DESIGN, CONSTRUCTION, AND PERFORMANCE TESTING OF A LANDSCAPE IRRIGATION RUNOFF MITIGATION SYSTEM

A Thesis

by

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Submitted to the Office of Graduate and Professional Studies of Texas A&M University in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE.

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ABSTRACT

The study of water-saving technology is critically important issue due to urban population growth, drought, and decreasing potable water supplies in Texas and throughout many parts of the world. Because current water supplies are not expected to meet water demand in the coming decades, this could have serious impacts on families, industrial growth, and economic stability. At the same time, water is wasted every year by inefficient or improper landscape irrigation practices. After a thorough research on similar products available in market today, it was found that no products exist with the function of managing lawn/landscape irrigation based on the detection of runoff. Thus, designing a device which could mitigate landscape runoff could potentially 1) offer greater landscape irrigation efficiency and water conservation, 2) improve water quality of streams and lakes, and 3) contribute to efforts aimed at addressing the future water crisis.

This research investigated a Landscape Irrigation Runoff Mitigation System (LIRMS) for minimizing irrigation water losses from residential or commercial landscapes. Four types of irrigation runoff sensors were designed and manufactured firstly. A central control module for receiving signals from sensors and controlling several irrigation valves at the same time was also designed. Afterwards, the prototypes were installed in the field and hardwired with the central control module

along with two control plots with no runoff sensors installed. The different types were evaluated based on their performance characteristics including the ability of each prototype to work reliably over an extended period of time and the runoff reduction rate.

A web was designed so that irrigation data could be accessed online. Also, a wireless communication module and an autonomous energy system were designed and tested to allow the wireless communication between the irrigation runoff sensor and the control unit as well as reducing energy consumption.

The Landscape Irrigation Runoff Mitigation System (LIRMS) equipped with the cubic float prototype/conductivity prototype showed the great capability of water conservation, leading to a runoff reduction rate of 40% - 50%. Further studies should focus on advancing the wireless communication module and conduct more tests under different irrigation strategies for reducing runoff and saving water.

DEDICATION

To Dr. Jorge L. Alvarado for his inspiration and support

To my parents, for all of their love and support.

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Finally, thanks to Mr. Xiaojian Men and Mrs. Airong Li, my parents, for their love, support and encouragements.

NOMENCLATURE

Variables C Specific Heat R Irradiance G Ground Soil Heat Flux Density ρ Pressure er Resistance Q Runoff Flow Rate N Rotational Speed Diameter D **Greek symbols** Rate that Saturation Specific Humidity Changes With Air Δ Temperature Change Psychrometric Constant γ **Subscripts** Net n Air a Surface S

p Constant Pressure

Acronyms

LIRMS Landscape Irrigation Runoff Mitigation System

SS Suspended Solids

VSS Volatile Suspended Solids

COD Chemical Oxygen Demand

BOD Biochemical Oxygen Demand

PAH Polycyclic Aromatic Hydrocarbons

DU Distribution Uniformity

ET Controller Evapotranspiration based Controller

SMS Soil Moisture Sensor

VWC Volume Water Content

GPM Gallons per Minute

RPM Rounds per Minute

ABS Acrylonitrile Butadiene Styrene

PVC Polyvinyl Chloride

PS Polystyrene

PCB Printed Circuit Board

SD Secure Digital

EIT Effective Irrigation Time

WT Wait Time

TIT Total Irrigation Time

IT Irrigation Time

WIF Weekly Irrigation Frequency

SI Start of the irrigation

RDT Runoff Detection Time

RET Runoff Existing Time

TABLE OF CONTENTS

| ABSTRACT |
|--|
| DEDICATION |
| ACKNOWLEDGEMENTS |
| NOMENCLATURE5 |
| TABLE OF CONTENTS |
| LIST OF FIGURES12 |
| LIST OF TABLES |
| 1. INTRODUCTION |
| 1.1 Background27 |
| 1.2 Irrigation Sensors and Strategies |
| 1.3 Motivation for Current Work |
| 2. LITERATURE REVIEW |
| 2.1 Current Circumstances and Effects of the Urban Runoff |
| 2.3 Potential and Commercial Products for Irrigation Control35 |
| 2.2 Water Conservation in Urban Areas |
| 2.4 Current Runoff Mitigation Strategies |
| 3. DESIGN AND FABRICATION OF LANDSCAPE IRRIGATION RUNOFF |
| MITIGATION SYSTEM 44 |

| | 3.1 Aim an | d Objective44 |
|------|-------------|---|
| | 3.2 Landsc | ape Irrigation Runoff Mitigation Sensor Prototype Design, |
| | Fabrication | n and Test45 |
| | 3.2.1 | General Working Requirements of the Landscape Irrigation Runoff |
| | Mitig | ation Sensor45 |
| | 3.2.2 | Materials Selection for Fabricating Prototypes46 |
| | 3.2.3 | Original Designs of the Landscape Irrigation Runoff Mitigation |
| | Senso | or Prototypes47 |
| | 3.2.4 | Fabrication Tools and Procedures |
| | 3.2.5 | Final Designs of the Landscape Irrigation Runoff Mitigation |
| | Senso | or Prototypes61 |
| | 3.3 I/O Con | mmunication and Control Module Design and Fabrication70 |
| | 3.3.1 | General Working Requirements of the I/O Communication and |
| | Contr | ol Module70 |
| | 3.3.2 | General Working Principle of the I/O Communication and Control |
| | Modu | ile70 |
| | 3.3.3 | Printed Circuit Board (PCB) Design and Fabrication72 |
| | 3.3.4 | Autonomous Power Supply Module Design and Fabrication79 |
| | 3.3.5 | Irrigation Results Analysis Website Design81 |
| 4. R | ESULTS A | ND DISCUSSION83 |

| 4.1 Lab Testing | Results of Different Prototypes | 83 |
|-------------------|---|-----|
| 4.1.1 Lat | Testing Results of Paddle Wheel Prototype | 83 |
| 4.1.2 Lab | Testing Results of Cubic Float Prototype | 84 |
| 4.1.3 Lab | Testing Results of Elbow Float Prototype | 86 |
| 4.1.4 Lab | Testing Results of Conductivity Prototype | 87 |
| 4.1.5 Wo | rking Ranges of Different Prototypes | 88 |
| 4.2 Qualitative I | Field Testing Results of Different Prototypes | 88 |
| 4.2.1 Qua | alitative Field Testing Results for April 8 th 2015 | 90 |
| 4.2.2 Qua | alitative Field Testing Results for April 15 th 2015 | 92 |
| 4.2.3 Qua | alitative Field Testing Results for June 16 th 2015 | 100 |
| 4.2.4 Qua | alitative Field Testing Results for June 24 th 2015 | 106 |
| 4.2.5 Qua | alitative Field Testing Results for June 30 th 2015 | 113 |
| 4.2.6 Qua | alitative Field Testing Results for July 11 th 2015 | 120 |
| 4.2.7 Qua | alitative Field Testing Results for July 14 th 2015 | 127 |
| 4.2.8 Qua | alitative Field Testing Results for July 21st 2015 | 134 |
| 4.2.9 Qua | alitative Field Testing Results for Aug 4 th 2015 | 141 |
| 4.2.10 Qua | alitative Field Testing Results for Aug 25 th 2015 | 148 |
| 4.2.11 Qua | alitative Field Testing Result Analysis | 154 |
| 4.3 Quantitative | Field Testing Results of Cubic Float and Conductivity | |
| Prototypes | | 156 |

| 4.3.1 | Quantitative Field Testing Results for Sept 17 th 2015 | 157 |
|--------------|---|-----|
| 4.3.2 | Quantitative Field Testing Results for Sept 19 th 2015 | 160 |
| 4.3.3 | Quantitative Field Testing Results for Sept 21st 2015 | 166 |
| 4.3.4 | Quantitative Field Testing Results for Sept 25 th 2015 | 170 |
| 5. CONCLUSIO | ON | 175 |
| 6. FUTURE WO | ORK | 177 |
| 6.1 Reducti | ion of Effective Irrigation Time | 177 |
| 6.2 Reducti | ion of Irrigation Frequency | 178 |
| 6.3 Self-adj | justable LIRMS for minimum runoff | 178 |
| REFERENCE | | 180 |
| APPENDIX A | | 183 |
| APPENDIX B | | 184 |

LIST OF FIGURES

| Figure 1. Amount of Water Needed and Supplied (Acre-Feet per Year) (Made from |
|--|
| the Data in Texas 2012 State Water Plan) |
| Figure 2. Wasted Irrigation Water Running Off a Residential Texas Landscape and |
| into Storm Sewer Drains |
| Figure 3. Structure of Water Eductor |
| Figure 4. Structure of Eductor Prototype |
| Figure 5. Structure of Infrared Prototype |
| Figure 6. Structure of Paddle Wheel Prototype |
| Figure 7. Structure of Tip Bucket Prototype53 |
| Figure 8. Structure of Float Prototype54 |
| Figure 9. Structure of Conductivity Prototype55 |
| Figure 10. Tools and Machines for Fabricating Runoff Prototypes59 |
| Figure 11. AutoCAD Drawings of the components of the Paddle Wheel prototypes for |
| the laser cutter |
| Figure 12. Structure of the Final Paddle Wheel Prototype |
| Figure 13. Structure of the Final Paddle Wheel Prototype (cutaway view)62 |
| Figure 14. Installed Paddle Wheel Prototype |
| Figure 15. Vertical Float Switch with Two Output Wires |

| Figure 16. Exploded View of the Cubic Float Prototype64 |
|--|
| Figure 17. A Cubic Float Prototype Equipped with an Energy Supply Module65 |
| Figure 18. Section View of the Elbow Float Prototype |
| Figure 19. An Assembled Elbow Float Prototype |
| Figure 20. Section View of the Conductivity Prototype |
| Figure 21. Section View of the Conductivity Prototype (45 Degree Angle)68 |
| Figure 22. Assembled Conductivity Prototype |
| Figure 23. Operating Principle of the I/O Communication and Control Module71 |
| Figure 24. Working Principle of the First Generation of I/O Communication and |
| Control Module |
| Figure 25. Structure of the Transmitter Board on the Irrigation Runoff Sensor Side .73 |
| Figure 26. Structure of the Receiver Board on the I/O Communication and Control |
| Module Side |
| Figure 27. A Fabricated and Assembled Transmitter Board |
| Figure 28. A Fabricated and Assembled Receiver Board |
| Figure 29. Structure of the Current I/O Communication and Control Module PCB 76 |
| Figure 30. A Fabricated and Assembled I/O Communication and Control Module |
| PCB |
| Figure 31. Working Principle of Acting as an Individual Irrigation Controller77 |

| Figure 32. Working Principle of Acting as an Add-On to an Existing Irrigation |
|---|
| Controller |
| Figure 33. Circuit Diagram of the Autonomous Power Supply Module80 |
| Figure 34. A Cubic Float Prototype with an Autonomous Power Supply Module |
| Installed in the Field |
| Figure 35. Webpage for Manually Uploading the Irrigation Results and Data82 |
| Figure 36. Webpage for Drawing the Irrigation Result Charts of Designated Dates 82 |
| Figure 37. Lab Test Results of Runoff Flow Rate and Rotational Speed of Paddle |
| Wheel Prototype84 |
| Figure 38. Lab Test Results of Runoff Flow Rates and Exit Orifice Diameters of |
| Cubic Float Prototype85 |
| Figure 39. Lab Test Results of Runoff Flow Rates and Exit Orifice Diameters of |
| Elbow Float Prototype86 |
| Figure 40. Lab Test Results of Runoff Flow Rates and Exit Orifice Diameters of |
| Conductivity Prototype87 |
| Figure 41. Different Time Variables for a Typical Irrigation Event |
| Figure 42. The Runoff Status of Plot 5 (Cubic Float Prototype) on April 8 th 201590 |
| Figure 43. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on April 8 th |
| 201591 |
| Figure 44. The Runoff Status of Plot 6 (Conductivity Prototype) on April 8 th 201591 |

