



## EEN-206: Power Transmission and Distribution

### Lecture -06

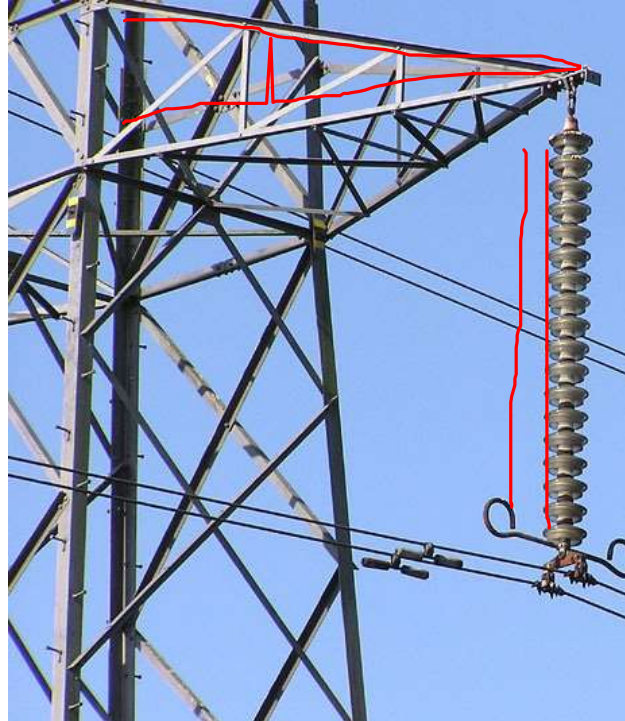
#### Chapter 2: Overhead Transmission Lines

- Mechanical Design

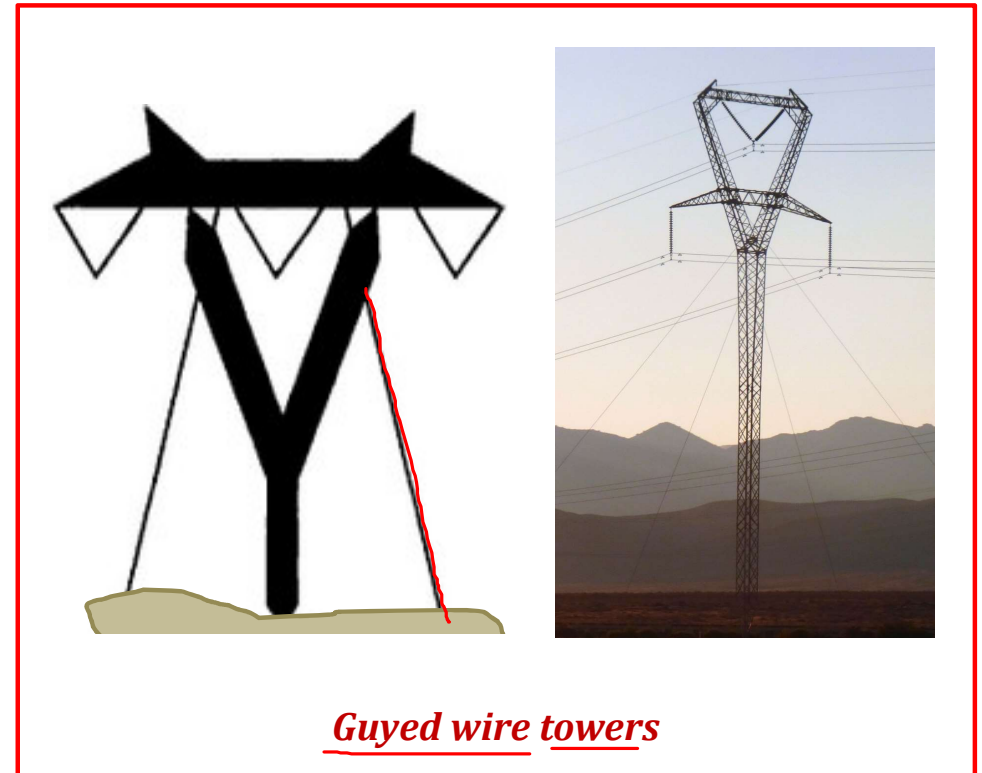
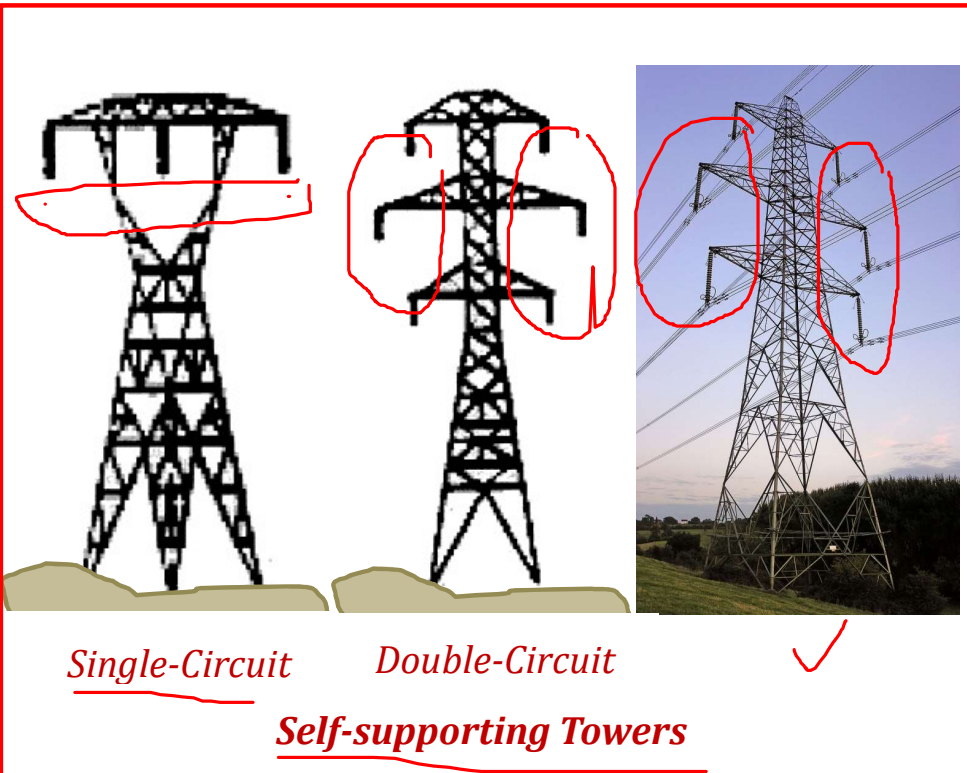


