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## **Control Systems 314 2018**

# **Lecture 11: Effects of Zeroes and Additional Poles**

**Japie Engelbrecht**



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Department of Electrical and Electronic Engineering

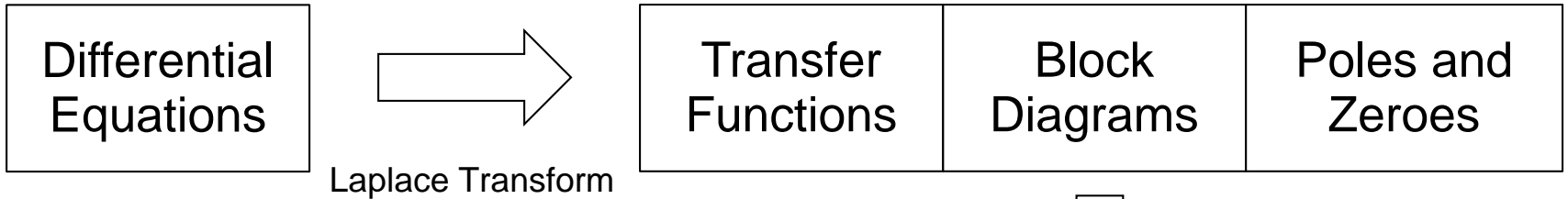
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# Lecture 11 Overview



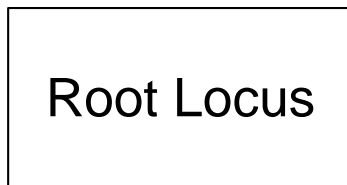
## MODELLING



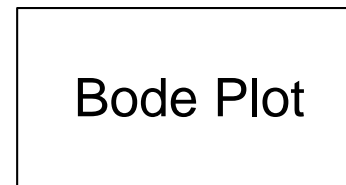
## ANALYSIS



## CONTROL



## TIME DOMAIN DESIGN



## FREQUENCY DOMAIN DESIGN



# Lecture 11 Overview

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- Effect of Zeroes on Transient Response
  - Second-Order Transfer Function with One Zero
  - Overshoot versus Zero Location
- Effect of Additional Poles on Transient Response
  - Second-Order Transfer Function with Extra Pole
  - Rise Time versus Extra Pole Location
- Transient Response of Higher-Order Systems – Dominant Poles
  - Fast and Slow Poles
  - Effect of Zeroes



- Effek van Zeros op Oorgangsverskynsels
  - Tweede-Orde Oordragsfunksie met Een Zero
  - Oorskiet versus Zero Ligging
- Effek van Addisionele Pool op Oorgangsverskynsels
  - Tweede-Orde Oordragsfunksie met Ekstra Pool
  - Stygtyd versus Ekstra Pool Ligging
- Oorgangsverskynsels van Hoër-Orde Stelsels – Dominante Pole
  - Vinnige en Stadige Pole
  - Effekte van Zeros



## Second-Order Transfer Function with One Zero



- To plot the effect of a zero for a wide range of cases, the transfer function is written in a form with normalised time and zero locations

$$H(s) = \frac{(s/\alpha\zeta\omega_n) + 1}{(s/\omega_n)^2 + 2\zeta(s/\omega_n) + 1}$$

- The poles are located at  $s = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$   
 $= -\sigma \pm j\omega_d$
- The zero is located at  $s = -\alpha\zeta\omega_n = -\alpha\sigma$
- In other words, the real zero is  $\alpha$  times the real part of the poles



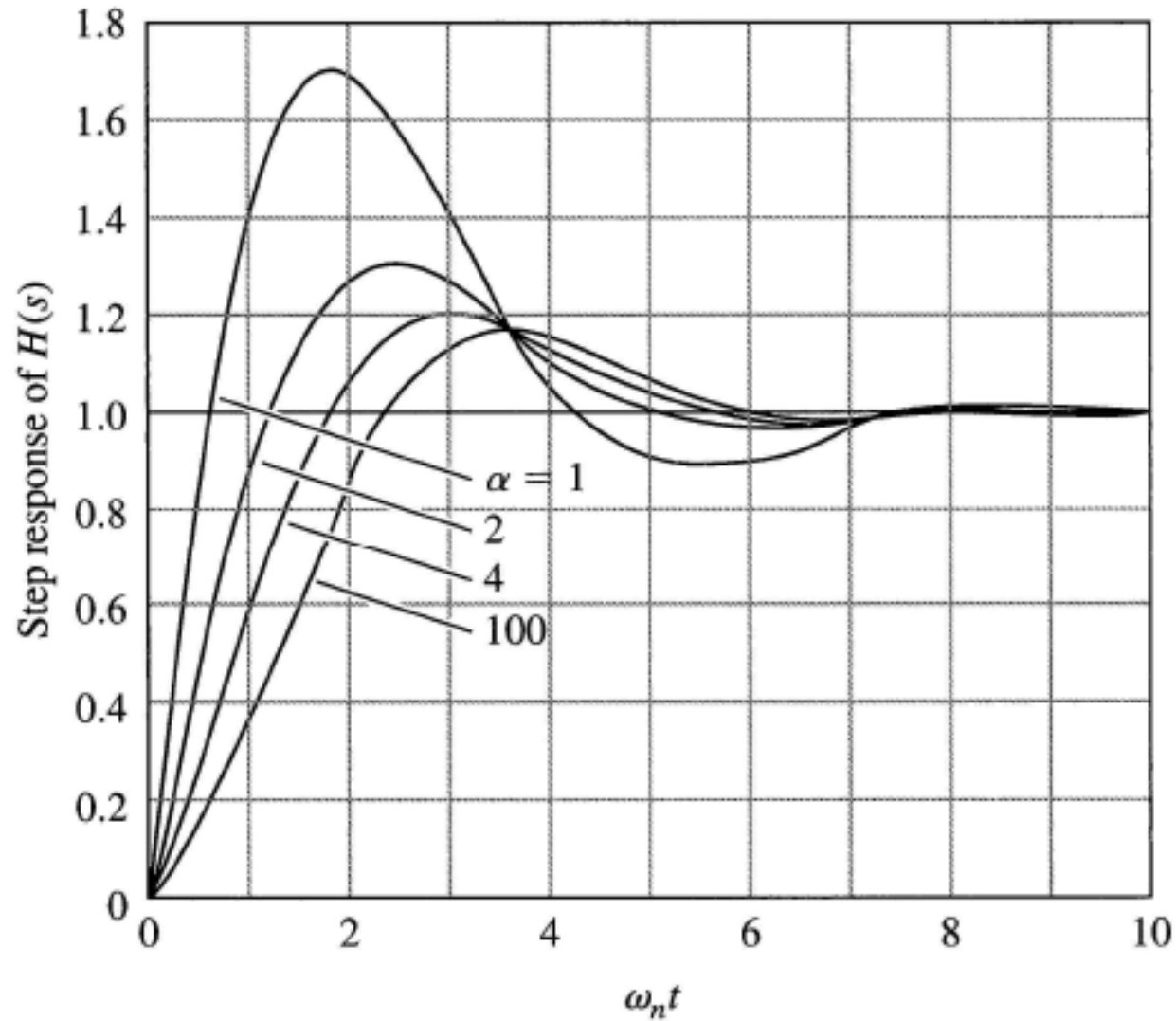
## Second-Order Transfer Function with One Zero



- If  $\alpha$  is large, the zero will be far removed from the poles, and will have little effect on the transient response
- If  $\alpha \approx 1$ , the zero will be close to the real part of the poles and can be expected to have a substantial effect on the transient response
- The step response curves for  $\zeta = 0.5$  and several values of  $\alpha$  are shown on the next pages
- The major effect of the zero is to increase the overshoot  $M_p$ , whereas it has little effect on the settling time



