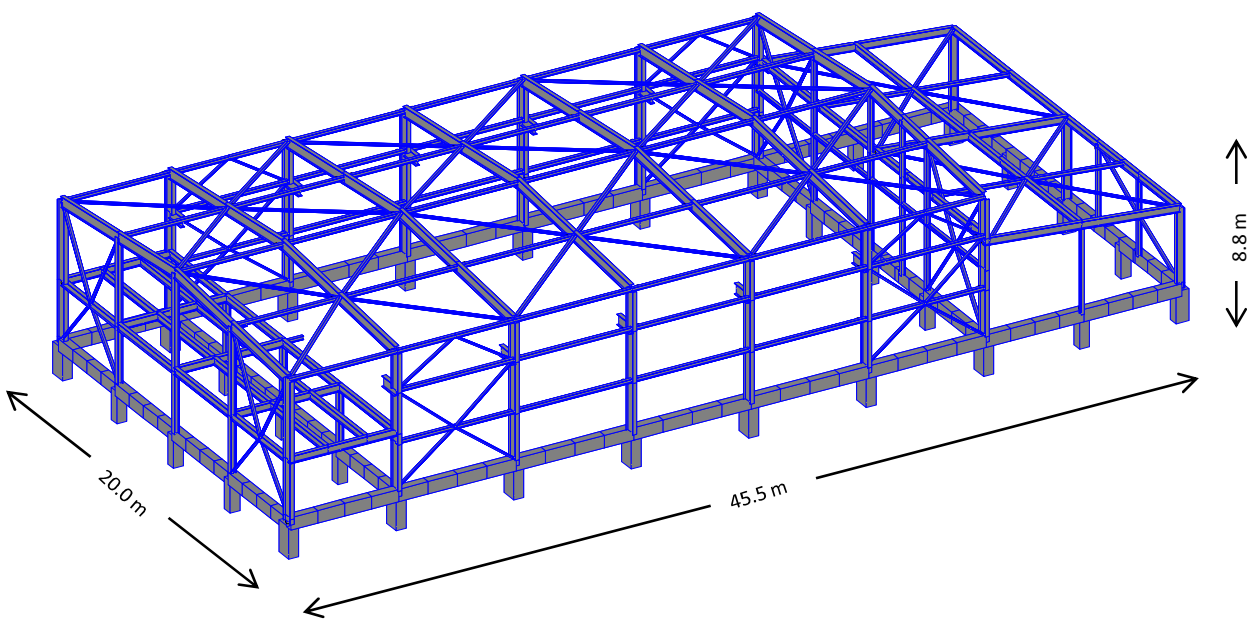
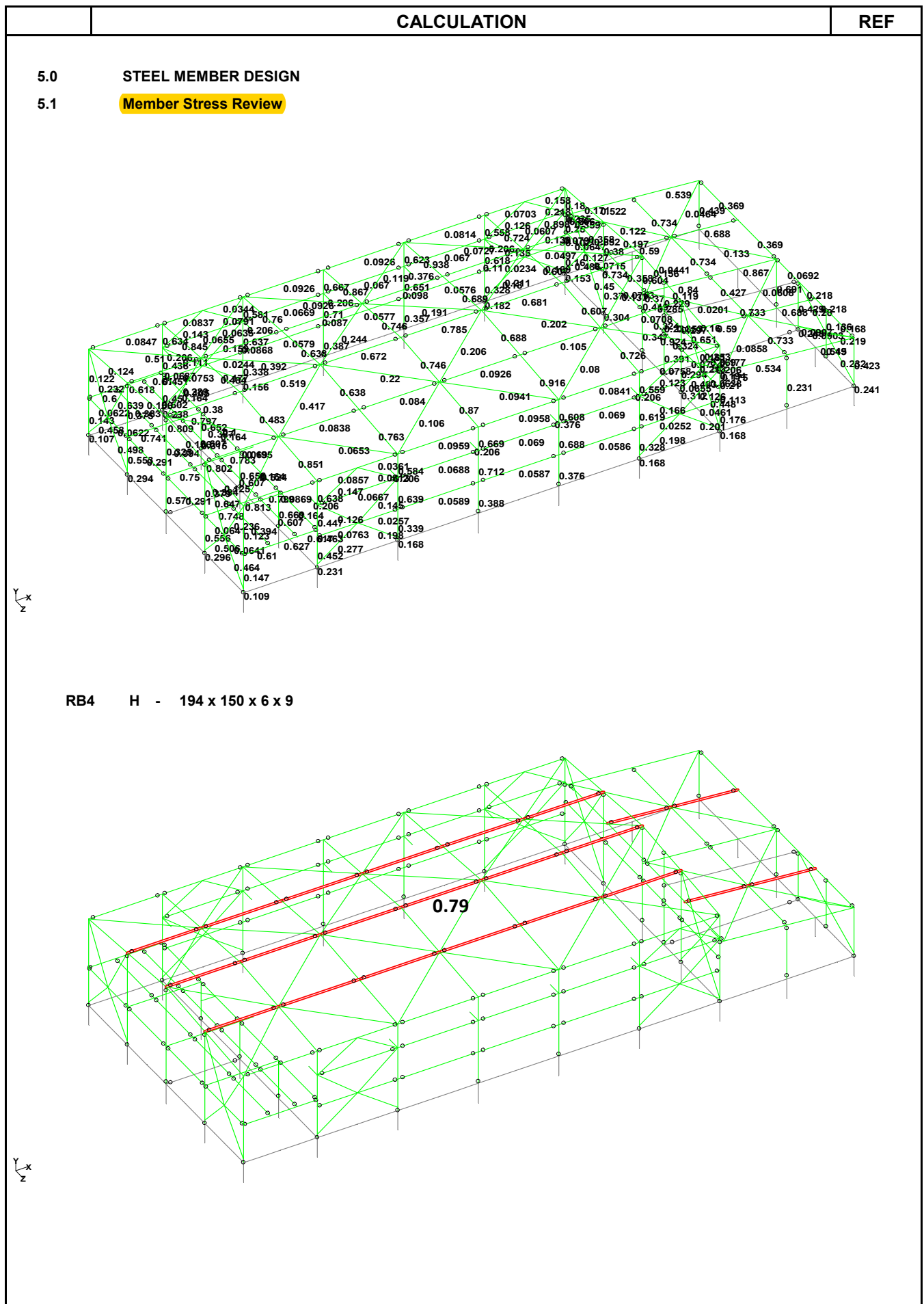


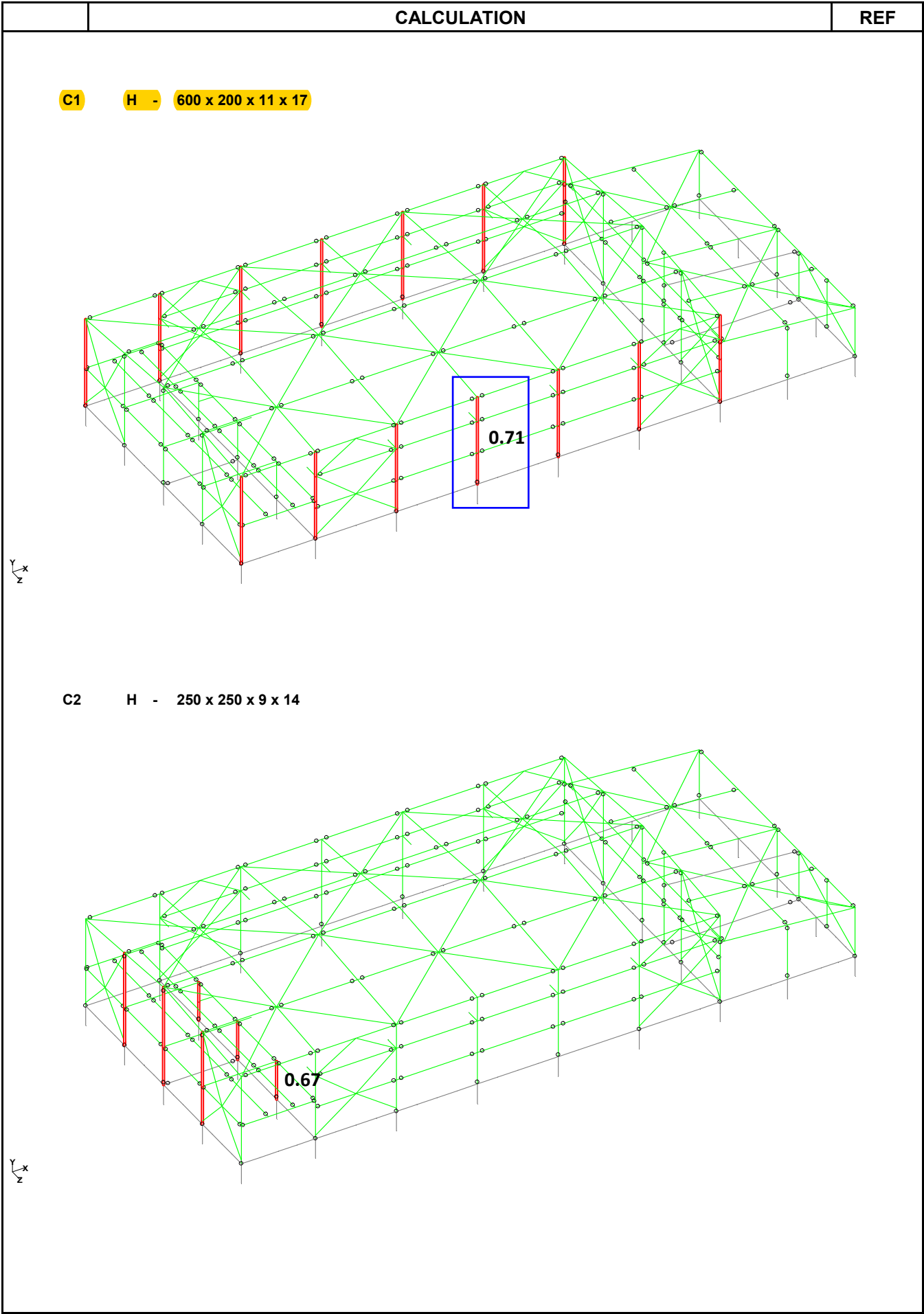
KALSELTENG 2 CFSP(2x100MW) - Workshop and Warehouse

| | CALCULATION | REF |
|-------|---|-----|
| 4.0 | FRAME ANALYSIS | |
| 4.1 | Modeling Geometry | |
| 4.1.1 | Frame Analysis Modeling Description | |
| | (1) Program : STAAD Pro V8i | |
| | (2) Building Name : Workshop & Warehouse | |
| | (3) Structure : Reinforced Concrete & Steel Structure | |
| | (4) Lateral Load Resisting System | |
| | Transverse : Ordinary reinforced concrete moment frame | |
| | Longitudinal : Ordinary reinforced concrete moment frame | |
| | (5) Building Size | |
| | Building Width : 20.0 m | |
| | Building Length : 45.5 m | |
| | Building Height : 8.80 m | |
| |  | |





KALSEL TENG 2 CFSP(2x100MW) - Workshop and Warehouse

| CALCULATION | | | | | | REF |
|-----------------|-------------|-------------------------|---------------|------------------|--------------|--------|
| Floor | Member Name | Section | Member Number | Load Combination | Stress Ratio | Remark |
| Roof Floor | RB4 | H - 194 x 150 x 6 x 9 | 402 | 103 | 0.79 | O.K. |
| | RG4 | H - 194 x 150 x 6 x 9 | 333 | 103 | 0.16 | O.K. |
| | RB8 | H - 400 x 200 x 8 x 13 | 233 | 103 | 0.73 | O.K. |
| | RG8 | H - 400 x 200 x 8 x 13 | 225 | 103 | 0.87 | O.K. |
| | RG11 | H - 600 x 200 x 11 x 17 | 342 | 103 | 0.94 | O.K. |
| Mezzanine Floor | MB8 | H - 400 x 200 x 8 x 13 | 167 | 102 | 0.61 | O.K. |