| Figure 45. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on April |
|---|
| 8 th 2015 |
| Figure 46. The Runoff Status of Plot 2 (Conductivity Prototype) on April 15 th 2015 93 |
| Figure 47. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on April |
| 15 th 201594 |
| Figure 48. The Runoff Status of Plot 4 (Cubic Float Prototype) on April 15 th 201594 |
| Figure 49. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on April |
| 15 th 201595 |
| Figure 50. The Runoff Status of Plot 5 (Cubic Float Prototype) on April 15 th 201595 |
| Figure 51. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on April |
| 15 th 201596 |
| Figure 52. The Runoff Status of Plot 6 (Conductivity Prototype) on April 15 th 2015 96 |
| Figure 53. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on April |
| 15 th 201597 |
| Figure 54. The Runoff Status of Plot 7 (Control) on April 15 th 201597 |
| Figure 55. The Effective Irrigation Time of Plot 7 (Control) on April 15 th 201598 |
| Figure 56. The Runoff Status of Plot 8 (Control) on April 15 th 201598 |
| Figure 57. The Effective Irrigation Time of Plot 8 (Control) on April 15 th 201599 |
| Figure 58. The Runoff Status of Plot 2 (Conductivity Prototype) on June 16 th 2015100 |

| Figure 59. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on June |
|--|
| 16 th 2015 |
| Figure 60. The Runoff Status of Plot 3 (Paddle Wheel Prototype) on June 16 th 2015103 |
| Figure 61. The Effective Irrigation Time of Plot 3 (Paddle Wheel Prototype) on June |
| 16 th 2015 |
| Figure 62. The Runoff Status of Plot 4 (Cubic Float Prototype) on June 16 th 2015102 |
| Figure 63. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on June |
| 16 th 2015 |
| Figure 64. The Runoff Status of Plot 5 (Cubic Float Prototype) on June 16 th 2015103 |
| Figure 65. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on June |
| 16 th 2015 |
| Figure 66. The Runoff Status of Plot 7 (Control) on June 16 th 2015104 |
| Figure 67. The Effective Irrigation Time of Plot 7 (Control) on June 16 th 2015105 |
| Figure 68. The Runoff Status of Plot 8 (Control) on June 16 th 2015105 |
| Figure 69. The Effective Irrigation Time of Plot 8 (Control) on June 16 th 2015106 |
| Figure 70. The Runoff Status of Plot 2 (Conductivity Prototype) on June 24 th 2015107 |
| Figure 71. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on June |
| 24 th 2015 |
| Figure 72. The Runoff Status of Plot 4 (Cubic Float Prototype) on June 24 th 2015108 |

| Figure 73. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on June |
|---|
| 24 th 2015 |
| Figure 74. The Runoff Status of Plot 5 (Cubic Float Prototype) on June 24 th 2015109 |
| Figure 75. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on June |
| 24 th 2015110 |
| Figure 76. The Runoff Status of Plot 6 (Conductivity Prototype) on June 24 th 2015110 |
| Figure 77. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on June |
| 24 th 2015 |
| Figure 78. The Runoff Status of Plot 7 (Control) on June 24 th 2015111 |
| Figure 79. The Effective Irrigation Time of Plot 7 (Control) on June 24 th 2015112 |
| Figure 80. The Runoff Status of Plot 8 (Control) on June 24 th 2015112 |
| Figure 81. The Effective Irrigation Time of Plot 8 (Control) on June 24 th 2015113 |
| Figure 82. The Runoff Status of Plot 2 (Conductivity Prototype) on June 30 th 2015114 |
| Figure 83. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on June |
| 30 th 2015115 |
| Figure 84. The Runoff Status of Plot 4 (Cubic Float Prototype) on June 30 th 2015115 |
| Figure 85. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on June |
| 30 th 2015116 |
| Figure 86. The Runoff Status of Plot 5 (Cubic Float Prototype) on June 30 th 2015, 116 |

| Figure 87. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on June |
|---|
| 30 th 2015117 |
| Figure 88. The Runoff Status of Plot 6 (Conductivity Prototype) on June 30 th 2015117 |
| Figure 89. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on June |
| 30 th 2015 |
| Figure 90. The Runoff Status of Plot 7 (Control) on June 30 th 2015118 |
| Figure 91. The Effective Irrigation Time of Plot 7 (Control) on June 30 th 2015119 |
| Figure 92. The Runoff Status of Plot 8 (Control) on June 30 th 2015119 |
| Figure 93. The Effective Irrigation Time of Plot 8 (Control) on June 30 th 2015120 |
| Figure 94. The Runoff Status of Plot 2 (Conductivity Prototype) on July 11 th 2015 121 |
| Figure 95. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on July |
| 11 th 2015 |
| Figure 96. The Runoff Status of Plot 4 (Cubic Float Prototype) on July 11 th 2015 122 |
| Figure 97. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on July 11 th |
| 2015 |
| Figure 98. The Runoff Status of Plot 5 (Cubic Float Prototype) on July 11 th 2015123 |
| Figure 99. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on July 11 th |
| 2015124 |
| Figure 100. The Runoff Status of Plot 6 (Conductivity Prototype) on July 11 th 2015124 |

| Figure 101. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on July |
|---|
| 11 th 2015 |
| Figure 102. The Runoff Status of Plot 7 (Control) on July 11 th 2015125 |
| Figure 103. The Effective Irrigation Time of Plot 7 (Control) on July 11 th 2015 126 |
| Figure 104. The Runoff Status of Plot 9 (Elbow Float Prototype) on July 11 th 2015126 |
| Figure 105. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on July |
| 11 th 2015 |
| Figure 106. The Runoff Status of Plot 2 (Conductivity Prototype) on July 14 th 2015128 |
| Figure 107. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on July |
| 14 th 2015 |
| Figure 108. The Runoff Status of Plot 4 (Cubic Float Prototype) on July 14 th 2015 129 |
| Figure 109. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on July |
| 14 th 2015 |
| Figure 110. The Runoff Status of Plot 5 (Cubic Float Prototype) on July 14 th 2015 130 |
| Figure 111. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on July |
| 14 th 2015 |
| Figure 112. The Runoff Status of Plot 6 (Conductivity Prototype) on July 14 th 2015131 |
| Figure 113. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on July |
| 14 th 2015 |
| Figure 114. The Runoff Status of Plot 7 (Control) on July 14 th 2015 |

| Figure 115. The Effective Irrigation Time of Plot 7 (Control) on July 14 th 2015 133 |
|--|
| Figure 116. The Runoff Status of Plot 9 (Elbow Float Prototype) on July 14 th 2015133 |
| Figure 117. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on July |
| 14 th 2015 |
| Figure 118. The Runoff Status of Plot 2 (Conductivity Prototype) on July 21st 2015135 |
| Figure 119. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on July |
| 21 st 2015 |
| Figure 120. The Runoff Status of Plot 4 (Cubic Float Prototype) on July 21st 2015.136 |
| Figure 121. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on July |
| 21 st 2015137 |
| Figure 122. The Runoff Status of Plot 5 (Cubic Float Prototype) on July 21st 2015.137 |
| Figure 123. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on July |
| 21 st 2015 |
| Figure 124. The Runoff Status of Plot 6 (Conductivity Prototype) on July 21st 2015138 |
| Figure 125. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on July |
| 21 st 2015 |
| Figure 126. The Runoff Status of Plot 7 (Control) on July 21st 2015139 |
| Figure 127. The Effective Irrigation Time of Plot 7 (Control) on July 21st 2015140 |
| Figure 128. The Runoff Status of Plot 9 (Elbow Float Prototype) on July 21st 2015 140 |

| Figure 129. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on July |
|--|
| 21 st 2015141 |
| Figure 130. The Runoff Status of Plot 2 (Conductivity Prototype) on Aug 4 th 2015 142 |
| Figure 131. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on Aug |
| 4 th 2015143 |
| Figure 132. The Runoff Status of Plot 4 (Cubic Float Prototype) on Aug 4 th 2015143 |
| Figure 133. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on Aug 4 th |
| 2015 |
| Figure 134. The Runoff Status of Plot 5 (Cubic Float Prototype) on Aug 4 th 2015144 |
| Figure 135. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on Aug 4 th |
| 2015145 |
| Figure 136. The Runoff Status of Plot 6 (Conductivity Prototype) on Aug 4 th 2015 145 |
| Figure 137. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on Aug |
| 4 th 2015146 |
| Figure 138. The Runoff Status of Plot 7 (Control) on Aug 4 th 2015146 |
| Figure 139. The Effective Irrigation Time of Plot 7 (Control) on Aug 4 th 2015147 |
| Figure 140. The Runoff Status of Plot 9 (Elbow Float Prototype) on Aug 4 th 2015.147 |
| Figure 141. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on Aug |
| 4 th 2015 |
| Figure 142. The Runoff Status of Plot 2 (Conductivity Prototype) on Aug 25 th 2015149 |

| Figure 143. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on Aug |
|--|
| 25 th 2015 |
| Figure 144. The Runoff Status of Plot 4 (Cubic Float Prototype) on Aug 25 th 2015 150 |
| Figure 145. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on Aug |
| 25 th 2015 |
| Figure 146. The Runoff Status of Plot 6 (Conductivity Prototype) on Aug 25 th 2015151 |
| Figure 147. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on Aug |
| 25 th 2015 |
| Figure 148. The Runoff Status of Plot 7 (Control) on Aug 25 th 2015 |
| Figure 149. The Effective Irrigation Time of Plot 7 (Control) on Aug 25 th 2015 153 |
| Figure 150. The Runoff Status of Plot 8 (Control Plot) on Aug 25 th 2015153 |
| Figure 151. The Effective Irrigation Time of Plot 8 (Control Plot) on Aug 25 th 2015154 |
| Figure 152. Plot 15 (Conductivity Prototype) Irrigation Results on Sept 17 th 2015157 |
| Figure 153. Plot 18 (Control) Irrigation Results on Sept 17 th 2015158 |
| Figure 154. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 17 th 2015 |
| (Scale: 0 to 0.2 L/s) |
| Figure 155. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 17 th 2015 |
| (Scale: 0 to 0.02 L/s) |
| Figure 156. Runoff Flow Rate of Plot 18 (Control) on Sept 17 th 2015159 |

| Figure 157. Plot 15 (Conductivity Prototype) Irrigation Results of the First 15-Min | nute |
|---|--------|
| Test on Sept 19 th 2015 | 161 |
| Figure 158. Plot 18 (Control) Irrigation Results of the First 15-Minute Test on Se | pt |
| 19 th 2015 | 162 |
| Figure 159. Plot 15 (Conductivity Prototype) Irrigation Results of the Second | |
| 15-Minute Test on Sept 19 th 2015 | 162 |
| Figure 160. Plot 18 (Control) Irrigation Results of the Second 15-Minute Test on S | Sept |
| 19 th 2015 | 163 |
| Figure 161. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 19 th 20 | 015163 |
| Figure 162. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 19 th 20 | 015164 |
| Figure 163. Runoff Flow Rate of Plot 18 (Control) on Sept 19 th 2015 | 164 |
| Figure 164. Plot 15 (Conductivity Prototype) Irrigation Results on Sept 21st 2015 | 167 |
| Figure 165. Plot 18 (Control) Irrigation Results on Sept 21 st 2015 | 167 |
| Figure 166. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 21st 20 | 015168 |
| Figure 167. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 21st 20 | 015168 |
| Figure 168. Runoff Flow Rate of Plot 18 (Control) on Sept 21st 2015 | 169 |
| Figure 169. Plot 15 (Conductivity Prototype) Irrigation Results on Sept 25 th 2015 | 171 |
| Figure 170. Plot 18 (Control) Irrigation Results on Sept 25 th 2015 | 171 |
| Figure 171. Runoff Flow Rate of Plot 15 (Cubic Float Prototype) on Sept 25 th 20 | 15172 |
| Figure 172. Runoff Flow Rate of Plot 15 (Cubic Float Prototype) on Sept 25 th 20 | 15172 |

