Internship Program Report

By

GUNJI USHA SRI - 19485A0240

GUDLAVALLERU ENGINEERING COLLEGE

(An Autonomous Institute with Permanent Affiliation to JNTUK, Kakinada)
(Sponsored by A. A. N. M & V. V. R. S. R Educational Society, Gudlavalleru)
Approved by AICTE, New Delhi and Permitted by AP State Government
Accredited by NAAC with 'A' Grade

Counselling Code : GDLV

In association with

Smart Internz

Contents

Introduction

Internship program arranged by GUDLAVALLERU ENGINEERING COLLEGE in association with Smart Internz, Hyderabad for the benefit of 3rd year EEE batch 2018-2022 on Electrical Detailed design Engineering for Oil& Gas, Power and Utility industrial sectors.

Program organizer

Smart Bridge, Hyderabad.

Pioneer in organising Internships, knowledge workshops, debates, hackathons, Technical

sessions and Industrial Automation projects.

Courtesy

Dr. Sri B. Dasu – HOD – EEE, GEC

Mr. G. Srinivasa Rao – Internship coordinator

Mr. Ramesh V - Mentor

Mr. Vinay Kumar - System Support

Mr. Harikanth – Software/Technical Support

Program details

Smart Internz program schedule: 4 weeks starting from 3rd May 2021

Daily schedule time shall be 4PM to 6.30PM

Mode of Classes: On line through ZOOM

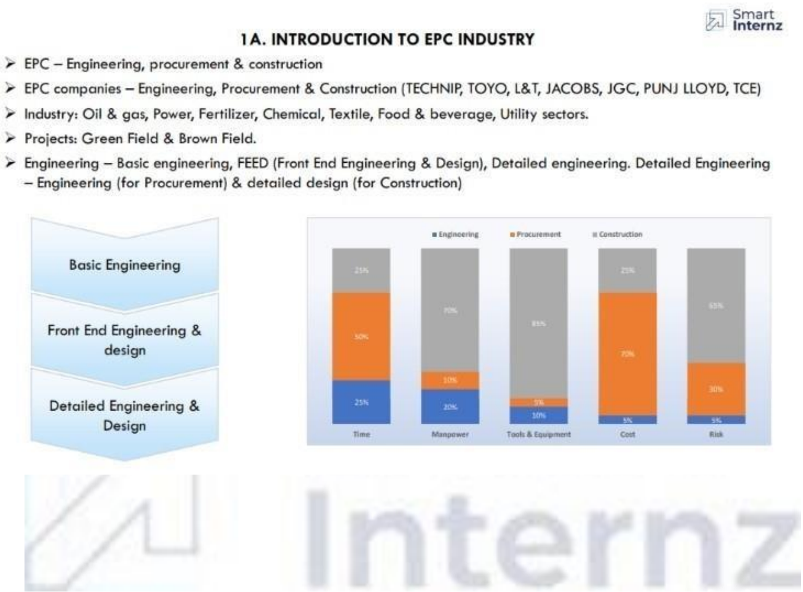
Presenter: Mr Ramesh V

Internship program

We have been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

3rd May2021: Introduction to EPC Industry

1	EPC Industry & Electrical Detailed Engineering	EPC Industry	Introduction
		Engineering	Types of Engineering
		Procurement	Engineering role in procurement
		Construction	Engineering role during construction

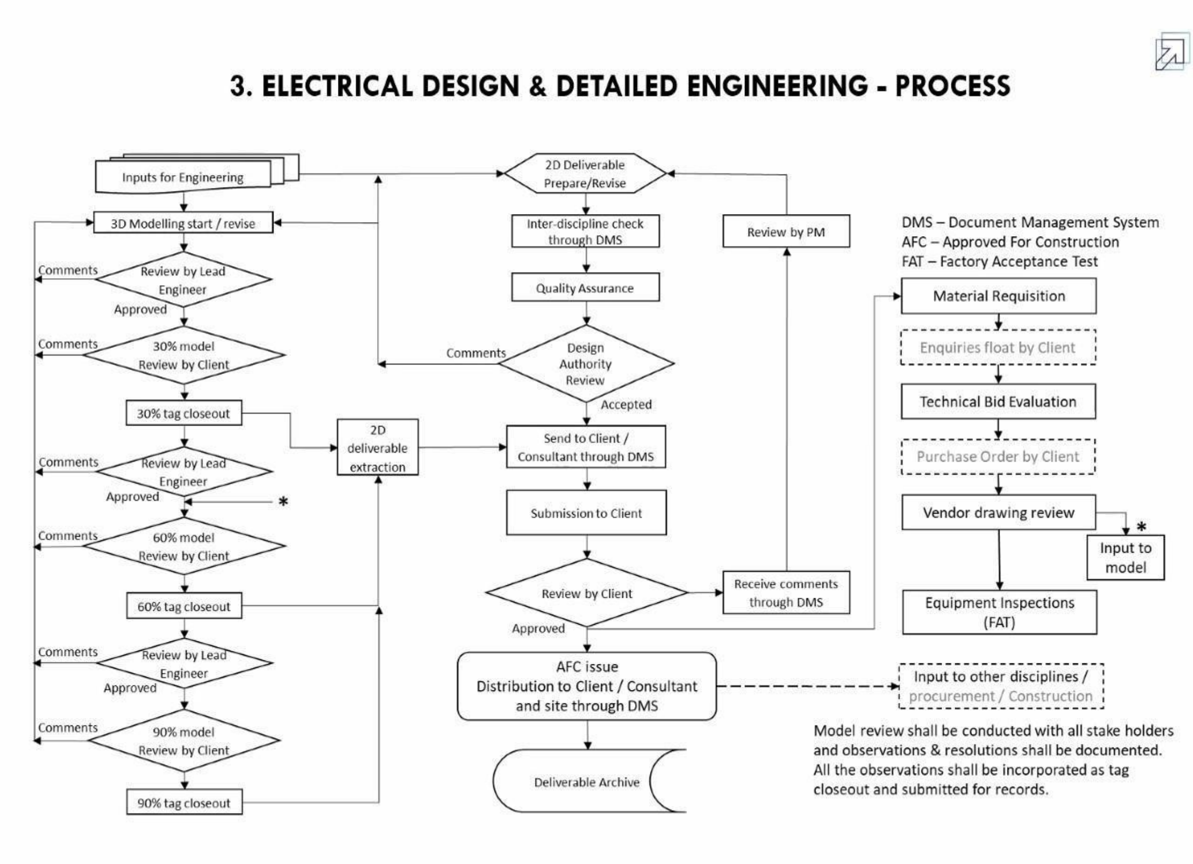


Topic details:

Engineering phases, Engineering deliverables (drawings & documents) list, Design Engineer role at various phases of project.

4th May2021: Engineering documentation for EPC projects

2	Electrical Design Documentation	Engineering Deliverables list	Sequence of deliverables
		Detailed Engineering work flow	Detailed engineering process
		Document transmission	Document submission and info exchange
		Deliverables types	Different types of deliverables



Topic details:

Engineering deliverables list, detailed engineering flow, engineering support flow,engineering support to procurements.

5th May2021: Engineering documentation for commands and formulae

3	Document & Drawing tools	MS Word	Report / Calculations formats
		MS Excel	Basic excel commands
		Auto cad	Basic line diagrams and layout commends

3C. AUTOCAD BASIC COMMANDS

Smart Internz

AUTOCAD BASIC KEYS							
STANDARD		DRAW		MODIFY		FORMAT	
NEW	Ctrl+N	LINE	L	ERASE	E	PROPERTIES	MO
OPEN	Ctrl+O	RAY	RAY	COPY	CO	SELECT COLOR	COL
SAVE	Ctrl+S	PLINE	PL	MIRROR	MI	LAYER	LA
PLOT	Ctrl+P	3DPOLY	3P	OFFSET	O	LINETYPE	LT
PLOT PREVIEW	PRE	POLIGONE	POL	ARRAY	AR	LINEWEIGHTS	LW
CUT	Ctrl+X	RECTANGLE	REC	MOVE	M	LT SCALE	LTS
COPY	Ctrl+C	ARC	A	ROTATE	RO	LIST	LI
PASTE	Ctrl+V	CIRCLE	C	SCALE	SC	DIMEN. STYLE	D
MATCH PROPE.	MA	SPLINE	SPL	STRECH	S	RENAME	REN
CLOSE	Ctrl+F4	ELLIPSE	EL	TRIM	TR	OPTION	OP
EXIT	Ctrl+Q	BLOCK	B	EXTENED	EX		
		POINT	PO	BRAKE	BR		
		HATCH	H	CHAMFER	CHA		
		GRADIENT	GD	FILLET	F		
		REGION	REG	EXPLODE	X		
		BOUNDARY	BO				
		DONUT	DO				

EXTRA				DRAFTING		PAPER SIZE
UNIT	UN	UCS	UCS	ORTHO	F8, Ctrl+L	A4=210*297
LIMITS	LIMITS	SINGLE TEXT	DT	OSNAP	F3, Ctrl+F	A3=297*420
(0,0; 1000,1000)		MULTILINE TEXT	MT	POLAR	F10, Ctrl+U	A2=420*594
ZOOM	Z	EDIT TEXT	ED	GRID	F7, Ctrl+G	A1=594*841
ALL	A	OBJECT SNAP	OB	OTRACK	F11	A0=841*1189
PAN	P	DIMENTION	DIM	SNAP	F9	
CLEAN SCREEN	Ctrl+0	HORIZONTAL	HOR			
COMMAMD WIN	Ctrl+9	VERTICAL	VER			