| | MG8 | H - 400 x 200 x 8 x 13 | 178 | 102 | 0.81 | O.K. |
| Crane Runway | BG1 | H - 194 x 150 x 6 x 9 | 281 | 119 | 0.07 | O.K. |
| | BR1 | H - 600 x 200 x 11 x 17 | 277 | 102 | 0.38 | O.K. |
| | WG1 | H - 194 x 150 x 6 x 9 | 191 | 103 | 0.32 | O.K. |
| | CG4 | H - 194 x 150 x 6 x 9 | 107 | 102 | 0.39 | O.K. |
| Column | C1 | H - 600 x 200 x 11 x 17 | 206 | 103 | 0.71 | O.K. |
| | C2 | H - 250 x 250 x 9 x 14 | 110 | 102 | 0.67 | O.K. |
| | C3 | H - 400 x 200 x 8 x 13 | 128 | 103 | 0.69 | O.K. |
| | C4 | H - 200 x 200 x 8 x 12 | 317 | 103 | 0.60 | O.K. |
| | C5 | H - 194 x 150 x 6 x 9 | 129 | 108 | 0.43 | O.K. |
| Brace | HBR1 | 2Ls - 100 x 100 x 10 | 358 | 103 | 0.92 | O.K. |
| | HBR2 | 2Ls - 100 x 100 x 10 | 223 | 118 | 0.13 | O.K. |
| | VBR1 | CT - 175 x 175 x 7 x 11 | 291 | 103 | 0.65 | O.K. |





KALSELTENG 2 CFSP(2x100MW) - Workshop and Warehouse

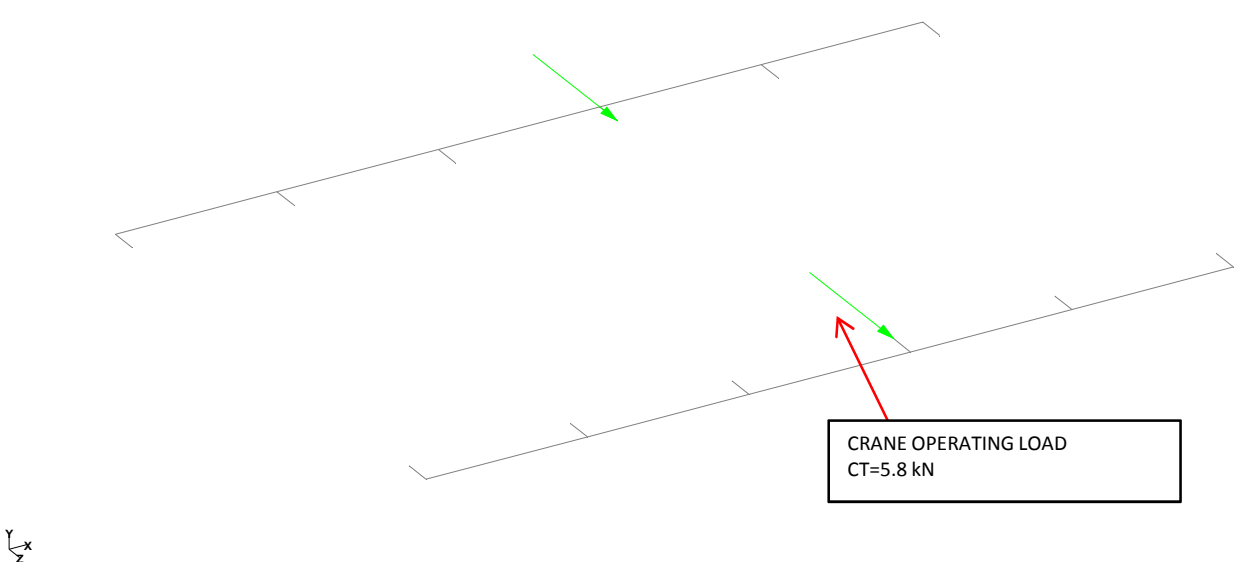
| CALCULATION | | | | | | | | | | REF |
|---|--|--|--|--|--|--|--|--|--|-----|
| 5.0 STEEL MEMBER DESIGN | | | | | | | | | | |
| 5.2 Design of Member | | | | | | | | | | |
| 5.2.1 C1 | | | | | | | | | | |
| ----- START OF DESIGN OUTPUT OF MEMBER 206 ----- | | | | | | | | | | |
| MEMBER NO: 206 CRITICAL RATIO: 0.712(PASS) LOAD: 103 | | | | | | | | | | |
| LOCATION (ft): 0.00 CONDITION: Eq. H1-1b | | | | | | | | | | |
| SECTION: ST H600X200X11 (JAPANESE SECTIONS) | | | | | | | | | | |
| UNIT: KIP FEET | | | | | | | | | | |
