

**Department of Applied Mechanics**  
**Indian Institute of Technology Delhi**  
**Major, First Semester 2021-22**

**Course Title: Advanced Finite Element Method**

**Course No.: AML 805**

**Date: 18 November 2021**

**Duration: 2.5 Hrs (9.00-11.30 AM)**

**Maximum Marks: 150**

**Instructions:**

- (i) You can refer your notes and books. It is an open notes, open book examination.
- (ii) Answer all the questions. Marks are indicated against each question. There are total 9 Questions.
- (iii) Write answers in your own handwriting.
- (iv) Start answer of each question on a new page.
- (v) Stop writing at 11.30 AM and start scanning and uploading pdf in gradescope. You should finish uploading answers before 11.50 AM.
- (vi) After uploading pdf, select pages for each question.
- (vii) If you have any doubt, call me on my mobile: 9213227603.

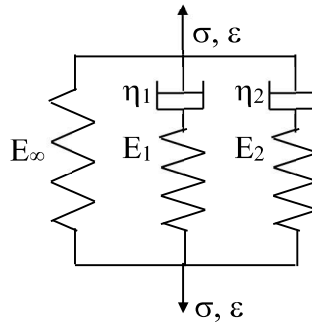
**Q.1:** The weak form of equilibrium equations for a 2D plane stress problem is given by:

$$\int_{V^0} \delta \{\mathbf{E}\}^T \{\mathbf{S}\} dV^0 - \int_{V^0} \delta \{\mathbf{U}\}^T \{\mathbf{f}_b\} dV^0 = 0 \text{ where}$$

$$\{\mathbf{E}\} = \begin{Bmatrix} E_{XX} \\ E_{YY} \\ E_{XY} \end{Bmatrix} = \begin{Bmatrix} \frac{\partial U}{\partial X} + \frac{1}{2} \left( \frac{\partial V}{\partial X} \right)^2 \\ \frac{\partial V}{\partial Y} + \frac{1}{2} \left( \frac{\partial V}{\partial Y} \right)^2 \\ \frac{\partial U}{\partial Y} + \frac{\partial V}{\partial X} + \frac{\partial V}{\partial X} \frac{\partial V}{\partial Y} \end{Bmatrix}; \{\mathbf{S}\} = \begin{Bmatrix} S_{XX} \\ S_{YY} \\ S_{XY} \end{Bmatrix}; \{\mathbf{U}\} = \begin{Bmatrix} U \\ V \end{Bmatrix}; \{\mathbf{f}_b\} = \begin{Bmatrix} f_{bX} \\ f_{bY} \end{Bmatrix}; \{\Delta \mathbf{S}\} = [\mathbf{C}_T] \{\Delta \mathbf{E}\}; U$$

and  $V$  are displacements along  $X$  and  $Y$  directions. Derive the incremental element level governing equation considering 4-noded isoparametric element. [20]

**Q. 2:** For the viscoelastic model shown, derive the relation:  $E(t) = E_\infty + \sum_{i=1}^2 E_i e^{-\frac{t}{\tau_i}}$ . [10]



**Q. 3:** State of stress at a point in a body is given by:  $\sigma_{xx} = 120 \text{ MPa}$ ,  $\sigma_{yy} = -80 \text{ MPa}$ ,  $\tau_{xy} = 0 \text{ MPa}$ ,  $\sigma_{zz} = \tau_{xz} = \tau_{yz} = 0$ . Consider isotropic strain hardening, von Mises yield function and associative flow rule ( $E = 200 \text{ GPa}$ ,  $\nu = 0$ , plastic modulus ( $H$ ) = 200 MPa, initial yield stress ( $\sigma_Y$ ) = 200 MPa).

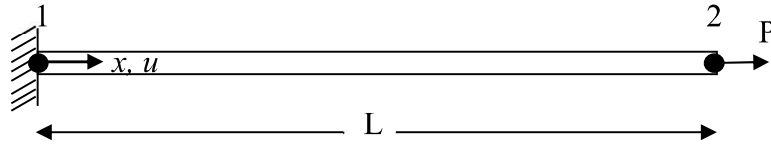
(i) Is the current state of stress elastic or elasto-plastic? [3]

