# 6. Solving the state equations

#### 6.1 Discrete-time solution

• The general linear discrete-time state-space model is given by:

$$\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}\mathbf{u}(k)$$
  
 $\mathbf{y}(k) = \mathbf{C}\mathbf{x}(k) + \mathbf{D}\mathbf{u}(k)$ 

• Here, we will restrict our attention to single-input single-output (SISO) systems, i.e. the input and output are scalar quantities:

$$\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}u(k)$$
$$y(k) = \mathbf{C}\mathbf{x}(k) + \mathbf{D}u(k)$$

where:

$$A \in R^{n \times n}, B \in R^{n \times 1}, C \in R^{1 \times n}, D \in R^{1 \times 1}, x(k) \in R^{n}, u(k), y(k) \in R^{1}$$

- The dynamics of the system are described by the state equation.
- Just like other difference/differential equations, it is solved by considering the unforced and forced responses separately.

#### **Unforced response:**

• This is where the input is set to zero for all time, i.e.:

$$u(k) = 0, \ \forall k$$

• The state equation then becomes:

$$\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k)$$

• Given an initial condition  $\mathbf{x}(0)$  we can calculate the response of the system as follows:

$$\mathbf{x}(1) = \mathbf{A}\mathbf{x}(0)$$
  
 $\mathbf{x}(2) = \mathbf{A}\mathbf{x}(1) = \mathbf{A}^2\mathbf{x}(0)$   
 $\mathbf{x}(3) = \mathbf{A}\mathbf{x}(2) = \mathbf{A}^3\mathbf{x}(0)$   
etc...

- Therefore, in general:  $\mathbf{x}(k) = \mathbf{A}^k \mathbf{x}(0)$
- The matrix  $A^k$  is known as the (*discrete-time*) state transition matrix.

#### **Forced response:**

• Now, consider the situation when the input is not zero:

$$\mathbf{x}(1) = \mathbf{A}\mathbf{x}(0) + \mathbf{B}u(0)$$

$$\mathbf{x}(2) = \mathbf{A}\mathbf{x}(1) + \mathbf{B}u(1)$$

$$= \mathbf{A}(\mathbf{A}\mathbf{x}(0) + \mathbf{B}u(0)) + \mathbf{B}u(1)$$

$$= \mathbf{A}^{2}\mathbf{x}(0) + \mathbf{A}\mathbf{B}u(0) + \mathbf{B}u(1)$$

$$\mathbf{x}(3) = \mathbf{A}\mathbf{x}(2) + \mathbf{B}u(2)$$

$$= \mathbf{A}(\mathbf{A}^{2}\mathbf{x}(0) + \mathbf{A}\mathbf{B}u(0) + \mathbf{B}u(1)) + \mathbf{B}u(2)$$

$$= \mathbf{A}^{3}\mathbf{x}(0) + \mathbf{A}^{2}\mathbf{B}u(0) + \mathbf{A}\mathbf{B}u(1) + \mathbf{B}u(2)$$
etc...

• In general, we get:

$$\mathbf{x}(k) = \mathbf{A}^{k} \mathbf{x}(0) + \mathbf{A}^{k-1} \mathbf{B} u(0) + \mathbf{A}^{k-2} \mathbf{B} u(1) + \dots + \mathbf{A}^{0} \mathbf{B} u(k-1)$$

$$= \mathbf{A}^{k} \mathbf{x}(0) + \sum_{i=1}^{k} \mathbf{A}^{k-i} \mathbf{B} u(i-1)$$
unforced response
$$\mathbf{z} \text{ forced response when } \mathbf{x}(0) = 0$$

#### **Output calculation:**

• Once the state has been determined, the output is easily computed as:

$$y(k) = \mathbf{C}\mathbf{x}(k) + \mathbf{D}u(k)$$
$$= \mathbf{C}\mathbf{A}^{k}\mathbf{x}(0) + \sum_{i=1}^{k} \left(\mathbf{C}\mathbf{A}^{k-i}\mathbf{B}u(i-1)\right) + \mathbf{D}u(k)$$

• Note, that **D** is usually zero.



• **Example 6.1:** Determine the output y(k) for the system:

$$\mathbf{A} = \begin{bmatrix} 0.5 & 0 \\ 0.25 & 0.25 \end{bmatrix}, \ \mathbf{B} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \ \mathbf{C} = \begin{bmatrix} 0.5 & 0 \end{bmatrix}, \ \mathbf{D} = \begin{bmatrix} 0 \end{bmatrix}$$

given that the input is  $u(k) = \delta(k)$  and  $x(0) = [0\ 0]^{T}$ .