# Main Components of Overhead Line

- Support Structure (Towers): Cost, voltage level, conductor size, conductor spacing (cross-arm length), etc.
  - Galvanized steel (for high voltage)
  - Wood, concrete, steel poles (for low voltage)
- Insulators: Voltage level
  - Porcelain ||
  - Glass
  - Polymer insulation
- Conductors: Thermal limit, weight, conductivity, mechanical strength, regulation, etc.

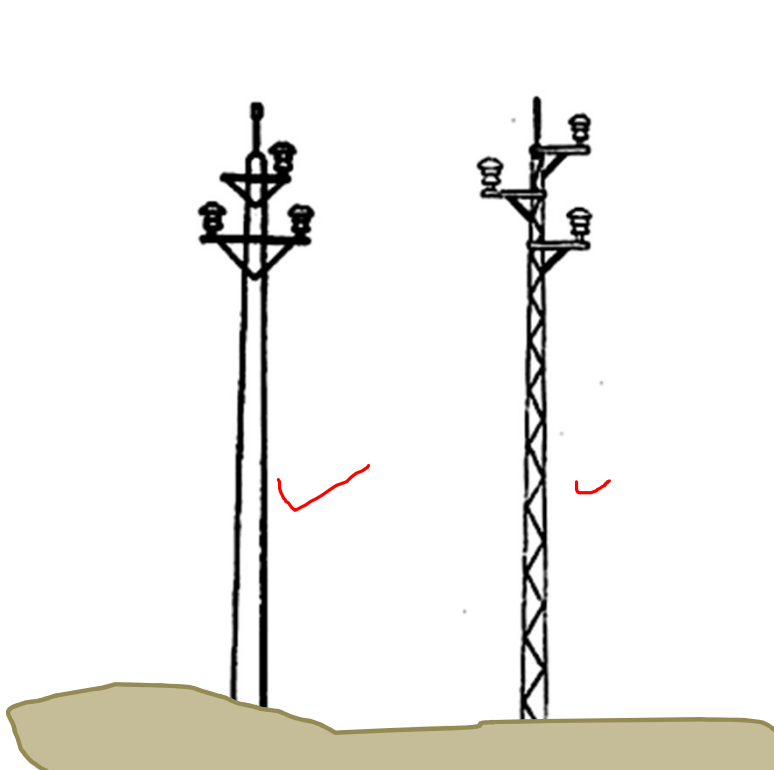


# Tower Structures (High Voltage Transmission)



- ❑ Galvanized steel (for high voltage)

## Tower Structures (Low Voltage Distribution)

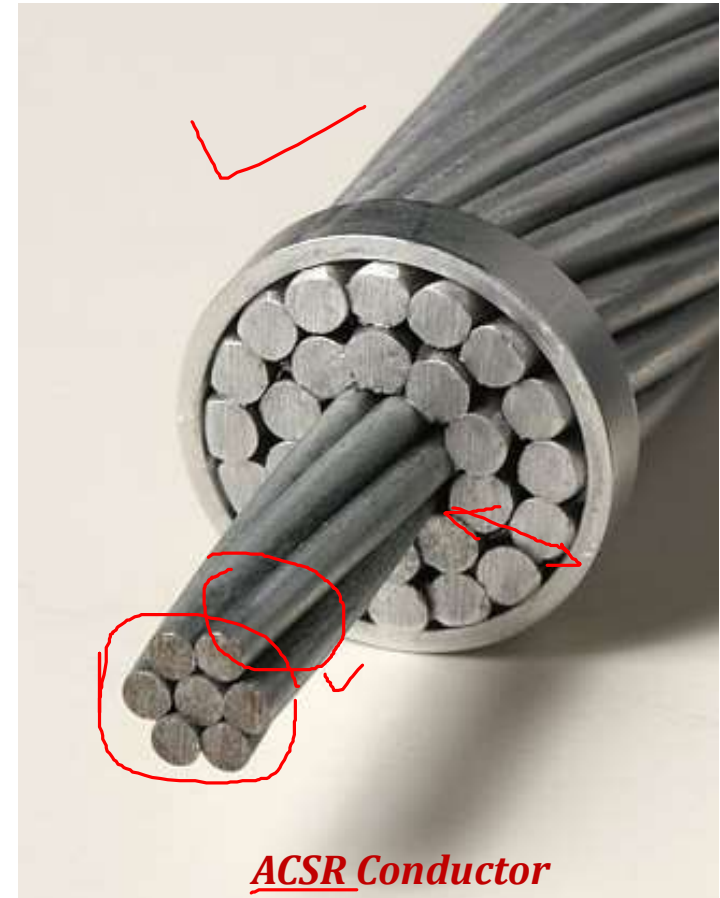


- Wood concrete, steel poles (for low voltage)



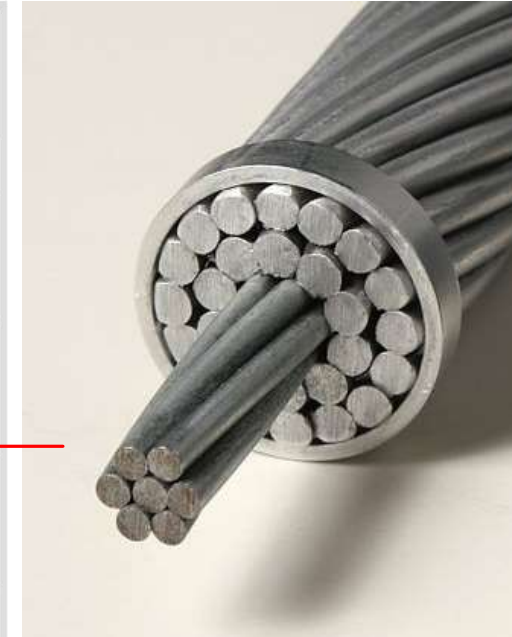
# Types of Conductor

- Copper: Good conductor, durable, high scrap value, tensile strength, but cost is high.
- Aluminum:
  - Cheaper,
  - lighter,
  - but less conductive (requires large cross section for same resistance)
  - less tensile strength than copper
- Types of Aluminum conductors
  - AAC (All Aluminum Conductor)
  - AAAC (All Aluminum Alloy Conductor)
  - ACSR (Aluminum Conductor Steel Reinforced)
  - ACAR (Aluminum Conductor Alloy Reinforced)
  - Expanded ACSR ←