| STRENGTH CHECKS: | | | | | | | | | | |
| CRITICAL RATIO: 0.712(PASS) LOAD CASE: 103 LOCATION (ft): 0.00 CONDITION: Eq. H1-1b | | | | | | | | | | |
| DESIGN FORCES: Fx: 42.27(C) Fy: 9.64 Fz: -0.03 | | | | | | | | | | |
| Mx: 2.15E-04 My: 1.23E-01 Mz: 1.83E+02 | | | | | | | | | | |
| SECTION PROPERTIES: AZZ: 7.027 AYY: 10.230 CW: 7182.915 | | | | | | | | | | |
| SZZ: 153.780 SYY: 13.852 | | | | | | | | | | |
| IZZ: 1816.297 IYY: 54.537 | | | | | | | | | | |
| MATERIAL PROPERTIES: FYLD: 34.084 FU: 58.000 | | | | | | | | | | |
| ACTUAL MEMBER LENGTH(ft): 9.514 | | | | | | | | | | |
| PARAMETERS: KZ: 1.500 KY: 1.500 NSF: 1.000 SLF: 1.000 CSP: 1.000 | | | | | | | | | | |
| SLENDERNESS: ACTUAL SLENDERNESS RATIO: 104.778 LOAD: 128 LOC.(ft): 0.000 | | | | | | | | | | |
| ALLOWABLE SLENDERNESS RATIO: 200.000 | | | | | | | | | | |
| <div><div>SECTION CLASS: FLANGE: I-I: I-Ip: I-Ir:</div><div>WEB:</div><div>COMPRESSION: Non-Slender 5.882 N/A 16.540</div><div>Slender 51.455 N/A 44.008</div><div>FLEXURE: Compact 5.882 11.223 29.535</div><div>Compact 51.455 111.053 168.352</div></div> <div><div>Flanges of rolled I-shaped sections, plates projecting from rolled I-shaped sections, outstanding legs of pairs of angles connected with continuous contact, flanges of channels, and flanges of tees</div><div>b/t</div><div>$0.56 \sqrt{\frac{E}{F_y}}$</div><div></div></div> <div><div>Webs of doubly symmetric rolled and built-up I-shaped sections and channels</div><div>h/tw</div><div>$1.49 \sqrt{\frac{E}{F_y}}$</div><div></div></div> | | | | | | | | | | |