**Solution:** 

$$y(k) = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.5 & 0 \\ 0.25 & 0.25 \end{bmatrix}^{k} \begin{bmatrix} 0 \\ 0 \end{bmatrix} + \sum_{i=1}^{k} \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.5 & 0 \\ 0.25 & 0.25 \end{bmatrix}^{k-i} \begin{bmatrix} 1 \\ 1 \end{bmatrix} \delta(i-1)$$

$$\delta(i-1) = 1 \text{ when } i = 1$$

$$= 0 \ \forall i \neq 1$$

$$\Rightarrow y(k) = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.5 & 0 \\ 0.25 & 0.25 \end{bmatrix}^{k-1} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \mathbf{C}\mathbf{A}^{k-1}\mathbf{B}$$

$$y(1) = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = 0.5$$

$$y(2) = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.5 & 0 \\ 0.25 & 0.25 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.5 \\ 0.5 \end{bmatrix} = 0.25$$

$$y(3) = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.5 & 0 \\ 0.25 & 0.25 \end{bmatrix} \begin{bmatrix} 0.5 & 0 \\ 0.25 & 0.25 \end{bmatrix} \begin{bmatrix} 1 \\ 0.25 & 0.25 \end{bmatrix} = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.25 \\ 0.25 \end{bmatrix} = 0.125$$

In general:

$$y(k) = \begin{bmatrix} 0.5 & 0 \end{bmatrix} \begin{bmatrix} 0.5^{k-1} \\ 0.5^{k-1} \end{bmatrix} = 0.5(0.5)^{k-1} = 0.5^{k}$$

$$A^{k-1}B = x(k)$$

- In this example we have succeeded in obtaining the solution of y(k) (and x(k)) in *closed* form.
- This implies that the solution is in terms of *k* only and, as a result, it is easy to work out answers for any value of *k*.

#### **Notes:**

- It is worth noting that we are fortunate in being able to get the general 'closed-form solution' for the elements of the state vector.
- The special case of zero initial conditions and (unit) impulse input helps to simplify things considerably.
- More computationally attractive methods are needed for calculating the transition matrix for general problems.
- We would like a solution that is easy to implement using computers.
- Two popular methods exist one uses canonical state transformations (to diagonalise A), the other uses the Cayley-Hamilton theorem.
- In this module, we will only consider the method of state transformation (and, in particular, using the modal matrix).
- Aside the Cayley-Hamilton theorem states that an  $n \times n$  matrix A satisfies its own characteristic equation:

$$p(\lambda) = |\lambda \mathbf{I} - \mathbf{A}| = \lambda^n + a_{n-1}\lambda^{n-1} + \dots + a_1\lambda + a_0 = 0$$

In other words, if we replace  $\lambda$  with A, then p(A) = 0.

This theorem is the basis of an alternative method used to calculate the state transition matrix – please refer to a suitable text book for detail.



#### 6.2 State transformations

- State-space representations are not unique. There are many selections of state variables which can describe a system.
- State variables can be real or fictitious.
- Some state representations lead to computationally attractive forms.
- Thus, by using the appropriate state transformation, we can obtain a state-space representation that leads to significantly easier computation.
- Consider the following state transformation:

$$\mathbf{x}(k) = \mathbf{Tz}(k)$$

• Here, T is any constant non-singular  $n \times n$  matrix. Since T is constant, we can write:

$$x(k+1) = Tz(k+1)$$

• Substituting these expressions into the state equation  $\mathbf{x}(k+1) = \mathbf{A}\mathbf{x}(k) + \mathbf{B}u(k)$  gives:

$$Tz(k+1) = ATz(k) + Bu(k)$$

• Finally, premultiplying by  $T^1$  gives us the new state equation:

$$\mathbf{z}(k+1) = \mathbf{T}^{-1}\mathbf{A}\mathbf{T}\mathbf{z}(k) + \mathbf{T}^{-1}\mathbf{B}u(k)$$
$$= \mathbf{A}_{7}\mathbf{z}(k) + \mathbf{B}_{7}u(k)$$

• The new output equation is:

$$y(k) = \mathbf{CTz}(k) + \mathbf{D}u(k)$$
  
=  $\mathbf{C}_{\mathbf{Z}}\mathbf{z}(k) + \mathbf{D}u(k)$ 

- Note the only condition on **T** is that it must be non-singular (i.e. invertible).
- Hence, there are an infinite number of state representations for the system.
- We are interested in finding a representation that leads to a diagonal A matrix as this will make our computation significantly easier.
- So the issue becomes one of finding a suitable T so that  $A_Z = T^1 A T$  is diagonal.

