

EE311FZ Final Paper (21-22 version)

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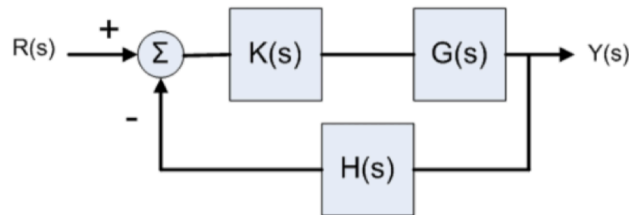
Merry Christmas, in 2022/12/25.

1 Q1 Root Locus

Question 1

[20 marks]

Given the following system:



where

$$G(s) = \frac{1}{(s+1)(s+3)}, \quad H(s) = \frac{1}{s+2}, \quad K(s) = k$$

1.1 (a) Asymptotes of the root loci.

开环传递函数 $G(s)K(s)H(s) = \frac{K}{(s+1)(s+2)(s+3)}$

对应的开环极点为 $p = -1, -2, -3$, $n = 3$

没有开环零点, $m = 0$, 因此根轨迹有3个分支

根据已知, 可以求出根轨迹的渐近线为:

1. 渐近线与实轴的夹角 $\varphi_a = \frac{(2k+1)\pi}{n-m}, k = 0, 1, 2, \varphi_1 = \frac{\pi}{3}, \varphi_2 = \pi, \varphi_3 = \frac{5\pi}{3}$
2. 渐近线与实轴的交点 $\sigma_a = \frac{\sum_{i=1}^n p_i}{3} = -2$

1.2 (b) Breakaway point & Corresponding k.

分离点, 使用试探法得到:

$$\frac{1}{d+1} + \frac{1}{d+2} + \frac{1}{d+3} = 0, \quad d_1 = -1.42, d_2 = -2.58,$$

根轨迹活动的范围是 $[-2, -1]$ and $[-\infty, -3]$, 所以选择 $d_2 = -1.4226$

将-1.4226带回原来的式子 $(s+1)(s+2)(s+3) = s^3 + 6s^2 + 11s + 6$

$$k = s^3 + 6s^2 + 11s + 6|_{-1.4226} = -0.3849 \quad (16)$$

因此, $k = -0.385$

1.3 (c) Root loci & Imaginary axis.

先求出对应的闭环传递函数 $G(s) = \frac{K(s+2)}{s^3+6s^2+11s+6+K}$ ，令 $D(s) = s^3 + 6s^2 + 11s + 6 + K = 0$ 带入 $s = j\omega$

得到 $j(-\omega^3 + 11\omega) + (-6\omega^2 + 6 + K) = 0$

因此 $\omega = \pm\sqrt{11}, K = 60$

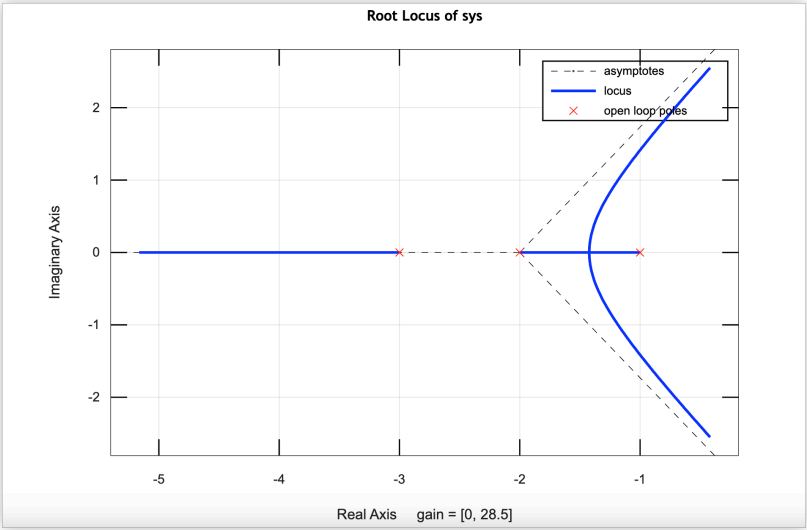
1.4 (d) Draw the root locus.