## Second-Order Transfer Function with One Zero

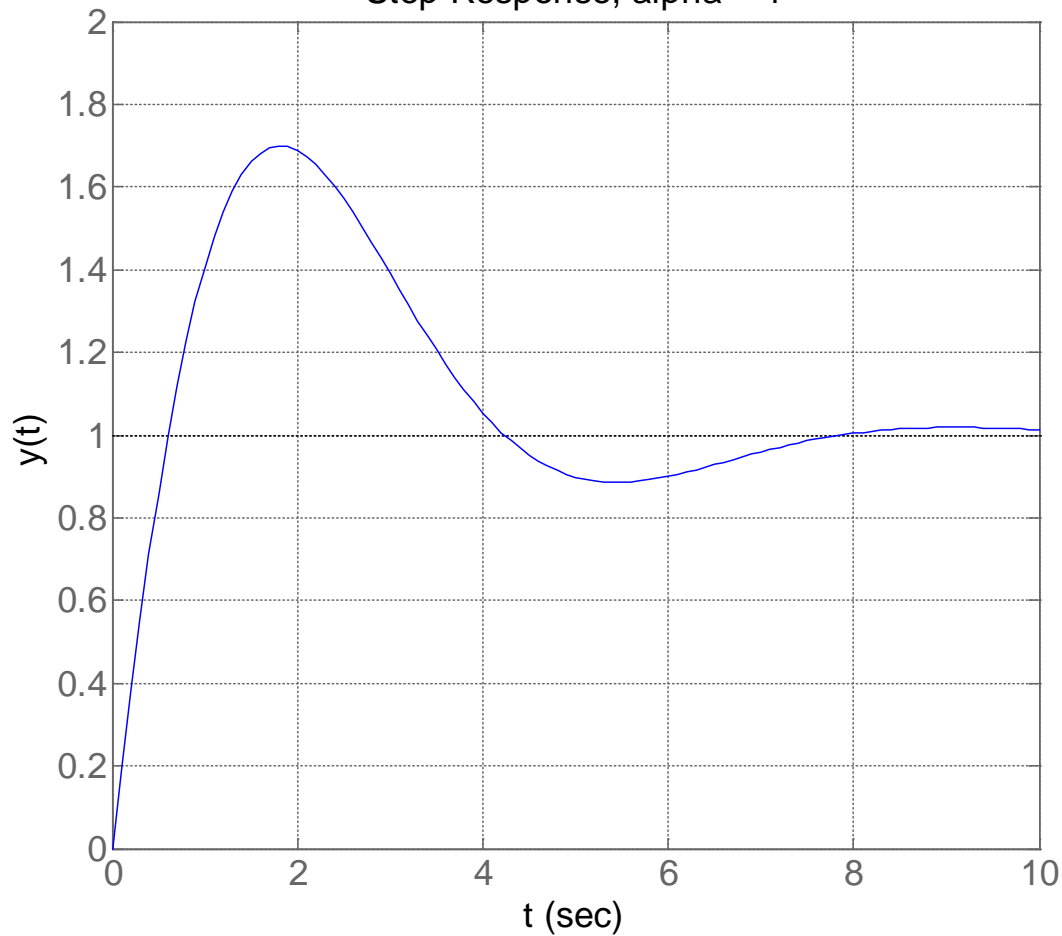




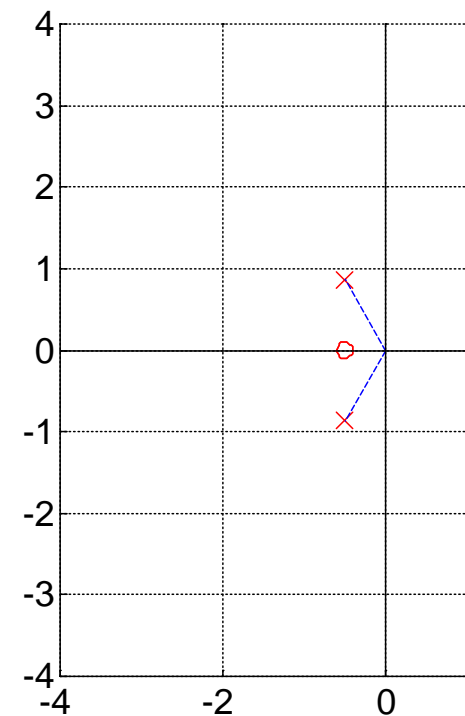
# Second-Order Transfer Function with One Zero



Step Response,  $\alpha = 1$



Pole-Zero Plot



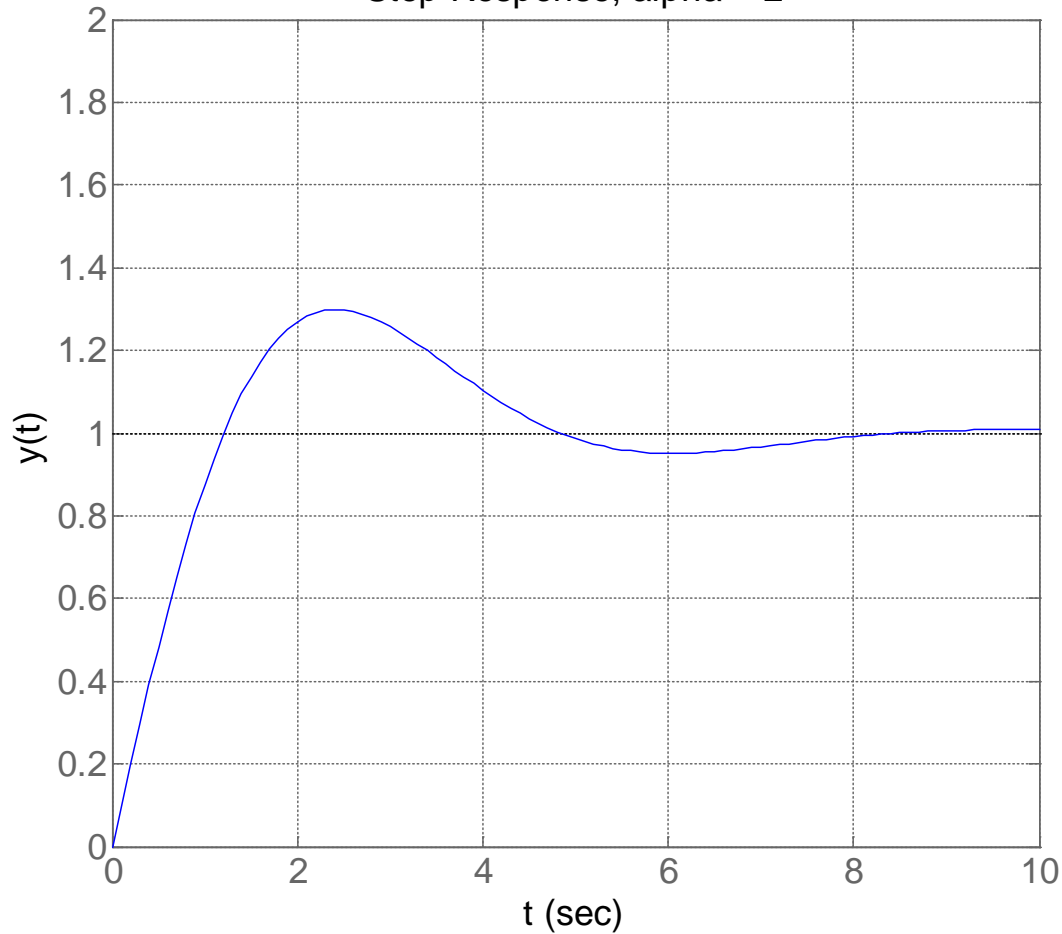




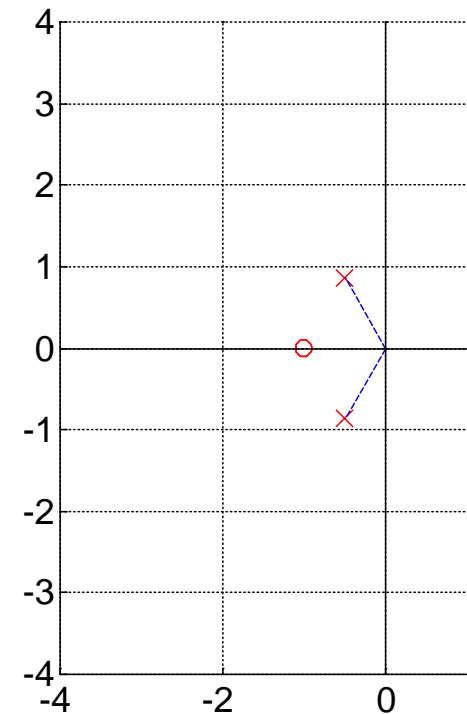
# Second-Order Transfer Function with One Zero



Step Response,  $\alpha = 2$

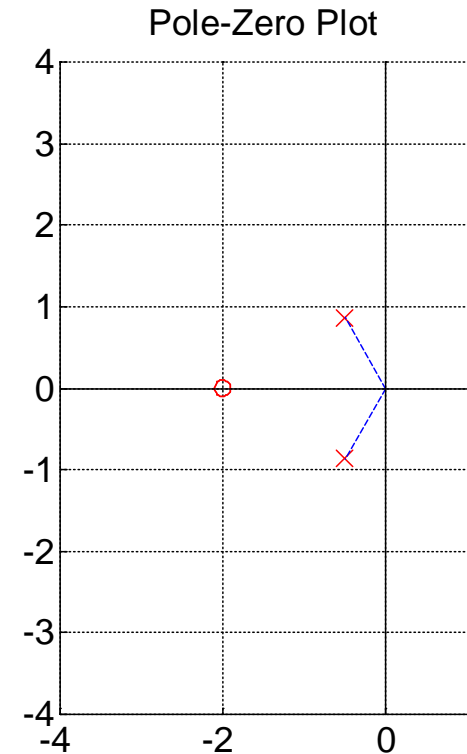
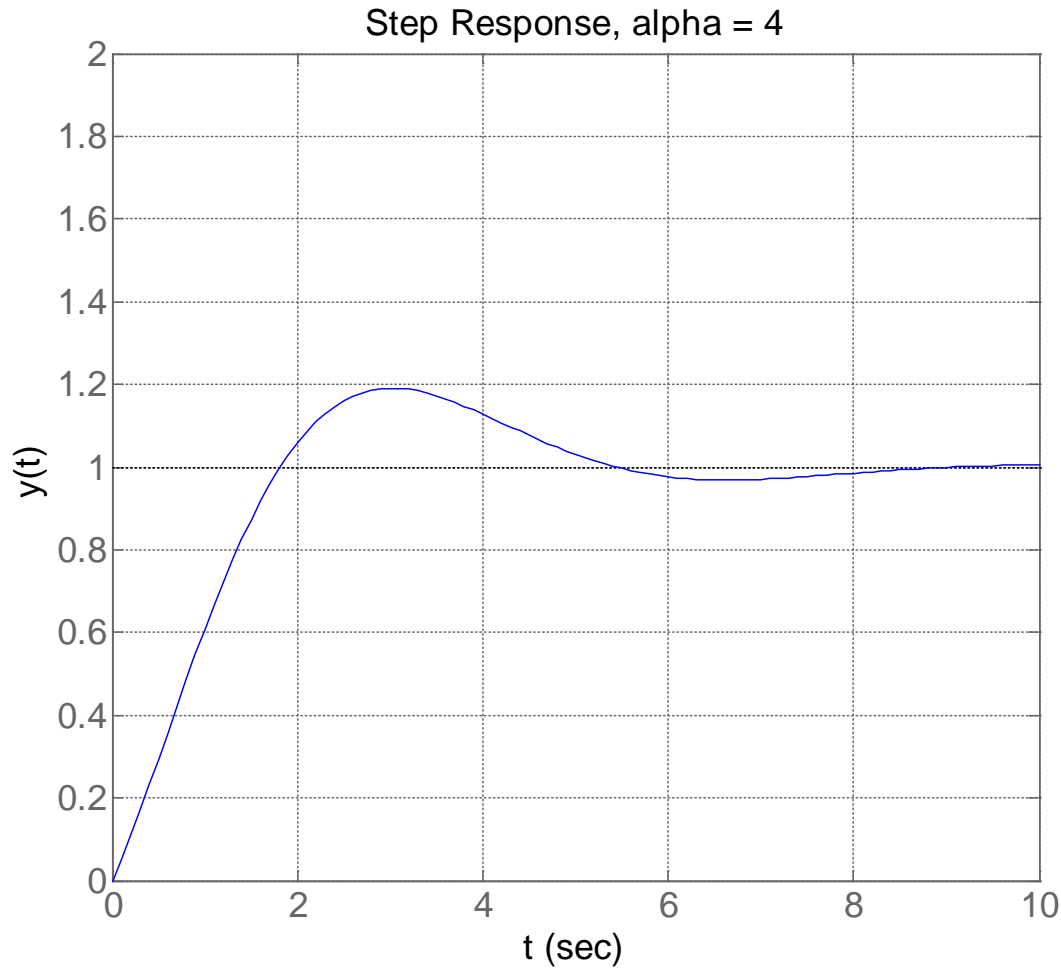