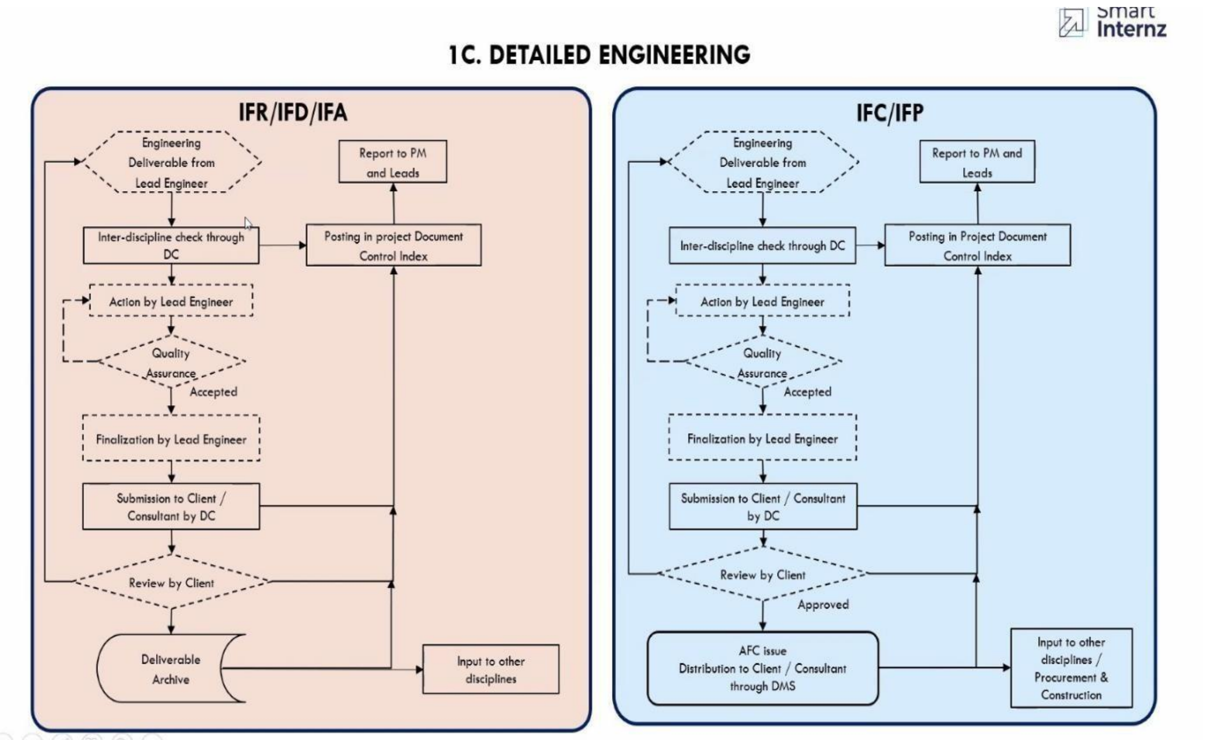
Topic details:

Here we need to learn the basis of the auto cad basic keys like standard, modify,draw,format,papersize etc..

7th May2021: Engineering documentation for Electrical system design

4	Electrical system design for a small small project	Overall plant description
		Sequence of approach
		Approach to detailed design

Topic details:



Here we observed that how to do a project and Sequence of approach, Approach to detail design and Overall plant distribution system.

10th May2021: Engineering documentation for Typical diagrams

5	Electrical system design for typical diagrams		
		Load lists schedule	Power flow diagram
		Single line diagram	Typical schematic diagram

S.No	Equipment No. (EQUIPMENT)	Description	Supply by	Vital	Essential	Non essential	Restarting	Absorbed load kW [A]	Equipment rating kW [B]	Load factor =A/B or nil [C] in decimals	Efficiency at load factor C [D] in decimals	Power factor at load factor C Cos φ	Continuous No.	Continuous kW [E]	Continuous kVAr	Intermittent and spares No.	Intermittent and spares kW [F]	Intermittent and spares kVAr	Stand-by No.	Stand-by kW [G]	Stand-by kVAr	Remarks	Revision
	PROCESS LOADS																						
1	PD-3431	Portable MEG Injection Pump Package	LEWA			x		27.00	37.00	0.73	0.91	0.83				1	29.67	19.94				Portable Skid (Please refer Note-d)	B
2	34-PM8401A	Liquid Return Pump Motor	LEWA			x		25.45	31.00	0.82	0.93	0.81				1	27.37	19.81					01
3	34-PM8401B	Liquid Return Pump Motor	LEWA			x		25.45	31.00	0.82	0.93	0.81							1	27.37	19.81		01
4	34-PM8402A	Booster Pump Motor (LRP Package)	LEWA			x		1.40	2.20	0.64	0.78	0.84				1	1.79	1.16					01
5	34-PM8402B	Booster Pump Motor (LRP Package)	LEWA			x		1.40	2.20	0.64	0.78	0.84							1	1.79	1.16		01
6	34-PM7902A	Corrosion Inhibitor Injection Pump Motor	LEWA			x		6.45	11.00	0.59	0.90	0.77	1	7.17	5.94								01
7	34-PM7902B	Corrosion Inhibitor Injection Pump Motor	LEWA			x		6.45	11.00	0.59	0.90	0.77							1	7.17	5.94		01
8	34-PM7903A	Batch Corrosion Inhibitor Injection Pump Motor	RAM			x		133.50	160.00	0.83	0.96	0.80							1	139.06	104.30		01
9	34-PM7903B	Batch Corrosion Inhibitor Injection Pump Motor	RAM			x		133.50	160.00	0.83	0.96	0.80							1	139.06	104.30		01
10	34-PM7904A	KHI Inhibitor Injection Pump Motor	LEWA			x		6.45	11.00	0.59	0.90	0.77	1	7.17	5.94							VSD for speed control	B
11	34-PM7904B	KHI Inhibitor Injection Pump Motor	LEWA			x		6.45	11.00	0.59	0.90	0.77							1	7.17	5.94	VSD for speed control	B
12	34-PM7905A	Scale Inhibitor Injection Pump Motor	FUTURE			x		3.00	4.00	0.75	0.85	0.81	1	3.53	2.56							Future	B
13	34-PM7905B	Scale Inhibitor Injection Pump Motor	FUTURE			x		3.00	4.00	0.75	0.85	0.81							1	3.53	2.56	Future	B
14	34-KM9602A	Nitrogen Compressor Motor	GENERON			x		30.00	37.50	0.80	0.90	0.80	1	33.33	25.00								01
15	34-KM9602B	Nitrogen Compressor Motor	GENERON			x		30.00	37.50	0.80	0.90	0.80	1	33.33	25.00								01
16	34-KM9602C	Nitrogen Compressor Motor	GENERON			x		30.00	37.50	0.80	0.90	0.80							1	33.33	25.00		01
17	34-EM9602A	Aftercooler for Nitrogen Compressor	GENERON			x		1.15	2.50	0.46	0.78	0.80				1	1.47	1.11					01
18	34-EM9602B	Aftercooler for Nitrogen Compressor	GENERON			x		1.15	2.50	0.46	0.78	0.80				1	1.47	1.11					01
19	34-EM9602C	Aftercooler for Nitrogen Compressor	GENERON			x		1.15	2.50	0.46	0.80	0.80							1	1.44	1.08		01
20	34-H9602	Nitrogen Heater						6.20	1.00	6.20	0.90	1.00											01
21	34-PM9701A	Hydraulic Fluid Pump - Wellhead HPU - Very High Pressure	FRAMES			x		0.19	0.55	0.35	0.80	0.70				1	0.24	0.24					B
22	34-PM9701B	Hydraulic Fluid Pump - Wellhead HPU - Very High Pressure	FRAMES			x		0.19	0.55	0.35	0.80	0.70				1	0.24	0.24					B
23	34-PM9702A	Hydraulic Fluid Pump - Wellhead HPU - Medium High Pressure	FRAMES			x		5.80	7.50	0.77	0.80	0.86				1	7.25	4.30					B
24	34-PM9702B	Hydraulic Fluid Pump - Wellhead HPU - Medium High Pressure	FRAMES			x		5.80	7.50	0.77	0.80	0.86				1	7.25	4.30					B
25	34-A9704A	Hydraulic Fluid Pump -IOPPS Valves HPU	LEDEEN			x		5.42	5.50	0.99	0.80	0.86				1	6.78	4.02					01
26	34-A9704B	Hydraulic Fluid Pump -IOPPS Valves HPU	LEDEEN			x		5.42	5.50	0.99	0.80	0.86				1	6.78	4.02					01
27	34-PM9705A	Hydraulic Fluid Pump - ESDV's HPU	LEDEEN			x		5.42	5.50	0.99	0.80	0.86				1	6.78	4.02					01
28	34-PM9705B	Hydraulic Fluid Pump - ESDV's HPU	LEDEEN			x		5.42	5.50	0.99	0.80	0.86				1	6.78	4.02					01
29	AC-3435	Crane motor	LIEBHERR			x		112.00	140.00	0.80	0.95	0.90				1	117.89	57.10					01
30	34-XZM8303	Lifeboat Recovery Starter Panel	SCHAT HARDING			x		8.74	9.39	0.93	0.91	0.82							1	9.60	6.70		01
31	CP34302	Flare Knock Out Drum Heater Control Panel	CHROMALOX			x		35.00	35.00	1.00	0.90	0.90				1	38.89	18.83					01
	HVAC LOADS																						
32	34-YH4201ACCU01	Air Cooled Condensing Unit - 01	CCTC		x			37.25	42.90	0.87	0.82	0.80	1	45.43	34.07								01
33	34-YH4201ACCU02	Air Cooled Condensing Unit - 02	CCTC		x			37.25	60.00	0.62	0.82	0.80							1	45.43	34.07		01
34	34-YH4201AHU01	Air Handling Unit - 01	CCTC		x			8.85	10.00	0.89	0.80	0.80	1	11.06	8.30								01
35	34-YH4201AHU02	Air Handling Unit - 02	CCTC		x			8.85	10.00	0.89	0.80	0.80							1	11.06	8.30		01
36	34-YH4201FF01	Fresh Air Fan - 01	CCTC		x			8.00	8.00	1.00	0.90	0.80	1	8.89	6.67								01
37	34-YH4201FF02	Fresh Air Fan - 02	CCTC		x			8.00	8.00	1.00	0.90	0.80							1	8.89	6.67		01
38	34-YH4201EF01	Exhaust Fan - Toilet	CCTC		x			1.00	1.00	1.00	0.90	0.80				1	1.11	0.83					01
39	34-YH4201EDH01	Duct heater - 01	CCTC		x			9.78	9.78	1.00	1.00	1.00				1	9.78	0.00					01
40	34-YH4201EDH02	Duct heater - 02	CCTC		x			4.69	4.69	1.00	1.00	1.00				1	4.69	0.00					01
41	34-YH4201EDH03	Duct heater - 03	CCTC		x			0.90	0.90	1.00	1.00	1.00				1	0.90	0.00					01
42	34-YH4201EDH04	Duct heater - 04	CCTC		x			4.98	4.98	1.00	1.00	1.00				1	4.98	0.00					01
	ELECTRICAL LOADS																						
43	AC-3431	Power Distribution Board	MASSEERA		x			41.00	51.50	0.80	0.98	0.80	1	41.84	31.38							Inclusive of MOV, Choke valve, Control valve and heat tracing loads	00
44	UPS-3441/3442/3443	UPS- Main/Bypass	GUTOR		x			24.00	24.00	1.00	0.82	0.80	1	29.27	21.95								B
45	BC-3442	Switchgear 24 V DC UPS	SAFT		x			1.20	1.20	1.00	0.80	0.80	1	1.50	1.13								00
46	LTR-3431	Lighting Transformer for LP-3431	SCHNEIDER		x			27.00	27.00	1.00	0.98	0.90	1	27.55	13.34							Inclusive of lighting load, convenience outlets and small power loads.	B
47	ELTR-3431	Lighting Transformer for ELP-3431	SCHNEIDER		x			27.00	27.00	1.00	0.98	0.90	1	27.55	13.34							Inclusive of lighting load, convenience outlets and small power loads.	B
48	WD-3431A	Welding Socket Outlet 1 - Upper Deck	STAHL			x		33.00	33.00	1.00	0.98	0.80							1	33.67	25.26		B
49	WD-3431B	Welding Socket Outlet 2 - Upper Deck	STAHL			x		33.00	33.00	1.00	0.98	0.80							1	33.67	25.26		B
50	WD-3432A	Welding Socket Outlet 1 - Lower Deck	STAHL			x		33.00	33.00	1.00	0.98	0.80							1	33.67	25.26		B
51	WD-3432B	Welding Socket Outlet 2 - Lower Deck	STAHL			x		33.00	33.00	1.00	0.98	0.80							1	33.67	25.26		B
52	WD-3433A	Welding Socket Outlet 1 - Mezz Deck	STAHL			x		33.00	33.00	1.00	0.98	0.80							1	33.67	25.26		B
53	WD-3433B	Welding Socket Outlet 2 - Mezz Deck	STAHL			x		33.00	33.00	1.00	0.98	0.80							1	33.67	25.26		B
54	WD-3434	Welding Socket Outlet - Cellar Deck	STAHL			x		33.00	33.00	1.00	0.98	0.80							1	33.67	25.26		B
	TOTAL													279	195		252	125		671	503		
	kVA = $\sqrt{kW^2+kVAr^2}$													339			282			838			