Figure 173. Runoff Flow Rate of Plot 18 (Control) on Sept 25th 2015173

LIST OF TABLES

| Table 1. Types of Irrigation Sensor Controllers under different Irrigation |
|---|
| Specifications (Revised and Organized from Table 1 in [12]) |
| Table 2. Comparison of Different Materials for Runoff Prototypes46 |
| Table 3. Design Decisions of Landscape Irrigation Runoff Mitigation Sensor |
| Prototypes57 |
| Table 4. Comparisons and Applications of Different Tools and Machines61 |
| Table 5. Comparison of Energy Consumptions between the Two Generations of the |
| I/O Communication and Control Module |
| Table 6. Lab Tests Results of the Cubic Float Prototype |
| Table 7. Lab Test Results of the Elbow Float Prototype |
| Table 8. Lab Test Results of the Conductivity Prototype |
| Table 9. Working Ranges of Different Prototypes under Lab Conditions |
| Table 10. Irrigation Specifications of Test on April 8 th 201590 |
| Table 11. Irrigation Specifications of Test on April 15 th 201593 |
| Table 12. Irrigation Specifications of Test on June 16 th 2015100 |
| Table 13. Irrigation Specifications of Test on June 24 th 2015107 |
| Table 14. Irrigation Specifications of Test on June 30 th 2015114 |
| Table 15. Irrigation Specifications of Test on July 11 th 2015 |

| Table 16. Irrigation Specifications of Test on July 14 th 2015 |
|---|
| Table 17. Irrigation Specifications of Test on July 21st 2015 |
| Table 18. Irrigation Specifications of Test on Aug 4 th 2015 |
| Table 19. Irrigation Specifications of Test on Aug 25 th 2015 |
| Table 20. Analysis and Comparison of the Performance of the Irrigation Runoff |
| Sensors during Qualitative Field Testing |
| Table 21. Irrigation Specifications of Test on Sept 17 th 2015 |
| Table 22. Water Usage and Runoff Analysis of Irrigation on Sept 17 th 2015 (TIT).160 |
| Table 23. Irrigation Specifications of Test on Sept 19 th 2015161 |
| Table 24. Water Usage and Runoff Analysis of Irrigation on Sept 19 th 2015165 |
| Table 25. Irrigation Specifications of Test on Sept 21 st 2015166 |
| Table 26. Water Usage and Runoff Analysis of Irrigation on Sept 21st 2015 |
| Table 27. Irrigation Specifications of Test on Sept 25 th 2015 |
| Table 28. Water Usage and Runoff Analysis of Irrigation on Sept 17 th 2015173 |
| Table 29. Changes of Specifications between the Experimental and the Control Plots177 |
| Table 30. Changes of Specifications between the Experimental and the Control Plots178 |
| Table 31. Case Scenario of the LIRMS System with Autonomous Learning Ability179 |

1. INTRODUCTION

1.1 Background

Greater stewardship of municipal water supplies has become critical in Texas, given the anticipated population growth between 2010 and 2060, which could be around 82%. This is likely to place strains on current water supplies in the state [1]. According to the Texas 2012 State Water Plan, water demand is expected to outpace water supplies by the year 2060. The amount of the water needed and supplied is depicted in Figure 1.

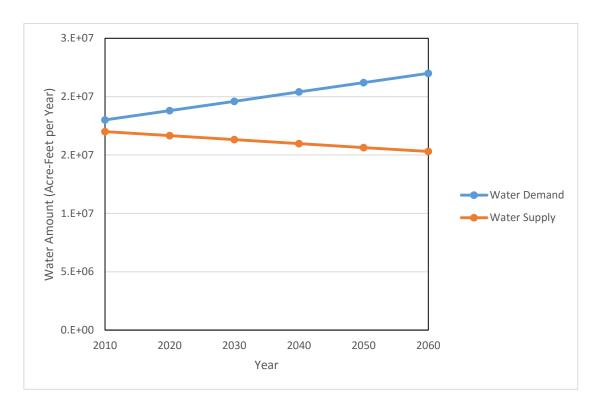


Figure 1. Amount of Water Needed and Supplied (Acre-Feet per Year) (Made from

the Data in Texas 2012 State Water Plan)

Municipal water conservation is a cost-effective means of ensuring water availability for the future. Second only to agricultural uses, urban-municipal uses are the second largest component of water use in Texas, which occupied 27% of water demand in Texas in 2010 [2]. Also, about 30 percent of residential water usage is devoted to outdoors uses, while this number could be as high as 60 percent in Southwest of United States [3]. Many households use much more water than is necessary for irrigating outdoors, which leads to the excess water running into the street, also referred to as 'runoff', shown in Figure 2.



Figure 2. Wasted Irrigation Water Running Off a Residential Texas Landscape and into Storm Sewer Drains

Runoff occurs when the irrigation processes and precipitations add water to the soil at the rate which is faster than the rate of absorption. It could also be affected by the soil and site characteristics [4]. While this is an obvious waste of water, it also is a concern because of the potential for transport of fertilizers and pesticides into storm sewers and eventually surface waters. With the increasing implementation of municipal water restrictions, irrigation events are often limited to only once a week or less. This has resulted in a tendency of homeowners to irrigate excessively on their given watering day, a problem which can be compounded further by poor soil quality.

According to the results of the research done by Dr. Ben Wherley at the Texas A&M Urban Landscape Runoff Field Laboratory, runoff amounts of up to 1/3 of the typical amount of water from irrigation occurred if cycle-soaking was not applied correctly.

Commercial add-on products used to enhance efficiency of irrigation have already appeared in the market. Developed with different working mechanisms, most of these are sold as 'add-on' features to existing irrigation controllers help manage irrigation. However, these add-on items are usually expensive, which narrow their expansion. Also, some of the add-ons, such as rain sensor, simply stops irrigation when raining and could not indeed prevent the excess irrigation of a user.

A sensor which is based on controlling irrigation based on detection of runoff could therefore be a great complement to these add-ons.

1.2 Irrigation Sensors and Strategies

In this study, an irrigation runoff sensor which bases its working principle on runoff has been designed. The irrigation runoff sensor interfaced with a central control unit, could detect the existence of runoff in the field and control the valves which provide water to the sprinklers. If runoff is detected by the sensor, it is able to communicate wirelessly with the central control unit and then the irrigation process would stop for a given period of time before restarting to finish the irrigation cycle. Upon resuming irrigation, the sensor will detect the runoff again and pause if the runoff is detected again. This working/pause schedule will continue until the total expected irrigation time is satisfied. Cycle-soaking is achieved by the working mechanism as a result.

The irrigation runoff sensor is required to be durable, reliable and low-cost. It is designed to be either a basic sensor which is installed at the construction phase or an add-on item for existing irrigation systems in a household or other areas. Since its advanced working principle, it could take place of some of the existing add-ons, such as rain sensors. It may have to be adapted to different types of soil conditions and provide reliable feedbacks of the runoff.

1.3 Motivation for Current Work

The study of water-saving technology is a critically important issue due to urban population growth, drought, and decreasing potable water supplies in Texas and throughout many parts of the world. Because current water supplies are not expected to meet water demand in the coming decades, this could have serious impacts on families, industrial growth, and economic stability. At the same time, water is wasted every year by inefficient or improper landscape irrigation practices. Thus, designing a device which could mitigate landscape runoff could potentially 1) offer greater landscape irrigation efficiency and water conservation, 2) improve water quality of streams and lakes, and 3) contribute to efforts aimed at addressing the future water crisis.

After a thorough research on similar products available in market today, it was found that no products exist with the function of managing lawn/landscape irrigation based on the detection of runoff. Therefore, the study of designing and characterizing a reliable, durable and low cost landscape irrigation runoff mitigation system was undertaken.

2. LITERATURE REVIEW

This section highlights many of the current issues and problems that have led to the need for development of a landscape irrigation runoff mitigation system (LIRMS). The section has been divided into four parts. The first part focuses on current circumstances and effects of the urban runoff. The second part discusses water conservation status in urban areas. In addition, the third part discusses the concepts and examples of commercial irrigation sensors. The fourth part focuses on current runoff mitigation strategies.

2.1 Current Circumstances and Effects of the Urban Runoff

Much research has been done to investigate the effects of urban runoff on the environment. Weibel et al. [5] introduced the study of role of urban land runoff in stream pollution as early as 1962. A residential area with a population of about 240 and a density of 9 persons/acre was chosen in the study. The sample area included family homes, stores, restaurants and other public buildings. It was also partially equipped with grassed or gravel gutters. The study showed the storm runoff increased suspended solids (SS) by 140 percent; volatile suspended solids (VSS) by 44 percent; chemical oxygen demand (COD) by 25 percent; biochemical oxygen demand (BOD) by 6 percent; phosphate by 9 percent; and nitrogen by 11 percent

within stream water bodies. As a result, urban runoff could not be neglected as a factor of pollution.

Gromaire-Mertz et al. [6] conducted research on urban runoff pollution in Paris. Growing population was considered to make urban runoff a major threat to both flow quantity and quality. In their work, a district named "Le Marais" was selected and three major urban runoff types were investigated: runoff from roofs; runoff from streets and runoff from courtyards, public areas and gardens. Their research found that heavy metal concentrations in runoff greatly exceeded level 2 water quality standards in France, especially for the Zn and Pb concentrations, which even exceeded the limits of industrial discharged water. Gromaire-Mertz et al.'s characterization confirmed that urban runoff could directly impact water quality.

A study by Kimbrough et al. [7] investigated pesticide levels in Colorado streams from April 1993 to April 1994. The study compared levels of pesticides in streams within both agricultural and an urban areas of the state. The water samples, which were analyzed for 47 pesticides, showed 30 pesticides were detected in agricultural areas, while 22 pesticides detected in urban areas. The study demonstrated that agricultural and urban areas both contribute to the spread of pesticides in streams. Similar research was conducted by Weston et al. [8]. The research focused on the pyrethroid pesticides carried by the residential runoff to urban streams. From earlier tests of 20 urban streams in California, pyrethroid

pesticides were found exceeding toxicity thresholds and it was believed that this situation was not unique to California only. Also, highest concentration of pyrethroid pesticides were found in drain outfalls from earlier work by Weston et al. and thus storm drains have been assumed to be a major source of the pollution in California streams. Later tests showed all samples collected from the streams contained pyrethroid pesticides and could kill H.azteca, leading to a survival rate between 9 and 70%. The research indicated that the storm runoff is the most significant cause of transporting pyrethroid pesticides to local creeks, while summer irrigation runoff could not be neglected as a source of pollution either.

Hoffman et al. [9] proposed that urban runoff could also result in the presence of polycyclic aromatic hydrocarbons (PAHs) in coastal areas. The author collected urban runoff from four storm drains, each linked to a different type of land use; specifically suburban residential, commercial, heavy industrial, and multilane highway. Collected samples were analyzed for PAH, with the amount of PAH created by a storm calculated by multiplying the concentration of PAH by drain flow rate and time interval. Results of the study showed PAH loading factors were similar between residential and commercial locations, with industrial locations also sharing a similar loading potential as highways. The results showed that the urban runoff was responsible for 71% of the total higher molecular weight of PAHs and 36% of the total PAHs that enter the Narragansett Bay.

2.3 Potential and Commercial Products for Irrigation Control

Commercial smart irrigation controllers have already been developed to conserve water and optimize the irrigation process. The mostly widely recognized smart irrigation controllers are evapotranspiration based controller, rain sensor and soil moisture sensor.

Based on the working mechanism, rain sensors are divided in to water weight, electrical conductivity of water and expansion disks. It was claimed that substantial savings of water could be expected with rain sensors, though no tests or figures have been listed. Bernard Cardenas-Lailhacar et al. [12] conducted experiments concentrating on the performances and potential water consumption savings of expanding disk rain sensor. Two different types of rain sensors, mini-click rain sensor and wireless rain-click rain sensor were selected. In the experiments, the mini-click rain sensors were divided into three groups with different thresholds while there was only one group of wireless rain-click rain sensor. During the experimental period, 62% of the time were rainy days. As a result, the wireless rain-click rain sensor could save up to 44% water, while the mini-click rain sensor with different thresholds could save between 3% and 30% of water.

Another study was conducted by McCready et al. [13] from 2006 to 2007 investigating on the performances and potentials of water conservation of the existing smart irrigation controllers, which includes ET controllers, rain sensors and

SMS controllers. In this study, two different types of ET controllers (the Toro Intelli-Sense and the Rain Bird ET Manager) were used as well as two different types of SMS controllers (the Acclima Digital TDT RS500 and the LawnLogic LL1004). The smart controllers were then set to different thresholds for testing purposes. The experiment groups and their descriptions are listed in Table 1.