Pole-Zero Plot



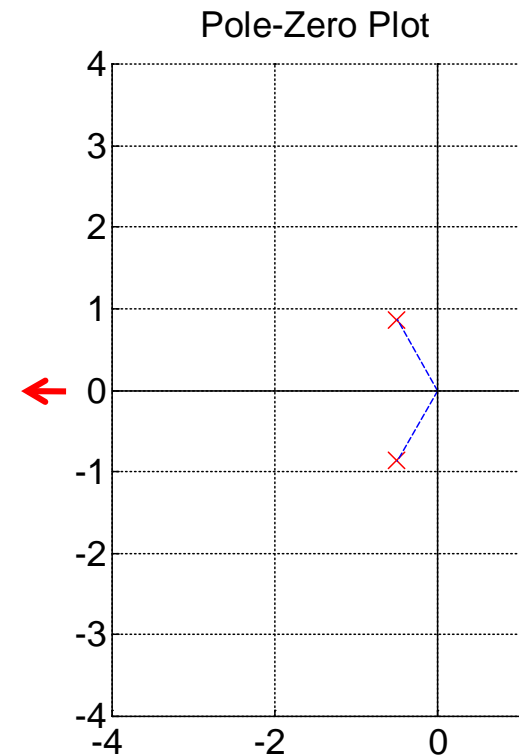
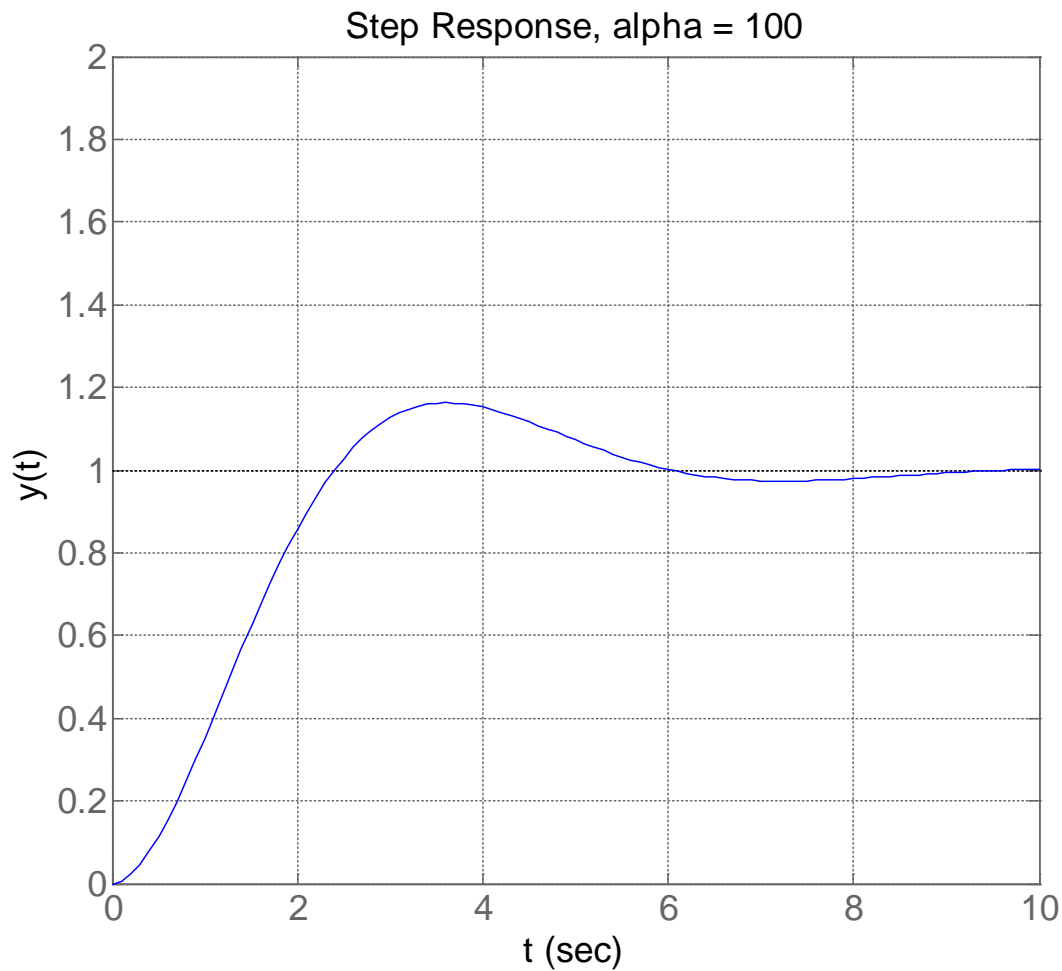


# Second-Order Transfer Function with One Zero





# Second-Order Transfer Function with One Zero

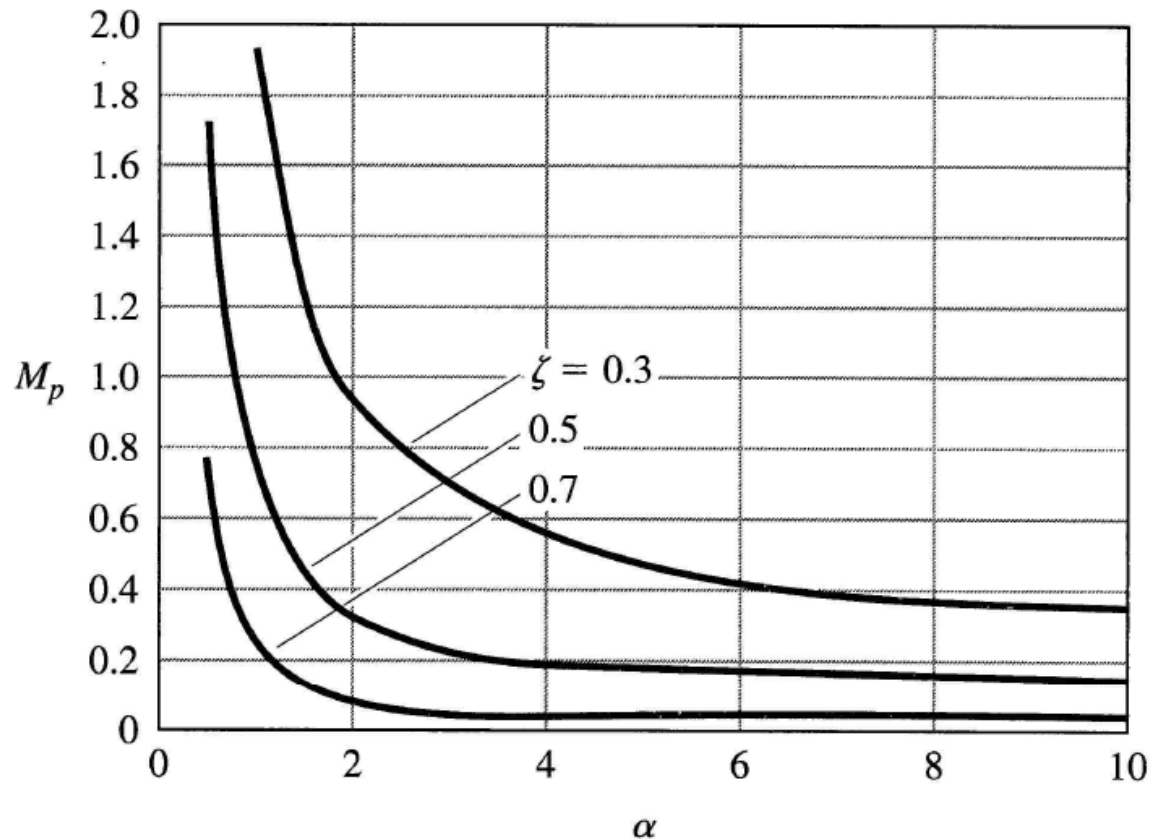




## Overshoot vs Zero Location



- A plot of the overshoot  $M_p$  versus the location of the zero relative to the real part of the poles  $\alpha$  is shown below for  $\zeta = 0.3, 0.5$  and  $0.7$





## Overshoot vs Zero Location



- The zero has very little effect on  $M_p$  if  $\alpha > 3$ , but as  $\alpha$  decreases below 3, has an increasing effect, especially when  $\alpha = 1$  or less
- This can be explained in terms of Laplace transform analysis
- Without loss of generality, assume  $\omega_n = 1$

$$H(s) = \frac{s/\alpha\zeta + 1}{s^2 + 2\zeta s + 1}$$

- We then write the transfer function as the sum of two terms

$$H(s) = \frac{1}{s^2 + 2\zeta s + 1} + \frac{1}{\alpha\zeta} \frac{s}{s^2 + 2\zeta s + 1}$$