Draw the root locus plot on graph paper and annotate important points on the plot.

上面我们已经计算出Re轴上的分离点，以及Im轴上的交点:

K	Re	Im
-0.385	-1.42	0
60	0	$\pm\sqrt{11}$

如下图所示：

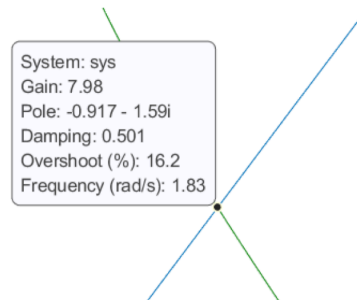
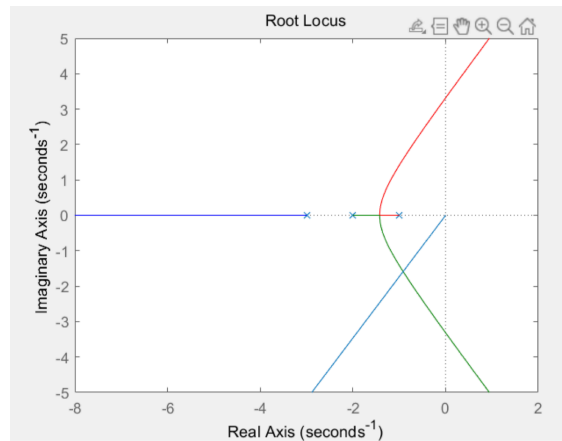


1.5 (e) Graphical approximations

Use the root locus plot to determine the value of k such that the closed-loop system has a damping ratio ζ of approximately 0.5. Calculations based on graphical approximations are acceptable. [Hint: $\zeta = \cos\varphi$]

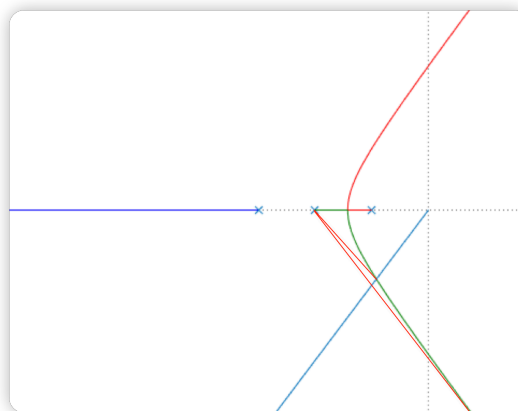
本题解仅供参考：

Method 1: 使用matlab计算得出精确值解



如图 $\zeta = 0.501$, $K = 7.98$, 为精确解

Method 2: 使用渐近线来近似



因为 $\zeta = \cos\varphi = 1/2$, 则 $\varphi = 60^\circ$

我们想要的点可以近似为 $(-1, \sqrt{3})$

代回幅值条件: $|G(s)H(s)| = 1$, 可以得出 $K = \sqrt{84}$

2 Q2 State-Space Basic

A continuous-time system is described by the following state-space matrices

$$A = \begin{bmatrix} 0 & 1 \\ -2 & -1 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, \quad C = \begin{bmatrix} 3 & 0 \end{bmatrix}$$

2.1 (a) Controllable

可控性的判据是 $C = [B \ AB \ A^2B \ \dots \ A^nB]$ 满秩，就可以确定可控

$$C = \begin{bmatrix} 0 & 1 \\ 1 & -1 \end{bmatrix} \quad (17)$$

$Rank(C) = 2$ ，满秩，是可控的

2.2 (b) Observable

可观性的判断是 $O = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \\ CA^n \end{bmatrix}$ 满秩，就可以判断可观性