Table 1. Types of Irrigation Sensor Controllers under different Irrigation

Specifications (Revised and Organized from Table 1 in [12])

| Sensor | Sensor | Irrigation | | |
|---------------|---------------|------------|--------------------------------|--|
| Controller | Controller | Frequency | Description | |
| Type | Brand | (day/week) | | |
| | Acclima | 2 | Volume Water Content (VWC): 7% | |
| | | 2 | VWC: 10% | |
| SMS | | 2 | VWC: 13% | |
| Controller | | 2 | Individually Controlled | |
| Controller | LawnLogic | 2 | Low setting | |
| | | 2 | Medium setting | |
| | | 2 | High setting | |
| | Rain Bird | | | |
| | ET | 2 | N/A | |
| ET Controller | Manager | | | |
| | Toro Intelli- | 2 | N/A | |
| | Sense | 2 | IV/A | |
| | | 1 | Threshold: 3 mm rainfall | |
| | | 2 | Threshold: 3 mm rainfall | |
| Rain Sensor | Rain Sensor | 7 | Threshold: 3 mm rainfall | |
| | | 1 | Threshold: 6 mm rainfall | |
| | | 2 | Threshold: 6 mm rainfall | |
| | | 7 | Threshold: 6 mm rainfall | |
| | | 2 | Reduced Irrigation | |
| Control | N/A | 2 | No sensor | |
| Control | N/A | 0 | No irrigation | |

In the study, the results showed that the rain sensor could reduce irrigation water consumption by 7% - 30%, while the SMS sensor could reduce by up to 74% and the ET sensor could lead to a 25% - 62% reduction. The investigation proved that irrigation water consumption could be greatly reduced with proper installation and use of the smart irrigation controllers without unacceptable defects to turfgrass qualities.

Although studies by Bernard Cardenas-Lailhacar et al. and McCready et al. proved that both rain sensors, i.e. SMS sensor and ET sensor could contribute to irrigation water conservation, major drawbacks prevent these sensors from further implementation. The rain sensors were characterized by faulty operating conditions [14] due to the presence of debris or disk malfunction. To be more specific, rain sensors could be divided into several different types and each one has its own advantages and disadvantages [15]. One type of rain sensor uses a bucket to collect rain to determine when irrigation cycles must pause. Its operating principle is based on the weight of collected rain. The major drawback of this type of sensor is its ability to be activated by other objects such as stones or leaves which might fall into the bucket. Electrodes are used in other rain sensors. The sensor needs periodical checks and maintenance, which are both tedious and time-consuming. The last type is the one with an expansion disk. However, disk malfunction is not rare in the applications of this type.

The SMS sensor, which is also capable of saving water, also has certain disadvantages that limit its applications. The usefulness of SMS sensor is limited when the landscape has a mixed plants layout with different water needs or root depth [16]. Also, SMS sensor requires precise calibrations and adjustments to adapt it to a specific soil type and its measurement accuracy could be easily affected by salinity, fertilizer content and temperature [17]. Based on the methods to measure soil moisture content, SMS sensor could be divided into four types [18]. The first type uses a tensiometer, a tube with a porous cup as end and vacuum gauge as top, to pull in or eject out water based on the soil moisture content. However, this type has a poor performance in coarse sand and the gauges are easily damaged since it is aboveground. The second type consists of electrical resistance blocks whose resistances could change with different moisture levels. The drawback of this type is the need of a specific meter for measuring the resistance and thus changing the settings. The third type is the neutron probe who uses a radioactive source to measure soil moisture. The fourth type is a Di-electric sensor which could measure the di-electric constant of soil (a characteristic that changes with soil moisture level). The common drawback of these two types is the high cost.

The ET controllers use various methods to collect data and calculate the amount of water needed [19]. The conventional ET method cannot account for unusual weather conditions and the sensor-based method leads to calculation

accuracy problems. The ET method is subject to bias since it relies on weather information obtained through the internet. Lastly, the on-site weather station method can be quite costly.

2.2 Water Conservation in Urban Areas

With declining water quality and potable water supplies occurring throughout much of the world, water conservation has become highly important within the last few decades and is likely to remain important in the future. Based on the 2012 Texas Water Plan [1], water demand is predicted to increase by 22 percent over the next 50 years. Moreover, ground water supplies are expected to decrease by 30 percent, though the surface waters will increase by 6 percent. As a result, water is likely to be in short supply, making water conservation circumstance high priority throughout the state. Bruce K. Ferguson [10] conducted research focusing on possible solutions to achieving water conservation in urban areas. Based on his findings, it is estimated that between 10 to 50 inches of water is used for managing lawns in the United States annually. Also, lawn irrigation use was greatest in arid western states. While some water conservation techniques have already been adopted in agriculture, these same techniques cannot be easily adapted for use in urban areas due to the differences between the two area uses. Three different aspects impacting water conservation have been identified by Ferguson: urban landscape design, irrigation hardware, and landscape maintenance. For the urban design, adapted plants should be used that fit the moisture requirements of the geographic location in order to minimize water use. Also, runoff from rainfall and irrigation and recycled waste water should be used for irrigation, if at all possible. From the aspect of irrigation hardware, new products such as efficient drip system and programmable automatic controllers are recommended for improving irrigation efficiency and minimizing wasteful water loss. Landscape maintenance practices were also identified as an approach to improving water conservation. This included, for example, reprogramming irrigation controllers frequently to match the changing water requirements of the plants in different seasons.

Finally, another method of approximating net evapotranspiration was mentioned by Allen et al. [11]. The evapotranspiration could be calculated by using Equation (1), Penman-Monteith Equation:

$$\lambda ET = \frac{\Delta(R_n - G) + \rho_a c_p \frac{(e_S - e_a)}{r_a}}{\Delta + \gamma (1 + \frac{r_s}{r_a})}$$
(1)

where R_n is the net irradiance, G is the ground soil heat flux, ρ_a is the dry air density, c_p is the specific heat of air at constant pressure, $(e_s - e_a)$ is the pressure deficit of air, r_a and r_s are the aerodynamic and surface resistances, Δ is the rate that saturation specific humidity changes with air temperature change and γ is the psychrometric constant. Based on Penman-Monteith Equation, Cabrera et al. [2] conducted an evaluation of urban landscape water use in Texas. The authors then introduced several methods which could be applied to conserve water. Using

water-saving plants and designing the ecogeographical region intelligently have been recommended as the basic method to conserve water. Also, precision landscape irrigation could be applied to any existing landscapes and shorten the excess irrigation water. Moreover, designing the irrigation systems specifically to the site, soil and plant type, tuning them after installation and properly utilizing the irrigation sensors could contribute to water conservation. Finally, alternative water sources such as recycled wastewater, condensate water and graywater have also been mentioned to be used to irrigate landscapes, thus alleviating demand for potable water supplies.

2.4 Current Runoff Mitigation Strategies

Various studies have been conducted on the strategies for mitigating runoff. Daniel et al. [20] used a green roof to mitigate the storm water runoff in urban areas. During the study, a green roof was fabricated and tested along with a control roof on a same commercial building. The results showed that the green roof could reduce storm runoff by up to 70 percent compared to a conventional roof. Elizabeth Fassman-Beck et al. [21] conducted further research on the effects of different specifications of extensive roofs on runoff mitigation. Four extensive green roofs and three conventional roofs have been tested. Based on the study, green roof could reduce peak flow rate by 62 to 90 percent compared to conventional roofs. Also, the

specifications of the roof, namely horizontal flow path length, drainage layer roughness and materials, could both affect the effectiveness of green roofs.

Another study conducted by Elizabeth A. Fassman et al. [22] investigated on the effectiveness of applying a permeable pavement system over impermeable soils to mitigate urban runoff. For the permeable pavement system, precipitation and runoff will flow over the surface and then infiltrate into a storage reservoir below the permeable surface. Afterwards, water in the storage reservoir will flow through the porous media around the reservoir and then infiltrate into the adjacent soil. During the experiments, a $200 \ m^2$ permeable pavement site was constructed and tested with an adjacent conventional asphalt section acting as a control site. The results showed that the permeable pavement system could mitigate the peak flow rate by up to 70 percent. The authors believed that the permeable pavement system should be considered as a low impact runoff control system, which requires correct installation to ensure proper function.

Betty et al. [23] has also conducted a study concentrating on how to design a parking lot to reduce runoff as well as pollution loads. Impervious pavements and basins with and without swales have been divided into four different groups. It turned out that the swales could reduce runoff by 30 percent while the basin could add another 10 percent runoff reduction. Other useful methods have also been

researched by other scientists to reduce runoff. However, very few methods which base their controls on the amounts of runoff have been considered and developed.

3. DESIGN AND FABRICATION OF LANDSCAPE IRRIGATION RUNOFF MITIGATION SYSTEM

3.1 Aim and Objective

The objective of the study was to design a Landscape Irrigation Runoff Mitigation System (LIRMS) equipped with a reliable, durable and low-cost irrigation runoff sensor for minimizing irrigation water losses from residential or commercial landscapes.

At the first step, four types of irrigation runoff sensors, based on different working principles, were designed and manufactured. Then, a central control unit which is capable of receiving signals from sensors and controlling several irrigation valves at the same time was designed.

The second step consisted of installing all the prototypes in the field and hardwiring them with the central control unit. Two control groups were set and the performances of four different types were compared. The amount of runoff was recorded as the index of performance. The different types were evaluated based on their performance characteristics including the ability of each prototype to work reliably over an extended period of time.

Internet access was added to the system to access the irrigation data online.

Wireless communication between the irrigation runoff sensors and the central

control unit was established. Quality of the wireless communication and the performances of the new wireless irrigation runoff sensor systems were evaluated.

An autonomous energy system was designed by combining solar panels and rechargeable batteries. The solar panels provided energy for the sensor and for recharging the batteries during daytime so the system could work in the evening. The performance of the autonomous energy system was tested.

3.2 Landscape Irrigation Runoff Mitigation Sensor Prototype Design,

Fabrication and Test

In this section the different types of runoff sensor designs including working mechanisms are discussed.

3.2.1 General Working Requirements of the Landscape Irrigation Runoff Mitigation Sensor

The runoff sensor itself is the essential part of the landscape irrigation runoff mitigation sensor system, converting the runoff signal into an electronic signal which can be utilized by a microcontroller to control the irrigation system. To ensure the proper function of the system, the runoff sensor needs to be reliable in all environmental circumstances and strong enough to endure impact or mechanical failure. Also, it needs to be low-cost for mass production purposes. Finally, an energy-saving version is desired in order to be environmental friendly.

3.2.2 Materials Selection for Fabricating Prototypes

The selected materials to build the prototypes need to be reliable in both hot and cold weathers, corrosion-resistant, impact-resistant and should be inexpensive. Different types of materials have been evaluated to construct the prototypes, including acrylonitrile butadiene styrene (ABS), polyvinyl chloride (PVC), polystyrene (PS) stainless steel and aluminum. The comparison of different materials have been listed in Table 2.

Table 2. Comparison of Different Materials for Runoff Prototypes

| Material | Advantages | Disadvantage s | Comments |
|----------|--|---|---|
| ABS | Low-hazard material, impact-resistant, tough, low cost | Narrow thermal tolerance range | Suitable for constructing the prototype due to the great impact-resistant and reliable features as well as the low cost. The temperature range works for the irrigation use (-20 - 80 C). |
| PVC | High hardness and good mechanical properties, good insulation properties, low cost | Poor heat stability | Suitable for constructing the prototype because it could be easily machined when heated. |
| PS | Hard, inexpensive | Highly flammable | Not selected due to the flammability. The hot weather and the heat produced by electronic devices increases the risk of fire. |

| Material | Advantages | Disadvantage s | Comments |
|--------------------|--|--|---|
| Stainless Steel | Tough and reliable, corrosion-resistant, impact-resistant, high thermal tolerance | Expensive, more tools are needed for machining | Not Selected due to the price and the higher requirements of machining tools. |
| Aluminum | Tough and reliable, corrosion-resistant, light in weight, impact-resistant, high thermal tolerance | Expensive aluminum alloys, more tools are needed for machining | Not selected due to the price and the higher requirements of machining tools. |

Taking both requirements into consideration, ABS and PVC have been chosen to fabricate the prototypes. For the elbow float prototype and the conductivity prototype, a commercial PVC elbow pipe has been selected to be the outer case, while a thin PVC sheet is used for the construction of the paddle wheel of the paddle-wheel prototype. Also, ABS has been chosen to build the cubic-float and paddle-wheel prototypes.

3.2.3 Original Designs of the Landscape Irrigation Runoff Mitigation Sensor Prototypes

Several different types of irrigation runoff sensor prototypes have been developed taking the prescribed requirements into consideration. They work on various principles including on-off or continuous operation, which requires a distinct process to convert runoff signals to data that could be used by the electronic system.

These designed runoff sensors include an eductor prototype, float sensor prototype, infrared prototype, paddle wheel prototype, tip bucket prototype and conductivity prototype.