Max. of normal running plant load: (Est. x %E + y %F) 353 kW, 232 kVAr, $\sqrt{kW^2 + kVAr^2}$ 423 kVA

Peak load: (Est. x %E + y %F + z%G) 420 kW, 282 kVAr, $\sqrt{kW^2 + kVAr^2}$ 506 kVA

x = 100, y = 30, z = 10

Power factor without compensation [Cos φ] 0.836

Power factor with compensation [Cos φ_1]

Reqd capacitor rat. [= kW (tan φ - tan φ_1)] kVAr

Notes :

a) **Load classification/restarting:** For definitions of "Vital", "Essential" and Non - Essential", services and application of "Restarting", see DEP 33.64.10.10 - Gen. Electrical engineering guidelines.

b) **Absorbed loads:**
- for pumps, shaft load on duty point.
- for instrumentation, computers, communication, & air condit'g, the required load during full operation of plant.
- for lighting, during dark hours.
- for workshops, the average total load in normal full operation.

c) Consumed loads:
E - "Continuous": all loads that may continuously be required for normal operation operation including lighting and workshops
F - "Intermittent and spares": the loads required for intermediate pumping, storage, loading, etc. and all electrical spares of electrically driven units.
G - "Stand - by": loads required in emergencies only, such as fire water pumps or those of not normally running electrically driven units & electrical stand - by for normally running steam - driven ones (e.g. charge pumps, boiler feed pumps)

d) The Panel shall feed Injection Pumps P7901A/B.

e) Batch Injection pump considered as standby load during normal running condition based on operating philosophy.

QATARGAS 3&4
OFFSHORE FACILITIES PROJECT
WELLHEAD PLATFORM 7

J RAY McDERMOTT

REVISION	DATE	PREPARED BY	DESCRIPTION OF REVISION
01	24-Jun-07	AK	APPROVED FOR CONSTRUCTION
00	22-Aug-07	PJ	APPROVED FOR CONSTRUCTION WITH HOLD
B	18-Jul-07	PJ	ISSUED FOR COMPANY REVIEW
A	26-Oct-06	JG	ISSUED FOR IDC

11th May2021: Classification of Transformers and Generators

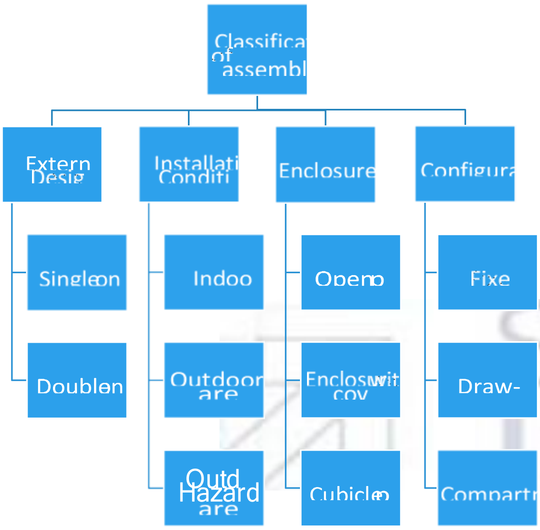
6	Classification of Transformers and Generators	Different types of Transformers	Different types of Generators

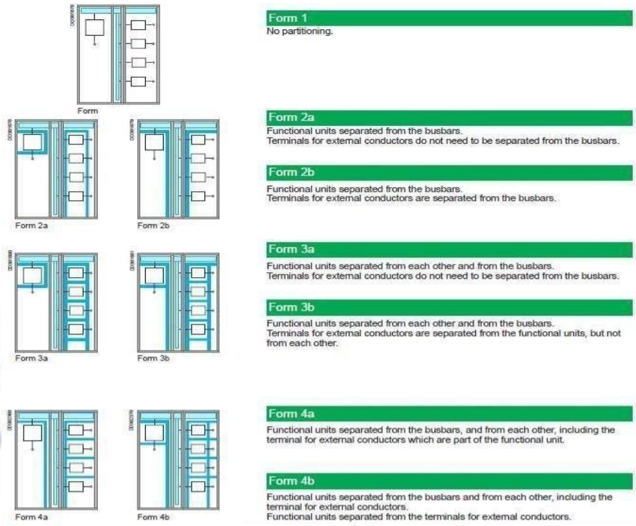
Topic details:

Classification of Transformers and Generators

12th May2021: Classification of Switch gear construction and power factor improvement

7	Classification of Switch gear construction and power factor improvement	Different types of Switch gear assembles	Power factor improvement



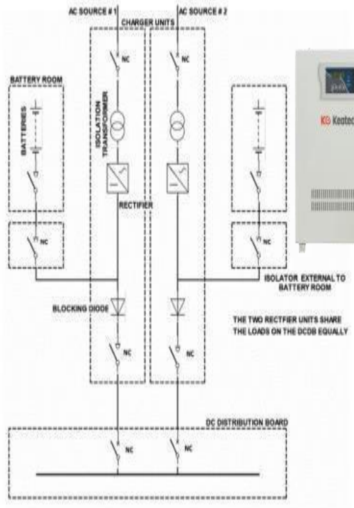


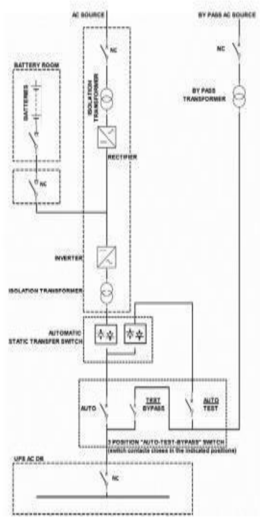
Topic details:

Classification of Switch gear construction and Power Factor Improvement

17th May2021: Detailing about UPS system and Bus ducts.

8	Detailing about UPS system and Bus ducts	Uninterruptible power supply system	Busduts of the system





110V or 220V DC UPS System

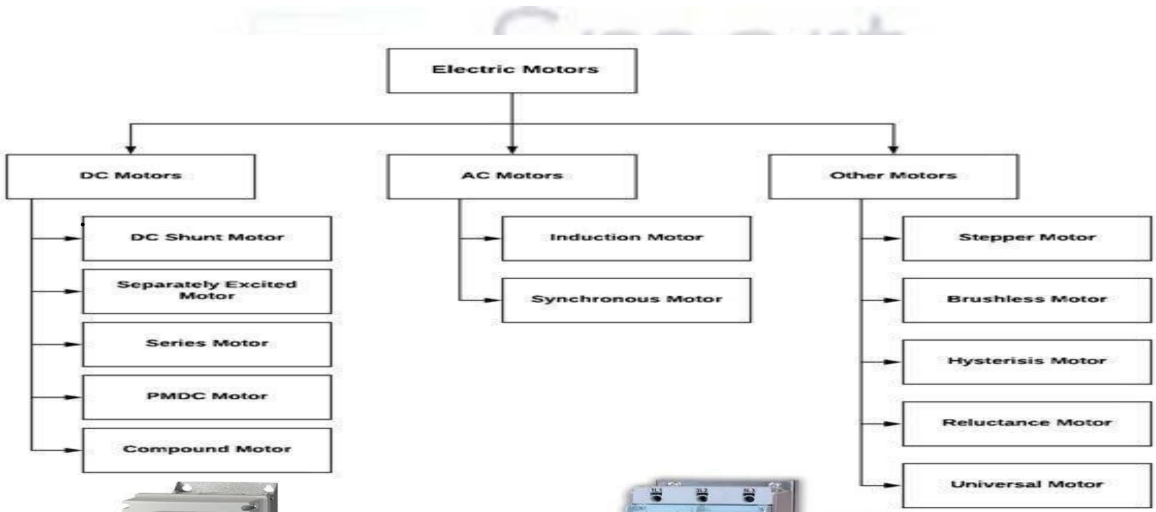
110V or 230V AC UPS System

Topic details: Power distribution of UPS system and Bus ducts.

UPS systems are designed to provide continuous power to a load, even with an interruption or loss of utility supply power. UPS generally involves a balance of cost Vs need.

18th May2021: Detailing about Motor Starters and Sizing of motors.

9	Detailing about Motor Starters and Sizing of motors	Motor starters and drives	Sizing and selection of motors



Topic details: Detailing about Motor Starter and Sizing of motors and their selection.