- Now consider a matrix A with distinct eigenvalues  $\lambda_1, \lambda_2, ... \lambda_n$  and let  $m_1, m_2, ... m_n$  be the corresponding eigenvectors.
- The *modal matrix*, M, is formed from these eigenvectors:  $\mathbf{M} = \begin{bmatrix} \mathbf{m}_1 & \mathbf{m}_2 & \cdots & \mathbf{m}_n \end{bmatrix}$
- Note that by definition,  $Am_i = \lambda_i m_i$ .
- Hence:

$$\mathbf{AM} = \mathbf{A} \begin{bmatrix} \mathbf{m}_1 & \mathbf{m}_2 & \cdots & \mathbf{m}_n \end{bmatrix}$$

$$= \begin{bmatrix} \mathbf{A} \mathbf{m}_1 & \mathbf{A} \mathbf{m}_2 & \cdots & \mathbf{A} \mathbf{m}_n \end{bmatrix}$$

$$= \begin{bmatrix} \lambda_1 \mathbf{m}_1 & \lambda_2 \mathbf{m}_2 & \cdots & \lambda_n \mathbf{m}_n \end{bmatrix}$$

$$= \mathbf{M} \Lambda$$

where:

$$\Lambda = \begin{bmatrix} \lambda_1 & 0 & \cdots & 0 \\ 0 & \lambda_2 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & \lambda_n \end{bmatrix}$$

- Since:  $\mathbf{AM} = \mathbf{M}\Lambda \implies \Lambda = \mathbf{M}^{-1}\mathbf{AM}$
- Thus, we can conclude that in order to obtain a diagonal state matrix, we choose the modal matrix *M* as the state transformation matrix.
- A state transformation by the modal matrix produces a set of *n* independent first order difference equations:

$$z_{1}(k+1) = \lambda_{1}z_{1}(k) + b_{1}u(k)$$

$$\vdots$$

$$z_{n}(k+1) = \lambda_{n}z_{n}(k) + b_{n}u(k)$$

### 6.2.1 Determining the modal matrix

• Recall that eigenvalues are calculated as the roots of the matrix characteristic equation:

$$\det(\lambda \mathbf{I} - \mathbf{A}) = |\lambda \mathbf{I} - \mathbf{A}| = 0$$

- The eigenvectors are then determined either by:
  - solving  $Am_i = \lambda_i m_i$

or

- evaluating the cofactors of a row of  $(\lambda I - A)$ 

• Example 6.2: Determine the modal matrix for  $\mathbf{A} = \begin{bmatrix} -1 & 2 \\ -1 & -4 \end{bmatrix}$ 

Solution: Eigenvalues:

$$\begin{vmatrix} \lambda \mathbf{I} - \mathbf{A} \end{vmatrix} = 0 \Rightarrow \begin{vmatrix} \begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} - \begin{bmatrix} -1 & 2 \\ -1 & -4 \end{bmatrix} \end{vmatrix} = 0 \Rightarrow \begin{vmatrix} \lambda + 1 & -2 \\ 1 & \lambda + 4 \end{vmatrix} = 0$$

$$\Rightarrow (\lambda + 1)(\lambda + 4) + 2 = 0$$

$$\Rightarrow \lambda^2 + 5\lambda + 6 = 0$$

$$\Rightarrow (\lambda + 2)(\lambda + 3) = 0$$

$$\Rightarrow \lambda_1 = -2, \lambda_2 = -3$$

Eigenvectors – method 1:

$$\mathbf{Am} = \lambda \mathbf{m} \Rightarrow \begin{bmatrix} -1 & 2 \\ -1 & -4 \end{bmatrix} \begin{bmatrix} m_1 \\ m_2 \end{bmatrix} = \lambda \begin{bmatrix} m_1 \\ m_2 \end{bmatrix} \Rightarrow \begin{aligned} -m_1 + 2m_2 &= \lambda m_1 \\ -m_1 - 4m_2 &= \lambda m_2 \end{aligned}$$

Solving for 
$$\lambda = -2 \Rightarrow \frac{-m_1 + 2m_2 = -2m_1}{-m_1 - 4m_2 = -2m_2} \Rightarrow \frac{m_1 = -2m_2}{m_1 = -2m_2} \Rightarrow \begin{bmatrix} -2\\1 \end{bmatrix}$$

Solving for 
$$\lambda = -3 \Rightarrow \begin{cases} -m_1 + 2m_2 = -3m_1 \\ -m_1 - 4m_2 = -3m_2 \end{cases} \Rightarrow \begin{cases} m_1 = -m_2 \\ m_1 = -m_2 \end{cases} \Rightarrow \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

$$\Rightarrow \mathbf{M} = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix}$$
 eigenvector for  $\lambda = -3$  eigenvector for  $\lambda = -2$ 

