# C6 Optical properties and applications of optical fibers

## SUPPLEMENTARY INFORMATION

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Name	Total	Model and parameters
Optical fiber	3	FC/PC; $\phi$ 62.5 $\mu$ m, $\phi$ 9 $\mu$ m, $\phi$ 4 $\mu$ m
Source-fiber coupling alignment jig	1	Range: $0 \sim 4mm$ ; Fine knob: $1\mu m$
Focusing lens	1	f = 5mm
Laser	1	
Optical fiber information experimental system	1	SGQ-3
Polarizer	3	
quarter wave plate	1	

## 1 Materials and instruments

Table S1: Materials and instruments

## 2 Exp.1 Source-fiber coupling and numerical aperture

#### 2.1 Supplementary data and figure

- 1. Tab. S2 Input light power
- 2. Tab. S3 Output light power
- 3. Tab. S4 Numerical aperture

2.34~mW	$2.33 \ mW$	2,30~mW	$2.27 \ mW$	2.28~mW

Table S2: Input light power

## 2.2 Reflection question

#### 2.2.1 Compare and evaluate the coupling efficiency of the two method

This has been discussed in the thesis in details. We found that compared to direct coupling, coupling through a lens gained a great improvement in reducing the coupling loss. The effectiveness is consistent in all three fibers, proving that coupling through a lens is an effective way to couple the light source and the fiber.

#### 2.2.2 Differences between single-mode fiber and multi-mode fiber

1. Multi-mode fiber usually has a larger core diameter comparing to the single-mode fiber, which makes it much easier to couple with the light source, thus reaches a higher coupling efficiency. However, theoretically, light passing through the single-mode fiber is not reflected too many times due to the narrow core comparing to the multi-mode fiber, which means that it shall have lesser attenuation. This is based on fully coupling at the connector, but due to the limitations of our instruments, loss at the connector played a major role, thus we obtained an inconsistent result.

Fiber	Direct coupling	Coupling through a lens
$\phi$ 62.5 $\mu m$	$6.98~\mu W$	1.73~mW
$\phi~62.5 \mu m$	$6.95~\mu W$	1.67~mW
$\phi~62.5 \mu m$	$6.90~\mu W$	1.72~mW
$\phi~62.5\mu m$	$6.92~\mu W$	1.68~mW
$\phi~62.5 \mu m$	$6.93~\mu W$	$1.70 \ mW$
$\phi 9 \mu m$	$0.193 \; \mu W$	1.63~mW
$\phi 9 \mu m$	$0.184~\mu W$	1.64~mW
$\phi \ 9\mu m$	$0.191~\mu W$	1.63~mW
$\phi \ 9\mu m$	$0.192~\mu W$	1.65~mW
$\phi 9 \mu m$	$0.193 \; \mu W$	$1.67 \ mW$
$\phi \ 4\mu m$	$0.072~\mu W$	1.004~mW
$\phi \ 4\mu m$	$0.071~\mu W$	1.005~mW
$\phi \ 4\mu m$	$0.072~\mu W$	$1.037 \ mW$
$\phi \ 4\mu m$	$0.073~\mu W$	1.026~mW
$\phi 4\mu m$	$0.071~\mu W$	1.064~mW

Table S3: Output light power

Distance $D$	Fiber $\phi$ 62.5 $\mu m$	Fiber $\phi$ 9 $\mu m$	Fiber $\phi \ 4\mu m$
4.50~cm	2.61~cm	1.53~cm	1.61~cm
5.50~cm	3.20~cm	1.92~cm	2.02~cm
6.50~cm	3.82~cm	2.23~cm	2.35~cm
7.50~cm	4.25~cm	2.70~cm	2.72~cm
8.50~cm	4.71~cm	3.13~cm	3.16~cm
9.50~cm	5.42~cm	3.69~cm	3.49~cm
10.50~cm	6.03~cm	4.08~cm	3.94~cm
11.50~cm	$6.78 \ cm$	4.51~cm	4.41~cm

Table S4: Numerical aperture

2. Multi-mode fiber can transfer multiple modes simultaneously, thus the exit spots are generally more diffused due to the blending of these lights, while the single-mode fiber can transfer only one specific type of mode, thus the exit spots generally show a concentrated pattern with high light intensity in the center and a blurred edges.