| TENSION: FORCE: CAPACITY: RATIO: CRITERIA: LOAD CASE: LOCATION(ft): | | | | | | | | | | |
| YIELDING: 0.000 416.630 0.000 Eq. D2-1 101 0.000 | | | | | | | | | | |
| RUPTURE: 0.000 591.993 0.000 Eq. D2-2 101 0.000 | | | | | | | | | | |
| COMPRESSION: FORCE: CAPACITY: RATIO: CRITERIA: LOAD CASE: LOCATION(ft): | | | | | | | | | | |
| MAJOR: 43.922 357.789 0.123 Eq. E7-1 103 9.514 | | | | | | | | | | |
| MINOR: 43.922 244.324 0.180 Eq. E7-1 103 9.514 | | | | | | | | | | |
| INTERMEDIATE: Ag: KL/r: Fcr: Fe: Pn: | | | | | | | | | | |
| MAJOR: 19.723 50.086 29.270 116.979 597.507 | | | | | | | | | | |
| MINOR: 20.414 104.778 19.988 26.730 408.021 | | | | | | | | | | |
| FLEX TOR BUCK: FORCE: CAPACITY: RATIO: CRITERIA: LOAD CASE: LOCATION(ft): | | | | | | | | | | |
| 43.922 351.644 0.125 Eq. E7-1 103 9.514 | | | | | | | | | | |
| INTERMEDIATE: Ag: Fcr: Pn: | | | | | | | | | | |
| | | | | | | | | | | |

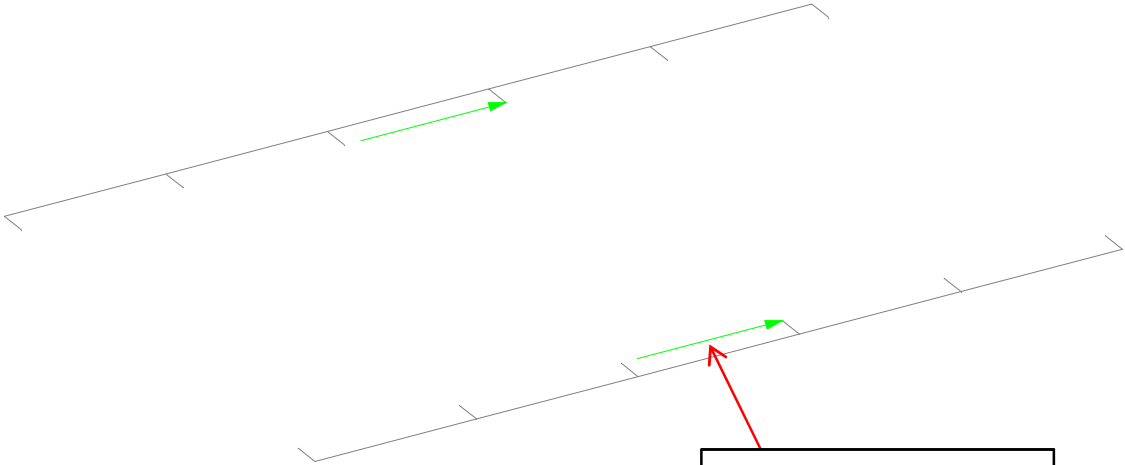
KALSEL TENG 2 CFSP(2x100MW) - Workshop and Warehouse

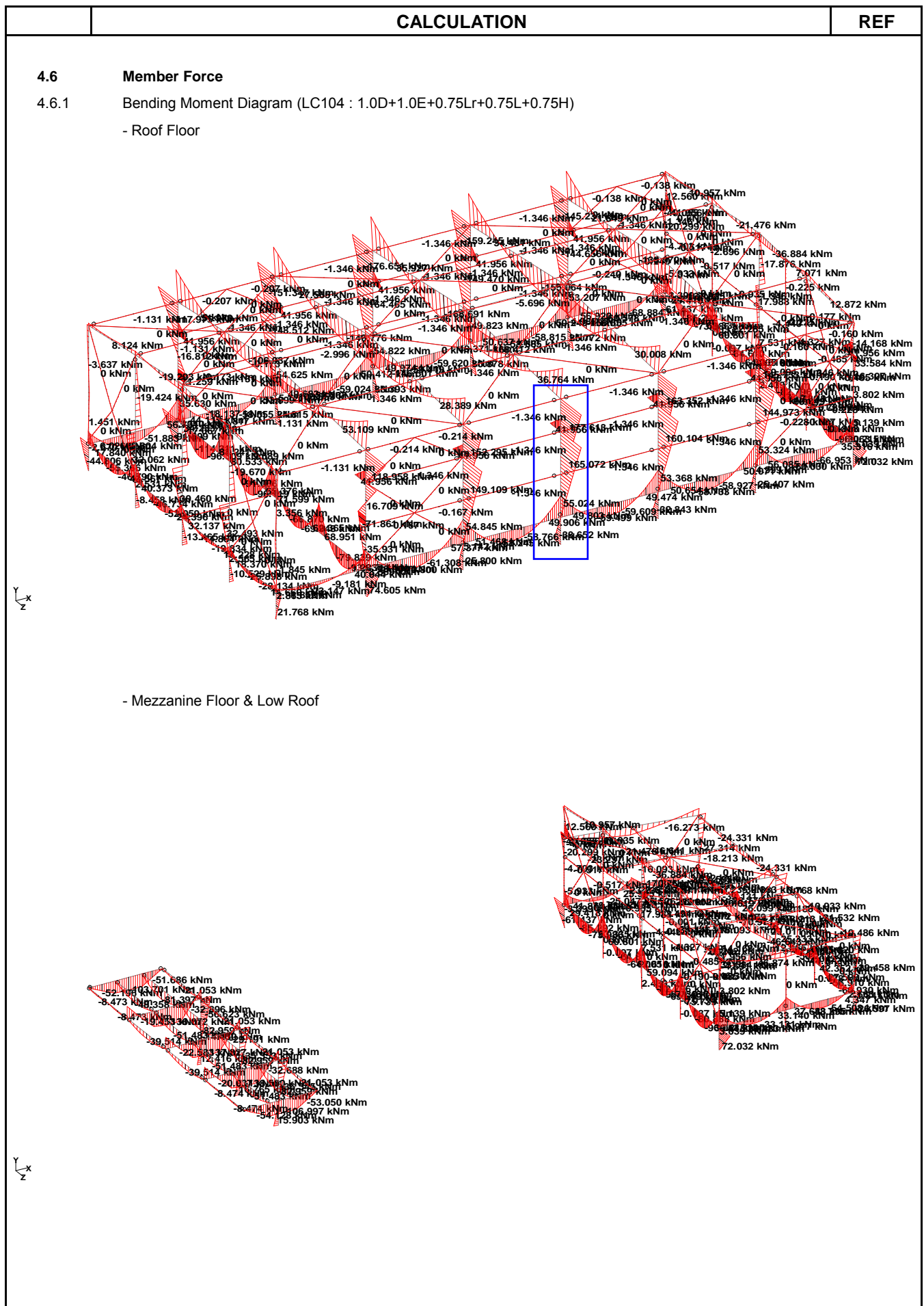
| | CALCULATION | | | | | | | REF |
|--|-------------|--------|---------|--|--|--|--|-----|
| | 19.792 | 28.767 | 587.245 | | | | | |