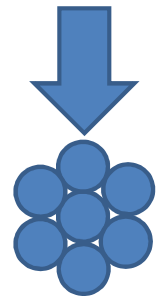
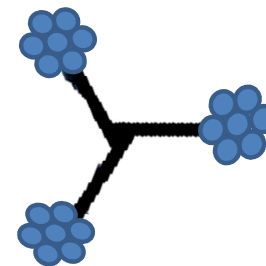
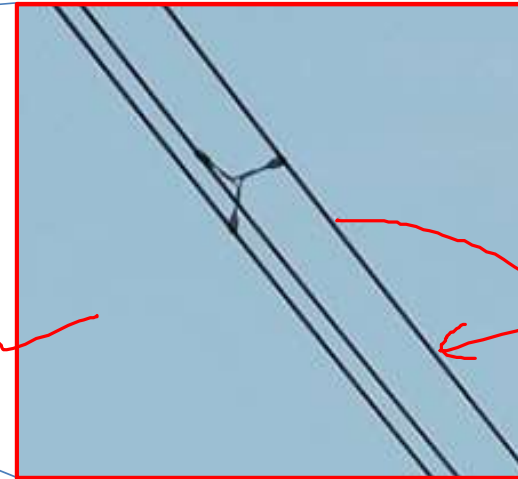
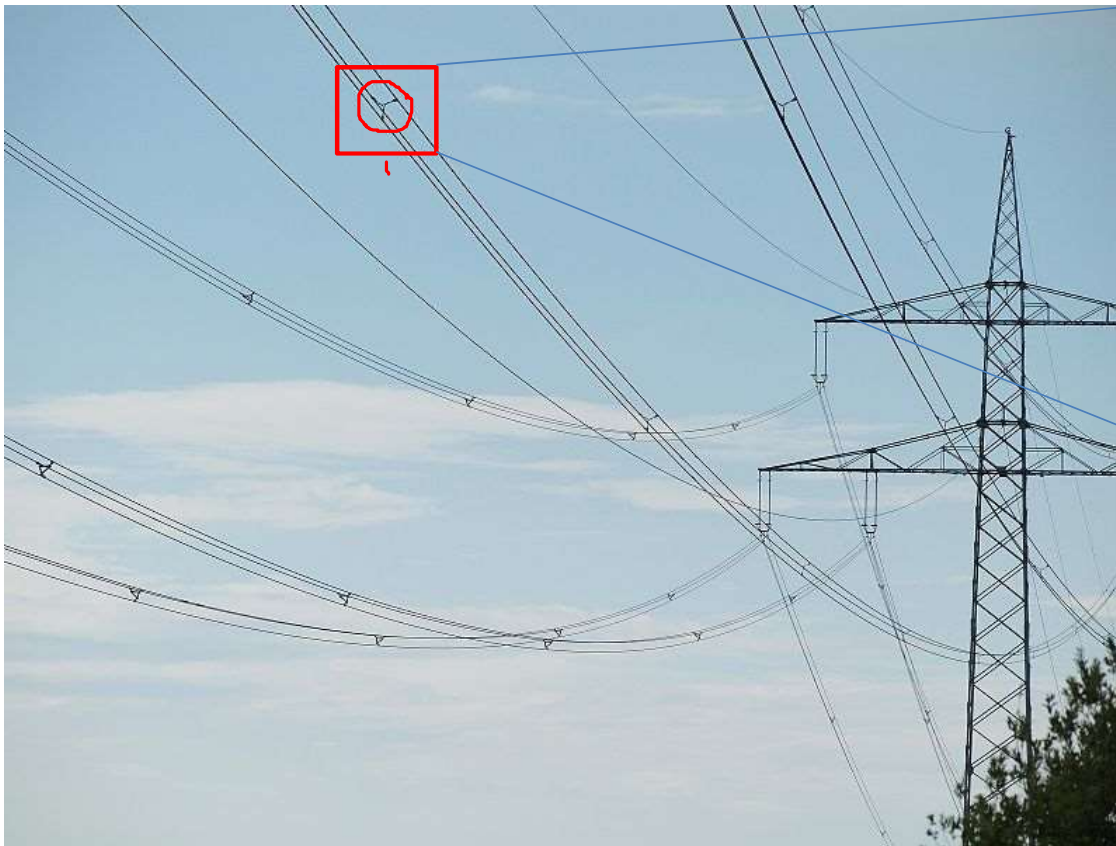


