

## Single Current Expression for All Operating Regimes of $V_{gs}$ and $V_{ds}$

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$$V_{ADIBLC} = \frac{(V_{gsteff} + 2V_t)}{\theta_{ROUT}(1 + P_{DIBLCB}V_{bseff})} \left( 1 - \frac{A_{bulk}V_{dsat}}{A_{bulk}V_{dsat} + V_{gsteff} + 2V_t} \right) \quad (3.5.5)$$

$$\theta_{ROUT} = P_{DIBLC1} \left[ \exp\left(-D_{ROUT} \frac{L_{eff}}{2l_{t0}}\right) + 2 \exp\left(-D_{ROUT} \frac{L_{eff}}{l_{t0}}\right) \right] + P_{DIBLC2} \quad (3.5.6)$$

$$\frac{1}{V_{ASCBE}} = \frac{P_{scbe2}}{L_{eff}} \exp\left(\frac{-P_{scbe1} l_{t0}}{V_{ds} - V_{dsat}}\right) \quad (3.5.7)$$

## 3.6 Single Current Expression for All Operating Regimes of $V_{gs}$ and $V_{ds}$

The  $V_{gsteff}$  function introduced in Chapter 2 gave a unified expression for the linear drain current from subthreshold to strong inversion as well as for the saturation drain current from subthreshold to strong inversion, *separately*. In order to link the continuous linear current with that of the continuous saturation current, a smooth function for  $V_{ds}$  is introduced. In the past, several smoothing functions have been proposed for MOSFET modeling [22-24]. The smoothing function used in BSIM3 is similar to that proposed in [24]. The final current equation for both linear and saturation current now becomes

$$I_{ds} = \frac{I_{dso}(V_{dseff})}{1 + \frac{R_{ds}I_{dso}(V_{dseff})}{V_{dseff}}} \left( 1 + \frac{V_{ds} - V_{dseff}}{V_A} \right) \left( 1 + \frac{V_{ds} - V_{dseff}}{V_{ASCBE}} \right) \quad (3.6.1)$$

Most of the previous equations which contain  $V_{ds}$  and  $V_{dsat}$  dependencies are now substituted with the  $V_{dseff}$  function. For example, Eq. (3.5.4) now becomes