Eigenvectors – *method 2 (cofactors)* – here, the eigenvectors are obtained by writing the cofactors of **any** row of  $(\lambda I - A)$  in column format (note – make sure to allow for the correct sign, as shown below):

$$(\lambda \mathbf{I} - \mathbf{A}) = \begin{bmatrix} \lambda + 1 & -2 \\ 1 & \lambda + 4 \end{bmatrix} \leftrightarrow \begin{bmatrix} + & - \\ - & + \end{bmatrix}$$

Take row 1, for example. The cofactor =  $\begin{bmatrix} \lambda + 4 \\ -1 \end{bmatrix}$ :  $\lambda = -2 \Rightarrow \begin{bmatrix} 2 \\ -1 \end{bmatrix}$ ,  $\lambda = -3 \Rightarrow \begin{bmatrix} 1 \\ -1 \end{bmatrix}$ 

Take row 2. The cofactor = 
$$\begin{bmatrix} 2 \\ \lambda + 1 \end{bmatrix}$$
:  $\lambda = -2 \Rightarrow \begin{bmatrix} 2 \\ -1 \end{bmatrix}$ ,  $\lambda = -3 \Rightarrow \begin{bmatrix} 2 \\ -2 \end{bmatrix}$ 

Here, each cofactor is an eigenvector and combining these for either row will give the modal matrix, as before.

- Note, in the last example, that the actual eigenvector values are not the same but this is not important.
- It is the relationship/ratio between each of the values in each eigenvector that is of key importance and this is the same in all cases.
- This effectively relates to direction, and it is the direction itself that is important and not the actual distance in that direction!
- Example 6.3: Determine the modal matrix for  $\mathbf{A} = \begin{bmatrix} 1 & 2 & 1 \\ 6 & -1 & 0 \\ -1 & -2 & -1 \end{bmatrix}$

**Solution:** 

Eigenvalues:

$$|\lambda \mathbf{I} - \mathbf{A}| = 0 \Rightarrow \begin{vmatrix} \lambda - 1 & -2 & -1 \\ -6 & \lambda + 1 & 0 \\ 1 & 2 & \lambda + 1 \end{vmatrix} = 0$$

$$\Rightarrow (\lambda - 1) ((\lambda + 1)^2) - (-2) ((-6)(\lambda + 1)) + (-1) (-12 - (\lambda + 1)) = 0$$

$$\Rightarrow (\lambda - 1) (\lambda^2 + 2\lambda + 1) - 12\lambda - 12 + 12 + \lambda + 1 = 0$$

$$\Rightarrow (\lambda^3 + \lambda^2 - \lambda - 1) - 11\lambda + 1 = 0$$

$$\Rightarrow \lambda^3 + \lambda^2 - 12\lambda = 0 \Rightarrow \lambda(\lambda^2 + \lambda - 12) = 0$$

$$\Rightarrow \lambda(\lambda - 3)(\lambda + 4) = 0 \Rightarrow \lambda = 0, 3, -4$$

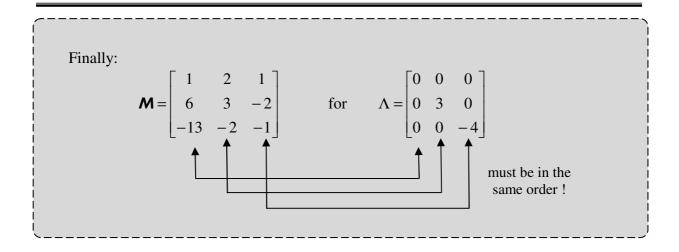
Eigenvectors – using cofactor method:

$$(\lambda \mathbf{I} - \mathbf{A}) = \begin{bmatrix} \lambda - 1 & -2 & -1 \\ -6 & \lambda + 1 & 0 \\ 1 & 2 & \lambda + 1 \end{bmatrix} \leftrightarrow \begin{bmatrix} + & - & + \\ - & + & - \\ + & - & + \end{bmatrix}$$

Take row 1: cofactor = 
$$\mathbf{M}(\lambda) = \begin{bmatrix} (\lambda+1)^2 \\ 6(\lambda+1) \\ -12 - (\lambda+1) \end{bmatrix} = \begin{bmatrix} (\lambda+1)^2 \\ 6(\lambda+1) \\ -13 - \lambda \end{bmatrix}$$
:

Hence: 
$$\lambda = 0 \Rightarrow \begin{bmatrix} 1 \\ 6 \\ -13 \end{bmatrix}$$
,  $\lambda = 3 \Rightarrow \begin{bmatrix} 16 \\ 24 \\ -16 \end{bmatrix} = \begin{bmatrix} 2 \\ 3 \\ -2 \end{bmatrix}$ ,  $\lambda = -4 \Rightarrow \begin{bmatrix} 9 \\ -18 \\ -9 \end{bmatrix} = \begin{bmatrix} 1 \\ -2 \\ -1 \end{bmatrix}$ 

Note – we have scaled the eigenvectors for convenience!