3.2.3.1 Conceptualized Eductor Prototype

The eductor prototype utilizes the concept of a water eductor. The structure of the water eductor is shown in Figure 3.

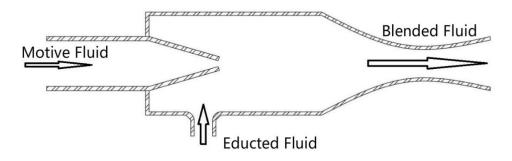


Figure 3. Structure of Water Eductor

As Figure 3 shows, the educted fluid will be extracted when there is motive liquid going through the chamber. The structure of the eductor prototype is shown in Figure 4.

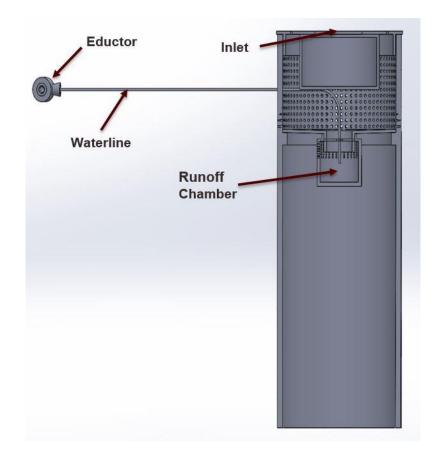


Figure 4. Structure of Eductor Prototype

The runoff will be collected in a chamber and when the water level reaches a certain level, then the eductor should extract the water out of the chamber. As a result, the runoff should be detected by using an instrument downstream from the device.

The eductor prototype is sensitive and reliable since it does not have moving parts. However, a highly efficient filter system is needed since the small diameter of the waterline could make it easy to be clogged. Also, the eductor prototype might be hard to install in the field.

3.2.3.2 Conceptualized Infrared Prototype

The infrared prototype is based on the use of an infrared sensor. The structure of the infrared prototype is shown in Figure 5.

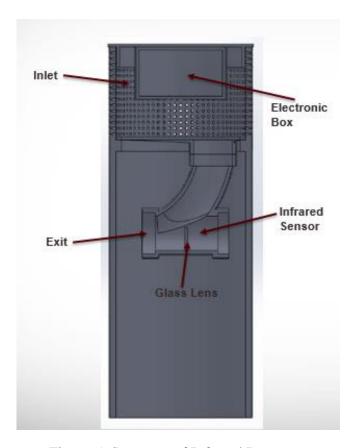


Figure 5. Structure of Infrared Prototype

A glass lens is set at the middle of the bottom cylindrical tube. When runoff enters the prototype and passes over the lens, a reflective angle will be created and should be detected by the infrared sensor. Then the runoff signal will be sent to the control part to adjust the irrigation progress.

The infrared prototype does not need much maintenance and is very reliable.

Also, the drain line is not necessary for the infrared prototype. However, it can be expensive and might require a complex software program.

3.2.3.3 Conceptualized Paddle Wheel Prototype

The paddle wheel prototype detects and measures runoff by using paddle wheel. The angular speed of the paddle wheel should be measured and calibrated to determine the true amount of runoff. A sensor is needed to detect the angular speed and send the signal to the microcontroller. The structure of the paddle wheel prototype is shown in Figure 6.

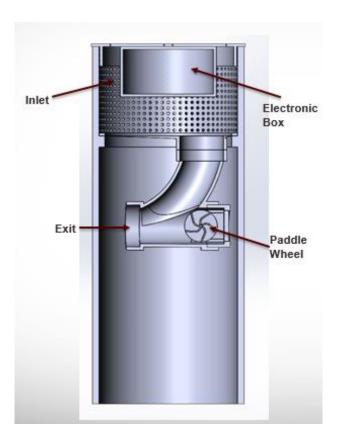


Figure 6. Structure of Paddle Wheel Prototype

When runoff occurs and enters the prototype from the top, it will flow through the prototype and then drive the paddle wheel at the downstream location. The relationship between the amount of runoff that enters the prototype and the rotational speed of the paddle wheel could be measured under lab conditions. As a result, this prototype should measure the amount of runoff that runs through it, which is the biggest advantage of this prototype when compared with other prototypes.

However, the paddle wheel prototype has some disadvantages. The moving parts in this prototype increase the risk of mechanical problems, while debris such as grass and stones could easily restrict the motion of the paddle wheel.

3.2.3.4 Conceptualized Tip Bucket Prototype

The tip bucket prototype utilizes a bucket to collect runoff. The structure of the tip bucket prototype is shown in Figure 7.

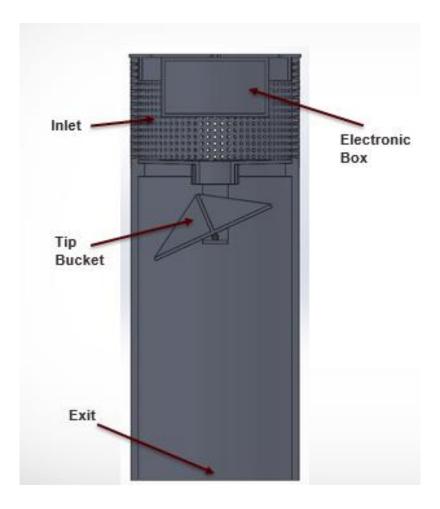


Figure 7. Structure of Tip Bucket Prototype

When runoff occurs, it will enter the prototype and gets collected in the bucket. As soon as the runoff is collected in the bucket, it reaches a certain threshold, then the bucket will tip and the runoff will fall down and leave the prototype. A switch or infrared sensor might be needed to detect the tips of the bucket.

The tip bucket prototype will be able to calculate the runoff flow rate once preliminary experiments have been conducted to investigate the amount of water that could make the bucket tip. Also, this prototype does not need much

maintenance. However, debris in the runoff could accumulate in the bucket and restrain the motion or even prevents the buckets from moving altogether, which will significantly affect the performance of the prototype.

3.2.3.5 Conceptualized Float Prototype

The float prototype is equipped with a float sensor to detect the runoff. The structure of the float prototype is shown in Figure 8.

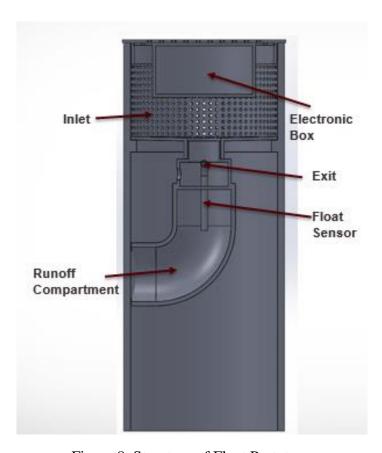


Figure 8. Structure of Float Prototype

Runoff enters the prototype and is accumulated in the runoff compartment. A float sensor is installed at the top of the compartment. When water level in the compartment reaches a set threshold, the float switch will be activated and the runoff signal would be sent to the controller.

The float runoff sensor has very few moving parts and it is very simple and reliable. However, this prototype also requires a very efficient filtering system. Also, it needs to accumulate some runoff before being activated, which could lead to a lagged response.

3.2.3.6 Conceptualized Conductivity Prototype

The conductivity prototype uses two electrodes as an ON/OFF switch to detect runoff. The structure of the conductivity prototype is shown in Figure 9.

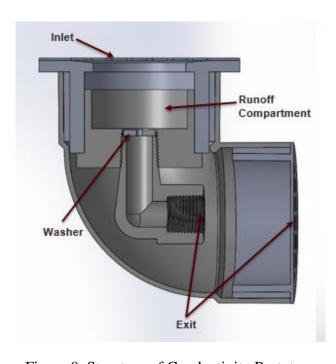


Figure 9. Structure of Conductivity Prototype

Runoff enters the prototype and is accumulated in the runoff compartment. One electrode is installed at the bottom of the compartment while the other one is installed at a set height above the bottom electrode. When water level in the compartment rises and the two electrodes are submerged in the water, water will act as a conductive medium and a small current should run from one electrode to the other. The electrodes should then activate the ON/OFF switch this way.

The conductivity runoff sensor does not have moving parts. It is very easy to make and it is durable. However, this prototype also requires a very efficient filtering system to avoid clogging issues. Also, just like the float prototype, it needs to accumulate some runoff before it can be activated, which could lead to a lagged response.

3.2.3.7 Design Decision Making Scheme

In order to down select design options, a list of attributes including advantages and disadvantages of each prototype has been identified and specified, as shown in Table 3.

Table 3. Design Decisions of Landscape Irrigation Runoff Mitigation Sensor Prototypes

| Device Type | Advantages | Disadvantages | Constructed? | Comments |
|------------------------------|--|---|--------------|--|
| Eductor Prototype | Sensitive Reliable No moving parts | Need high efficiency filter system to avoid clogging issue Hard to install Need power input | No | Based on the working principle of the eductor prototype, the waterline should have a very small diameter, which could get clogged very easily. Also, it needs an extra power input, which requires more energy. Thus this idea has not been adopted. |
| Infrared Prototype | Do not need drain line Reliable Do not need much maintenance | High cost Complex program | No | The high cost and complex program make this prototype not suitable for a low-cost and user-friendly runoff sensor. Thus this idea has not been adopted. |
| Paddle Wheel Prototype | 1. Could measure the amount of runoff that runs through the sensor | Has moving parts Clogging issue Debris may affect the motion of the paddle | Yes | Despite the disadvantages mentioned, its greatest feature is its ability to measure runoff on a continuous basis, which is direct and useful for performance evaluation and irrigation control. Thus this prototype has been constructed. |

| Device Type | Advantages | Disadvantages | Constructed? | Comments |
|---------------------------|--|--|--------------|--|
| Tip Bucket Prototype | 1. Could measure the amount of runoff that runs through the sensor 2. Do not need much maintenance | Has moving parts Clogging issue Debris may accumulate in the buckets and affect the motion of it | No | The tip bucket prototype has a very similar working principle and mechanism as the paddle wheel prototype. Since the paddle wheel prototype has been constructed, the tip bucket prototype has not been adopted. |
| Float Prototype | Simple Reliable No moving parts | Need high efficiency filter system to avoid clogging issue Lag in response time | Yes | The float prototype is simple and easy to build, plus it is reliable and inexpensive. Though it exhibits a lagging response, it has been constructed and adopted. |
| Conductivity Prototype | Easy to build Heavy-built No moving parts | Need high efficiency filter system to avoid clogging issue Lag in response time Rust on electrodes | Yes | The conductivity prototype is reliable and inexpensive. It can endure great impact and could also be constructed quickly. Though it exhibits a lagging response, it has been constructed and adopted. |

Based on the advantages/disadvantages listed in the table, the paddle wheel prototype, the float prototype and the conductivity prototype have been constructed for further tests.

3.2.4 Fabrication Tools and Procedures

Taking into account the advantages and disadvantages of different prototypes, the float prototype, the paddle wheel prototype and the conductivity prototype have been manufactured. ABS and PVC have been utilized for the prototypes to fulfill the goals of having a reliable, low-cost and easy to machine device. Various tools and machines have been used during the fabrication processes, as shown in Figure 10.



Figure 10. Tools and Machines for Fabricating Runoff Prototypes

The jig and the hot air gun have been used for manufacturing the curved sheet of the paddle wheels. PVC sheets could be bent easily when heating them with the hot air gun, which allowed for the fabrication of the curved paddle wheel fins.

The band saw has been used for cutting large rectangular ABS boards for fabricating the outer shells of the different prototypes, while the laser cutter has been used for precise manufacturing of inside components of all the prototypes. Drawings should be specifically designed for the laser cutter with the width of the laser taken into consideration, as shown in Figure 11.

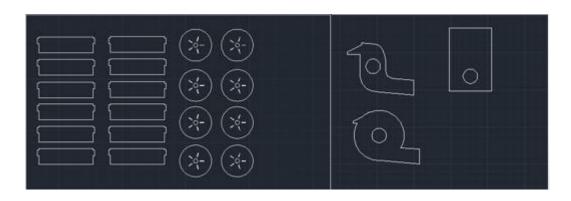


Figure 11. AutoCAD Drawings of the components of the Paddle Wheel prototypes for the laser cutter

The advantages, disadvantages and applications of different tools and machines have been listed in Table 4, as shown below.