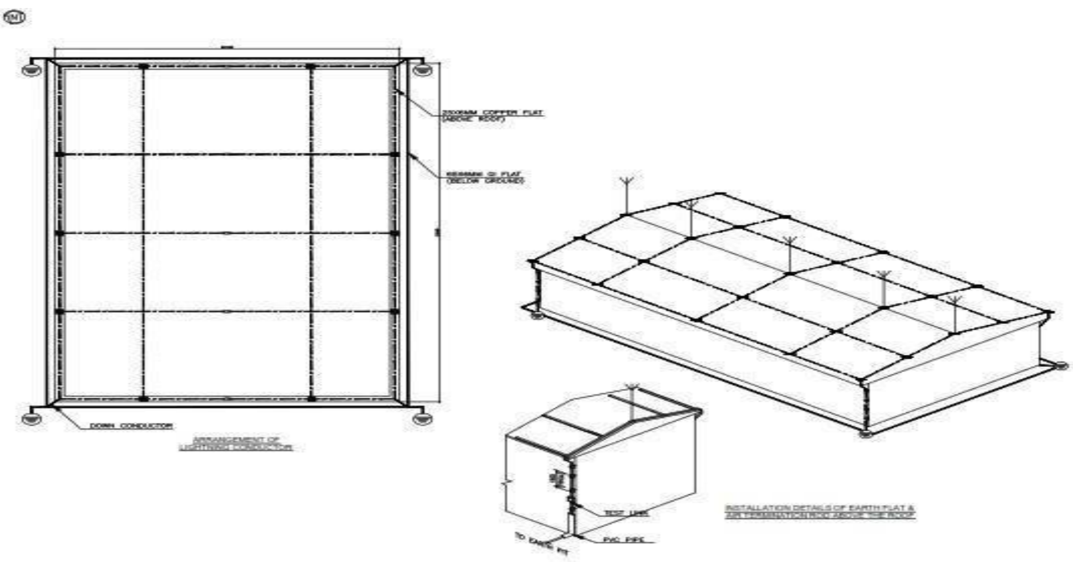
The principal function of a motor starter is to start and stop the respective motor connected with specially designed electromechanical switches which are similar in some ways to relays. The main difference between a relay and a starter is that a starter has overload protection for the motor that is missing in a relay.

Different types of motor starters are as follows:

- Direct-On-Line Starter
- Rotor Resistance Starter
- Stator Resistance Starter
- Auto Transformer Starter

19th May2021: Discribing about Earthing system and Lighting Protection.

10	Describing about Earthing system and Lighting Protection.	Plant Earthing system	Lighting Protection materials



Topic details: Describing about Earthing system and Lighting Protection.

Lightning protection required for high rise structures and important buildings against lightning currents during thunder storms. Primarily Lightning protection system calculations are done based on soil resistivity, conductor material, coverage structure / Building to determine whether lightning protection is required or not

20th May2021: Lighting or illumination systems and calculations.

11	Lighting or Illumination systems and Calculations	Lighting or illumination systems	Lighting calculations

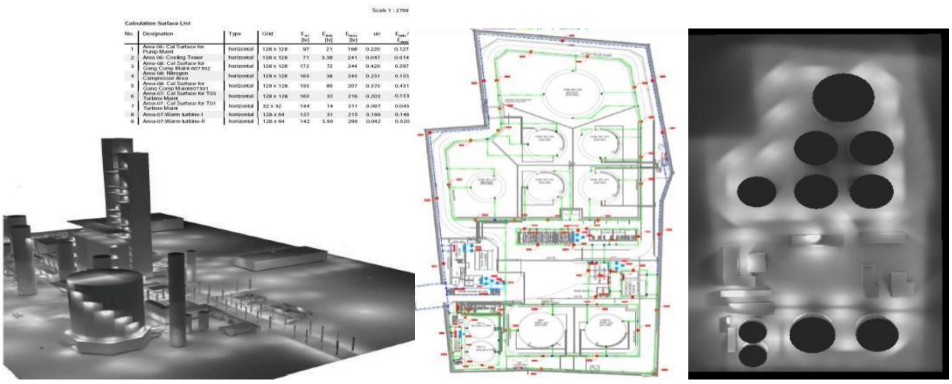
Topic details: Lighting or Illumination systems and Calculations.

All outdoor lighting fittings shall be connected with armoured PVC cable of suitable no. of cores and size. Necessary type and no. of junction boxes shall be provided for branch connections. Indoor light fittings shall be connected with FRLS PVC wires laid in cable trunks or conduits.

Inputs required: Equipment and cable routing layouts, lighting calculations, Design basis for type of light fittings to be used, required lux levels

Lighting calculations software: Dialux, Chalmlite, Calculux, Relux, Luxicon, CG

Lux Applicable Standards: IS 6665: Code of practice for industrial lighting, IS



3646: Code of practice for interior illumination, IEC 60598: Luminaires, IEC 62493: Assessment of lighting equipment related to human exposure to electromagnetic field

Deliverables: Indoor Lighting layouts, socket outlet layouts, Street lighting and area lighting layouts. BOQ.

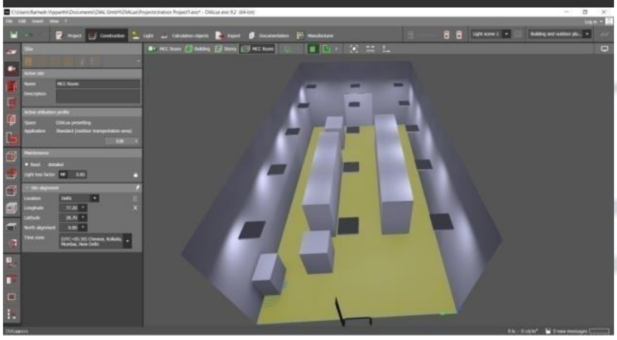
Types of light fittings: Industrial, flame proof type (EX d), increased safety type (Ex e).

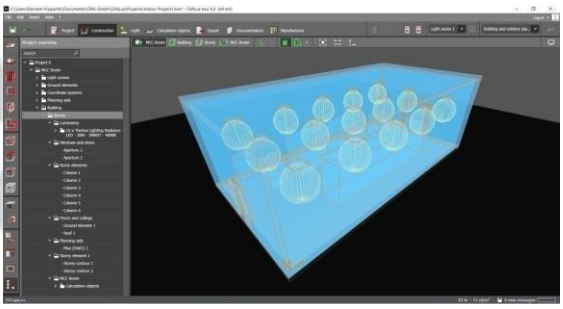
21th May2021: Lighting or illumination systems using DIALUX software.

12	Lighting or Illumination using DIALUX software	Lighting or illumination systems	Operation of dialux software

Topic details: Lighting or Illumination Calculations using DIALUX software.

Here we are using this Dialux evo 5.9.2 software windows to construct the power plant and we can perform the operation from this software.

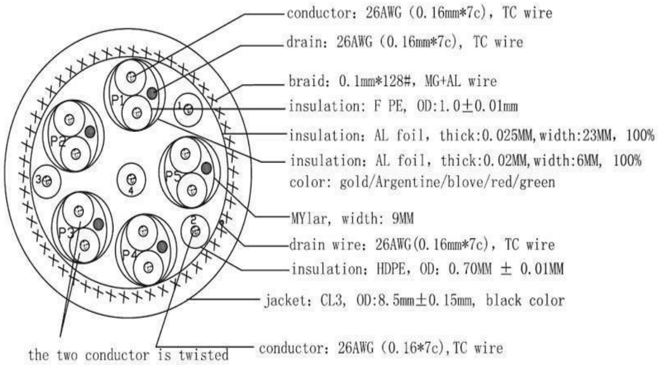


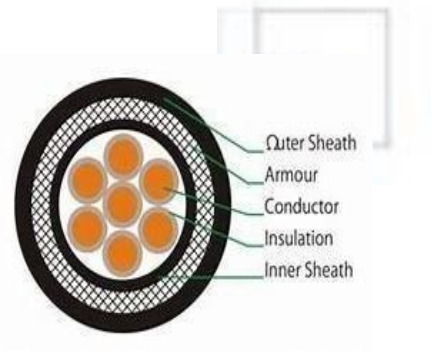


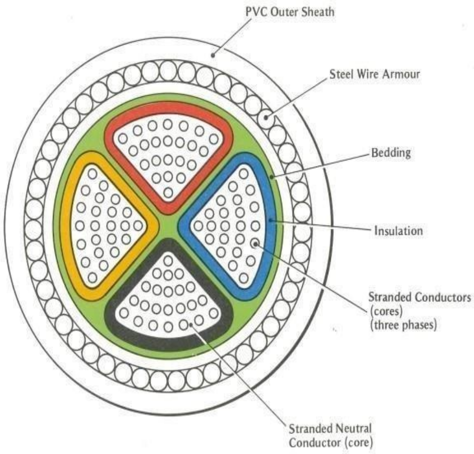
24th May2021: Cabling and their calculations and types.

13	Cabling and their Type and calculations	Cabling calculations	Types of cabling materials

Topic details: Cabling and their types and calculations .







Electrical cables must be properly supported to relieve mechanical stresses on the conductors, and protected from harsh conditions such as abrasion which might degrade the insulation.

Cables generally laid in the cable trays above ground, direct buried underground and in metallic or PVC conduits. Derating factors may be applicable for each type of cable laying conditions.

25th May2021: Cabling calculations and Cable gland selection.

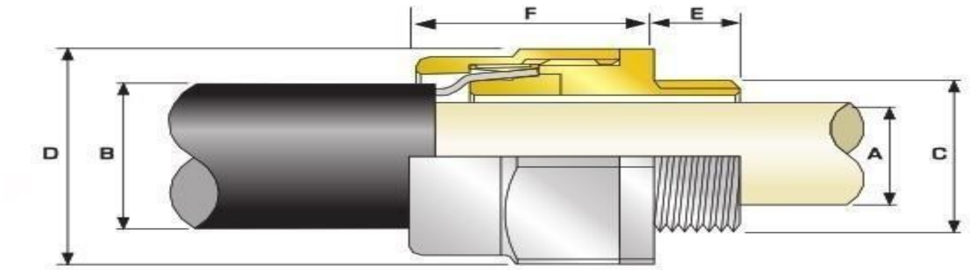
14	Cabling claculations and cable gland selection	Cabling calculations	Cable gland selection

Topic details: Cable sizing calculation and cable gland selection.

Inputs required: Load List, Design basis, Electrical equipment layout, cable schedule, vendor catalogues for cable tray.

Cable tray sizing shall be performed for each branch of cable tray routing up to the load point. Results shall be checked with specified limits mentioned in design basis.

Cable gland:



28th May2021: Load calculations and Transformer sizing calculations

15	Load calculations and TR calculations	Load calculations	TR calculations

Cable Gland Selection Table
Refer to illustration at the top of the page.

Cable Gland Size	Available Entry Threads "C" (Alternate Metric Thread Lengths Available)		Cable Bedding Diameter "A"	Overall Cable Diameter "B"	Armour Range		Across Flats "D"	Across Corners "D"	Protrusion Length "F"
	Metric	Thread Length (Metric) "E"	Max	Max	Min	Max	Max	Max	
20S16	M20	10.0	8.7	13.2	0.8	1.25	24.0	26.4	35.2
20S	M20	10.0	11.7	15.9	0.8	1.25	24.0	26.4	32.2
20	M20	10.0	14.0	20.9	0.8	1.25	30.5	33.6	30.6
25	M25	10.0	20.0	26.2	1.25	1.6	36.0	39.6	36.4
32	M32	10.0	26.3	33.9	1.6	2.0	46.0	50.6	32.6
40	M40	15.0	32.2	40.4	1.6	2.0	55.0	60.5	36.6
50S	M50	15.0	38.2	46.7	2.0	2.5	60.0	66.0	39.6
50	M50	15.0	44.1	53.1	2.0	2.5	70.1	77.1	39.1
63S	M63	15.0	50.0	59.4	2.0	2.5	75.0	82.5	52.0
63	M63	15.0	56.0	65.9	2.0	2.5	80.0	88.0	49.8
75S	M75	15.0	62.0	72.1	2.0	2.5	90.0	99.0	63.7
75	M75	15.0	68.0	78.5	2.5	3.0	100.0	110.0	57.3
90	M90	24.0	80.0	90.4	3.15	4.0	114.3	125.7	66.6

Topic details:

List of electrical load calculations.