• By choosing T = M we get:

$$z(k+1) = M^{-1}AMz(k) + M^{-1}Bu(k) \qquad \equiv A_Z z(k) + B_Z u(k)$$
$$= \Lambda z(k) + B_Z u(k)$$

• The state transition matrix for this system is given as:

$$\begin{cases}
\Lambda^{k} = \begin{bmatrix}
\lambda_{1}^{k} & 0 & \cdots & 0 \\
0 & \lambda_{2}^{k} & \cdots & 0 \\
\vdots & \vdots & \ddots & \vdots \\
0 & 0 & \cdots & \lambda_{n}^{k}
\end{bmatrix}
\end{cases}$$

- We can also easily obtain a closed form for the transition matrix  $A^k$  of the original system  $\mathbf{x}(k+1) = A\mathbf{x}(k) + B\mathbf{u}(k)$  as follows.
- Since:

$$\Lambda = \mathbf{M}^{-1}\mathbf{A}\mathbf{M} \Rightarrow \mathbf{A} = \mathbf{M}\Lambda\mathbf{M}^{-1}$$

• Then:

$$\mathbf{A}^k = (\mathbf{M} \Delta \mathbf{M}^{-1})^k = \mathbf{M} \Delta \mathbf{M}^{-1} \mathbf{M} \Delta \mathbf{M}^{-1} \dots \mathbf{M} \Delta \mathbf{M}^{-1} = \mathbf{M} \Delta^k \mathbf{M}^{-1}$$

• Hence:

$$\mathbf{A}^{k} = \mathbf{M} \Lambda^{k} \mathbf{M}^{-1}$$

• **Example 6.4:** Determine the state transition matrix for the autonomous (i.e. no input) system:

$$\mathbf{x}(k+1) = \begin{bmatrix} -1 & 2\\ -1 & -4 \end{bmatrix} \mathbf{x}(k)$$

and hence evaluate its response at k = 10, for the initial state  $x(0) = \begin{bmatrix} 1 & 0 \end{bmatrix}^T$ .

#### **Solution:**

From example 6.2:

$$\mathbf{A} = \begin{bmatrix} -1 & 2 \\ -1 & -4 \end{bmatrix} \rightarrow \lambda = -2, -3 \rightarrow \mathbf{M} = \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix}$$

Now:  $x(k) = A^k x(0)$ 

$$A^{k} = M\Lambda^{k}M^{-1}$$

$$= \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} -2 & 0 \\ 0 & -3 \end{bmatrix}^{k} \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix}^{-1}$$

$$= \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} (-2)^{k} & 0 \\ 0 & (-3)^{k} \end{bmatrix} \left( \frac{1}{2-1} \right) \begin{bmatrix} -1 & -1 \\ -1 & -2 \end{bmatrix}$$

$$= \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} (-2)^{k} & 0 \\ 0 & (-3)^{k} \end{bmatrix} \begin{bmatrix} -1 & -1 \\ -1 & -2 \end{bmatrix}$$

$$= \begin{bmatrix} -2 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} -(-2)^{k} & -(-2)^{k} \\ -(-3)^{k} & -2(-3)^{k} \end{bmatrix}$$

$$\Rightarrow A^{k} = \begin{bmatrix} 2(-2)^{k} - (-3)^{k} & 2(-2)^{k} - 2(-3)^{k} \\ -(-2)^{k} + (-3)^{k} & (-2)^{k} + 2(-3)^{k} \end{bmatrix}$$

Hence: 
$$\mathbf{x}(k) = \mathbf{A}^{k} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 2(-2)^{k} - (-3)^{k} \\ -(-2)^{k} + (-3)^{k} \end{bmatrix}$$

For 
$$k = 10$$
:  $\mathbf{x}(10) = \begin{bmatrix} 2(-2)^{10} - (-3)^{10} \\ -(-2)^{10} + (-3)^{10} \end{bmatrix} = \begin{bmatrix} -57001 \\ 58025 \end{bmatrix}$ 

### 6.3 Continuous-time solution

• The general linear SISO continuous-time state-space model is given by:

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$

$$y(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t)$$

• Once again, we will consider the unforced and forced responses separately.