## Overshoot vs Zero Location

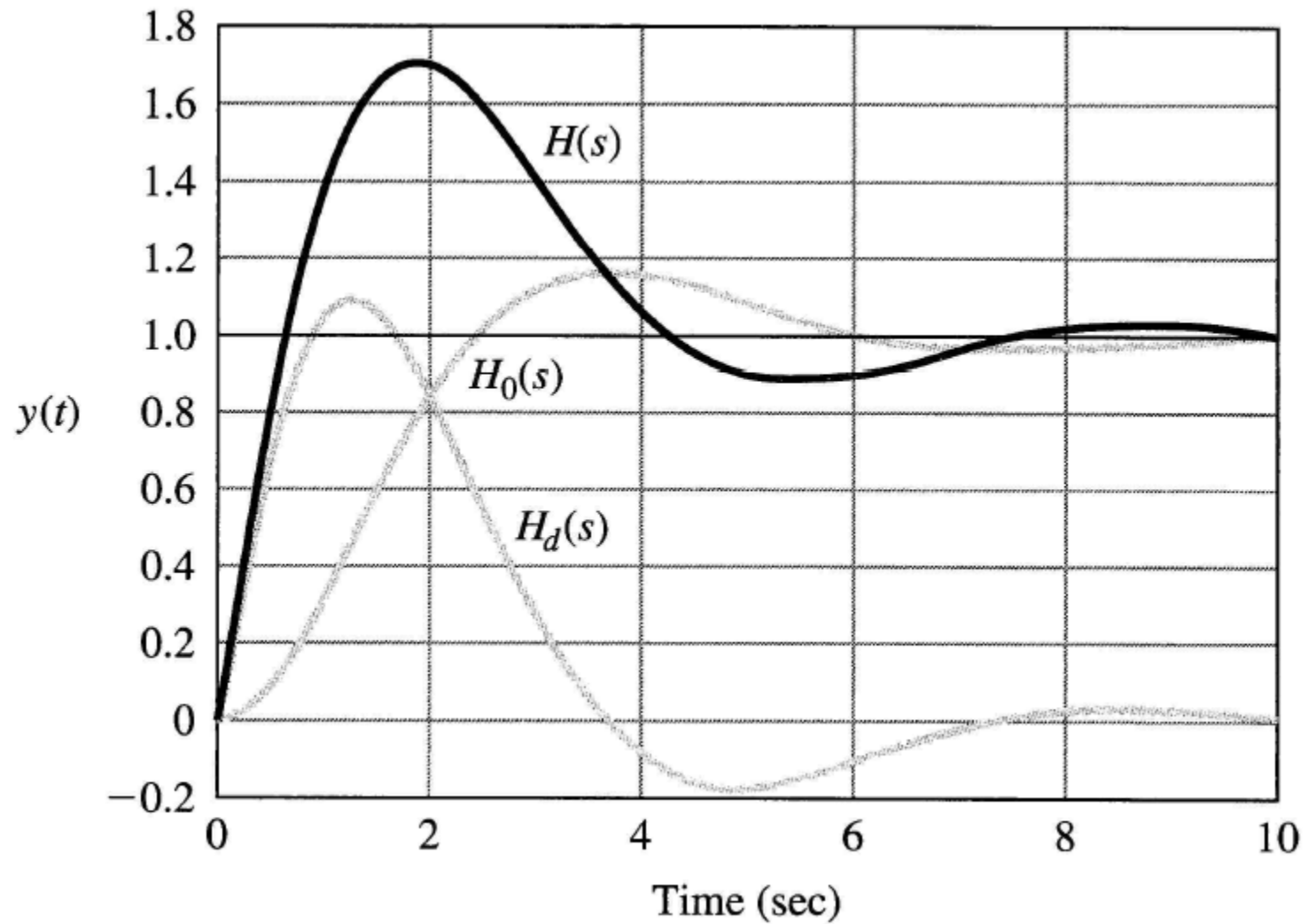


$$\begin{aligned} H(s) &= \frac{1}{s^2 + 2\zeta s + 1} + \frac{1}{\alpha\zeta} \frac{s}{s^2 + 2\zeta s + 1} \\ &= H_0(s) + H_d(s) \end{aligned}$$

- The first term  $H_0(s)$  is the original transfer function with no zeroes
- The second term  $H_d(s)$  is a constant  $(1/\alpha\zeta)$  times  $sH_0(s)$ , which is the time derivative of  $H_0(s)$
- The step response of  $H(s)$  is therefore the weighted sum of the original second-order transfer function (with no zeroes) and its time derivative
- The larger the value of  $\alpha$ , the less the contribution of the derivative
- The smaller the value of  $\alpha$ , the greater the contribution of the derivative



## Overshoot vs Zero Location





## Overshoot vs Zero Location

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- The step responses of  $H_0(s)$  and  $H_d(s)$  explain why the zero increases the overshoot
- The derivative  $H_d(s)$  has a large peak in the early part of the curve
- Adding this to the original  $H_0(s)$  lifts up the total response  $H(s)$  to produce the overshoot
- The amount of additional overshoot is determined by the relative weight of  $H_0(s)$  and  $H_d(s)$  as determined by the relative location  $\alpha$  of the zero to the poles

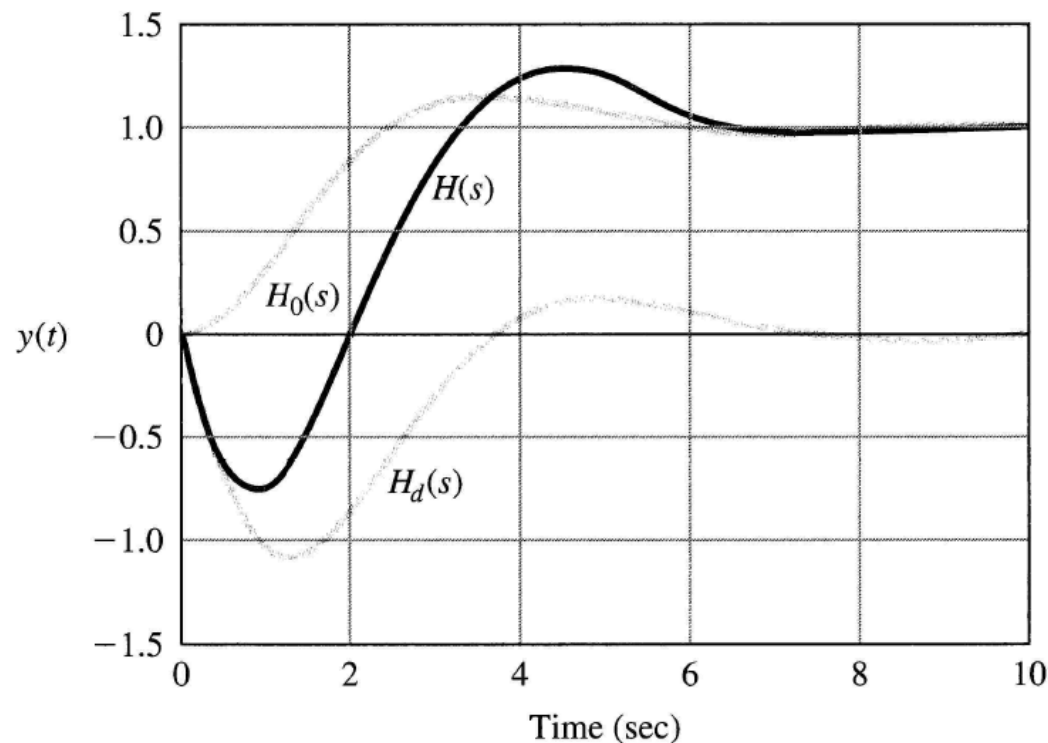




## Effect of Nonminimum-Phase Zero



- When the zero is in the right half-plane, i.e. when the zero has a positive real value ( $\alpha < 0$ ), then the derivative term is subtracted rather than added. A RHP zero is called a nonminimum phase zero.

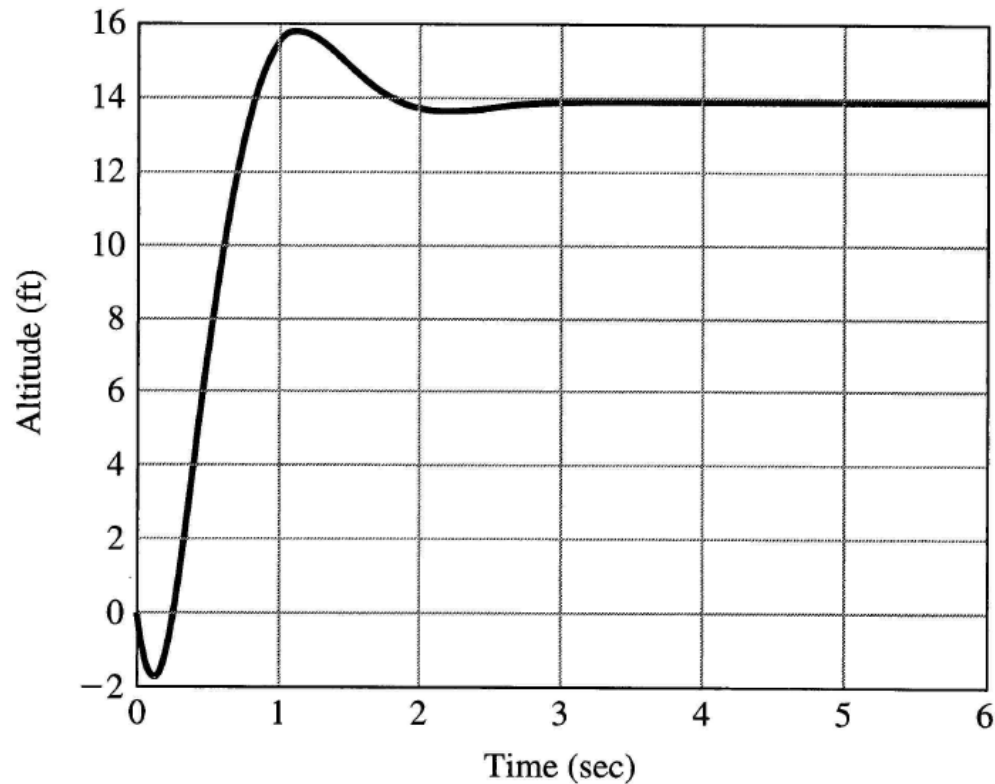




## Effect of Nonminimum-Phase Zero



- The step response of a system with a nonminimum phase zero starts of in wrong direction, e.g response of aircraft altitude to impulsive elevator input





## Second-Order Transfer Function with Extra Pole



- Consider the effects of an extra pole on the standard second-order step response

$$H(s) = \frac{1}{(s/\alpha\zeta\omega_n + 1)\left[(s/\omega_n)^2 + 2\zeta(s/\omega_n) + 1\right]}$$

- The original poles are located at  $s = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$   
 $= -\sigma \pm j\omega_d$
- The extra pole is located at  $s = -\alpha\zeta\omega_n = -\alpha\sigma$
- In other words, the extra pole is located at  $\alpha$  times the real part of the original poles