ELECTRICAL LOAD CALCULATIONS LV MCC

SL No.	Equipment No.	Equipment Description	Breaker Rating A	Breaker Type	Breaker No. of Poles	ELCB Rating mA	Absorbed Load [A] kW	Motor / Load Rating [B] kW	Load Factor [A]/[B] [C] decimal	Efficiency at Load Factor [C] [D] decimal	Power Factor at Load Factor [C] cos φ	kW = [A]/[D] Continuous kW	kVAR	Consumed Load Intermittent kW	kVAR	kVAR = kW x tan φ Stand-by kW	kVAR	Remarks
1	PU2315	Silica filter feed pump					43.84	45.00	0.97	0.91	0.78	48.18	38.65					
2	PU 2314-A	Absorbent/Neutral oil pump (W)					12.73	15.00	0.85	0.85	0.73	15.0	14.0					
3	PU 2314 B	Absorbent/Neutral oil pump (S)					10.96	11.00	1.00	0.85	0.73					12.9	12.1	
4	PU2305	Feed Pump (Seperator)					44.28	45.00	0.98	0.91	0.78	48.7	39.0					
5	MX2305	MIXER (W)					44.62	45.00	0.99	0.91	0.78	49.0	39.3					
6	MX 2308	MIXER (S)					44.62	45.00	0.99	0.91	0.78					49.0	39.3	
7	BW2313	Blower					19.16	22.00	0.87	0.91	0.78	21.1	16.9					
8	Rotary valve	TK 2313B (I)					1.86	2.20	0.85	0.85	0.73			2.2	2.0			
9	SC2314	Screw conveyor (I)					4.30	4.70	0.91	0.85	0.73			5.06	4.74			
10	AG 2324A	Citric acid tan agitator (W)					3.23	3.70	0.87	0.85	0.73	3.80	3.56					
11	AG 2324B	Citric acid tank agitator (S)					3.23	3.70	0.87	0.85	0.73					3.8	3.6	
12	AG 2305	Citric oil rection vessel agitator					11.75	15.00	0.78	0.85	0.73	13.82	12.94					
13	AG 2309	Lye oil reaction vessel agitator					4.27	4.70	0.91	0.85	0.73	5.02	4.70					
14	AG 2310	Lye oil reaction vessel agitator					4.27	4.70	0.91	0.85	0.73	5.02	4.70					
15	AG 2314	Soap Adsorbant Tank Agitator					7.48	7.50	1.00	0.85	0.73	8.80	8.24					

Maximum of normal running plant load : (Est. x%E + y%F)	220.5 kW	184.1 kVAR	sqrt (kW² +kVAR²) = 287.3 kVA	TOTAL	218.37	182.09	7.25	6.78	65.73	54.97
Peak Load : (Est. x%E + y%F + z%G)	227.1 kW	189.6 kVAR	sqrt (kW² +kVAR²) = 295.9 kVA	kVA	284.32		9.93		85.68	

Assumptions

1) Load factor, Efficiency and Power factor.

Load Rating (kW)	Efficiency	Power factor
<= 20	0.85	0.73
>20 - <= 45	0.91	0.78
>45 - < 150	0.93	0.82
>= 150	0.94	0.91

2) Coincidence factors x= 1.0, y= 0.3, and z=0.1 considered for contnious, intermittent and standby load.

Transformer Calculations:

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	218.4	182.1	284.32	--- (i)
b. Intermittent load / Diversity Factor	7.25	6.8	9.93	--- (ii)
c. Stand-by load required as consumed load	65.73	55.0	85.71	--- (iii)
Max. Consumed load = (i) + 30%(ii) +10%(iii)	227.1	189.6	295.88	
Future expansion load (20%capacity)	45.4	37.9	59.18	
Total Load =	272.5	227.6	355.06	

1.2 Calculation for 3.3kV/0.433kV transformer capacity

Max. Consumed load = 295.9 kVA
Spare capacity = 59.2 kVA
Required capacity = 355.1 kVA
Transformer rated capacity = 120 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW), while all the other loads running, the voltage regulation is as

P = 355 KVA (%Z) = 4.12 [illegible] 5.8

Hence %R = 1.027 %

%X = 3.98 %

P_M = 45 KW having (K = 6 & C = 1 & Cos θ = 0.78 & Eff. = 0.91 & Cos θst = 0.25

P_s = 360.4 KVA

Cos $θ_s$ = 0.25 Corresponding to Angle $θ_s$ = 75.52 Degrees for which Sin $θ_s$ = 0.97

P_L = 263 KVA & PB in KW is = 223.6 & P_L in Kvar = 255.11 Cos $θ_L$ = 0.850

Cos $θ_L$ = 0.85 Corresponding to Angle $θ_L$ = 31.79 Degrees for which Sin $θ_L$ = 0.53

P_{kw} = 316.6 KW

P_{kvar} = 623.4 KVAR

P_t = 700.1 KVA

Cos $θ_t$ = 0.456 where as Sin $θ_t$ = 0.890

Voltage Regulation = 7.6 %

Result: During starting of max. capacity motor, while all other loads are running, the voltage regulation at Transformer secondary terminals is approx. 5.3%, which meets the criteria to maintain less than 15% voltage regulation.

1.4 Selection of rated capacity

120 KVA transformer selected.

29th May2021: DG set calculations

Topic details:

Transformer and DG set calculations,types ,sizing or selections.

	DG SIZING CALCULATIONS	
	Design Data	
	Rated Volatge	415
	Power factor (CosØ)	0.87
	Efficiency	0.74
	Total operating load on DG set in kVA at 0.87 power factor	287.3
	Largest motor to start in the sequence - load in KW	45
	Running kVA of last motor (CosØ= 0.91)	70
	Starting current ratio of motor	6
	Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	419
	Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	217
A	**Continous operation under load -P1**	
	Capacity of DG set based on continuous operation under load P1	217
B	**Transient Voltage dip during starting of Last motor P2**	
	Total momentary load in KVA	637
	(Starting KVA of the last motor+Base load of DG set in KVA	
	Subtransient Reactance of Generator (Xd")	7.91%
	Transient Reactance of Generator (Xd')	10.065%
	Xd"' =(Xd"+Xd')/2	0.089875
	Transient Voltage Dip	15%
	Transient Voltage dip during Soft starter starting of Last motor P2 = Total momentary load in KVA x Xd"' x (1-Transient Voltage Dip) / (Transient Voltage Dip)	324
C	**Overload capacity P3**	
	Capacity of DG set required considering overload capacity	
	Total momentary load in KVA	637
	overcurrent capacity of DG (K)	150%
	(Ref: IS/IEC 60034-1, Clause 9.3.2)	
	Capacity of DG set required considering overload capacity (P3) = Total momentary load in KVA / overcurrent capacity of DG (K)	425
	Considering the last value amongst P1, P2 and P3	
	Continous operation under load -P1	217
	Transient Voltage dip during Soft starter starting of Last motor P2	324
	Overload capacity P3	425
	Considering the last value amongst P1, P2 and P3	425
	Hence, Existing Generator 425 KVA is adequate to cater the loads as per re-scheduled loads	
	NOTE :VOLTAGE DIP CONSIDERED - 15%	

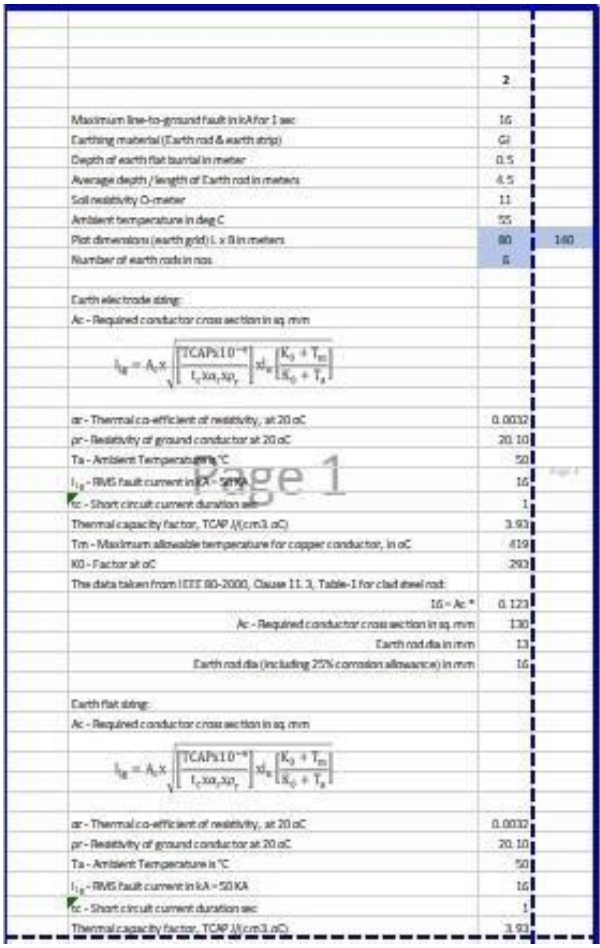
2nd june2021: Calculations of Earthing and Lighting protection.