# ACSR Conductor Data Sheets

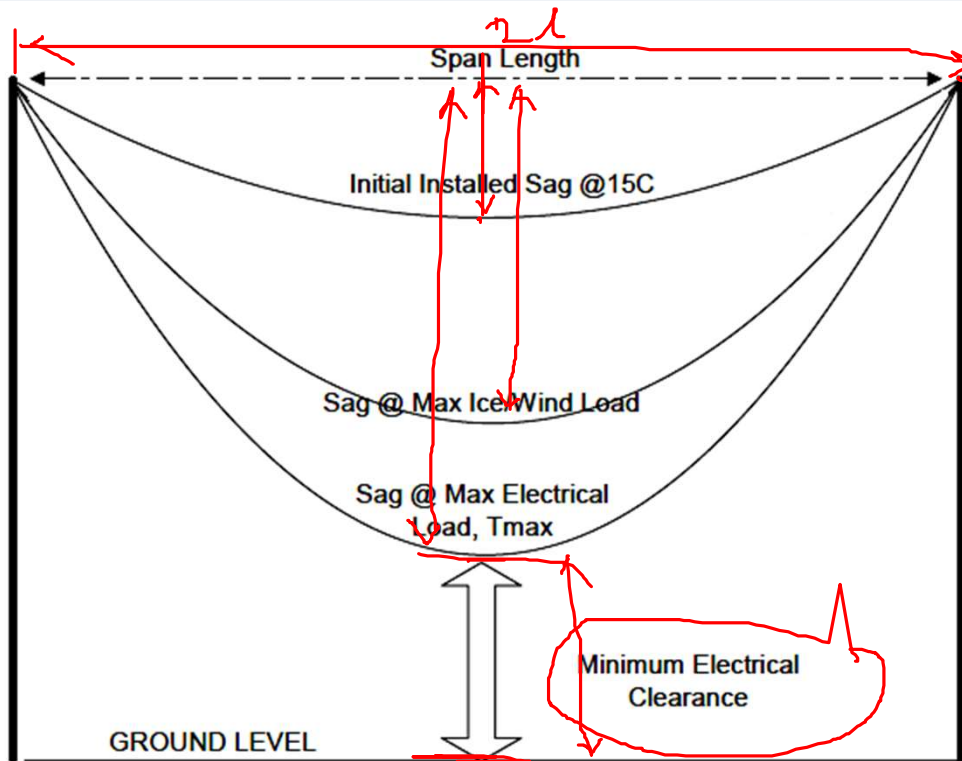
CODE NAME	NOMINAL ALUMINIUM AREA	EQUIVALENT COPPER AREA	CONDUCTOR CONSTRUCTION		APPROX. OVERALL DIAMETER	CALCULATED AREA	APPROX. WEIGHT	NOMINAL BREAKING LOAD	MAX. DC RESISTANCE AT 20°C	CURRENT RATING
			ALUMINIUM	STEEL						
	mm <sup>2</sup>	mm <sup>2</sup>	No./mm		mm	mm <sup>2</sup>	kg/km	N	Ω/km	Amp
GOPHER	25	16.1	6/2.36	1/2.36	7.08	30.62	106	9600	1.093	77
WEASEL	30	19.4	6/2.59	1/2.59	7.77	36.88	128	11400	0.9077	84
FERRET	40	25.8	6/3.00	1/3.00	9.00	49.48	172	15200	0.6766	98
RABBIT	50	32.3	6/3.35	1/3.35	10.05	61.70	214	18400	0.5426	112
HORSE	70	45.2	12/2.59	7/2.79	13.95	116.2	538	61200	0.3936	148
DOG	100	64.5	6/4.72	7/1.57	14.15	118.5	394	32700	0.2733	153
WOLF	150	96.8	30/2.59	7/2.59	18.13	194.9	726	69200	0.1828	162
DINGO	150	97.9	18/3.35	1/3.35	16.75	167.5	506	35700	0.1815	179
LYNX	175	113.0	30/2.79	7/2.79	19.53	226.2	842	79800	0.1576	178
CARACAL	175	113.7	18/3.61	1/3.61	18.05	194.5	587	41000	0.1563	205
PANTHER	200	129	30/3.00	7/3.00	21.00	261.5	974	92200	0.1363	191
BISON	-	226	54/3.00	7/3.00	27.00	431.3	1444	120900	0.07571	208
JAGUAR	200	130	18/3.86	1/3.86	19.30	222.3	671	46600	0.13670	197
ZEBRA	400	258	54/3.18	7/3.18	28.62	484.5	1621	131900	0.06740	202



# Bundled Conductors



# Sag and Tension:

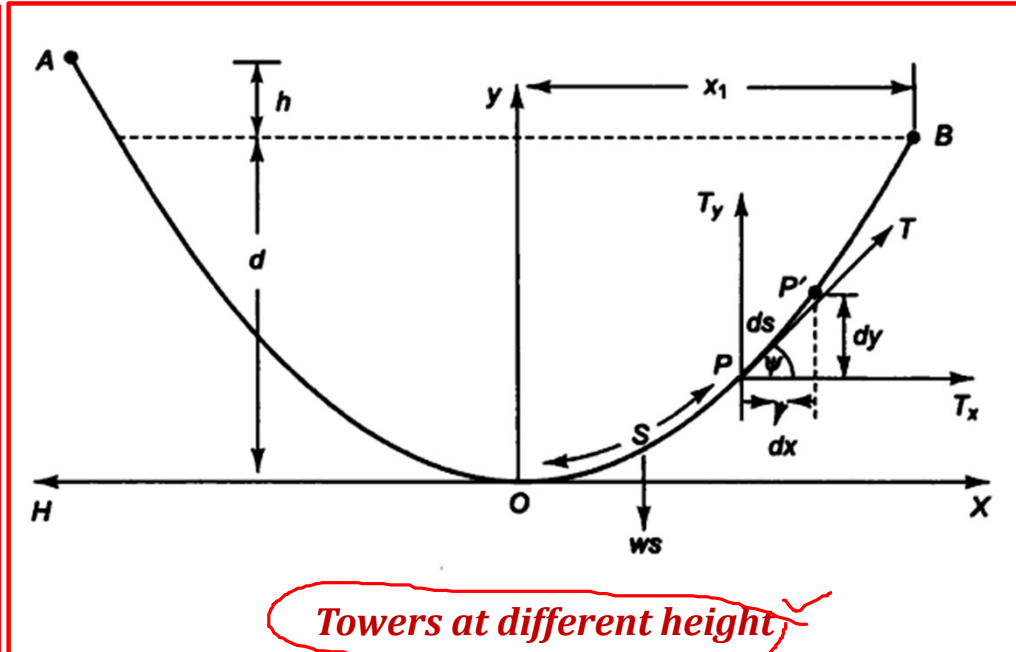
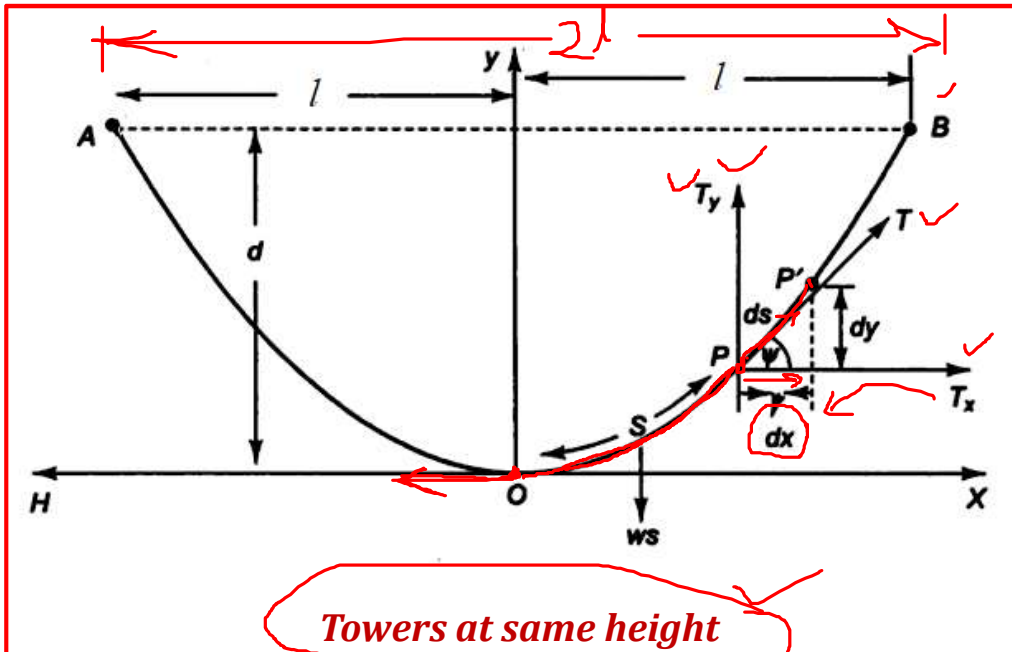