#### **Unforced response:**

- This is where the input is set to zero for all time, i.e.:  $u(t) = 0, \forall t$
- The state equation then becomes:  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t)$
- Solving this first order differential equation gives:  $\mathbf{x}(t) = e^{\mathbf{A}t}\mathbf{x}(0)$
- In this case, the matrix  $e^{At}$  is known as the (*continuous-time*) state transition matrix.

#### **Forced response:**

- Now, consider the situation when the input is not zero:  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$
- The solution for this can be written as:  $\mathbf{x}(t) = e^{\mathbf{A}t}\mathbf{x}(0) + \int_{0}^{t} e^{\mathbf{A}(t-\tau)}\mathbf{B}u(\tau)d\tau$

#### **Output calculation:**

• Once the state has been determined, the output is easily computed as:

$$y(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}u(t)$$

$$= \mathbf{C}e^{At}\mathbf{x}(0) + \int_{t_0}^{t} \mathbf{C}e^{A(t-\tau)}\mathbf{B}u(\tau)d\tau + \mathbf{D}u(t)$$

- Aside note these equations are similar in form to those obtained for the discrete-time state-space models but  $\Sigma \to \int$  and  $\mathbf{A}^k \to e^{\mathbf{A}t}$ .
- Just as in the discrete case, we need efficient ways of computing the state transition matrix.
- The Modal matrix and Cayley-Hamilton methods described for  $A^k$  can also be applied to  $e^{At}$  with some minor modifications.

### 6.3.1 The Modal matrix (or state transformation) method

- Consider  $e^{\mathbf{A}t}$  when  $\mathbf{A} = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}$ .
- Expanding  $e^{\mathbf{A}t}$  as a power series gives:

$$\exp\left[\begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} t\right] = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} t + \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}^2 \frac{t^2}{2!} + \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}^3 \frac{t^3}{3!} + \dots$$

$$= \begin{bmatrix} 1 + \lambda_1 t + \lambda_1^2 \frac{t^2}{2!} + \lambda_1^3 \frac{t^3}{3!} + \dots & 0 \\ 0 & 1 + \lambda_2 t + \lambda_2^2 \frac{t^2}{2!} + \lambda_2^3 \frac{t^3}{3!} + \dots \end{bmatrix}$$

$$= \begin{bmatrix} e^{\lambda_1 t} & 0 \\ 0 & e^{\lambda_2 t} \end{bmatrix}$$

- Thus, when A is a diagonal matrix, calculating  $e^{At}$  is straightforward.
- Consider:  $\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t)$
- Let  $\mathbf{x}(t) = \mathbf{Mz}(t)$ , where  $\mathbf{M}$  is the modal matrix for  $\mathbf{A}$ .
- This gives:  $\dot{z}(t) = M^{-1}AMz(t) = \Omega z(t)$
- Solving this equation, we obtain:  $\mathbf{z}(t) = e^{\Omega t} \mathbf{z}(0)$

• Note: 
$$\Omega = \mathbf{M}^{-1} \mathbf{A} \mathbf{M} = \begin{bmatrix} \lambda_1 & 0 \\ & \ddots \\ 0 & \lambda_n \end{bmatrix}$$

- But  $\mathbf{z}(t) = \mathbf{M}^{-1}\mathbf{x}(t)$ , hence:  $\mathbf{x}(t) = \mathbf{M}\mathbf{z}(t) = \mathbf{M}e^{\Omega t}\mathbf{z}(0) = \mathbf{M}e^{\Omega t}\mathbf{M}^{-1}\mathbf{x}(0)$
- Previously, we noted that  $\mathbf{x}(t) = e^{At}\mathbf{x}(0)$ , hence:  $\mathbf{M}e^{\Omega t}\mathbf{M}^{-1}\mathbf{x}(0) = e^{At}\mathbf{x}(0)$
- Thus, the state transition matrix  $e^{\mathbf{A}t}$  can be computed as:

$$e^{At} = \mathbf{M}e^{\Omega t}\mathbf{M}^{-1}$$

• Note the similarity with the discrete-time equivalent.