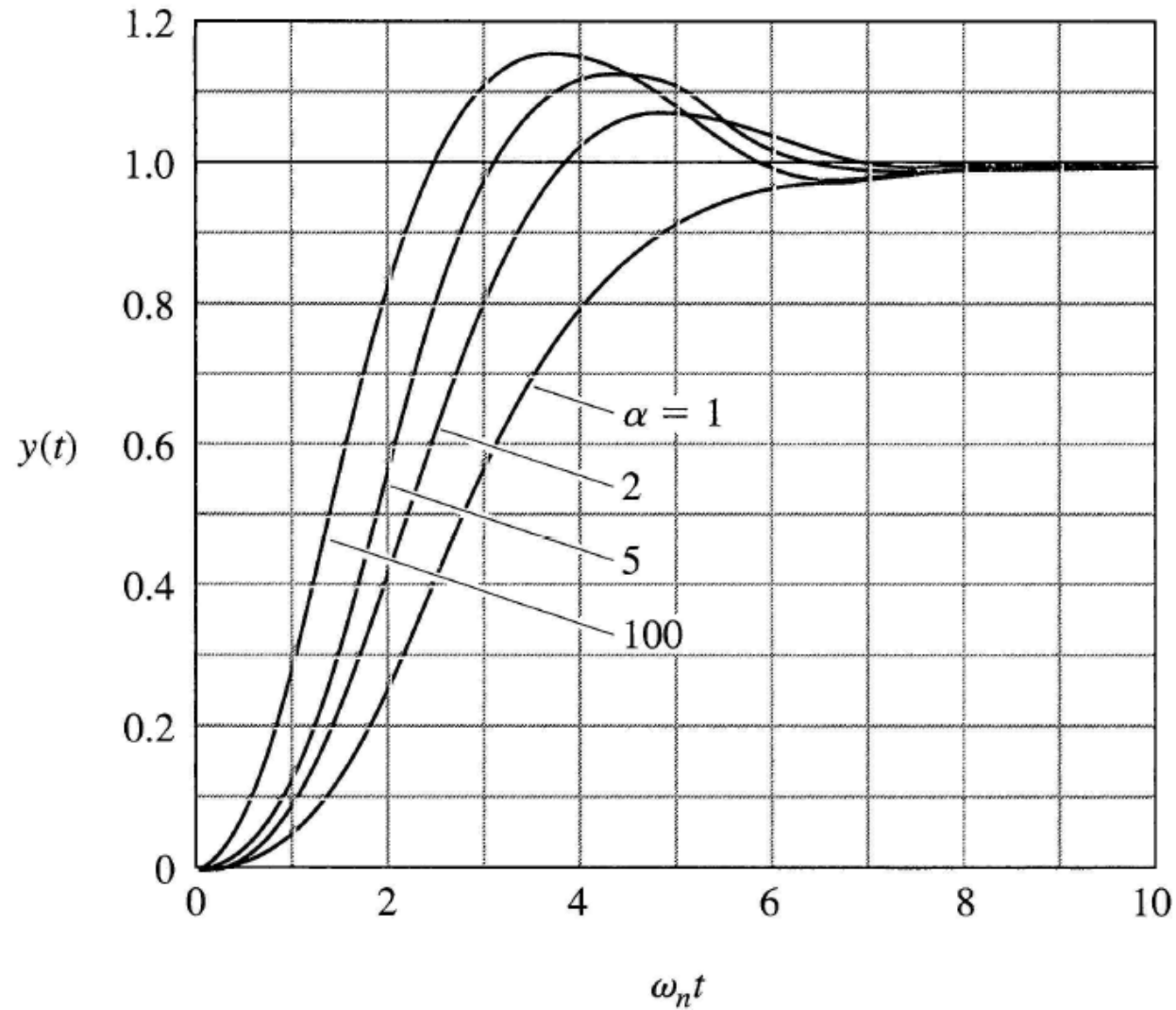
## Second-Order Transfer Function with Extra Pole



- If  $\alpha$  is large, the extra pole will be far removed from the original poles, and will have little effect on the transient response
- If  $\alpha \approx 1$ , the extra pole will be close to the real part of the original poles and can be expected to have a substantial effect on the transient response
- The step response curves for  $\zeta = 0.5$  and several values of  $\alpha$  are shown on the next pages
- The major effect of the extra pole is to increase the rise time  $t_r$
- Also note how the transient response changes from a dominantly second-order response to a dominantly first-order response

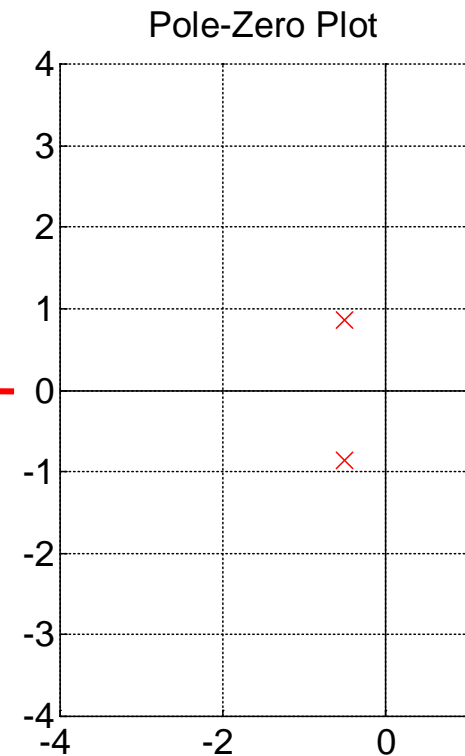
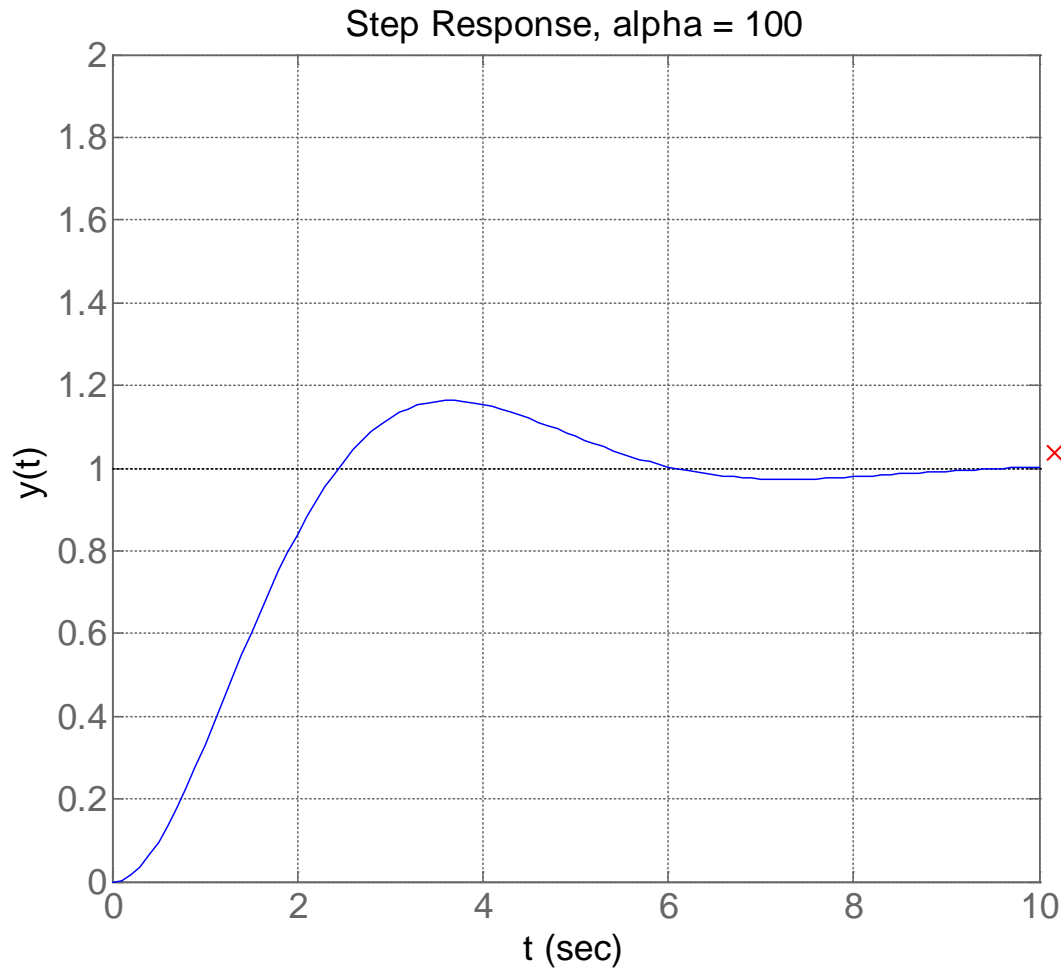