17	Calculation of Earthing and Lighting protection calculations	Earthing calculations	Lighting protection calculation

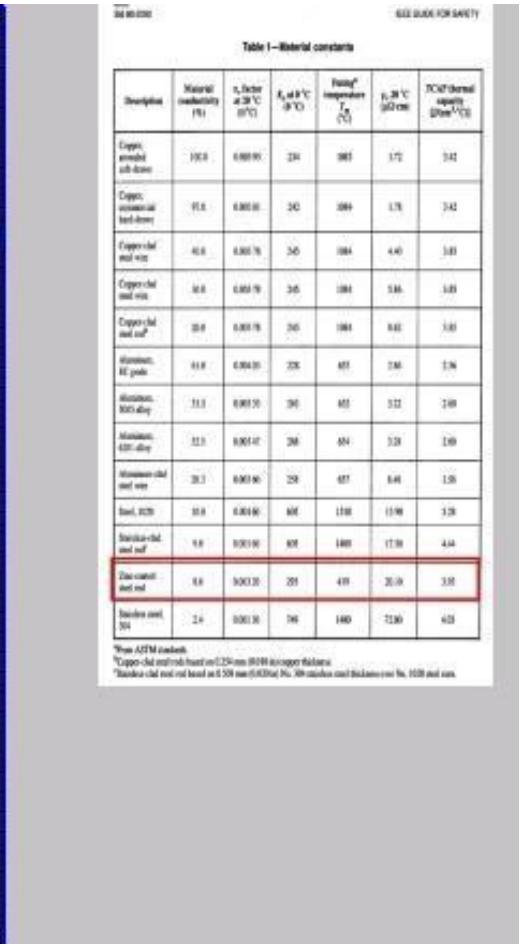
Topic details:

Calculation of Earthing and Lighting protection calculations

Earthing calculations:



	2	
Maximum line-to-ground fault in kA for 1 sec	16	
Earthing material (Earth rod & earth strip)	GI	
Depth of earth flat burial in meter	0.5	
Average depth / length of Earth rod in meters	4.5	
Soil resistivity Ω-meter	11	
Ambient temperature in deg C	55	
Plot dimensions (earth grid) L x B in meters	80	140
Number of earth rods in nos	6	
Earth electrode sizing:		
Ac - Required conductor cross section in sq. mm		
$I_g = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c x\alpha_r x\rho_r}\right] x l_n \left[\frac{K_0 + T_m}{K_0 + T_a}\right]}$		
αr - Thermal co-efficient of resistivity, at 20 oC	0.0032	
ρr - Resistivity of ground conductor at 20 oC	20.10	
Ta - Ambient Temperature °C	50	
I_g - RMS fault current in kA - 50KA	16	
tc - Short circuit current duration sec	1	
Thermal capacity factor, TCAP J/(cm3.oC)	3.93	
Tm - Maximum allowable temperature for copper conductor, in oC	419	
K0 - Factor at oC	293	
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:		
16 = Ac *	0.123	
Ac - Required conductor cross section in sq. mm	130	
Earth rod dia in mm	13	
Earth rod dia (including 25% corrosion allowance) in mm	16	
Earth flat sizing:		
Ac - Required conductor cross section in sq. mm		
$I_g = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c x\alpha_r x\rho_r}\right] x l_n \left[\frac{K_0 + T_m}{K_0 + T_a}\right]}$		
αr - Thermal co-efficient of resistivity, at 20 oC	0.0032	
ρr - Resistivity of ground conductor at 20 oC	20.10	
Ta - Ambient Temperature is °C	50	
I_g - RMS fault current in kA = 50 KA	16	
tc - Short circuit current duration sec	1	
Thermal capacity factor, TCAP J/(cm3.oC)	3.93	



Tm – Maximum allowable temperature for copper conductor, in oC	419
K0 – Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	
16 – Ac *	0.123
Ac – Required conductor cross section in sq. mm	130
Earth flat area in mm	13
Earth flat area (including 25% corrosion allowance) in mm	16
Selected flat size W * Thk in sq mm	20

Rg – Grid resistance

Grid resistance can be calculated using Eq. 52 of IEEE 80

$$R_g = \rho\left[\frac{1}{L} + \frac{1}{\sqrt{20 \times A}}\left[1 + \frac{1}{1 + h\sqrt{20/A}}\right]\right]$$

ρ – Soil resistivity in Ω-meter~	11
L – Total buried length of ground conductor in meter	480
h – Depth of burial in meter	0.5
A – Grid area in sq. meter	11200
Rg – Grid resistance	0.071

Rr – Earth Electrode resistance

Grid resistance can be calculated using Eq. 55 of IEEE 80

$$R_2 = \frac{\rho}{2 \times \pi \times n_R \times L_R}\left\{\ln\left[\frac{4 \times L_R}{b}\right] - 1 + \frac{2 \times k_1 \times L_R}{\sqrt{A}}\left(\sqrt{n_R} - 1\right)^2\right\}$$

ρ – Soil resistivity in Ω-meter, 16.96	11
n – No of earth electrodes	6
Lr – Length of earth electrode in meter	4.5
b – Diameter of earth electrode in meter	0.020
k1 – co-efficient	1
A – Area of grid in square metre	11200
Rr – Earth Electrode resistance	4.04156

Grounding system resistance

Grounding system resistance can be calculated using equation 53 of IEEE 80 as follows:

$$R_g = \frac{R_1 \times R_2 - R_m^2}{R_1 + R_2 - 2R_m}$$

R_m – Mutual ground resistance between the group of ground conductors, R_1 and group of electrodes, R_2 in Ω. Neglected R_m since this is for homogenous soil

Rt – Total earthing system resistance	0.070	Ohms

The calculated resistance grounding system is less than the allowable 1 Ω value.

Lightining Calculations:

		1					
	Location	Gwalior					
	Building	Concrete, Hospital					
	Type of Building	Flat Roofs (a)					
	Building Length (L)	20					
	Building breadth (W)	9					
	Building Height (H)	7					
	Risk Factor Calculation						
1	**Collection Area (A_c)**						
	A_c			=	(L*W) + (2*L*H) + (2*W*H) + (3.14*H*H)		
					739.86		
2	**Probability of Being Struck (P)**						
	P			=	Ac * Ng * 10-6		
					0.002737482		
3	**Overall weighing factor**						
	a) Use of structure (A)			=	1.7		
	b) Type of construction (B)			=	1.0		
	c) Contents or consequential effects (C)			=	1.7		
	d) Degree of isolation (D)			=	1.0		
	e) Type of country (E)			=	0.3		
	Wo Overall weighing factor			=	A * B * C * D * E		
				=	0.510		
4	**Overall Risk Factor**		Po	=	P * Wo		
			Po	=	0.001396116		
			Pa		10^{-5}		
	As per clause no. 9.7 of BS 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}						
	Since Po > Pa lightning protection required.						
5	**Air Terminations**						
	Perimeter of the building			=	2(L+W)		
				=	58	Mts.	
6	**Down Conductors**						
	Perimeter of building			=	58	Mts.	
	No. of down conductors based on perimeter			=	3	Nos.	
	Hence 3 nos. of Down conductors have been selected.						
	Size of Down conductor			=	20 X 2.5 mm Galvanized Steel Strip		
	(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross section of the conductor. The minimum size of Down conductors : 20mm X 2.5 mm Galvanized Steel Strip)						

5thjune 2021: Cable sizing and cable tray sizing calculations.

18	Cable sizing and cable tray sizing calculations	Cable sizing calculations	Cable tray calculation

Topic details:

Cable sizing and cable tray sizing calculations for LV cables and MV/HV cables.

S.NO.	Description	Equipment No.	Description	Consumed Load KW	Load Rating KW	Voltage (V)	No. of ph	Full Load Current	Motor Starting Current	Load P.F. Running	SIN Φ Running	Motor P.F Staring	SIN Φ Starting	T	No. of Ru	No. of Co	Size (m	Current Rati (A	Derating fact k1	Derating fact k2	Derating fact k3	Derating fact k4	Overall Derating fact k	Derated Cu	Cable Le	Cable Resistance (Ohms/kM)	Cable Reactance (Ohms/kM)	Voltage drop (Running)	Voltage drop (Running)	Voltage drop (Starting) (V)	Voltage drop (starting)	Cable size result	ODof Cable (mm)	Gland size
3	LV MCC	PU2315	Silica filter feed pump	43.84	45.00	415	3	78.2	457.44	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	95	0.9300	0.0816	9.95	2.40	59.07	14.23	OK	22	20
4	LV MCC	PU2322A	Soft water pump	12.73	15.00	415	3	22.1	132.83	0.8	0.6	0.8	0.5	2	1	4.0	10	68	0.98	0.9	1	1	0.882	58.2	95	2.3400	0.0852	7.01	1.69	41.84	10.08	OK	18	20s
5	LV MCC	PU 2314A	Absorbent/Neutral oil pump	10.98	11.00	415	3	19.1	114.38	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	60	5.9000	0.0947	9.48	2.28	56.86	13.65	OK	17	20s
6	LV MCC	PU2324	Citric Acid Tank pump	44.28	45.00	415	3	77.0	462.03	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	85	0.9300	0.0816	8.99	2.17	53.38	12.86	OK	22	20s
7	LV MCC	PU2333	Soap Oil pump	44.82	45.00	415	3	77.6	465.58	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	75	0.9300	0.0816	7.99	1.93	47.46	11.44	OK	22	20s
8	LV MCC	PU 23228	Soft water pump-Stand by	44.82	45.00	415	3	77.6	465.58	0.8	0.6	0.8	0.5	2	1	4.0	35	148	0.98	0.9	1	1	0.882	130.5	105	0.6710	0.0794	8.25	1.99	48.81	11.76	OK	24	20s
9	LV MCC	PU2321A	Lye/Simplex Metering Pump	19.16	22.00	415	3	33.3	199.92	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	100	1.4700	0.0815	7.07	1.70	42.13	10.15	OK	21	20s
10	LV MCC	PU2321B	Lye storage tank pump	1.86	2.20	415	3	3.2	19.41	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	100	5.9000	0.0947	2.68	0.64	16.03	3.86	OK	17	20s
11	LV MCC	PU2305	Feed Pump(Separator)	4.30	4.70	415	3	7.5	44.87	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	3.11	0.75	18.63	4.49	OK	18	20
12	LV MCC	PU2332	Soap Stock Pump	3.23	3.70	415	3	5.6	33.70	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	110	9.4800	0.1007	8.18	1.97	49.02	11.81	OK	18	20s
13	LV MCC	MX2305	Mixer	3.23	3.70	415	3	5.6	33.70	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	2.34	0.56	14.00	3.37	OK	18	20
14	LV MCC	MX2308	Mixer	11.75	15.00	415	3	20.4	122.60	0.8	0.6	0.8	0.5	2	1	4.0	10	68	0.98	0.9	1	1	0.882	58.2	105	2.3400	0.0852	7.15	1.72	42.69	10.29	OK	18	20
15	LV MCC	CF2312	Separator	4.27	4.70	415	3	7.4	44.55	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	85	0.9300	0.0816	0.87	0.21	5.15	1.24	OK	22	32
16	LV MCC	BW2313	Blower	4.27	4.70	415	3	7.4	44.55	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	95	9.4800	0.1007	9.34	2.25	55.97	13.49	OK	18	20s
17	LV MCC	RV 2314	Rotary valve	7.48	7.50	415	3	13.0	78.05	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	65	5.9000	0.0947	7.00	1.69	41.89	10.09	OK	17	20s
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Basis:

1. Overall derating factor k = k1 x k2 x k3 x k4
   - K1=Rating factor for variation in air/ground temperature
   - K2=Rating factor for depth of laying
   - K3=Rating factor for spacing between two circuits
   - K4=Rating factor for variation in thermal resistivity of the soil
2. LT Motors : Running Voltage Drop = 3%, Starting Voltage Drop = 15%
3. Cable type
   - TYPE 1: Al Conductor, XLPE Insulated, Armoured, PVC outer sheathed
   - TYPE 2: Cu Conductor, XLPE Insulated, Armoured, PVC outer sheathed
4. Effect of Frequency Variation ± 5%
5. Combined Effect of Voltage & Frequency Variation ±10%

Conclusion

We have been taught many aspects of engineering activities during the EPC stages for all electrical and related other disciplines also.