**Example 6.5 (a):** Determine the **state transition matrix** for the autonomous system:

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 2 \\ -3 & -5 \end{bmatrix} \mathbf{x}$$

**Solution:** 

 $\lambda = -2, -3$ Eigenvalues:

(... verify for yourself)

Modal matrix: 
$$\mathbf{M} = \begin{bmatrix} -1 & -2 \\ 1 & 3 \end{bmatrix}$$

(... verify for yourself)

Thus:

$$\mathbf{M}^{-1} = \begin{bmatrix} -3 & -2 \\ 1 & 1 \end{bmatrix}$$

Hence:

$$e^{At} = \begin{bmatrix} -1 & -2 \\ 1 & 3 \end{bmatrix} e^{\begin{bmatrix} -2 & 0 \\ 0 & -3 \end{bmatrix} t} \begin{bmatrix} -3 & -2 \\ 1 & 1 \end{bmatrix}$$
$$= \begin{bmatrix} -1 & -2 \\ 1 & 3 \end{bmatrix} \begin{bmatrix} e^{-2t} & 0 \\ 0 & e^{-3t} \end{bmatrix} \begin{bmatrix} -3 & -2 \\ 1 & 1 \end{bmatrix}$$
$$= \begin{bmatrix} 3e^{-2t} - 2e^{-3t} & 2e^{-2t} - 2e^{-3t} \\ -3e^{-2t} + 3e^{-3t} & -2e^{-2t} + 3e^{-3t} \end{bmatrix}$$

Example 6.5 (b): Determine the evolution of the state vector for the system:

$$\dot{\mathbf{x}}(t) = \begin{bmatrix} 0 & 2 \\ -3 & -5 \end{bmatrix} \mathbf{x}(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

if the input u(t) is a step and the initial state  $x(0) = [1 - 1]^{T}$ .

**Solution:** 

We need to determine:  $\mathbf{x}(t) = e^{\mathbf{A}t}\mathbf{x}(0) + \int_{0}^{t} e^{\mathbf{A}(t-\tau)}\mathbf{B}u(\tau)d\tau$ 

$$e^{\mathbf{A}t}\mathbf{x}(0) = \begin{bmatrix} 3e^{-2t} - 2e^{-3t} & 2e^{-2t} - 2e^{-3t} \\ -3e^{-2t} + 3e^{-3t} & -2e^{-2t} + 3e^{-3t} \end{bmatrix} \begin{bmatrix} 1 \\ -1 \end{bmatrix} = \begin{bmatrix} e^{-2t} \\ -e^{-2t} \end{bmatrix}$$

$$\int_{0}^{t} e^{\mathbf{A}(t-\tau)} \mathbf{B} u(\tau) d\tau \to e^{\mathbf{A}t} \int_{0}^{t} e^{-\mathbf{A}\tau} \mathbf{B} u(\tau) d\tau 
= e^{\mathbf{A}t} \int_{0}^{t} \begin{bmatrix} 3e^{2\tau} - 2e^{3\tau} & 2e^{2\tau} - 2e^{3\tau} \\ -3e^{2\tau} + 3e^{3\tau} & -2e^{2\tau} + 3e^{3\tau} \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} (1) d\tau 
= e^{\mathbf{A}t} \int_{0}^{t} \begin{bmatrix} 2e^{2\tau} - 2e^{3\tau} \\ -2e^{2\tau} + 3e^{3\tau} \end{bmatrix} d\tau 
= e^{\mathbf{A}t} \left( \begin{bmatrix} e^{2\tau} - \frac{2}{3}e^{3\tau} \\ -e^{2\tau} + e^{3\tau} \end{bmatrix} \Big|_{0}^{t} \right) 
= e^{\mathbf{A}t} \left( \begin{bmatrix} e^{2t} - \frac{2}{3}e^{3t} - 1 + \frac{2}{3} \\ -e^{2t} + e^{3t} + 1 - 1 \end{bmatrix} \right) 
= \begin{bmatrix} 3e^{-2t} - 2e^{-3t} & 2e^{-2t} - 2e^{-3t} \\ -3e^{-2t} + 3e^{-3t} & -2e^{-2t} + 3e^{-3t} \end{bmatrix} \begin{bmatrix} e^{2t} - \frac{2}{3}e^{3t} - \frac{1}{3} \\ -e^{2t} + e^{3t} \end{bmatrix} 
= \begin{bmatrix} (3 - 2e^{t} - e^{-2t} - 2e^{-t} + \frac{4}{3} + \frac{2}{3}e^{-3t} \\ -3 + 2e^{t} + e^{-2t} + 3e^{-t} - 2 - e^{-3t} \end{pmatrix} + \left( -2 + 2e^{t} + 2e^{-t} - 2 \right) 
= \begin{bmatrix} -e^{-2t} + \frac{2}{3}e^{-3t} + \frac{1}{3} \\ e^{-2t} - e^{-3t} \end{bmatrix}$$

Hence:

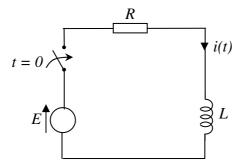
$$\mathbf{x}(t) = e^{At}\mathbf{x}(0) + \int_{0}^{t} e^{A(t-\tau)}\mathbf{B}u(\tau)d\tau$$

$$\Rightarrow \mathbf{x}(t) = \begin{bmatrix} e^{-2t} \\ -e^{-2t} \end{bmatrix} + \begin{bmatrix} -e^{-2t} + \frac{2}{3}e^{-3t} + \frac{1}{3} \\ e^{-2t} - e^{-3t} \end{bmatrix}$$

$$\Rightarrow \mathbf{x}(t) = \begin{bmatrix} \frac{2}{3}e^{-3t} + \frac{1}{3} \\ -e^{-3t} \end{bmatrix}$$

## 6.4 The trilogy of solutions

- In general linear systems can be represented using differential equations, transfer functions or state-space models.
- Each of these are solved in very different ways but will ultimately yield the same solution!
- By way of example, recall the series R-L circuit from EE214:



• The first order **differential equation model** for this simple circuit is given by:

$$L\frac{di}{dt} + Ri = E$$

• Solving this equation directly gives us the solution:

$$i(t) = \frac{E}{R} \left( 1 - e^{\frac{-R}{L}t} \right)$$

• Using Laplace Transforms, we obtain the **transfer function model** for this system as:

$$I(s) = \frac{E}{s(R + sL)}$$

• Solving this model using partial fractions and Inverse Laplace Transforms gives us the exact same solution, as expected, i.e.:

$$i(t) = \frac{E}{R} \left( 1 - e^{\frac{-R}{L}t} \right)$$

- Refer to EE214 notes for details of the above solutions.
- Here, we will complete the 'trilogy' of solutions, by obtaining a state space model for the R-L circuit and solving this model directly.

### 6.4.1 The state-space model and solution for the series R-L circuit

- We know the first-order differential equation is:  $L\frac{di}{dt} + Ri = E$
- Here, we only have a *first-order* differential equation and hence only one state:  $x_1 = i$
- We now obtain an expression for  $\dot{x}_1$ :

$$\dot{x}_1 = \frac{di}{dt} = \frac{E}{L} - \frac{R}{L}i$$

• Rewriting this equation in terms of state  $x_1$ , and letting input u = E, we get:

$$\dot{x}_1 = \frac{-R}{L}x_1 + \frac{1}{L}u$$

• The output  $y = i(t) = x_1$ . Hence, our simple **state-space model** is expressed, in full, as:

$$\left[\dot{x}_{1}\right] = \left[\frac{-R}{L}\right] \left[x_{1}\right] + \left[\frac{1}{L}\right] \left[u\right]$$

$$[y] = [1][x_1]$$

• Since  $y = x_1$ , to solve for the output we simply need to evaluate the expression:

$$\mathbf{x}(t) = e^{\mathbf{A}t} \mathbf{x}(0) + \int_{0}^{t} e^{\mathbf{A}(t-\tau)} \mathbf{B}u(\tau) d\tau$$

• Here, we have only one state and, also, the initial condition is  $x_1(0) = 0$ . Hence:

$$y = x(t) = 0 + \int_0^t e^{-\frac{R}{L}(t-\tau)} \left(\frac{1}{L}\right) E d\tau$$

$$= \frac{E}{L} e^{-\frac{R}{L}t} \int_0^t e^{\frac{R}{L}\tau} d\tau = \frac{E}{L} e^{-\frac{R}{L}t} \left(e^{\frac{R}{L}\tau} \left(\frac{L}{R}\right)\right)_0^t = \frac{E}{R} e^{-\frac{R}{L}t} \left(e^{\frac{R}{L}t} - 1\right)$$

$$= \frac{E}{R} \left(1 - e^{-\frac{R}{L}t}\right)$$

• Once again, we obtain the same solution.

- Hence, we have shown that we can represent systems using three different models and the solutions to each of these models, as expected, are the same.
- The key benefit of using state-space models is that the model and its solution scales easily for higher-order problems.
- Differential equations, on the other hand, become more complex to solve for higher orders.
- Transfer function models do not allow for initial conditions and can only be written for an individual input-output relationship.
- State-space models can allow represent multi-input multi-output systems in the same model, caters for initial conditions and offers the same solution methodology irrespective of the order of the model.
- In the next section, we will examine the issue of stability from the state-space model viewpoint.



"IT JUST SEEMED LOGICAL TO HAVE A SCREEN FOR EACH DIMENSION"