| <p>SHEAR: FORCE: CAPACITY: RATIO: CRITERIA: LOAD CASE: LOCATION(ft):</p> <p>MAJOR(VZ): 0.047 86.044 0.001 Eq. G2-1 106 0.000</p> <p>MINOR(VY): 9.643 139.471 0.069 Eq. G2-1 103 0.000</p> <p>INTERMEDIATE: Aw: Cv: Kv: h/tw: Vn:</p> <p>MAJOR(VZ): 7.027 1.000 1.200 5.882 143.694</p> <p>MINOR(VY): 10.230 1.000 0.000 51.455 209.207</p> <p>UNIT: KIP FEET</p> <p>YIELDING: FORCE: CAPACITY: RATIO: CRITERIA: LOAD CASE: LOCATION(ft):</p> <p>MAJOR: -1.83E+02 3.01E+02 0.610 Eq. F2-1 103 0.000</p> <p>MINOR: -3.51E-01 3.72E+01 0.009 Eq. F6-1 106 9.514</p> <p>INTERMEDIATE: Mnr: My: Cb:</p> <p>MAJOR: 5.03E+02 0.00E+00 1.000</p> <p>MINOR: 6.20E+01 0.00E+00 1.000</p> <p>UNIT: KIP FEET</p> <p>LAT TOR BUCK: FORCE: CAPACITY: RATIO: CRITERIA: LOAD CASE: LOCATION(ft):</p> <p>MAJOR: -1.83E+02 2.81E+02 0.653 Eq. F2-2 103 0.000</p> <p>INTERMEDIATE: Mn: Me: Cb: Lp: Lr: Lb:</p> <p>MAJOR: 4.70E+02 0.00E+00 1.000 7.080 21.587 9.514</p> <p>UNIT: KIP FEET</p> <p>INTERACTION: RATIO: CRITERIA: LOAD CASE: LOCATION(ft):</p> <p>FLEXURE COMP: 0.160 Eq. H1-1b 108 6.343</p> <p>FLEXURE TENS: 0.656 Eq. H1-1b 103 0.000</p> <p>INTERMEDIATE: Mcx: Mcy: Mrx: Mr: Pc: Pr:</p> <p>FLEXURE COMP: 2.81E+02 3.72E+01 -3.02E+01 -1.23E-02 244.324 25.370</p> <p>FLEXURE TENS: 2.81E+02 3.72E+01 -1.83E+02 1.23E-01 416.630 0.000</p> <p>UNIT: KIP FEET</p> <p>INTERACTION: RATIO: CRITERIA: LOAD CASE: LOCATION(ft):</p> <p>IN PLANE FLEX: 0.712 Eq. H1-1b 103 0.000</p> <p>OUT PLANE FLEX: 0.670 Eq. H1-2 103 0.000</p> <p>INTERMEDIATE: Pc: Pr: Mc: Mr:</p> <p>IN PLANE FLEX: 3.58E+02 4.23E+01 281.195 -183.481</p> <p>OUT PLANE FLEX: 2.44E+02 4.23E+01 281.195 -183.481</p> <p>----- END OF DESIGN OUTPUT OF MEMBER 206 -----</p> | | | | | | | | |