220 kV line: GC 7.0 m, SL 380, and CC 5.1 m  
 400 kV line: GC 8.8 m, SL 400, and CC 7.0 m

- **Sag (d)** is defined as vertical distance between the point where the line is joined to the tower to the lowest point on the line.
- Sag depends on the **tension (T)** with which conductors are pulled.
- **Span Length (SL)** is horizontal distance between two towers.
- Vertical distance between lowest point on line to the ground plane is called **ground clearance (GC)**.
- Values of sag and tension at **winter and summer condition** and at **various loading conditions** must be known.
- **Mechanical loadings**
  - Weight of conductor itself
  - Weight of ice or snow clinging to wire
  - Wind blowing against wire



# Calculation of Sag and Tension



- $w$  = weight per unit length
- $H$  = tension at point O
- $T$  = tension at point P

- $2l$  = Span length
- O is the lowest point on the wire

# Calculation of Sag and Tension

$$H = T_x$$

$$T_y = ws$$

$$\tan \psi = \frac{dy}{dx} = \frac{T_y}{T_x} = \frac{ws}{H}$$

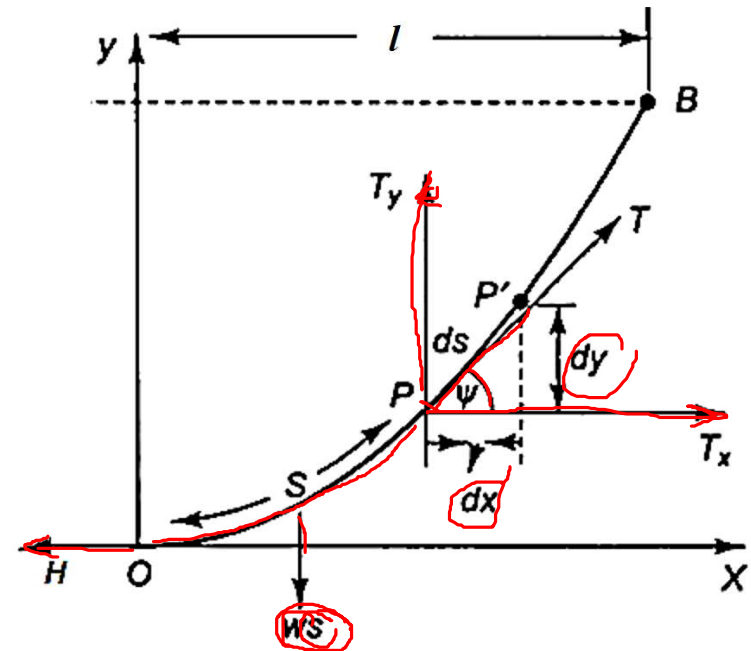
$$ds^2 = dx^2 + dy^2$$

$$\frac{ds^2}{dx^2} = 1 + \frac{dy^2}{dx^2}$$

$$\frac{ds}{dx} = \sqrt{1 + \left(\frac{dy}{dx}\right)^2}$$

$$\frac{ds}{dx} = \sqrt{1 + w^2 s^2 / H^2}$$

$$dx = \frac{ds}{\sqrt{1 + w^2 s^2 / H^2}}$$



# Calculation of Sag and Tension

$$dx = \frac{ds}{\sqrt{1 + w^2 s^2 / H^2}}$$

Integrating

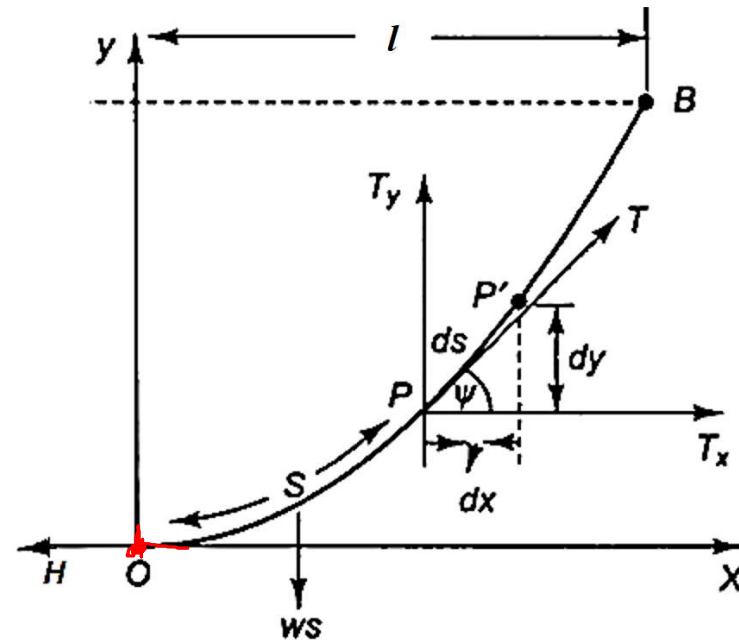
$$\int dx = \int \frac{ds}{\sqrt{1 + w^2 s^2 / H^2}}$$