$$O = \begin{bmatrix} 3 & 0 \\ 0 & 3 \end{bmatrix} \quad (18)$$

$Rank(O) = 2$ ，满秩，是可观的

2.3 (c) Transfer function & Stability

转换公式为 $G(s) = C(sI - A)^{-1}B$

首先要知道矩阵求逆的步骤，假设我们已知矩阵F，要求逆矩阵，首先要确定该矩阵不是奇异矩阵，即 $\det(F) \neq 0$

$$F^{-1} = \frac{adj(F)}{\det(F)} \quad (19)$$

其中分子是F的伴随矩阵，伴随矩阵的求法是，主对角线对调，其余的元素改变符号

因此，对于本题目：

$$\begin{aligned}
G(s) &= C(sI - A)^{-1}B \\
G(s) &= [3 \quad 0] \begin{bmatrix} s & -1 \\ 2 & s+1 \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \\
&= [3 \quad 0] \frac{\begin{bmatrix} s+1 & 1 \\ -2 & s \end{bmatrix}}{s^2 + s + 2} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \\
&= \frac{3}{s^2 + s + 2}
\end{aligned} \tag{20}$$

$s^2 + s + 2 = 0$, 那么 $s_1 = -0.5 + 1.32i$, $s_2 = -0.5 - 1.32i$

两者都在左半平面，所以是稳定的

2.4 (d) Performance Specs (unit step input)

2.4.1 (i) the steady-state system response

Hint: Laplace final value Theorem 终值定理

终值定理 $\lim_{s \rightarrow \infty} G(s) = \lim_{s \rightarrow 0} sG(s)$

带入之后 $\lim_{s \rightarrow 0} \frac{1}{s} sG(s) = \lim_{s \rightarrow 0} \frac{3}{s^2 + s + 2} = \frac{3}{2}$

2.4.2 (ii) the settling time for the system

已知 $T_s = \frac{4}{\xi\omega_n}$

我们通过传递函数可以知道两个参数 $\xi = \sqrt{2}/4$, $\omega_n = \sqrt{2}$

那么 $T_s = \frac{4}{\xi\omega_n} = 8s$

2.4.3 (iii) the PO% overshoot for the system

系统的超调计算公式为 $PO = e^{\frac{-\xi\pi}{\sqrt{1-\xi^2}}}$

带入数据可以得到 $PO = 30.5\%$

2.4.4 (iv) the frequency of oscillation of the response

知道 $\omega_d = \sqrt{1 - \xi^2}\omega_n = 1.3229$

2.5 (e) State feedback Controller

- (e) It is desired that the closed-loop system will have poles of $[-2, -3]$. Design a state feedback controller $u = [k_1 \quad k_2] x$ to achieve these specifications (determine the value of k_1 and k_2).

$$\begin{aligned}
|sI - A + BK| &= (s+2)(s+3) \\
\begin{vmatrix} s & -1 \\ 2+k_1 & s+1+k_2 \end{vmatrix} &= s^2 + 5s + 6 \\
s(s+1+k_2) + 2+k_1 &= s^2 + 5s + 6 \\
s^2 + s + k_2s + 2 + k_1 &= s^2 + 5s + 6 \\
k_1 = 4, k_2 &= 4
\end{aligned} \tag{21}$$

Hence, the state feedback controller is:

$$u = [4, 4]x \tag{22}$$

2.6 (f) State Observer

- (f) Due to an inability to measure the states, a state estimator is required. Design a state observer to place the poles of the observer at $[-6, -6]$. (You should write down the observer dynamics and then calculate the observer gain $K_e = [k_{e,1} \ k_{e,2}]^T$)

$$\begin{aligned}
|sI - A + KC| &= \det \begin{bmatrix} s+3k_1 & -1 \\ 2+3k_2 & s+1 \end{bmatrix} \\
&= s^2 + (3k_1+1)s + 3k_1+3k_2+2
\end{aligned} \tag{23}$$

Because pole is $[-6, -6]$, the expected characteristic equation is:

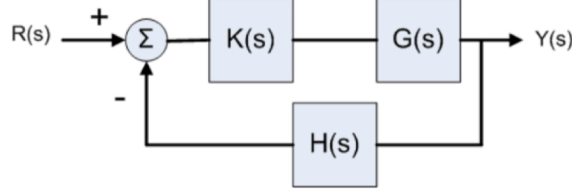
$$\begin{aligned}
&s^2 + 12s + 36 \\
k_1 &= \frac{11}{3}, k_2 = \frac{23}{3}
\end{aligned} \tag{24}$$