| <div>Chapter H. Design of Members for Combined Forces and Torsion</div> <div>H1. Doubly and Signly Symmetric Members Subject to Flexure and Compression</div> | | | | | | | | |

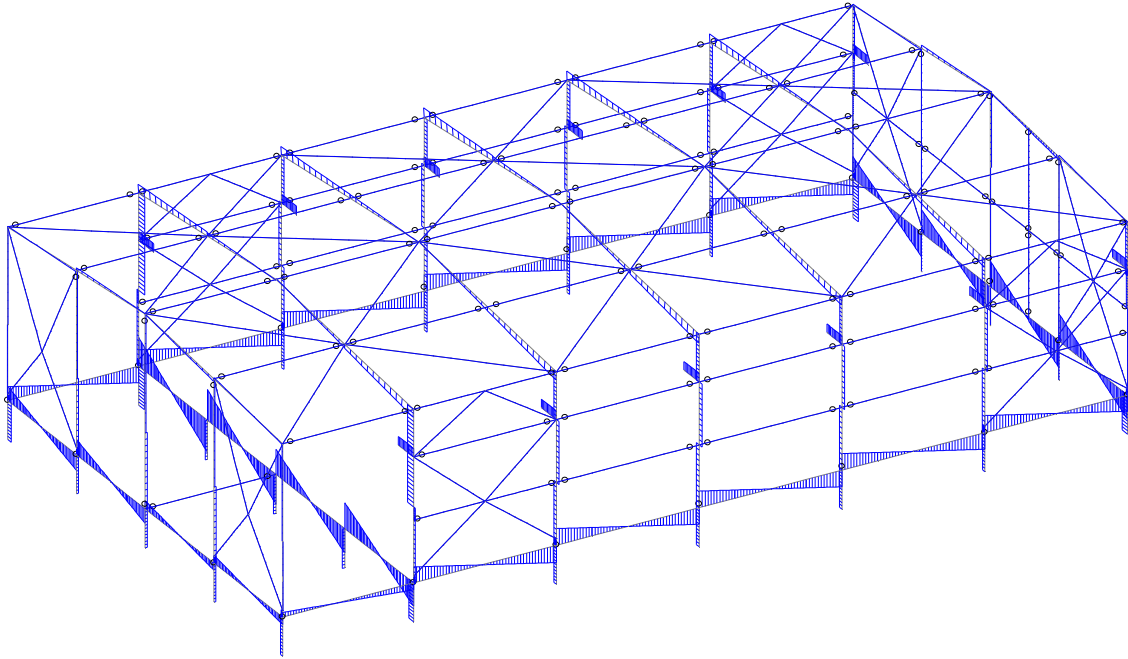
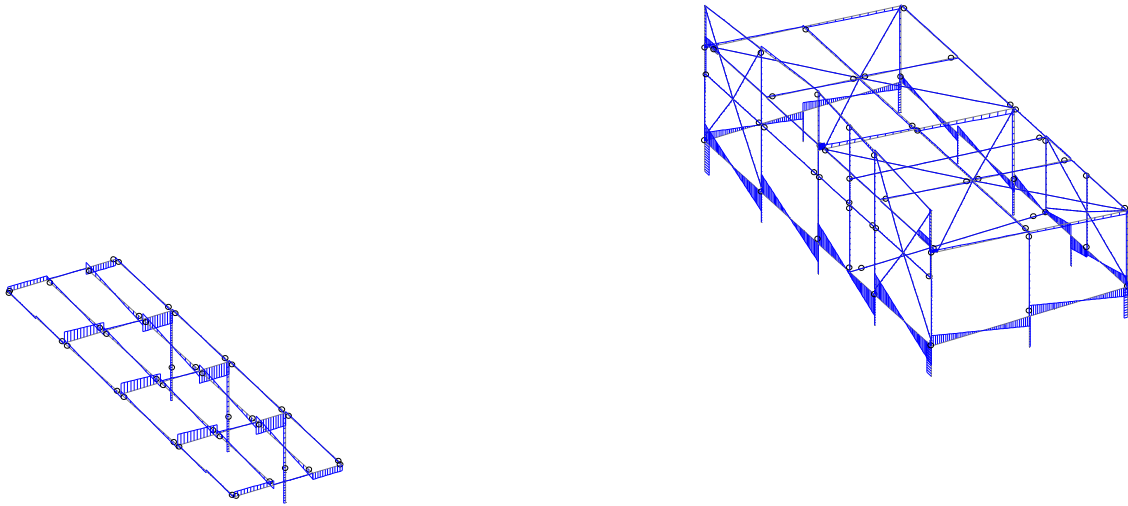
| NO. | CALCULATION | | | | | | | | | | | | | | | | REF |
|--|-------------|------|------|------|-------|------|-------|------|------|------|------|------|---------|------|------|------|--------|
| 3.7.2 LOAD COMBINATIONS | | | | | | | | | | | | | | | | | |
| 1) Load Combinations For Steel Member Design, Deflection, Soil bearing and Stability Check | | | | | | | | | | | | | | | | | |
| Load Combination | Dead | | Live | | Crane | | | | Wind | | | | Seismic | | | | Remark |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | |
| | D | E | Lr | L | Cd | Cv | Ct | Cl | Wx+ | Wx- | Wz+ | Wz- | Ex+ | Ex- | Ez+ | Ez- | |
| LC #101 | 1.00 | 1.00 | | | | | | | | | | | | | | | |
| LC #102 | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | 1.00 | | | | | | | | | |
| LC #103 | 1.00 | 1.00 | 1.00 | | | 1.00 | 1.00 | 1.00 | | | | | | | | | |
| LC #104 | 1.00 | 1.00 | 0.75 | 0.75 | | 1.00 | 1.00 | 1.00 | | | | | | | | | |
| LC #105 | 1.00 | 1.00 | | | | 1.00 | | | 0.60 | | | | | | | | |
| LC #106 | 1.00 | 1.00 | | | | 1.00 | | | | 0.60 | | | | | | | |