Table 4. Comparisons and Applications of Different Tools and Machines

| Method | Advantages | Disadvantages | Applications |
|-------------------------|---|--|---|
| Jig & Hot Air Gun | Could make fine curved surface | Need expertise Need to make the wood jig first | Fabricate the paddle wheels and curved outer shells of the paddle wheel prototype |
| Laser Cut | Fast. Precise Could make very complex shape precisely | Need to take shrinking into consideration to make specific mechanical drawings for the machine to use Some materials are not suitable for laser-cutting, especially for those which are vulnerable to heat | Fabricate the outer shells and cut the holes with large diameters on the parts of the cubic float prototype |
| Band Saw | Fast Easy to use | Not for precise cutting if lacking expertise. | Fabricate the parts of float prototype and conductivity prototype |
| Drill | N/A | N/A | Drill holes for screws for both prototypes |

3.2.5 Final Designs of the Landscape Irrigation Runoff Mitigation Sensor

Prototypes

The paddle wheel prototype, the float prototype and the conductivity prototype have been manufactured for testing purposes. While the working principles remain the same between the original and final designs of each prototype; however, the inner structures and layouts of the original designs have been changed to make the devices easier to fabricate.

3.2.5.1 Final Paddle Wheel Prototype

The original paddle wheel prototype has been revised to fit the testing facility. The prototype was redesigned to accommodate the electronic system responsible for relaying information to the main controller. Furthermore, the water receiving end was modified so water did not have to go through the entire system. The mechanical

system was separated from the electronic side by using a shaft. The structure of it is shown in Figures 12 and 13.

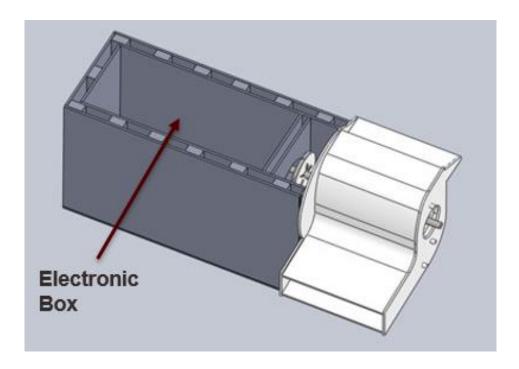


Figure 12. Structure of the Final Paddle Wheel Prototype

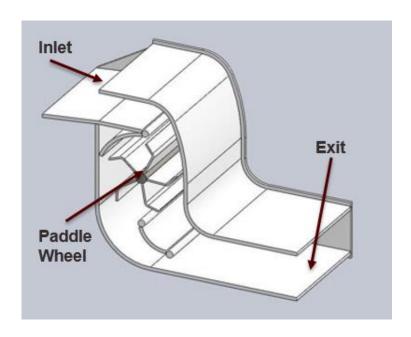


Figure 13. Structure of the Final Paddle Wheel Prototype (cutaway view)

The photo of the fabricated paddle wheel prototype is shown in Figure 14.



Figure 14. Installed Paddle Wheel Prototype

3.2.5.2 Final Cubic Float Prototype

The float prototype has been further developed into two different designs: the cubic float prototype and the elbow float prototype. Both designs share the same working principle. The only difference between the two prototypes is the shape.

The cubic float prototype has been redesigned to be equipped with an electronic box for the controller. Furthermore, the shape of the float prototype has been redesigned to accommodate an inlet conduit for higher efficiency of gathering runoff. The cubic float prototype consists of the inlet conduit, the cubic runoff compartment, the electronic box, the vertical float switch and the exit orifice. The vertical float switch and the cubic float prototype's layout are shown in Figure 15 and 16.



Figure 15. Vertical Float Switch with Two Output Wires

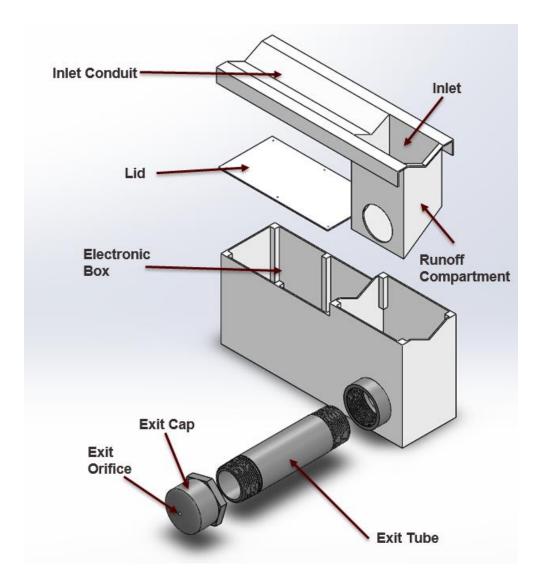


Figure 16. Exploded View of the Cubic Float Prototype

The runoff enters the runoff compartment, where the float switch is installed, through the inlet conduit. When the runoff flow rate exceeds the maximum flow rate that the exit hole allows to escape the runoff compartment, runoff starts to accumulate in the compartment and activates the float switch when fluid reaches a certain water level. The two output wires are extended either directly to the main irrigation controller which controls the valves, or into the electronic box where the wireless communication module is installed.

The photo of the fabricated cubic float prototype is shown in Figure 17.



Figure 17. A Cubic Float Prototype Equipped with an Energy Supply Module

3.2.5.3 Final Elbow Float Prototype

The elbow float prototype has been designed by using the same outer shell as the conductivity prototype. The new layout accommodates a vertical float sensor, which leads to a more compact and heavy-built prototype comparing to the cubic float one. Its structure is shown in Figure 18.

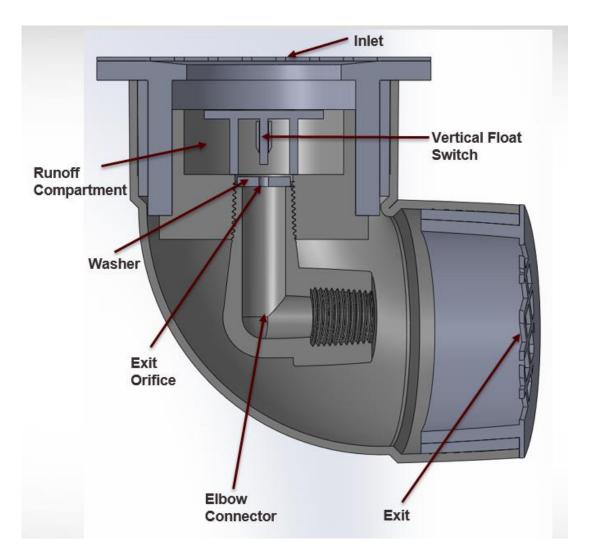


Figure 18. Section View of the Elbow Float Prototype

Its working principle is the same as the one of the cubic float prototype. The vertical type switch is installed in the elbow float prototype. Compared to the cubic

one, the elbow float prototype is more heavy-built and compact. The elbow float prototype has a changeable orifice size by using as washer as shown in Figure 18.

The photo of the fabricated elbow float prototype is shown in Figure 19.

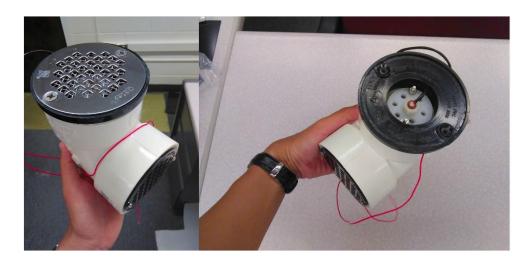


Figure 19. An Assembled Elbow Float Prototype

3.2.5.4 Final Conductivity Prototype

The conductivity prototype has remained its original design, which is shown in Figures 20 and 21.

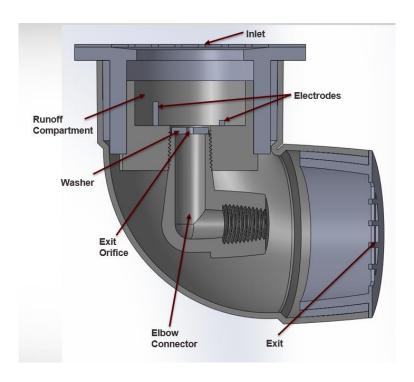


Figure 20. Section View of the Conductivity Prototype

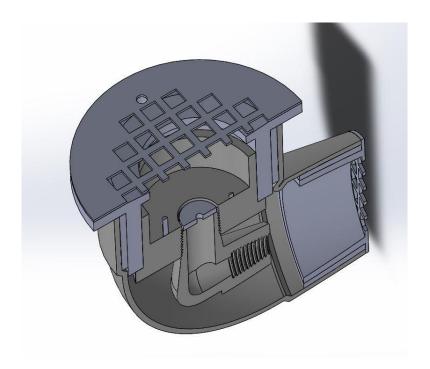


Figure 21. Section View of the Conductivity Prototype (45 Degree Angle)

When runoff occurs, it enters the runoff compartment through the inlet. Runoff starts to accumulate when the flow rate reaches a certain flow rate that exceeds the flow rate through the exit of the runoff compartment. As a result, accumulated runoff acts as the conductive medium between the two electrodes when the electrodes are submerged in water. Similar to the float prototype, each electrode is connected to a wire, and the two output wires are extended either directly to the main irrigation controller which control the valves, or into the electronic box where the wireless communication module is installed. The exit orifice of the conductivity prototype can be changed by changing the size of the washer.

The photo of the fabricated elbow float prototype is shown in Figure 22.



Figure 22. Assembled Conductivity Prototype

3.3 I/O Communication and Control Module Design and Fabrication

In this section the design and development of the I/O communication and control module is discussed.

3.3.1 General Working Requirements of the I/O Communication and Control Module

The I/O communication and control module is the brain of the landscape irrigation runoff mitigation sensor system. It receives the runoff signals from the irrigation runoff sensors and then controls the irrigation process intelligently. The I/O communication and control module needs to fulfill the cycle-soaking process when working together with an irrigation runoff sensor and has to be reliable in all environmental circumstances. Also, an I/O communication and control module needs to control multiple field plots at the same time and should be able to store the irrigation data securely. Finally, a low energy consumption module is desired so it can operate uninterruptedly.

3.3.2 General Working Principle of the I/O Communication and Control Module

The I/O communication and control module has to be able to control the irrigation cycle by setting the system on ON and OFF mode based on the received runoff signals from the irrigation runoff sensors. Its working principle is shown in Figure 23.

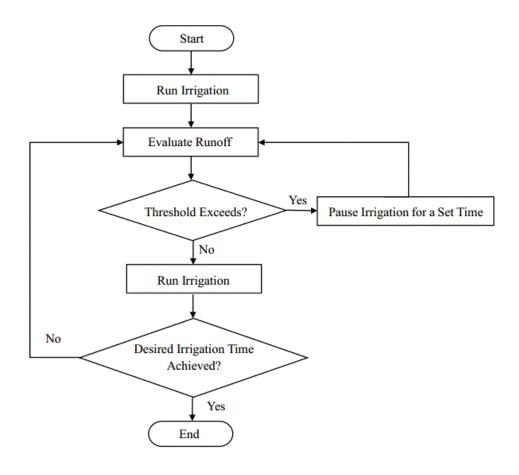


Figure 23. Operating Principle of the I/O Communication and Control Module

An I/O communication and control module is able to control the irrigation for multiple plots at the same time. When the irrigation starts, it will open all the valves so that the sprinklers could spray water to the field. As soon as the irrigation runoff sensors detect runoff and the I/O communication and control module receives the runoff signals, the valves of the plots with runoff detected will be closed and the irrigation will be switched to OFF mode for a set amount of time. After that the I/O communication and control module checks the runoff status, it will keep the valves

closed if runoff has been detected again. If no runoff has been detected, the sprinklers will work until the desired irrigation time has been reached for all the plots.

3.3.3 Printed Circuit Board (PCB) Design and Fabrication

Two generations of printed circuit boards (PCB) have been designed to be the I/O communication and control module. The first generation has a transmitter board on the irrigation runoff sensor side and a receiver board on the I/O communication and control module side. The second generation has only one board installed on the I/O communication and control module side.

3.3.3.1 Design and Fabrication of the First Generation of the I/O Communication and Control Module with Transmitters and Receivers

The first generation of the I/O communication and control module has been equipped with the ATmega328 microcontroller and consists of one transmitter board and one receiver board. The working principle is shown in Figure 24.