Thus

$$x + c_1 = \frac{H}{w} \sinh^{-1} \left( \frac{ws}{H} \right)$$

At  $x=0$ ,  $s=0$ , therefore  $c_1=0$

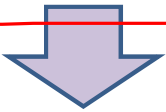
$$x = \frac{H}{w} \sinh^{-1} \left( \frac{ws}{H} \right)$$



$$s = \frac{H}{w} \sinh \frac{wx}{H}$$

# Calculation of Sag and Tension

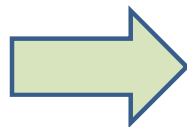
$$s = \frac{H}{w} \sinh \frac{wx}{H}$$



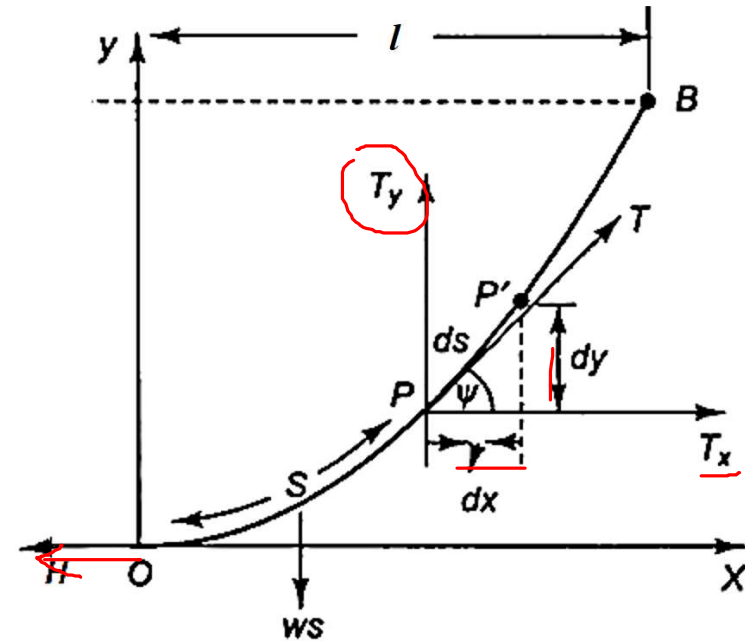
$$\frac{ws}{H} = \sinh \left( \frac{wx}{H} \right)$$

Also  $\frac{dy}{dx} = \frac{ws}{H}$

$$\frac{dy}{dx} = \sinh \left( \frac{wx}{H} \right)$$



$$dy = \sinh \frac{wx}{H} dx$$





# Calculation of Sag and Tension

$$dy = \sinh \frac{wx}{H} dx$$

Integrating

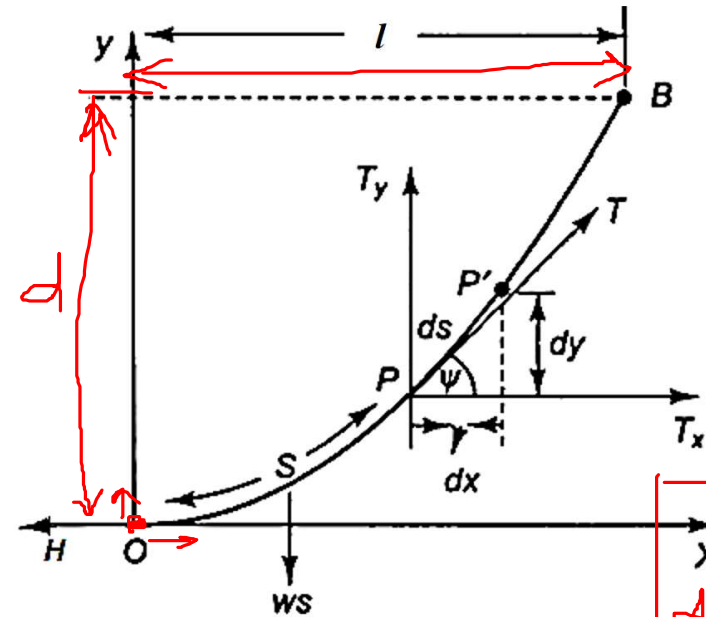
$$\int dy = \int \sinh \frac{wx}{H} dx$$

Thus  $y = \frac{H}{w} \cosh \left( \frac{wx}{H} \right) + c_2$

At  $x=0, y=0$  therefore  $c_2 = -\frac{H}{w}$

$$y = \frac{H}{w} \cosh \left( \frac{wx}{H} \right) - \frac{H}{w}$$

$$\cosh x = 1 + \frac{x^2}{2!} + \frac{x^4}{4!} + \frac{x^6}{6!} + \dots$$



$$y = \frac{H}{w} \left( \cosh \frac{wx}{H} - 1 \right)$$

$$y = \frac{H}{w} \left( 1 + \frac{w^2 x^2}{2H^2} - 1 \right) = \frac{wx^2}{2H}$$