Feedback

Smart Bridge

They conduct summer internships, work shops, debates, hackthons, technical sessions.

Method of conducting program

Online virtual program with presentation slides and explanation on the topic and practical usage of topic and with some examples.

Program highlights

It is for the detailed design of any industrial sectors.

Material

The material was good .

Benefits

It has been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

ELECTRICAL LOAD CALCULATIONS LV MCC

Assignment 1

Sl. No.	Equipment No.	Equipment Description	Breaker Rating	Breaker Type	Breaker No. of Poles	ELCB Rating	Absorbed Load [A]	Motor / Load Rating [B]	Load Factor [A] / [B] [C]	Efficiency at Load Factor [C] [D]	Power Factor at Load Factor [C]	Consumed Load (kW = [A] / [D]; kVAR = kW x tan φ) Continuous		Intermittent		Stand-by		Remarks
			A			mA	kW	kW	decimal	decimal	cos φ	kW	kVAR	kW	kVAR	kW	kVAR	
1	PU2315	Silica filter feed pump					43.84	45.00	0.97	0.91	0.78	48.18	38.65					
2	PU 2314-A	Absorbesnt/Neutral oil pump (W)					12.73	15.00	0.85	0.85	0.73	15.0	14.0					
3	PU 2314 -B	Absorbesnt/Neutral oil pump (S)					10.96	11.00	1.00	0.85	0.73					12.9	12.1	
4	PU2305	Feed Pump (Seperator)					44.28	45.00	0.98	0.91	0.78	48.7	39.0					
5	MX2305	MIXER (W)					44.62	45.00	0.99	0.91	0.78	49.0	39.3					
6	MX 2308	MIXER (S)					44.62	45.00	0.99	0.91	0.78					49.0	39.3	
7	BW2313	Blower					19.16	22.00	0.87	0.91	0.78	21.1	16.9					
8	Rotary valve	TK 2313B (I)					1.86	2.20	0.85	0.85	0.73			2.2	2.0			
9	SC2314	Screw conveyor (I)					4.30	4.70	0.91	0.85	0.73			5.06	4.74			
10	AG 2324A	Citric acid tan agitator (W)					3.23	3.70	0.87	0.85	0.73	3.80	3.56					
11	AG 2324B	Citric acid tank agitator (S)					3.23	3.70	0.87	0.85	0.73					3.8	3.6	
12	AG 2305	Citric oil rection vessol agitator					11.75	15.00	0.78	0.85	0.73	13.82	12.94					
13	AG 2309	Lye oil reaction vessel agitator					4.27	4.70	0.91	0.85	0.73	5.02	4.70					
14	AG 2310	Lye oil reaction vessel agitator					4.27	4.70	0.91	0.85	0.73	5.02	4.70					
15	AG 2314	Soap Adsorbant Tank Agitator					7.48	7.50	1.00	0.85	0.73	8.80	8.24					
											TOTAL	218.37	182.09	7.25	6.78	65.73	54.97	
											kVA	284.32		9.93		85.68		

Maximum of normal running plant load : 220.5 kW 184.1 kVAR sqrt (kW² +kVAR²) = 287.3 kVA
(Est. x%E + y%F)

Peak Load : 227.1 kW 189.6 kVAR sqrt (kW² +kVAR²) = 295.9 kVA
(Est. x%E + y%F + z%G)

Assumptions

1) Load factor, Efficiency and Power factor.

Load Rating (kW)	Efficiency	Power factor
<= 20	0.85	0.73
> 20 - <= 45	0.91	0.78
> 45 - < 150	0.93	0.82
>= 150	0.94	0.91

2) Coincidence factors x= 1.0, y= 0.3, and z=0.1 considered for contnious, intermittent and standby load.

DG SIZING CALCULATIONS

	Design Data	
	Rated Volatge	415
	Power factor (CosØ)	0.87
	Efficiency	0.74
	Total operating load on DG set in kVA at 0.87 power factor	**287.3**
	Largest motor to start in the sequence - load in KW	45
	Running kVA of last motor (CosØ= 0.91)	70
	Starting current ratio of motor	6
	Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	**419**
	Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	**217**
A	**Continous operation under load -P1**	
	Capacity of DG set based on continuous operation under load P1	**217**
B	**Transient Voltage dip during starting of Last motor P2**	
	Total momentary load in KVA	637
	(Starting KVA of the last motor+Base load of DG set in KVA	
	Subtransient Reactance of Generator (Xd'')	7.91%
	Transient Reactance of Generator (Xd')	10.065%
	Xd''' =(Xd"+Xd')/2	0.089875
	Transient Voltage Dip	15%
	Transient Voltage dip during Soft starter starting of Last motor P2 = Total momentary load in KVA x Xd'" x $\frac{\text{(1-Transient Voltage Dip)}}{\text{(Transient Voltage Dip)}}$	**324**
C	**Overload capacity P3**	
	Capacity of DG set required considering overload capacity	
	Total momentary load in KVA	637
	overcurrent capacity of DG (K)	150%

(Ref: IS/IEC 60034-1, Clause 9.3.2)

Capacity of DG set required considering overload capacity (P3) = Total momentary load in KVA / overcurrent capacity of DG (K)	**425**

Considering the last value amongst P1, P2 and P3

Continous operation under load -P1	217
Transient Voltage dip during Soft starter starting of Last motor P2	324
Overload capacity P3	425
Considering the last value amongst P1, P2 and P3	**425**

Hence, Existing Generator 425 KVA is adequate to cater the loads as per re-scheduled loads

NOTE:VOLTAGE DIP CONSIDERED - 15%

Assignment-3

Calculation for Transformer Capacity

Example of calculation for Transformer Capacity
Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	218.37	182.1	284.33	--- (i)
b. Intermittent load / Diversity Factor	7.25	6.8	9.94	--- (ii)
c. Stand-by load required as consumed load	65.73	55.0	85.71	--- (iii)
Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	227.1	189.6	295.88	
Future expansion load (20% capacity)	45.4	37.9	59.18	
Total Load =	272.5	227.6	355.06	

Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	295.9 kVA
Spare capacity	=	59.2 kVA
Required capacity	=	355.1 kVA
Transformer rated capacity	=	120 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follow

P_T = 355 KVA (%Z)= 4.12 & Ratio X/R = 3.8

Hence , **%R** = = 1.037 %

%X = = 3.99 %

P_M = 45 KW having (K = 6 & C = 1 & Cos θ = 0.78 & Eff.η = 0.91 & Cos Θs = 0.25

P_S = = 380.389 KVA

Cos θ_S = 0.25 ,Corresponding to Angle θ_s = 75.5225 Degrees for which Sin θ_s = 0.97

P_B = 263 KVA & PB in KW is = 223.55 & P_B in Kvar = 255.11 ∴ Cos θ_B = 0.850

Cos θ_B = 0.85 ,Corresponding to Angle θ_s = 31.7883 Degrees, for which Sin θ_s = 0.53

P_{CP} = = 318.647 KW

P_{CQ} = = 623.42 KVAR

P_C = = 700.135 KVA

Cos θ_C = = 0.45512 , where as Sin θ_C = 0.890

Voltage Regulation ε = 7.9 %

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals is approx. 5.3% , which meets the criteria to maintain less than 15% voltage regulation.

1.4 Selection of rated capacity

120 kVA transformer selected.

Assignment-4 2

Earthing calculations:

Maximum line-to-ground fault in kA for 1 sec	16
Earthing material (Earth rod & earth strip)	GI
Depth of earth flat burrial in meter	0.5
Average depth / length of Earth rod in meters	4.5
Soil resistivity Ω-meter	11
Ambient temperature in deg C	55
Plot dimensions (earth grid) L x B in meters	80
Number of earth rods in nos.	6

Earth electrode sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c x \alpha_r x \rho_r}\right] x l_n \left[\frac{K_0 + T_m}{K_0 + T_a}\right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
$I_{l\text{-}g}$ - RMS fault current in kA = 50 KA	16
tc - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:	
16 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	130
Earth rod dia in mm	13
Earth rod dia (including 25% corrosion allowance) in mm	16

Earth flat sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c x \sqrt{\left[\frac{TCAPx10^{-4}}{t_c x \alpha_r x \rho_r}\right] x l_n \left[\frac{K_0 + T_m}{K_0 + T_a}\right]}$$

αr - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρr - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
$I_{l\text{-}g}$ - RMS fault current in kA = 50 KA	16
tc - Short circuit current duration sec	1

Thermal capacity factor, TCAP J/(cm3.oC)	3.93
Tm - Maximum allowable temperature for copper conductor, in oC	419
K0 - Factor at oC	293

The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:

16 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	130
Earth flat area in mm	13
Earth flat area (including 25% corrosion allowance) in mm	16
Selected flat size W * Thk in sq mm	20

Rg - Grid resistance

Grid resistance can be calculated using Eq. 52 of IEEE 80

$$R_g = \rho \left\{ \frac{1}{L} + \frac{1}{\sqrt{20 \ x \ A}} \left[1 + \frac{1}{1 + h \ \sqrt{20 \ /A}} \right] \right\}$$

ρ - Soil resistivity in Ω-meter=	11
L - Total buried length of ground conductor in meter	440
h - Depth of burial in meter	0.5
A - Grid area in sq. meter	11200

Rg - Grid resistance	0.071

Rr - Earth Electrode resistance

Grid resistance can be calculated using Eq. 55 of IEEE 80

$$R_r = \frac{\rho}{2 \ x \ \pi \ x \ n_r \ x \ L_r} \left\{ l_n \left[\frac{4 \ x \ L_r}{b} \right] - 1 + \frac{2 \ x \ k_1 \ x \ L_r}{\sqrt{A}} \left(\sqrt{n_r} - 1 \right)^2 \right\}$$

ρ - Soil resistivity in Ω-meter, 16.96	11
n - No of earth electrodes	6
Lr - Length of earth electrode in meter	4.5
b - Diameter of earth electrode in meter	0.020
k1 - co-efficient	1
A - Area of grid in square metre	11200

Rr - Earth Electrode resistance	4.04156

Grounding system resistance

Grounding system resistance can be calculated using equation 53 of IEEE 80 as follows:

$$R_g \ x \ R_2 - R_m^{\ 2}$$

$$R_S = \frac{}{R_g + R_2 - 2R_m}$$

R_m - Mutual ground resistance between the group of ground conductors, R_g and group of electrodes, R_r in Ω. Neglected R_m, since this is for homogenous soil

Rs - Total earthing system resistance 0.070

The calculated resistance grounding system is less than the allowable 1 Ω value.