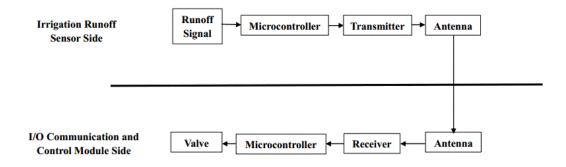


Figure 24. Working Principle of the First Generation of I/O Communication and Control Module

The transmitter board (the upper part of Figure 24) is installed on the irrigation runoff sensor side, while the receiver board (the lower part of Figure 24) is on the I/O communication and control side. When runoff has been detected, the microcontroller on the transmitter board receives the runoff signal and then sends that to the transmitter. This signal is amplified by the antenna to ensure signal quality. Then the signal will be captured by the receiver on the receiver board and processed by the microcontroller installed on it. Thus the microcontroller will close the valve for a set time. The structures of the transmitter board and the receiver board are shown in Figure 25 and 26.

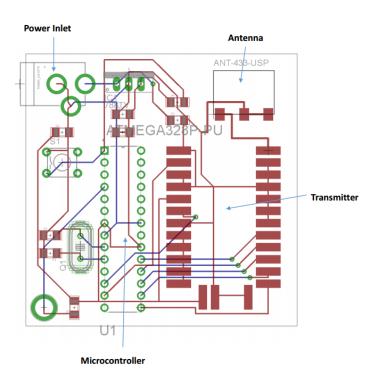


Figure 25. Structure of the Transmitter Board on the Irrigation Runoff Sensor Side

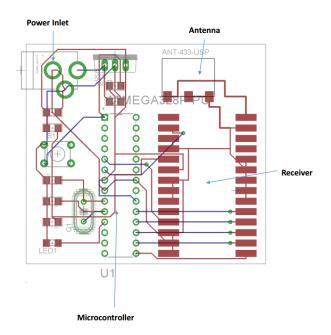


Figure 26. Structure of the Receiver Board on the I/O Communication and Control

Module Side

The photos of the transmitter board and the receiver board are shown in Figure 27 and 28.

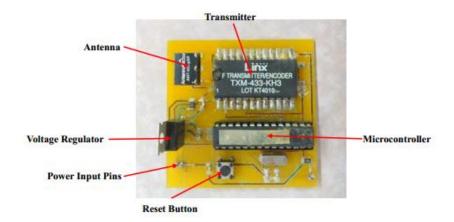


Figure 27. A Fabricated and Assembled Transmitter Board

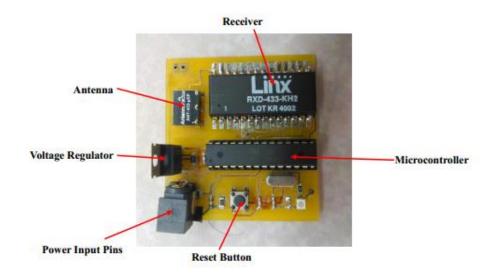


Figure 28. A Fabricated and Assembled Receiver Board

The first generation of the I/O communication and control module is capable of wireless communication between the irrigation runoff sensor and the controller. The prototype boards have achieved the desired functions and are able to establish a stable wireless communication for up to 30 meters during the field tests. However, the quality of the wireless communication could be dramatically affected by a nearby signal tower or other interference. Also, each irrigation runoff sensor must be equipped with a transmitter board and a receiver board, which could result in a high cost.

3.3.3.2 Design and Fabrication of the Second Generation of I/O Communication and Control Module

The second generation of the I/O communication and control module has been equipped with the ATmega328P microcontroller and just has one PCB. Its structure is shown in Figure 29.

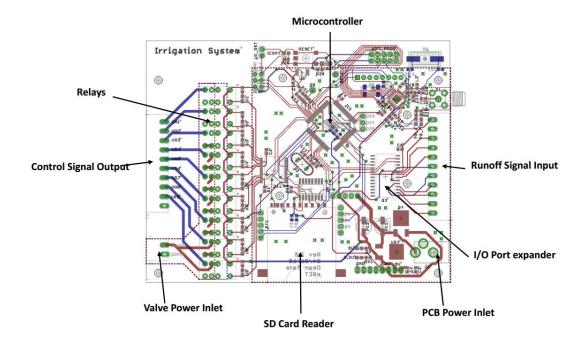


Figure 29. Structure of the Current I/O Communication and Control Module PCB

For this version of the I/O communication and control module, all the irrigation runoff sensors have been hardwired to the PCB through the Runoff Signal Input ports as shown in Figure 29. When runoff occurs, the irrigation runoff sensor detects it and sends the signal to the runoff signal input on the PCB. Then the microcontroller on the PCB receives the signal and controls the relay. The relay is located between the power supply and the valve. The microcontroller opens the relay when runoff is detected so that the valve has no power, which turns the irrigation system off. It closes the relay to continue irrigation in the field when no runoff is detected. The irrigation results and data are stored in the secure digital (SD) card. The photo of the PCB is shown in Figure 30.

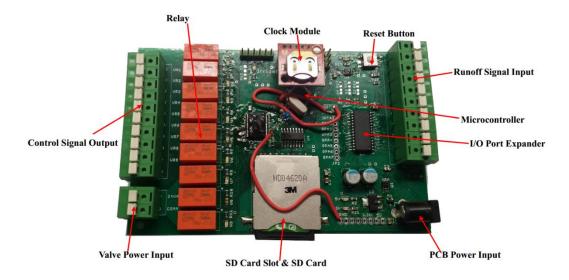


Figure 30. A Fabricated and Assembled I/O Communication and Control Module
PCB

The I/O communication and control module provides precise and reliable controls for up to 9 plots during the field tests. It could either work as a stand-alone irrigation controller or as an add-on item to an existing controller, as shown in Figures 31 and 32.

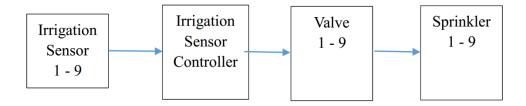


Figure 31. Working Principle of Acting as an Individual Irrigation Controller

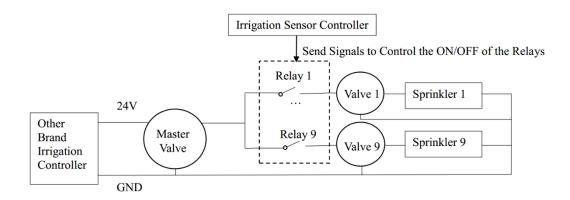


Figure 32. Working Principle of Acting as an Add-On to an Existing Irrigation

Controller

When the I/O communication and control module works as an individual irrigation controller, runoff signals are sent to the PCB and the PCB will control the sprinklers by opening and closing the corresponding valves. If the I/O communication and control module works as an add-on item to an existing irrigation controller, the existing irrigation controller of other brand will control the master valve directly to control the water supply to the system. When the master valve is open and the runoff signals are detected, the I/O communication and control module will control the sprinklers by controlling the corresponding relays and valves.

Compared to the first generation, the second generation of the I/O communication and control module is low cost and could hardly be affected by the surroundings or environmental noise. Also, the first generation maintains a constant energy consumption level 24 hours a day for 7 day, which requires more energy in the long run. The second generation I/O system relies on a sleep model, which turn the whole system off when it is not in operation. Therefore, it does not consume energy when it is not in operation (i.e. irrigating). The energy consumption comparison

between the two generations based on a one hour weekly irrigation event for a 9-plot field is shown in Table 5. The second generation results in 78.6% saving in energy compared to the first generation.

Table 5. Comparison of Energy Consumptions between the Two Generations of the I/O Communication and Control Module

| | Voltage (V) | Current (A) | Power (W) | Number of PCB Needed | Weekly Working Time (h) | Weekly Energy Consumption (Watt-Hour) |
|-------------------------------|----------------|-------------|-----------|----------------------------|-------------------------------|--|
| 1 st Generation | 5 | 0.05 | 0.25 | 9 | 168 | 42 |
| 2 nd Generation | 9 | 1 | 9 | 1 | 1 | 9 |

With all these advantages, the second generation turns out to be the final option for the I/O communication and control module.

3.3.4 Autonomous Power Supply Module Design and Fabrication

The I/O communication and control module has been desired to use as little energy possible. An autonomous power supply module consisting of solar panels and rechargeable batteries has been designed to provide the I/O communication and control module with needed power. The circuit diagram is shown in Figure 33.

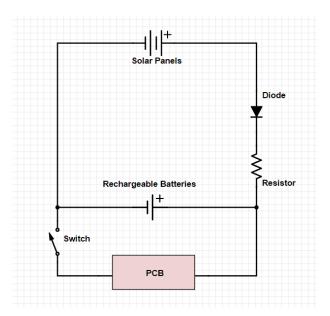


Figure 33. Circuit Diagram of the Autonomous Power Supply Module

During daytime, the solar panels of the autonomous power supply module provides the energy for the PCB which recharges the batteries. During times without sunlight, the rechargeable batteries provide the PCB with the energy. Moreover, the batteries could not charge the solar panels due to the diode. The switch in Figure 33 is used to open and close the autonomous power supply module.

The autonomous power supply module has been tested in the field and functions as desired. The installation is shown in Figure 34.



Figure 34. A Cubic Float Prototype with an Autonomous Power Supply Module

Installed in the Field

3.3.5 Irrigation Results Analysis Website Design

An irrigation results analysis website (http://irrigationrom-kossel.rhcloud.com/) has been designed to store the irrigation data in the web server and plot the irrigation result charts, as needed. The irrigation data and results in the SD card could be manually uploaded to the web server, as shown in Figure 35.

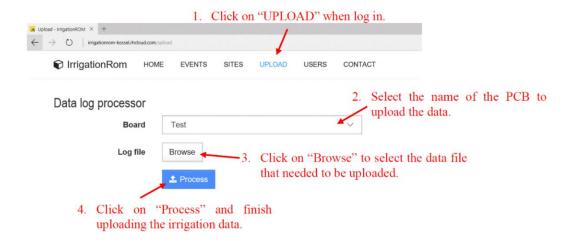


Figure 35. Webpage for Manually Uploading the Irrigation Results and Data

The website is also capable of storing results and data in the web server and drawing the irrigation result charts for designated dates automatically, as shown in Figure 36.

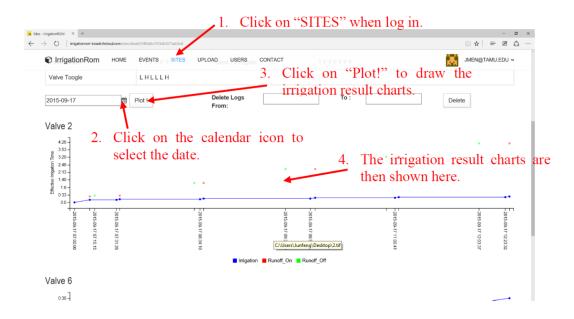


Figure 36. Webpage for Drawing the Irrigation Result Charts of Designated Dates

4. RESULTS AND DISCUSSION

This chapter includes the tests results of the irrigation runoff prototypes under different situations. The first section deals with the lab testing of different prototypes. The second section focuses on the qualitative field testing of all the prototypes. Finally, the last section discusses the quantitative field testing results of different irrigation runoff sensor prototypes.

4.1 Lab Testing Results of Different Prototypes

Lab tests were conducted to evaluate the effectiveness of the designed and built prototypes. The paddle wheel, cubic float, elbow float and the conductivity prototypes have been tested and validated in the lab as described below.

4.1.1 Lab Testing Results of Paddle Wheel Prototype

During the lab tests, the runoff flow rates and corresponding rotational speeds of the paddle wheel were recorded and a correlation equation between both variables was derived, as shown in Figure 37.

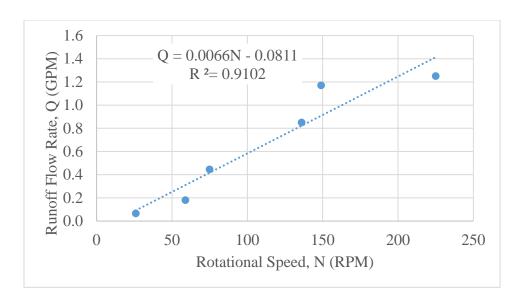


Figure 37. Lab Test Results of Runoff Flow Rate and Rotational Speed of Paddle

Wheel Prototype

Based on Figure 37, the relation between the runoff flow rate in gallons per minute Q (GPM) and the rotational speed in rounds per minute N (RPM) is as follows:

$$Q[GPM] = 0.0066 \times N[RPM] - 0.0811 \tag{2}$$

With Eq. (2), the amount of the water that runs through the prototype can be estimated by recording the rotational speed.