## Second-Order Transfer Function with Extra Pole



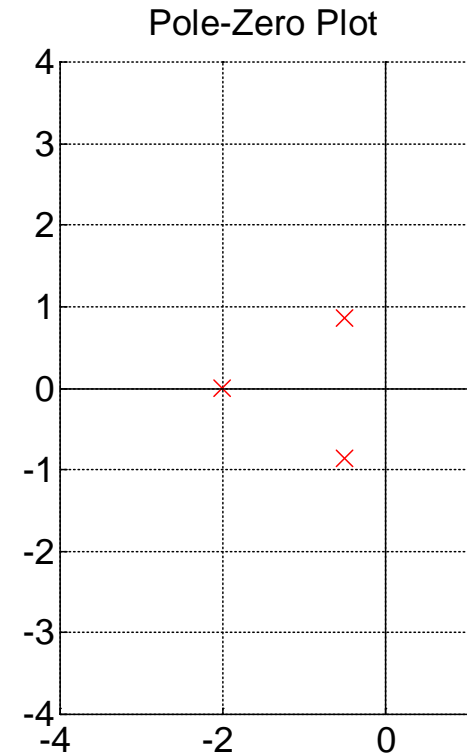
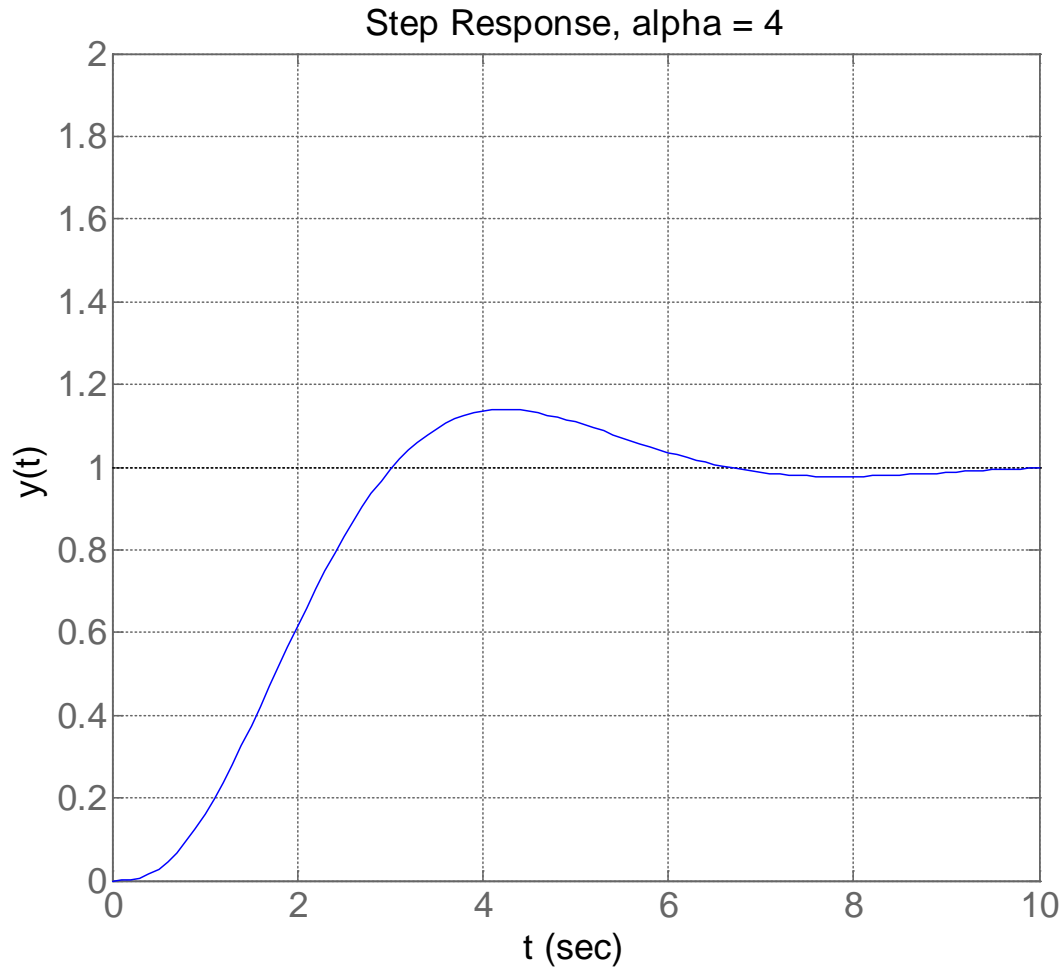


# Second-Order Transfer Function with Extra Pole



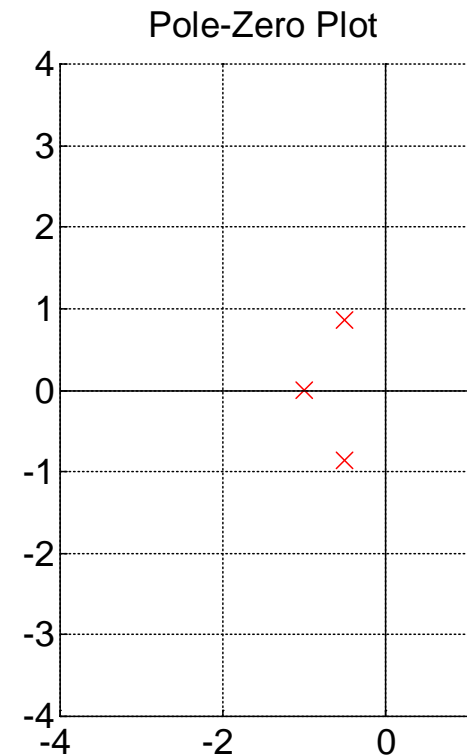
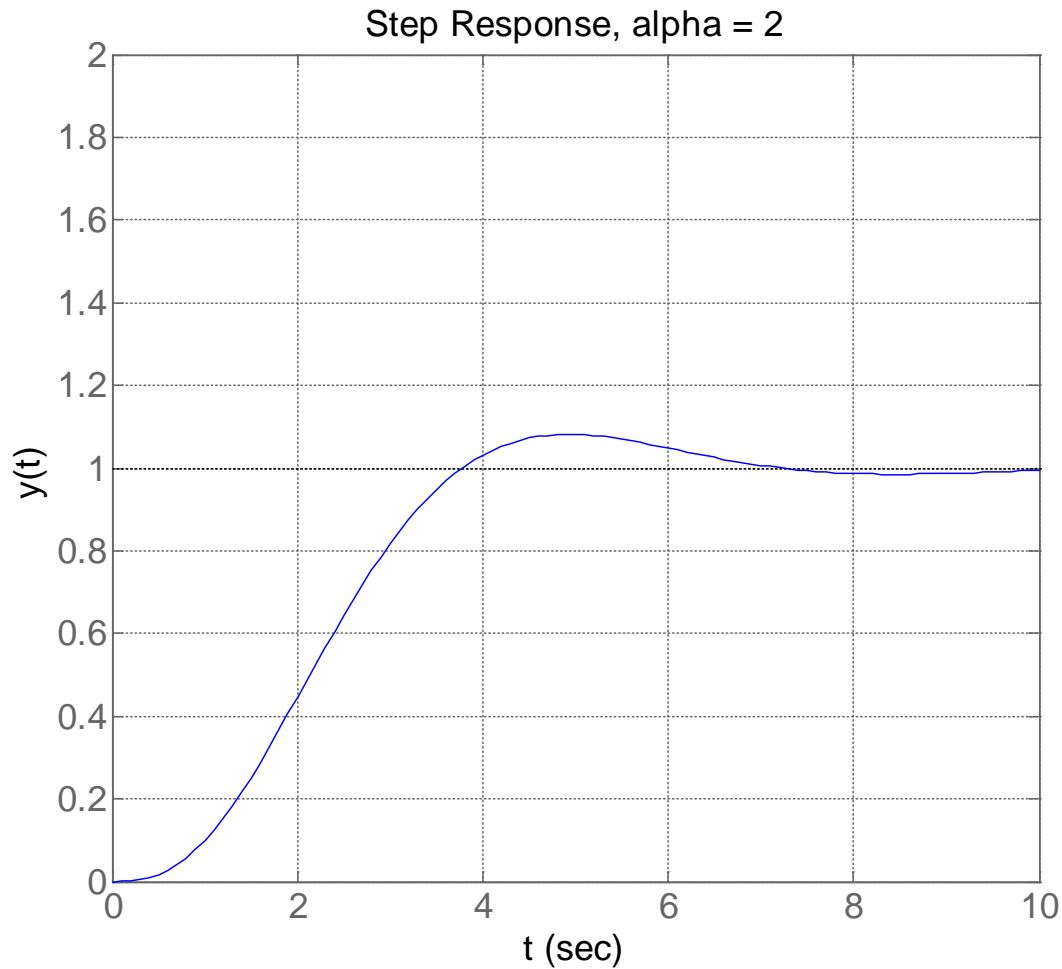