$$d = \frac{wl^2}{2H}$$

$$y = \frac{wx^2}{2H}$$

## Calculation of Sag and Tension

For tension at point  $P$ ,

$$\underline{T^2 = T_x^2 + T_y^2}$$

$$= H^2 + \cancel{w^2} s^2$$

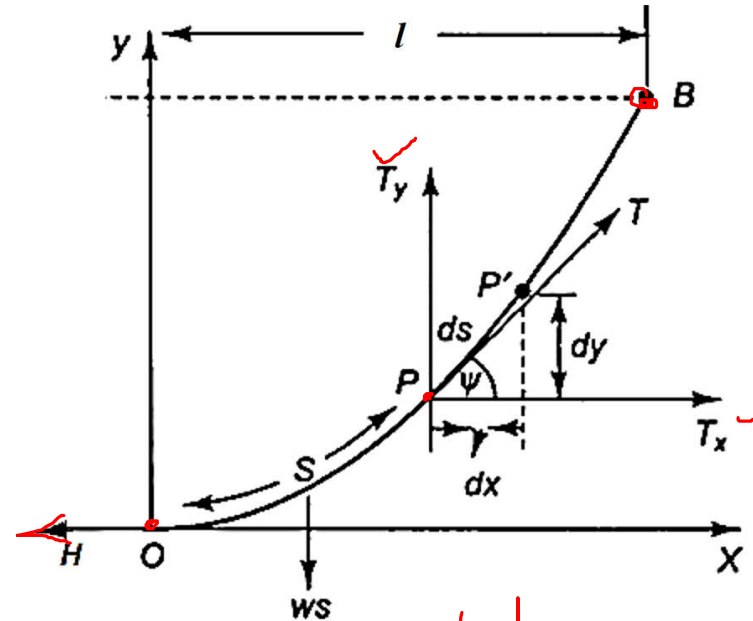
We know

$$s = \frac{H}{w} \sinh \frac{wx}{H}$$

$$T^2 = H^2 + H^2 \sinh^2 \left( \frac{wx}{H} \right)$$

$$= H^2 \left( 1 + \sinh^2 \left( \frac{wx}{H} \right) \right)$$

$$T^2 = H^2 \cosh^2 \left( \frac{wx}{H} \right)$$



$$T = H \cosh \frac{wx}{H}$$

# Support at Same Heights

If the towers at same height and span is  $2l$ , i.e. half span is  $l$

$$s = \frac{H}{w} \sinh \frac{wx}{H}$$

$$S = \frac{H}{w} \sinh \left( \frac{wl}{H} \right)$$

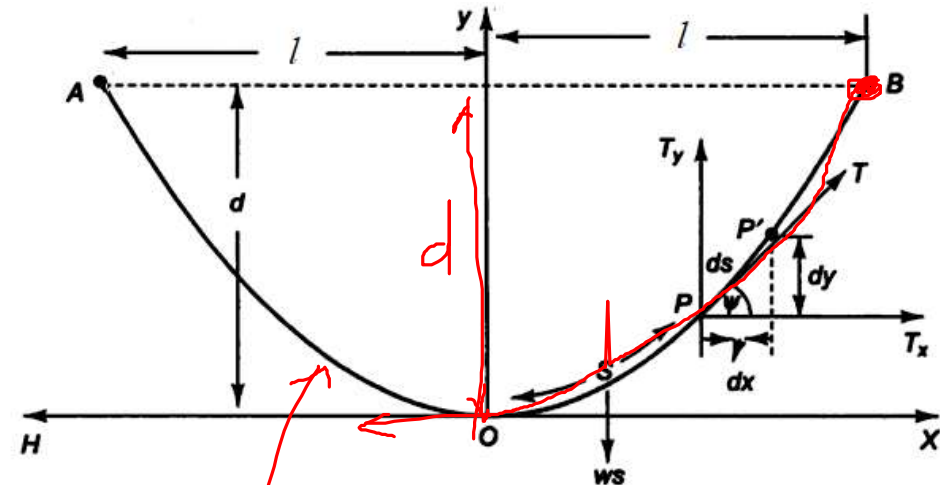
$$y = \frac{H}{w} \left( \cosh \frac{wx}{H} - 1 \right)$$

$$d = \frac{H}{w} \left( \cosh \frac{wl}{H} - 1 \right)$$

$$T = H \cosh \frac{wx}{H}$$

$T$  at Ends

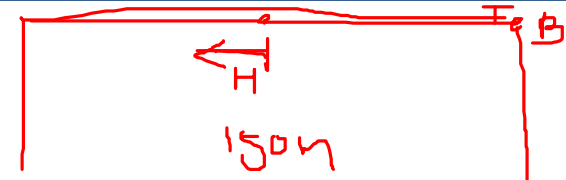
$$T = H \cosh \frac{wl}{H}$$



$$\frac{1000N}{2} = 500$$

# Approximate Formulae for Sag and Tension

$$T \approx H \cosh \frac{wl}{H} \Rightarrow T \approx H \left( 1 + \frac{w^2 l^2}{2H^2} \right)$$



$$d = \frac{H}{w} \left( \cosh \frac{wl}{H} - 1 \right) \Rightarrow d \approx \frac{H}{w} \left( 1 + \frac{w^2 l^2}{2H^2} - 1 \right) \Rightarrow d \approx \frac{wl^2}{2H}$$

200w  
Sag

$$S = \frac{H}{w} \sinh \left( \frac{wl}{H} \right) \Rightarrow S \approx \frac{H}{w} \left( \frac{wl}{H} + \frac{w^3 l^3}{6H^3} \right) \Rightarrow S \approx l + \frac{w^2 l^3}{6H^2}$$