# 3 Exp.2 Strain and temperature sensor based on opticalfiber-based Mach-Zehnder interferometer

### 3.1 Main parameters

Item	parameters
Fiber	$\phi \ 4\mu m$

Table S5: Parameters adopted in Exp. 2

#### 3.2 Supplementary data and figure

- 1. Tab. S6 and S7 Strain sensor
- 2. Tab. S8 and S9 Temperature sensor

n	S increase cm	S decrease cm	n	Strain increase cm	Strain decrease cm
0	0.215	0.050	0	0.030	0.150
1	0.369	0.211	1	0.135	0.270
2	0.531	0.366	2	0.343	0.452
3	0.770	0.567	3	0.472	0.550
4	0.851	0.742	4	0.643	0.730
5	1.004	0.919	5	0.778	0.835
6	1.140	1.038	6	0.930	1.020
7	1.321	1.273	7	1.112	1.151
8	1.464	1.442	8	1.253	1.281
9	1.649	1.551	9	1.406	1.455
10	1.808	1.750	10	1.535	1.585
11	1.968	1.967	11	1.704	1.751
12	2.101	2.104	12	1.850	1.919
13	2.298	2.282	13	2.030	2.041
14	2.472	2.470	14	2.179	2.189
15	2.628	2.628	15	2.355	2.355

Table S6: Strain sensor, test 1

Table S7: Strain sensor, test 2

## 3.3 Reflection question

#### 3.3.1 Other types of fiber-based sensor[1]

Fiber sensors based on interferometer have been widely used in medicine. There're 4 major types of fiber biosensors:

n	T increase $cm$	T decrease $cm$	n	T increase $cm$	T decrease $cm$
0	25.0	35.0	0	25.0	35.0
5	25.5	34.5	5	25.5	34.6
10	25.9	34.1	10	26.0	34.0
15	26.5	33.6	15	26.6	33.5
20	27.0	33.1	20	27.1	33.0
25	27.4	32.6	25	27.5	32.6
30	28.0	32.2	30	28.1	32.0
35	28.6	31.5	35	28.6	31.5
40	29.0	31.0	40	29.1	31.0
45	29.5	30.4	45	29.5	30.4
50	30.1	30.0	50	30.1	30.0
55	30.6	29.6	55	30.5	29.6
60	31.1	29.0	60	31.1	29.0
65	31.6	28.5	65	31.5	28.5
70	32.0	28.0	70	32.0	28.1
75	32.4	27.6	75	32.5	27.5
80	33.0	27.0	80	33.0	27.0
85	33.5	26.4	85	33.4	26.6
90	34.0	26.0	90	34.0	26.0
95	34.4	25.5	95	34.5	25.6
100	35.1	25.0	100	35.0	25.1

Table S8: Temperature sensor, test 1

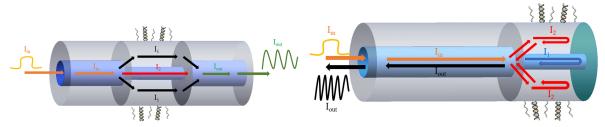
Table S9: Temperature sensor, test 2

Fiber biosensors based on Mach-Zehnder interferometer The light is split into two beams via a coupler or splice point. A net phase difference is accumulated as the beams through the length of the fiber leading to Mach-Zehnder interference when the two beams are recombined. (Fig. S1a)

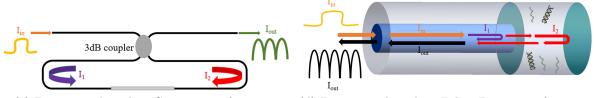
Fiber biosensors based on Michelson interferometer The light is divided into two beams in the coupler and transmitted along the fiber and then reflected at the reflective end face of the fiber end, thus cause a Michelson interference spectrum when the two beams are recombined in the coupler. (Fig. S1b)