# Second-Order Transfer Function with Extra Pole





# Second-Order Transfer Function with Extra Pole



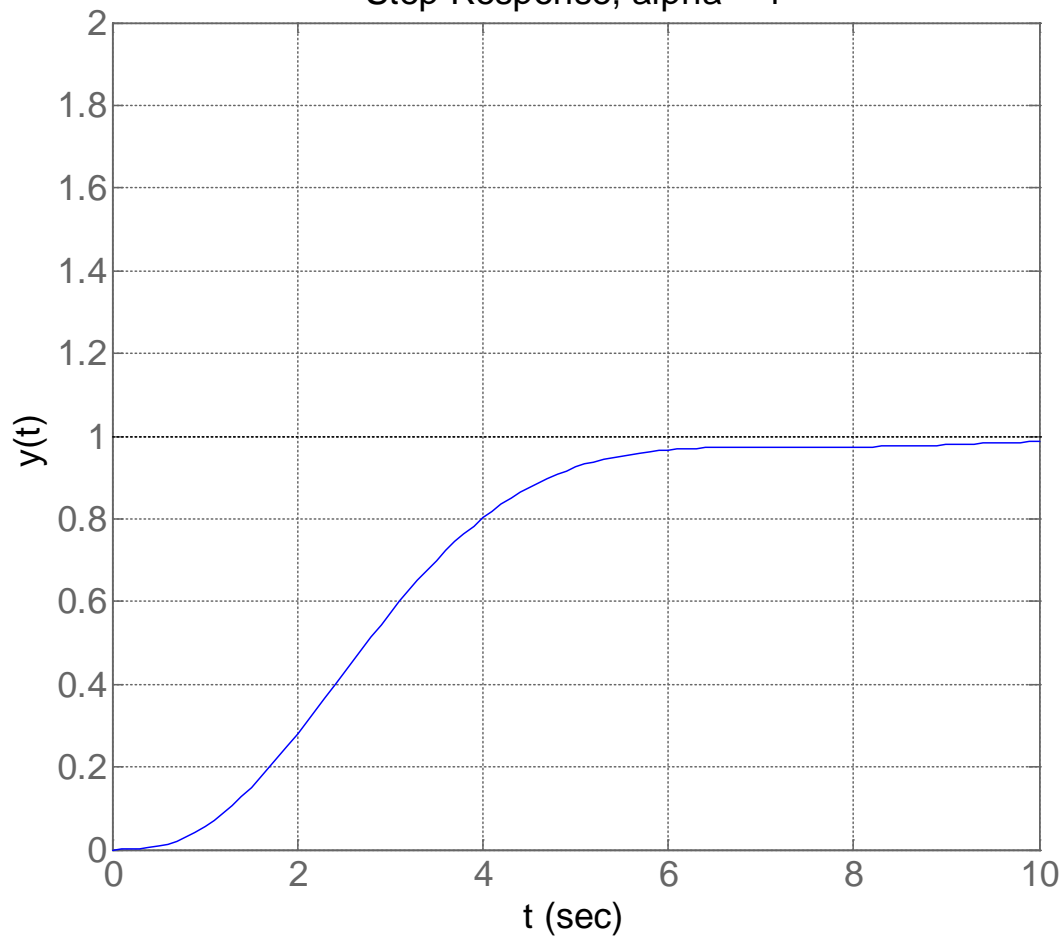




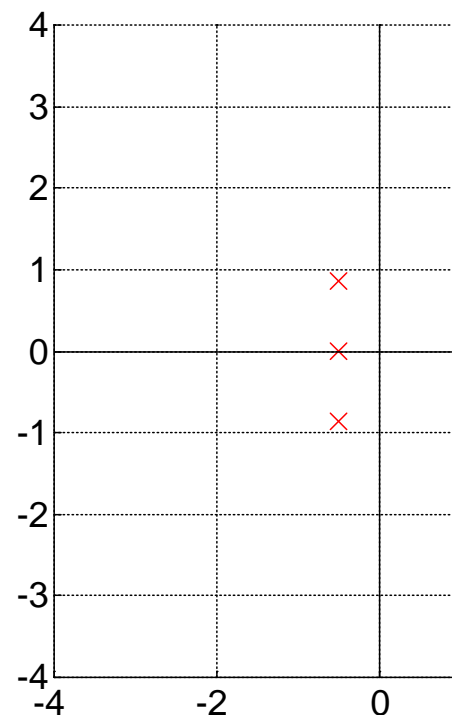
# Second-Order Transfer Function with Extra Pole



Step Response,  $\alpha = 1$



Pole-Zero Plot

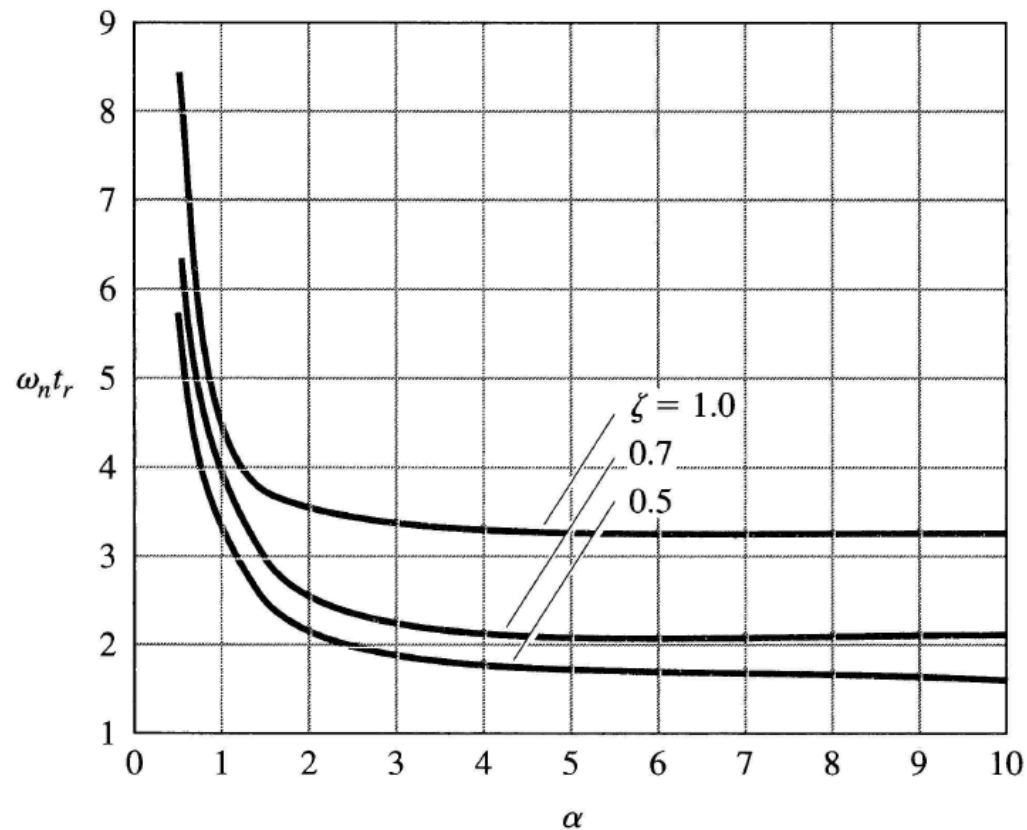




## Rise time vs Extra Pole Location



- A plot of the rise time  $t_r$  versus the location of the extra pole relative to the real part of the original poles  $\alpha$  is shown for  $\zeta = 1, 0.7$  and  $0.5$





## Summary



- For a second-order system with **no finite zeroes**

Rise time:  $t_r \approx \frac{1.8}{\omega_n}$

Peak time:  $t_p = \frac{\pi}{\omega_d}$

Overshoot:  $M_p = e^{-\pi\zeta/\sqrt{1-\zeta^2}}, \forall 0 \leq \zeta < 1$

Settling time:  $t_{s\ 2\%} \approx \frac{4}{\sigma}$



## Summary

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- A zero in the left half-plane (LHP) will increase the overshoot if the zero is within a factor of 4 of the real part of the complex poles. *Use relevant figure in Franklin, Powell and Emami-Naeini to determine new overshoot value.*
- A zero in the right half-plane (RHP) will depress the overshoot and may cause the step response to start out in the wrong direction.
- An additional pole in the left half-plane (LHP) will increase the rise time significantly if the extra pole is within a factor of 4 of the real part of the complex poles. *Use relevant figure in Franklin, Powell and Emami-Naeini to determine new rise time.*



# Dominant Poles

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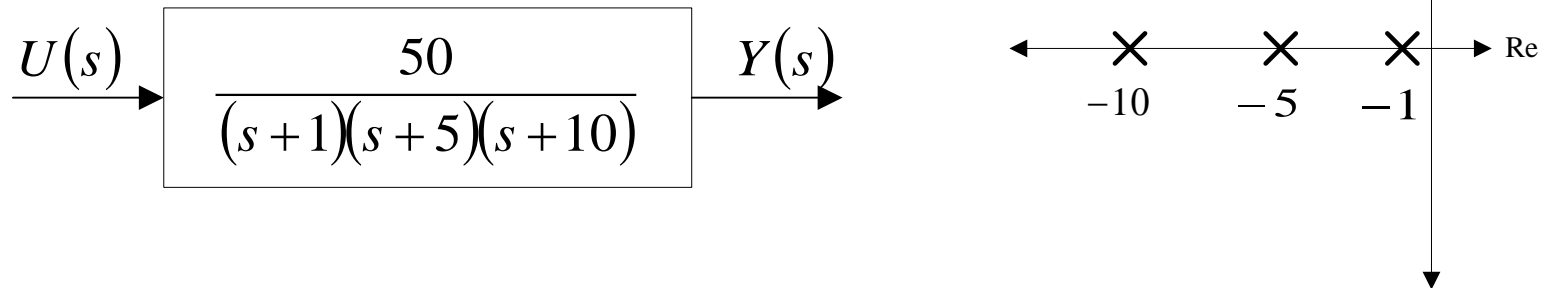
- In higher-order systems, there usually exist one or more dominant poles. These are the poles that have the most influence on the system response
- In other words, if a step input is applied to the input of the system, the system output will mostly respond as if its transfer function only contained the dominant poles
- The dominance of poles are affected by:
  - Fast and slow poles
  - Effect of zeroes



## Dominant Poles – Fast and Slow Poles



- Consider the higher-order system with three poles



- The step response may be obtained mathematically by applying a step input and performing partial fraction expansion

$$\begin{aligned} Y(s) &= H(s)U(s) = \frac{50}{(s+1)(s+5)(s+10)} \cdot \frac{1}{s} \\ &= 1 - \frac{25}{18} \left( \frac{1}{s+1} \right) + \frac{1}{2} \left( \frac{1}{s+5} \right) - \frac{1}{9} \left( \frac{1}{s+10} \right) \end{aligned}$$



