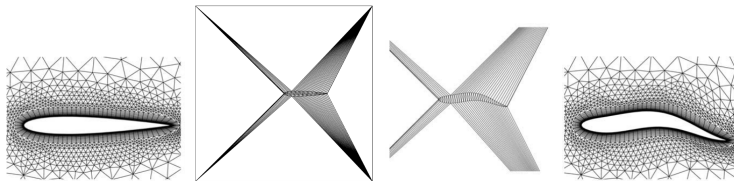
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<sup>11</sup>P.-O. Persson and J. Peraire. "Curved mesh generation and mesh refinement using lagrangian solid mechanics". In: *47<sup>th</sup> AIAA Aerospace Sciences Meeting*. 2009.

# Elasticity-based methods

- Advantages: stiffened linear elasticity is found to be robust, and nonlinear elasticity is claimed to be very robust.
- Disadvantage: expensive!
- Also, implementation is dependent on element type and spatial dimension.

# Delaunay graph mapping



**Figure :** The DGM process (from left to right): original mesh, Delaunay graph, deformed Delaunay graph, deformed mesh (ref:<sup>12</sup>)

<sup>12</sup>X. Liu, N. Qin, and H. Xia. “Fast dynamic grid deformation based on Delaunay graph mapping”. In: *Journal of Computational Physics* 211 (2006), pp. 405–423.

# Mesh quality metrics

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