Hence, the state observer is

$$K_e = \begin{bmatrix} \frac{11}{3} \\ \frac{23}{3} \end{bmatrix} \tag{25}$$

3 Q3 Nyquist Stability Criterion

3.1 (a) Nyquist Plot



where

$$G(s) = \frac{200}{(s+5)(s+10)}, \quad H(s) = \frac{1}{s+1}, \quad K(s) = 1$$

$$G_{op}(s) = \frac{200}{(s+1)(s+5)(s+10)} = \frac{200(50 - 16\omega^2) + 200j(-65\omega - \omega^3)}{(1 + \omega^2)(25 + \omega^2)(100 + \omega^2)}$$

$$|G_{op}(j\omega)| = \frac{200}{\sqrt{1 + \omega^2} \sqrt{25 + \omega^2} \sqrt{100 + \omega^2}} \quad (26)$$

$$\angle G_{op}(j\omega) = 0 - \arctan \omega - \arctan \frac{\omega}{5} - \arctan \frac{\omega}{10}$$

$$G(s)H(s) = \frac{200}{(s+1)(s+5)(s+10)}$$

$$s = j\omega$$

$$\begin{aligned} & \frac{200}{(j\omega + 1)(j\omega + 5)(j\omega + 10)} \\ & \frac{200(1 - j\omega)(5 - j\omega)(10 - j\omega)}{(j\omega + 1)(j\omega + 5)(j\omega + 10)(1 - j\omega)(5 - j\omega)(10 - j\omega)} \\ & \frac{200(j\omega^3 - 16\omega^2 - 65j\omega + 50)}{(1 + \omega^2)(25 + \omega^2)(100 + \omega^2)} \end{aligned}$$

$$Im[G_{(j\omega)}] = 0, \omega = \pm 8.06226$$

$$\omega = \pm 8.06226 :$$

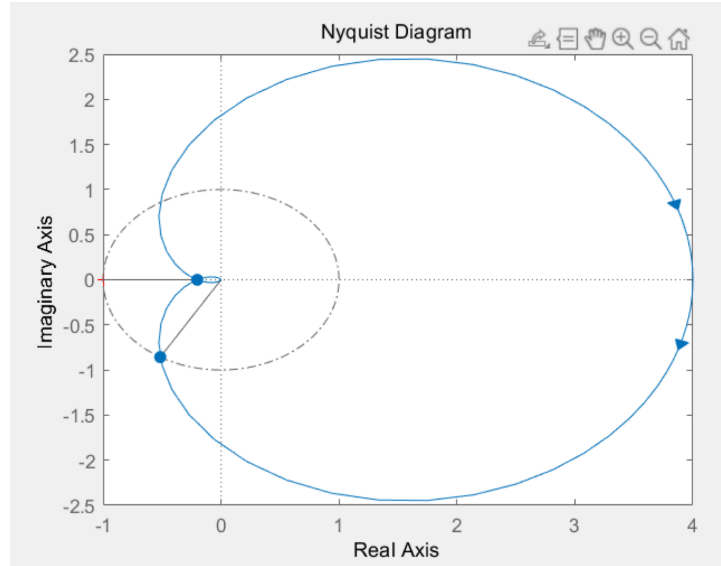
$$Re[G_{(j8.06226)}] = \frac{-198000}{980100} = -0.20202$$

$$Re[G_{(j\omega)}] = 0, \omega = \pm 1.76777$$

$$Im[G_{(j\pm 1.76777)}] = \frac{-21,876}{11964} = -1.82848$$

画奈氏图步骤：

Frequency	Amplitude	Phase
0	4	0
∞	0	-270°
± 8.06226		
± 1.76777		



3.2 (b) Gain Margin

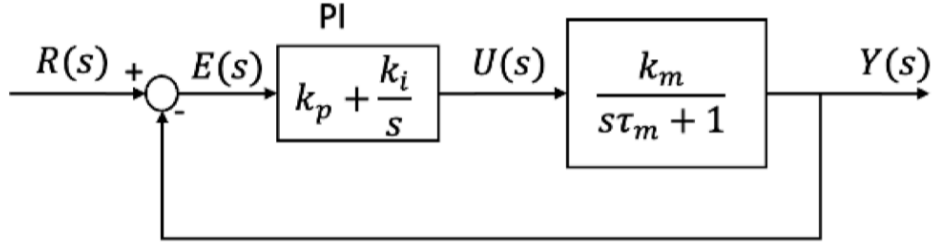
由上可知 cross phase frequency为:

$$\omega_g = \pm 8.06226$$

$$\frac{1}{|G(j\omega_g)|} = \frac{(\sqrt{\omega_g^2 + 1})(\sqrt{\omega_g^2 + 25})(\sqrt{\omega_g^2 + 100})}{200} = 4.95 \quad (27)$$

$$GM = 20 \log 4.95 = 13.892dB$$

4 Q4 PID Controller



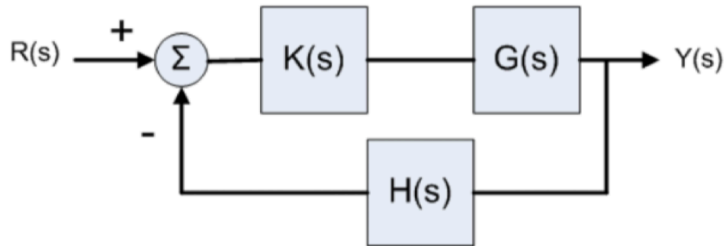
4.1 (a) PI-controlled system & Steady-state error

$$\begin{aligned}\frac{Y(s)}{R(s)} &= \frac{(sKp + Ki)(Km)}{s(s\tau_m + 1) + (sKp + Ki)Km} \\ \frac{E(s)}{R(s)} &= \frac{R(s) - Y(s)}{R(s)} = \frac{s(s\tau_m + 1)}{s(s\tau_m + 1) + (sKp + Ki)Km} \\ \lim_{t \rightarrow \infty} E(s) &= \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} s \frac{s(s\tau_m + 1)}{s(s\tau_m + 1) + (sKp + Ki)Km} \frac{1}{s} = 0\end{aligned}\quad (28)$$

4.2 (b) only P-controlled & Steady-state error

$$\begin{aligned}\frac{Y(s)}{R(s)} &= \frac{KpKm}{s\tau_m + 1 + KpKm} \\ \frac{E(s)}{R(s)} &= \frac{R(s) - Y(s)}{R(s)} = \frac{s\tau_m + 1}{s\tau_m + 1 + KpKm} \\ \lim_{t \rightarrow \infty} E(s) &= \lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} s \frac{s\tau_m + 1}{s\tau_m + 1 + KpKm} \frac{1}{s} = \frac{1}{1 + KpKm}\end{aligned}\quad (29)$$

4.3 (c) PID controller using closed-loop ZN method



where

$$G(s) = \frac{100}{(s+1)(s+2)(s+3)}, \quad K(s) = k_p + k_d s + \frac{k_i}{s}, \quad H(s) = 1$$

[10 marks]

For your convenience, the closed-loop Ziegler-Nichols rules are given in the following table ($k_d = k_p t_d$, $k_i = k_p/t_i$)

	k_p	t_i	t_d
P	$0.5k_c$		
PI	$0.45k_c$	$t_c/1.2$	
PID	$0.6k_c$	$t_c/2$	$t_c/8$

$$\begin{aligned}
&1 + G(s)k_p = 0 \\
&1 + \frac{100k_p}{s^3 + 6s^2 + 11s + 6} = 0 \\
&s^3 + 6s^2 + 11s + 6 + 100k_p = 0 \\
&-j\omega^3 - 6\omega^2 + 11j\omega + 6 + 100k_p = 0 \\
&\begin{cases} -j\omega^3 + 11j\omega = 0 \\ -6\omega^2 + 6 + 100k_p = 0 \end{cases} \\
&k_c = 0.6, \omega_c = \sqrt{11}rad/s \\
&t_c = 2\pi/\omega_c = 1.8945 \\
&k_P = 0.36, t_i = 0.9472, t_d = 0.2368 \\
&K_P = 0.36, K_i = 0.38, K_d = 0.08525
\end{aligned} \tag{30}$$