## Dominant Poles – Fast and Slow Poles



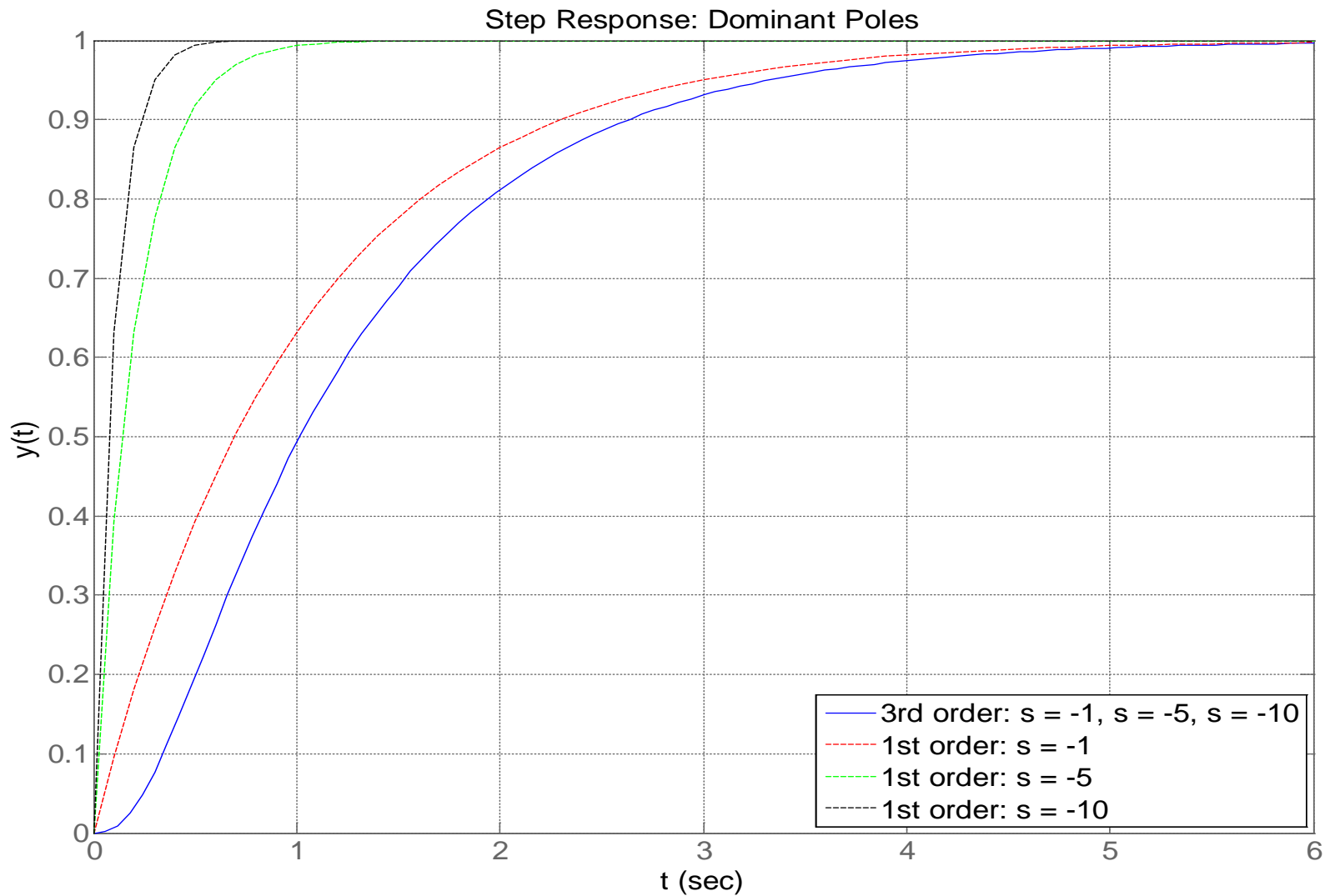
- The step response in the time domain may be obtained by taking the inverse Laplace transform

$$y(t) = 1 - \frac{25}{18}e^{-t} + \frac{1}{2}e^{-5t} - \frac{1}{9}e^{-10t}$$

- Note that:
- The coefficient of the  $e^{-t}$  term is the largest
- It takes much longer for  $e^{-t}$  to decay than either  $e^{-5t}$  or  $e^{-10t}$
- $-\frac{25}{18}e^{-t}$  is the dominant term and that  $s = -1$  is the dominant pole
- **Conclusion:** The dynamic response of a higher-order system is dominated by the slowest poles



# Dominant Poles – Fast and Slow Poles



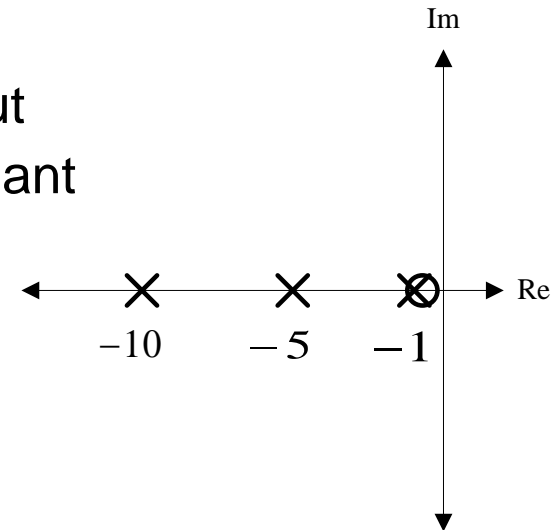
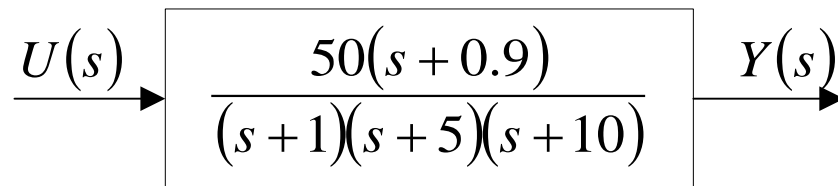




## Dominant Poles – Effect of Zeroes



- Consider the same third-order system, but with a zero at  $s = -0.9$ , close to the dominant pole at  $s = -1$



- The step response may be obtained mathematically by applying a step input and performing partial fraction expansion

$$\begin{aligned} Y(s) = H(s)U(s) &= \frac{50(s+0.9)}{(s+1)(s+5)(s+10)} \cdot \frac{1}{s} \\ &= 0.9 + \frac{5}{36} \left( \frac{1}{s+1} \right) - \frac{41}{20} \left( \frac{1}{s+5} \right) + \frac{91}{90} \left( \frac{1}{s+10} \right) \end{aligned}$$



## Dominant Poles – Effect of Zeroes



- The step response in the time domain may be obtained by taking the inverse Laplace transform

$$y(t) = 0.9 + \frac{5}{36}e^{-t} - \frac{41}{20}e^{-5t} + \frac{91}{90}e^{-10t}$$

- Note that:
- Now the coefficient of the  $e^{-5t}$  term larger than that of the  $e^{-t}$  term
- Now  $-\frac{41}{20}e^{-5t}$  is the dominant term and  $s = -5$  is the dominant pole



## Dominant Poles – Effect of Zeroes



- Let us compare the coefficients of the transfer function with and without the zero

- No zeroes:

$$y(t) = 1 - \frac{25}{18}e^{-t} + \frac{1}{2}e^{-5t} + \frac{1}{9}e^{-10t}$$

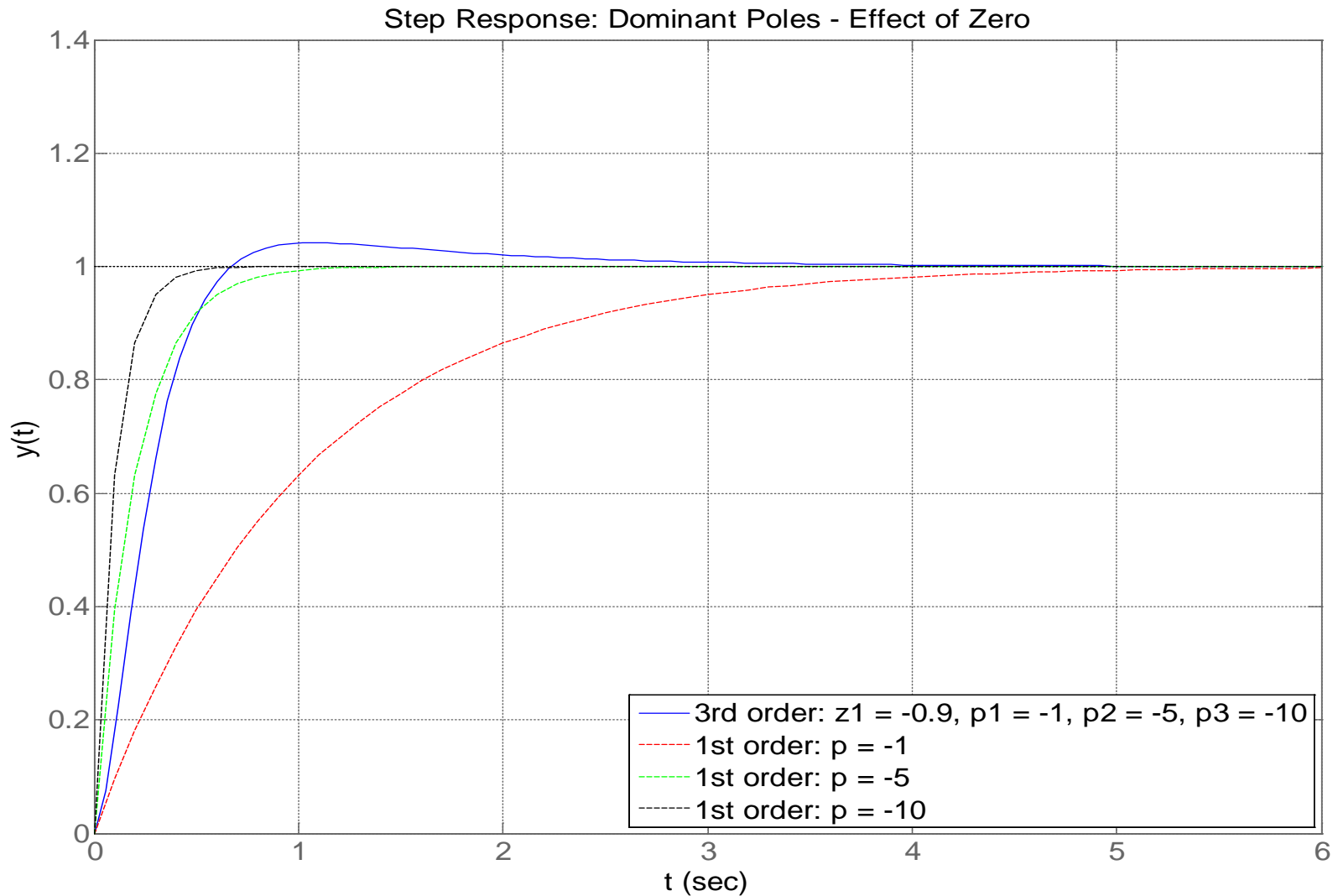
- With zero at  $s = -0.9$ :

$$y(t) = 0.9 + \frac{5}{36}e^{-t} - \frac{41}{20}e^{-5t} + \frac{91}{90}e^{-10t}$$

- When there are no zeroes present, the  $e^{-t}$  has the largest coefficient, and the pole at  $s = -1$  is dominant
- With the addition of the zero at  $s = -0.9$ , the coefficient of the  $e^{-t}$  becomes significantly smaller than the coefficients of the  $e^{-5t}$  and  $e^{-10t}$  terms, and the pole at  $s = -1$  is no longer dominant



# Dominant Poles – Effect of Zeroes





## Dominant Poles – Effect of Zeroes

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- **Conclusion:** A zero close to a pole reduces the influence of the pole on the transient response, because it causes the pole to have a smaller residue (partial fraction constant)



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# Reference: Chapter 3.5



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