Fiber biosensors based on Sagnac interferometer Light from a broad-band source is split into clockwise and counterclockwise beams via a coupling zone as it enters the loop. A net phase difference is accumulated as the two polarization fundamental modes (ie,  $I_1$  and  $I_2$ ) through the length of the birefringent fiber, leading to Sagnac interference when the clockwise and counterclockwise beams are recombined at the coupling zone. (Fig. S1c)

Fiber biosensors based on Fabry-Perot interferometer The light is reflected at the two reflective surfaces, then FP interference occurs due to the existence of the optical path difference. (Fig. S1d)



(a) Biosensors based on Mach-Zehnder interferome- (b) Biosensors based on Michelson interferometer



(c) Biosensors based on Sagnac interferometer (d) Biosensors based on Fabry-Perot interferometer

Figure S1: Fiber-based biosensor

#### Exp.3 Impact of transmission in a fiber on the polar-4 ization state

#### 4.1 Main parameters

Item	parameters
Fiber	$\phi \ 4\mu m$

Table S10: Parameters adopted in Exp. 3

#### Supplementary data and figure 4.2

1. Fig. S2 Fluctuation of the light power after the fiber transmission

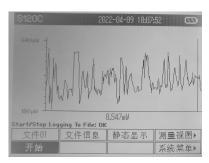
#### 4.3 Reflection question

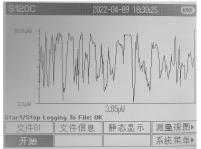
#### Analyze the experimental results and compare with the theoretical value. 4.3.1 Analyze possible deviation.

This question has been discussed in details in the thesis.

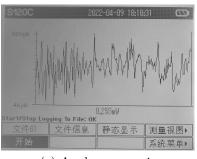
#### Mechanism of the polarization-maintaining fibers.

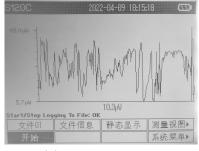
Polarization-maintaining fiber is specialty fiber with a strong built-in birefringence (highbirefringence fiber or HIBI fiber). Provided that the polarization of light launched into the

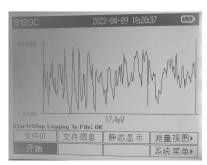




- (a) linearly polarized light
- (b) Right-handed polarized light







- (c) Analyzer: x-axis
- (d) Analyzer: y-axis

(e) Analyzer:  $\frac{\pi}{4}$ 

Figure S2: Fluctuation of the light power after the fiber transmission

fiber is aligned with one of the birefringent axes, this polarization state will be preserved even if the fiber is bent. The propagation constants of the two polarization modes are significantly different due to the strong birefringence, so that the relative phase of such copropagating modes rapidly drifts away. Therefore, any disturbance along the fiber can effectively couple both modes only if it has a significant spatial Fourier component with a wavenumber which matches the difference of the propagation constants of the two polarization modes.

A commonly used method for introducing strong birefringence is to include two (not necessarily cylindrical) stress rods of a modified glass composition (typically boron-doped glass, with a different degree of thermal expansion) in the preform on opposite sides of the core. (Fig. S3)

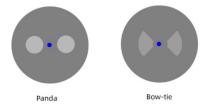


Figure S3: Polarization-maintaining fiber

# 5 Data and code availability

Data and code are available at https://github.com/Jeg-Vet/SYSU-PHY-EXP/tree/main/

# Reference

[1] LI X, CHEN N, ZHOU X, et al. A Review of Specialty Fiber Biosensors Based on Interferometer Configuration[J/OL]. Journal of Biophotonics, 2021, 14(6): e202100068 [2022-04-12]. https://onlinelibrary.wiley.com/doi/abs/10.1002/jbio.202100068. DOI: 10.1002/jbio.202100068 (:4).