| LC #107 | 1.00 | 1.00 | | | | 1.00 | | | | | 0.60 | | | | | | |
| LC #108 | 1.00 | 1.00 | | | | 1.00 | | | | | | 0.60 | | | | | |
| LC #109 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | 0.30 | | | | | | | | |
| LC #110 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | | 0.30 | | | | | | | |
| LC #111 | 1.00 | 1.00 | | | | 1.00 | 1.00 | | | | 0.30 | | | | | | |
| LC #112 | 1.00 | 1.00 | | | | 1.00 | -1.00 | | | | | 0.30 | | | | | |
| LC #113 | 1.00 | 1.00 | | | 1.00 | | | | | | | | 0.70 | | 0.21 | | |
| LC #114 | 1.00 | 1.00 | | | 1.00 | | | | | | | | | 0.70 | | 0.21 | |
| LC #115 | 1.00 | 1.00 | | | 1.00 | | | | | | | | 0.21 | | 0.70 | | |
| LC #116 | 1.00 | 1.00 | | | 1.00 | | | | | | | | | 0.21 | | 0.70 | |
| LC #117 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | | | 0.45 | | | | | | | | |
| LC #118 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | | | | 0.45 | | | | | | | |
| LC #119 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | | | | | 0.45 | | | | | | |
| LC #120 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | | | | | | 0.45 | | | | | |
| LC #121 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | 0.75 | | 0.23 | | | | | | | | |
| LC #122 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | 0.75 | | | 0.23 | | | | | | | |
| LC #123 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | 0.75 | | | | 0.23 | | | | | | |
| LC #124 | 1.00 | 1.00 | 0.75 | 0.75 | | 0.75 | -0.75 | | | | | 0.23 | | | | | |