(ii) For the next load step, finite element solution gives incremental strains:  $\Delta\epsilon_{xx} = 0.0009$ ,  $\Delta\epsilon_{yy} = 0.0009$ ,  $\Delta\gamma_{xy} = \Delta\gamma_{zz} = \Delta\gamma_{xz} = \Delta\gamma_{yz} = 0$ . Show that the new state of stress calculated assuming elastic behavior lies outside the yield surface. [5]

(iii) Calculate the factor  $\beta$  such that state of stress at the point reaches to the yield surface for strain increments:  $\Delta\epsilon_{xx} = 0.0009 \beta$ ,  $\Delta\epsilon_{yy} = 0.0009 \beta$ ,  $\Delta\gamma_{xy} = \Delta\gamma_{zz} = \Delta\gamma_{xz} = \Delta\gamma_{yz} = 0$ . [12]

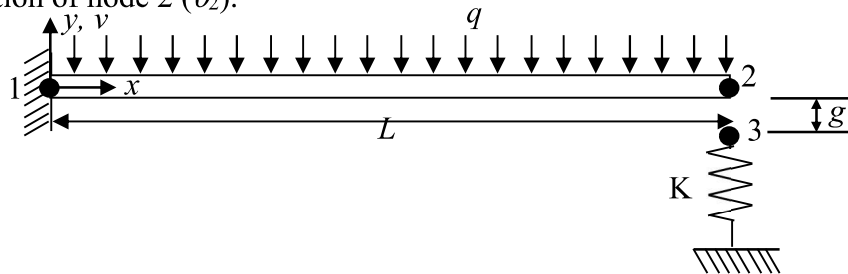
**Q. 4:** Derive the expressions for first ( $I_1$ ) and second ( $I_2$ ) invariants of Right Cauchy Green deformation tensor in terms of Green Lagrange Strain tensor components. For incompressible material ( $I_3=1$ ) with  $E_{YY}=E_{ZZ}$ , express  $E_{YY}$  and  $E_{ZZ}$  in terms of  $E_{XX}$  if  $E_{XY} = E_{YZ} = E_{ZX} = 0$ . [10]

**Q. 5:** Perform one iteration for the solution of the truss member as shown ( $EA = 100$  N,  $L = 1$  m,  $P = 10$  N,  $q = 0$ ). Model the truss using one two-noded truss element considering Finite Deformation. The initial guess is given by  $\{u_1 \ u_2\}^T = \{0.0 \ 0.1\}^T$ . [20]

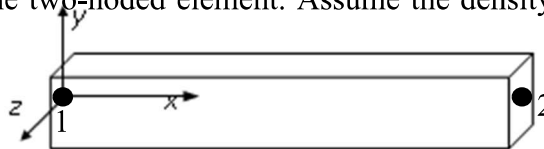


You may note that due to boundary conditions:  $\Delta u_1 = 0$ .

**Q. 6:** For the cantilever beam as shown ( $EI = 1$  N m<sup>2</sup>,  $L = 1$  m,  $q = 0.16$  N/m,  $K = 12$  N/m,  $g = 0.01$  m). Model the beam using one Euler-Bernoulli beam element and find displacements of nodes 2 ( $v_2$ ) and 3 ( $v_3$ ) and rotation of node 2 ( $\theta_2$ ). [20]



**Q. 7:** Derive the mass matrix of a two-noded frame element with the displacements:  $u(x, y, t) = u_0(x, t) - y\theta_z(x, t)$ ;  $v(x, y, t) = v(x, t)$ .  $\theta_z$  is an independent variable. Interpolate  $u_0$ ,  $v$  and  $\theta_z$  using shape functions for the two-noded element. Assume the density and cross-section constant within the element. [20]



**Q. 8:** For a 4-noded isoparametric Mindlin plate bending reduced integration element with nodal coordinates as:  $(x_1, y_1) = (0, 0)$ ;  $(x_2, y_2) = (1, 0)$ ;  $(x_3, y_3) = (1, 1)$ ;  $(x_4, y_4) = (0, 1)$ , find the hourglass stabilization matrix corresponding to transverse displacement  $w$ . You can leave your answer in terms of stabilization constant  $c_1$ . [10]

**Q. 9:** Set-up the element level governing equation for the solution of nonlinear differential equation:

$-\frac{d^2u}{dx^2} + \left(\frac{du}{dx}\right)^2 - 4 = 0$ . Use two-noded element for the interpolation of  $u$  and take element length as

$l$ . In the weak form, do the integration by parts only for the first term involving second derivative of  $u$ .  
[20]