Assignment-5

Lightning calculations:

	1	2	3
Location	Mangalore	Bangalore	Visakhapatnam
Building	Concrete, Industrial	Srtuctural, Industrial	Concrete, Hospital
Type of Building	Flat Roofs (a)	Triangle Roofs (c)	Flat Roofs (a)
Building Length (L)	14	18	20
Building breadth (W)	4	8	9
Building Height (H)	5	6	8

4	5	6	7	8
Nellore	Karnool	Jaipur	Udaipur	Rajkot
Concrete, School	Concrete, Industrial	Srtuctural, Industrial	Concrete, Hospital	Concrete, School
Triangle Roofs (c)	Flat Roofs (a)	Triangle Roofs (c)	Flat Roofs (a)	Triangle Roofs (c)
22	15	19	17	15
8	5	7	7	6
9	6	7	9	7

9	10	11	12	13
Surat	Vadodara	Gwalior	Bellari	Bhopal
Concrete, Industrial	Srtuctural, Industrial	Concrete, Hospital	Concrete, School	Concrete, Industrial
Flat Roofs (a)	Triangle Roofs (c)	Flat Roofs (a)	Triangle Roofs (c)	Flat Roofs (a)
14	13	20	21	15
8	7	9	8	6
5	6	7	8	6

14	15	16	17	18
Delhi	Raichur	Rajkot	Khammam	Hyderabad
Srtuctural, Industrial	Concrete, Hospital	Concrete, School	Concrete, Industrial	Srtuctural, Industrial
Triangle Roofs (c)	Flat Roofs (a)	Triangle Roofs (c)	Flat Roofs (a)	Triangle Roofs (c)
11	17	12	11	9
7	7	6	7	6
5	9	8	9	7

19
Nizamabad
Concrete, Hospital
Flat Roofs (a)
12
7
9

Location	Gwalior
Building	Concrete, Hospital
Type of Building	Flat Roofs (a)
Building Length (L)	20
Building breadth (W)	9
Building Height (H)	7

Risk Factor Calculation

1 Collection Area (A_c)

A_c = (L*W) + (2*L*H) + (2*W*H)

739.86

2 Probability of Being Struck (P)

P = Ac * Ng * 10-6

0.002737482

3 Overall weighing factor

a) Use of structure (A)	=	1.7
b) Type of construction (B)	=	1.0
c) Contents or consequential effects (C)	=	1.7
d) Degree of isolation (D)	=	1.0
e) Type of country (E)	=	0.3
Wo - Overall weighing factor	=	A * B * C * D * E
	=	0.510

4 Overall Risk Factor

Po	=	P * Wo
Po	=	0.001396116
Pa		10^{-5}

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}

Since Po > Pa lightning protection required.

5 Air Terminations

Perimeter of the building	=	2(L+W)	
	=	58	Mts.

6 Down Conductors

Perimeter of building	=	58	Mts.
No. of down conductors based on perimeter	=	3	Nos.

Hence 3 nos. of Down conductors have been selected.

Size of Down conductor = 20 X 2.5 mm Galvanized Ste

(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip

Assignment-6

S.NO.	Description	Equipment No.	Description	Consumed Load KW	Load Rating KW	Voltage (V)	No. of ph	Full Load Current (A)	Motor Starting Current (A)	Load P.F. Running	SIN Φ Running	Motor P.F Staring	SIN Φ Staring	Type	No. of Runs	No. of Cores	Size (mm2)	Current Rating (A)	Derating factor k1	Derating factor k2	Derating factor k3	Derating factor k4	Overall Derating factor k	Derated Current (A)	Cable Length (M)	Cable Resistance (Ohms/kM)	Cable Reactance (Ohms/kM)	Voltage drop (Running) (V)	Voltage drop (Running) (%)	Voltage drop (Starting) (V)	Voltage drop (starting) (%)	Cable size result	OD of Cable (mm)	Gland size
3	LV MCC	PU2315	Silica filter feed pump	43.84	45.00	415	3	76.2	457.44	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	95	0.9300	0.0816	9.95	2.40	59.07	14.23	OK	22	20
4	LV MCC	PU2322A	Soft water pump	12.73	15.00	415	3	22.1	132.83	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	95	2.3400	0.0852	7.01	1.69	41.84	10.08	OK	18	20s
5	LV MCC	PU 2314A	Absorbesnt/Neutral oil pump	10.96	11.00	415	3	19.1	114.36	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	60	5.9000	0.0947	9.46	2.28	56.66	13.65	OK	17	20s
6	LV MCC	PU2324	Citric Acid Tank pump	44.28	45.00	415	3	77.0	462.03	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	85	0.9300	0.0816	8.99	2.17	53.38	12.86	OK	22	20s
7	LV MCC	PU2333	Slop Oil pump	44.62	45.00	415	3	77.6	465.58	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	75	0.9300	0.0816	7.99	1.93	47.46	11.44	OK	22	20s
8	LV MCC	PU 2322B	Soft water pump-Stand by	44.62	45.00	415	3	77.6	465.58	0.8	0.6	0.8	0.5	2	1	4.0	35	148	0.98	0.9	1	1	0.882	130.5	105	0.6710	0.0794	8.25	1.99	48.81	11.76	OK	24	20s
9	LV MCC	PU2321A	Lye/Simplex Metering Pump	19.16	22.00	415	3	33.3	199.92	0.8	0.6	0.8	0.5	2	1	4.0	16	85	0.98	0.9	1	1	0.882	75.0	100	1.4700	0.0815	7.07	1.70	42.13	10.15	OK	21	20s
10	LV MCC	PU2321B	Lye storage tank pump	1.86	2.20	415	3	3.2	19.41	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	100	5.9000	0.0947	2.68	0.64	16.03	3.86	OK	17	20s
11	LV MCC	PU2305	Feed Pump(Seperator)	4.30	4.70	415	3	7.5	44.87	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	3.11	0.75	18.63	4.49	OK	18	20
12	LV MCC	PU2332	Saop Stock Pump	3.23	3.70	415	3	5.6	33.70	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	110	9.4800	0.1007	8.18	1.97	49.02	11.81	OK	16	20s
13	LV MCC	MX2305	Mixer	3.23	3.70	415	3	5.6	33.70	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	2.34	0.56	14.00	3.37	OK	18	20
14	LV MCC	MX2308	Mixer	11.75	15.00	415	3	20.4	122.60	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	105	2.3400	0.0852	7.15	1.72	42.69	10.29	OK	18	20
15	LV MCC	CF2312	Separator	4.27	4.70	415	3	7.4	44.55	0.8	0.6	0.8	0.5	2	1	4.0	25	122	0.98	0.9	1	1	0.882	107.6	85	0.9300	0.0816	0.87	0.21	5.15	1.24	OK	22	32
16	LV MCC	BW2313	Blower	4.27	4.70	415	3	7.4	44.55	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	95	9.4800	0.1007	9.34	2.25	55.97	13.49	OK	16	20s
17	LV MCC	RV 2314	Rotary valve	7.48	7.50	415	3	13.0	78.05	0.8	0.6	0.8	0.5	2	1	4.0	4	38	0.98	0.9	1	1	0.882	33.5	65	5.9000	0.0947	7.00	1.69	41.89	10.09	OK	17	20s
18																																		
19																																		
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Basis:

1. Overall derating factor k = k1 x k2 x k3 x k4
   - K1=Rating factor for variation in air/ground temperature
   - K2=Rating factor for depth of laying
   - K3=Rating factor for spacing between two circuits
   - K4=Rating factor for variation in thermal resistivity of the soil
2. LT Motors : Running Voltage Drop = 3%, Starting Voltage Drop = 15%
3. Cable type:
   - TYPE 1: Al Conductor, XLPE Insulated, Armoured, PVC outer sheathed
   - TYPE 2: Cu Conductor, XLPE Insulated, Armoured, PVC outer sheathed
4. Effect of Frequency Variation ± 5%
5. Combined Effect of Voltage & Frequency Variation ±10%

Assignment-7

		ASSIGNMENT-7							
LT CABLES									
CABLE TRAY: FROM		LT-4		TO	LT-5				
Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm2)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)	Remarks
1	PU2315	4	16	1	21	21	1	1	
2	PU2322A	4	10	1	18	18	0.9	0.9	
3	PU 2314A	4	2.5	1	16	16	0.5	0.5	
4	PU2316	4	16	1	21	21	1	1	
5	PU2322A	4	16	1	21	21	1	1	
6	PU 2314A	4	25	1	22	22	1.4	1.4	
7	PU2317	4	10	1	18	18	0.9	0.9	
8	PU2322A	4	10	1	18	18	0.9	0.9	
9	PU 2314A	4	6	1	18	18	0.7	0.7	
10	PU2318	4	2.5	1	16	16	0.5	0.5	
11	PU2322A	4	6	1	18	18	0.7	0.7	
12	PU 2314A	4	6	1	18	18	0.7	0.7	
13	PU2319	4	25	1	22	22	1.4	1.4	
14	PMCC-2 TO AUXILIARY PANEL-3(A/C)	4	2.5	1	16	16	0.5	0.5	
15	PMCC-2 TO COOLING TOWER DOSING SYSTEM PACKAGE	4	2.5	1	16	16	0.5	0.5	
	Total			15		279	12.6	12.6	

Calculation			Result		
Maximum Cable Diameter:	22	mm	Selected Cable Tray width:	O.K	
Consider Spare Capacity of Cable Tray:	30%		Selected Cable Tray Depth:	O.K	
Distance between each Cable:	0	mm	Selectrd Cable Tray Weight:	O.K	Including Spare Capacity
Calculated Width of Cable Tray:	363	mm	Selected Cable Tray Size:	O.K	Including Spare Capacity
Calculated Area of Cable Tray:	7979	Sq.mm			
No of Layer of Cables in Cable Tray:	1		Required Cable Tray Size:	600 x 100	mm
Selected No of Cable Tray:	1	Nos.	Required Nos of Cable Tray:	1	No
Selected Cable Tray Width:	600	mm	Required Cable Tray Weight:	90.00	Kg/Meter/Tray
Selected Cable Tray Depth:	100	mm	Type of Cable Tray:	Ladder	
Selected Cable Tray Weight Capacity:	90	Kg/Meter			
Type of Cable Tray:	Ladder		Cable Tray Width Area Remaning	40%	
Total Area of Cable Tray:	60000	Sq.mm	Cable Tray Area Remaning:	87%	