| LC #125 | 1.00 | 1.00 | | 0.75 | 0.75 | | | | | | | | 0.53 | | 0.16 | | |
| LC #126 | 1.00 | 1.00 | | 0.75 | 0.75 | | | | | | | | | 0.53 | | 0.16 | |
| LC #127 | 1.00 | 1.00 | | 0.75 | 0.75 | | | | | | | | 0.16 | | 0.53 | | |
| LC #128 | 1.00 | 1.00 | | 0.75 | 0.75 | | | | | | | | | 0.16 | | 0.53 | |
| LC #129 | 0.60 | 0.60 | | | | | | | 0.60 | | | | | | | | |
| LC #130 | 0.60 | 0.60 | | | | | | | | 0.60 | | | | | | | |
| LC #131 | 0.60 | 0.60 | | | | | | | | | 0.60 | | | | | | |
| LC #132 | 0.60 | 0.60 | | | | | | | | | | 0.60 | | | | | |
| LC #133 | 0.60 | 0.60 | | | | | | | | | | | 0.70 | | 0.21 | | |
| LC #134 | 0.60 | 0.60 | | | | | | | | | | | | 0.70 | | 0.21 | |
| LC #135 | 0.60 | 0.60 | | | | | | | | | | | 0.21 | | 0.70 | | |
| LC #136 | 0.60 | 0.60 | | | | | | | | | | | | 0.21 | | 0.70 | |

| | CALCULATION | REF |
|-------|--|-----|
| 4.4.6 | <div>Crane Operating Vertical Load</div> <div><p>CRANE OPERATING LOAD CV=76 kN</p></div> | |

| | CALCULATION | REF |
|-------|--|-----|
| 4.4.7 | <div>Crane Operating Lateral Load</div> <div></div> | |

| | CALCULATION | REF |
|-------|--|-----|
| 4.4.8 | <div>Crane Operating Longitudinal Load</div> <div><p>CRANE OPERATING LOAD CL= 7.7 kN</p></div> | |



| | CALCULATION | REF |
|-------|--|-----|
| 4.6.2 | <div>Shear Force Diagram (LC104 : 1.0D+1.0E+0.75Lr+0.75L+0.75H)</div> <div>- Roof Floor</div> <div></div> <div>- Mezzanine Floor & Low Roof</div> <div></div> | |