Short Spans

$$T \approx H$$

$$d \approx \frac{wl^2}{2T}$$

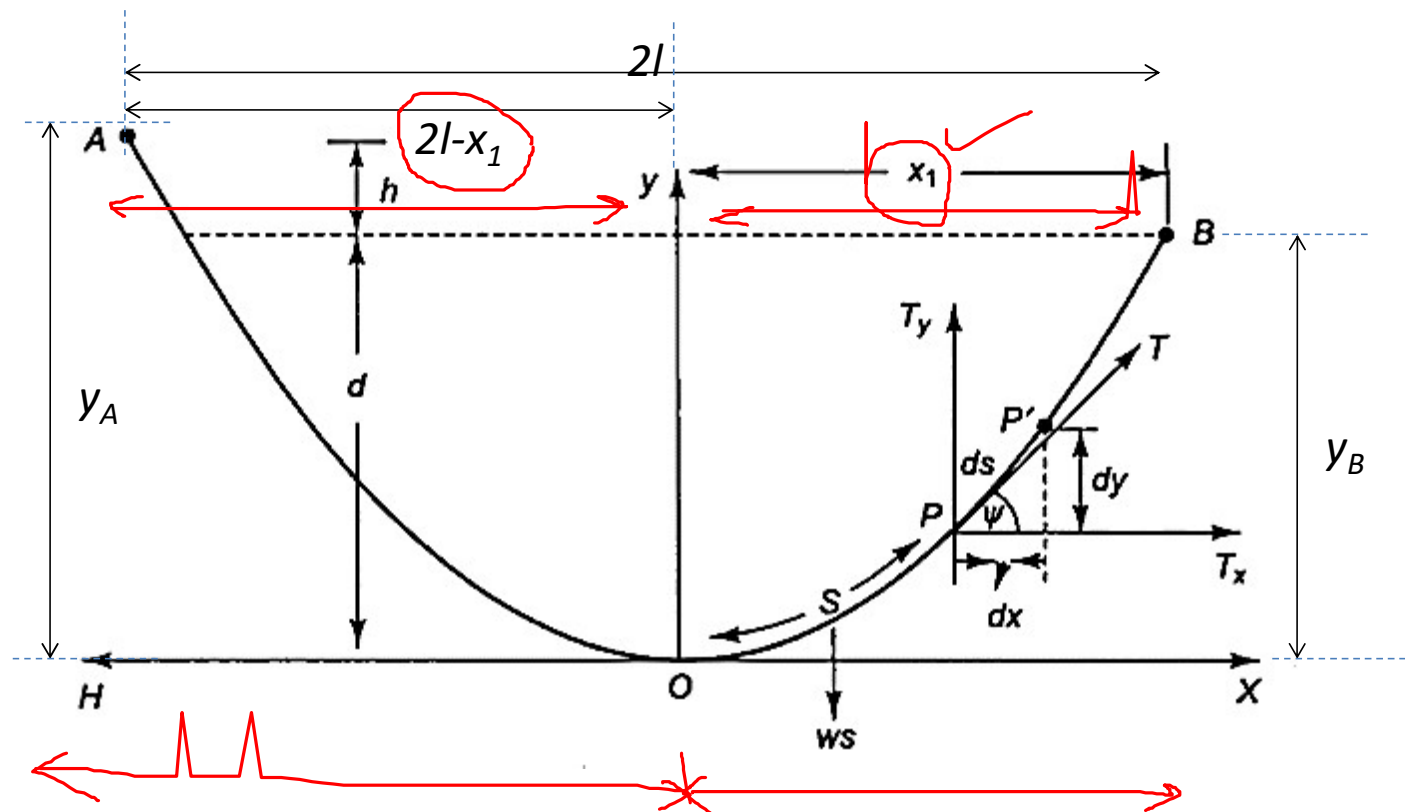
and

$$S \approx l + \frac{w^2 l^3}{6T^2}$$

$$\sinh x = x + \frac{x^3}{3!} + \frac{x^5}{5!} + \frac{x^7}{7!} + \dots \quad \text{and} \quad \cosh x = 1 + \frac{x^2}{2!} + \frac{x^4}{4!} + \frac{x^6}{6!} + \dots$$



# Supports at Different Heights



# Supports at Different Heights

For tower B

$$y_B = \frac{H}{w} \left( \cosh \frac{wx_1}{H} - 1 \right)$$

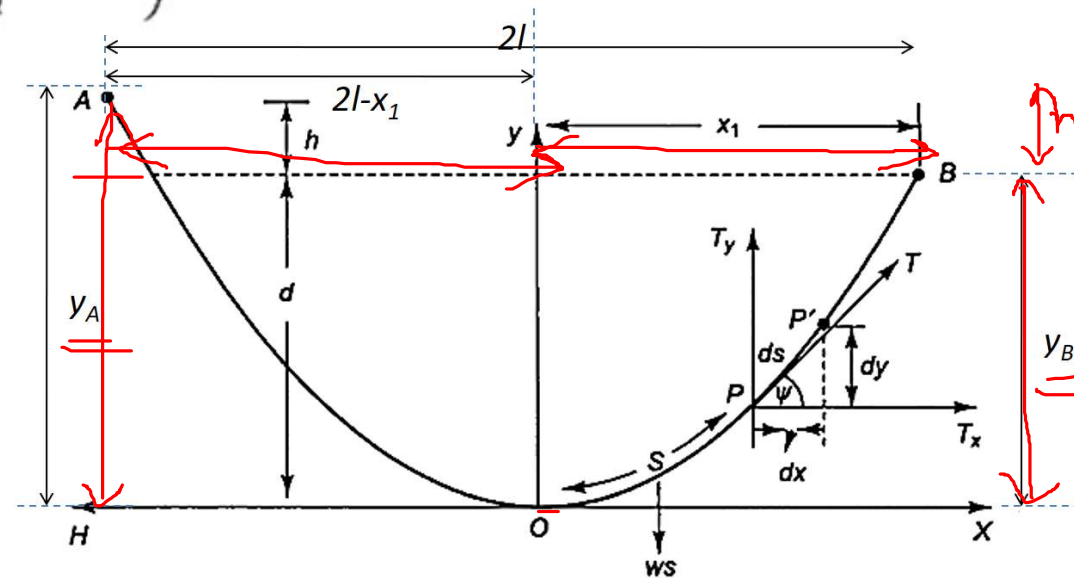
$$y = \frac{H}{w} \left( \cosh \frac{wx}{H} - 1 \right)$$

For tower A

$$y_A = d + h = \frac{H}{w} \left( \cosh \frac{w(2l - x_1)}{H} - 1 \right)$$

Therefore, difference in tower heights

$$h = \frac{H}{w} \left( \cosh \frac{w(2l - x_1)}{H} - \cosh \frac{wx_1}{H} \right)$$





Thank  
You