4.1.2 Lab Testing Results of Cubic Float Prototype

The cubic float prototype has also been tested in the lab. The exit orifice diameters with the corresponding runoff flow rates have been documented as shown in Table 6.

Table 6. Lab Tests Results of the Cubic Float Prototype

| Exit Orifice Diameter (inch) | Runoff Flow Rate (GPM) |
|------------------------------|------------------------|
| 0.25 | 0.296 |
| 0.1875 | 0.156 |
| 0.125 | 0.071 |
| 0.0625 | 0.018 |

The relationship between the runoff flow rate and exit orifice diameter is shown in Figure 38.

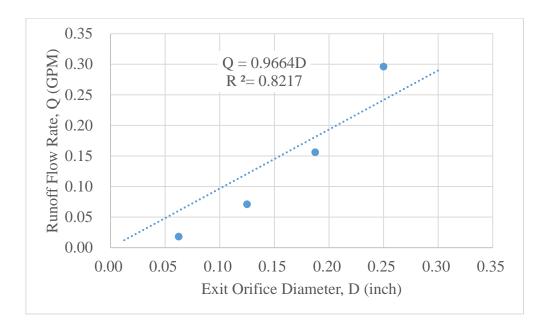


Figure 38. Lab Test Results of Runoff Flow Rates and Exit Orifice Diameters of Cubic Float Prototype

Based on Figure 38, the relation between the runoff flow rates in gallons per minute Q (GPM) and the exit orifice diameters D (inch) is as follows:

$$Q[GPM] = 0.9664 \times D[inch] \tag{3}$$

4.1.3 Lab Testing Results of Elbow Float Prototype

During lab tests, the runoff flow rate which could activate the elbow float switch has been documented as shown in Table 7.

Table 7. Lab Test Results of the Elbow Float Prototype

| Exit Orifice Diameter (inch) | Runoff Flow Rate (GPM) |
|------------------------------|------------------------|
| 0.5 | 1.183 |
| 0.25 | 0.598 |
| 0.125 | 0.253 |

The relationship between the runoff flow rates and exit orifice diameters is shown in Figure 39.

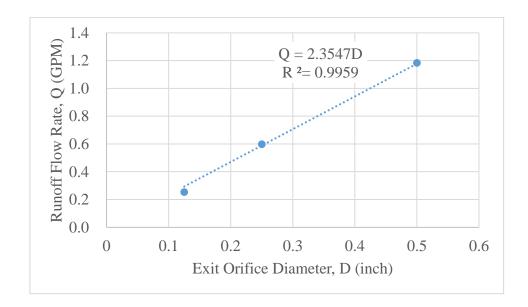


Figure 39. Lab Test Results of Runoff Flow Rates and Exit Orifice Diameters of Elbow Float Prototype

Based on Figure 39, the relation between the runoff flow rates in gallons per minute Q (GPM) and the exit orifice diameters D (inch) is as follows:

$$Q[GPM] = 2.3547 \times D[inch] \tag{4}$$

4.1.4 Lab Testing Results of Conductivity Prototype

During lab tests, the runoff flow rates which could activate the conductivity prototype with different exit orifice diameters have been documented as shown in Table 8.

Table 8. Lab Test Results of the Conductivity Prototype

| Exit Orifice Diameter (inch) | Runoff Flow Rate (GPM) |
|------------------------------|------------------------|
| 0.125 | 0.22 |
| 0.6875 | 1.4 |
| 0.75 | 1.61 |

The relationship between the runoff flow rates and exit orifice diameters is shown in Figure 40.

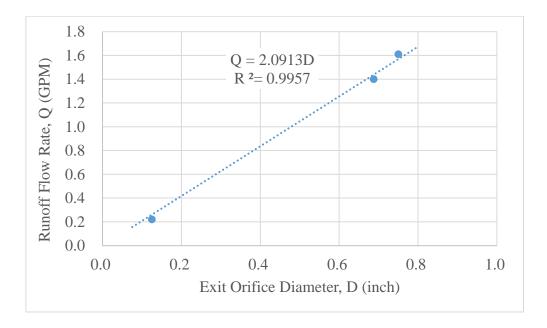


Figure 40. Lab Test Results of Runoff Flow Rates and Exit Orifice Diameters of Conductivity Prototype

Based on Figure 40, the relation between the runoff flow rates in gallons per minute Q (GPM) and the exit orifice diameters D (inch) is as follows:

$$Q[GPM] = 2.0913 \times D[inch] \tag{5}$$

4.1.5 Working Ranges of Different Prototypes

The working ranges of different prototypes has been tested and recorded, as shown in Table 9.

Table 9. Working Ranges of Different Prototypes under Lab Conditions

| Prototype | Working Range (GPM) |
|------------------------|---------------------|
| Paddle Wheel Prototype | 0.08 - 1.78 |
| Cubic Float Prototype | 0.01 - 0.3 |
| Elbow Float Prototype | 0.05 - 1.4 |
| Conductivity Prototype | 0.05 - 1.7 |

As the table shows, the paddle wheel prototype and the conductivity prototype have the greatest range. On the other hand, cubic float prototype has a narrower range of operation, which makes the device more sensitive to runoff. The cubic float prototype, the elbow float prototype and the conductivity prototype can detect small flow rate when a small exit orifice hole is used. However, small orifices are more prone to clogging and may require regular cleaning.

4.2 Qualitative Field Testing Results of Different Prototypes

The qualitative field testing aims at evaluating the functionalities and effectiveness of different sensor prototypes. Several performance related parameters, including effective irrigation time, wait time, start time, total irrigation time and the

irrigation time were used to control the irrigation process. The effective irrigation time (EIT) is the total amount of the time when the sprinklers are on during an irrigation event. Also, the wait time (WT) is a manually set value of the pause time of the irrigation system when runoff is detected. Meanwhile, the start time is the time of the day when the irrigation is set to begin. The real irrigation time (IT) is the total time that the whole system is in operation. Lastly, the total irrigation time (TIT) acts as top or maximum limit, which should not be exceeded. When IT is equal or larger than TIT, the whole system will be closed permanently until next irrigation day no matter EIT is reached or not. Figure 41 shows the different time variables for a typical irrigation event.

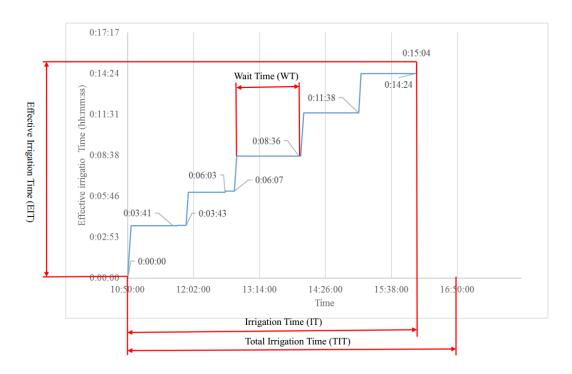


Figure 41. Different Time Variables for a Typical Irrigation Event

4.2.1 Qualitative Field Testing Results for April 8th 2015

A cubic float prototype and a conductivity prototype have been also tested. The irrigation specifications are shown in Table 10.

Table 10. Irrigation Specifications of Test on April 8th 2015

| Start Time | 7:00 AM |
|---------------------------------|--|
| Effective Irrigation Time (EIT) | 30 minutes |
| Wait Time (WT) | 20 minutes |
| # of Tested Plot | 5 (Cubic Float Prototype), 6 (Conductivity Prototype) |

The results of the irrigation are shown in Figure 42 - 45.

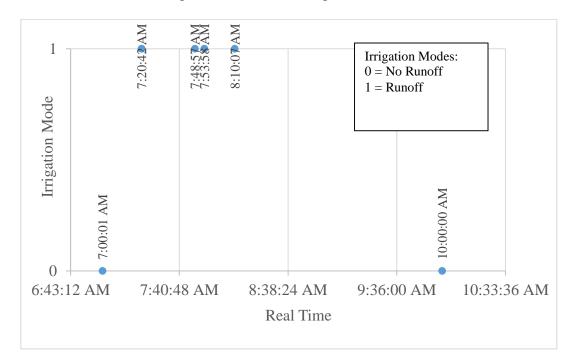


Figure 42. The Runoff Status of Plot 5 (Cubic Float Prototype) on April 8th 2015

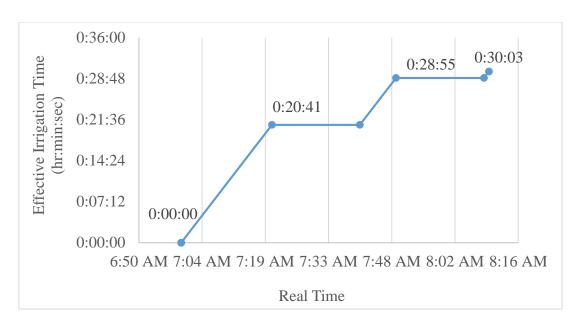


Figure 43. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on April 8th 2015

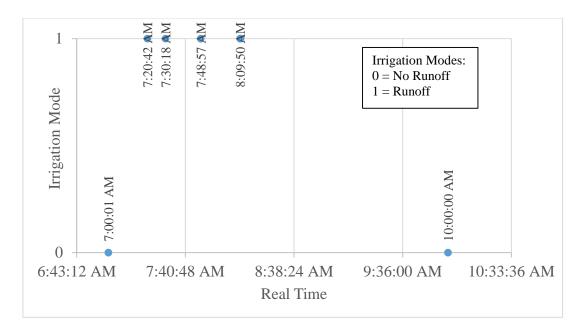


Figure 44. The Runoff Status of Plot 6 (Conductivity Prototype) on April 8th 2015

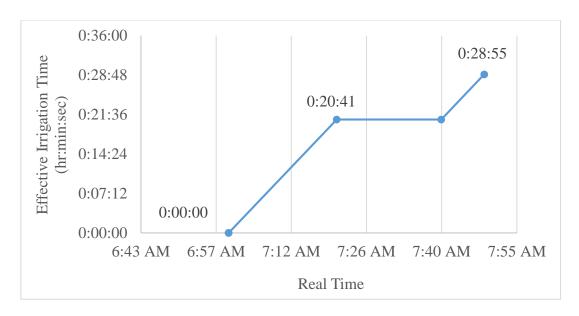


Figure 45. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on April 8th 2015

Based on the irrigation results, both prototypes have shown the capability of detecting runoff and fulfilling the complete cycle-soaking. However, the different EITs of the two devices may be caused by the interference or noises on the PCB, which interrupted the operation of the irrigation system for plot 6. As a result, the ETI of the conductivity prototype was less than expected. Insulating panels have been applied to the PCB to avoid the noise as a hardware method.

4.2.2 Qualitative Field Testing Results for April 15th 2015

Two cubic float prototypes, two conductivity prototypes and two control plots without irrigation runoff sensors have been tested. The irrigation specifications for those tests are shown in Table 11.

Table 11. Irrigation Specifications of Test on April 15th 2015

| Start Time | 7:30 AM |
|---------------------------------|-----------------------------|
| Effective Irrigation Time (EIT) | 30 minutes |
| Wait Time (WT) | 20 minutes |
| | 2 (Conductivity Prototype), |
| | 4 (Cubic Float Prototype), |
| # of Tested Plot | 5 (Cubic Float Prototype), |
| # Of Tested Flot | 6 (Conductivity Prototype), |
| | 7 (Control Plot), |
| | 8 (Control Plot) |

The results of the irrigation are shown in Figure 46 - 57.

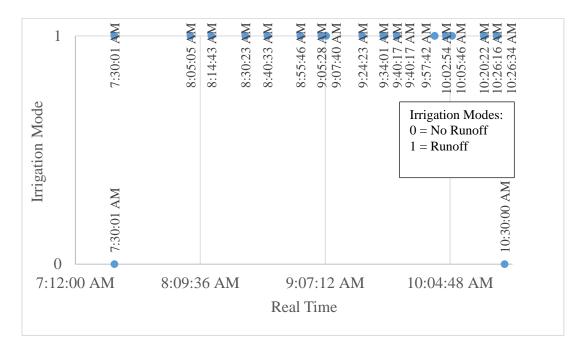


Figure 46. The Runoff Status of Plot 2 (Conductivity Prototype) on April 15th 2015

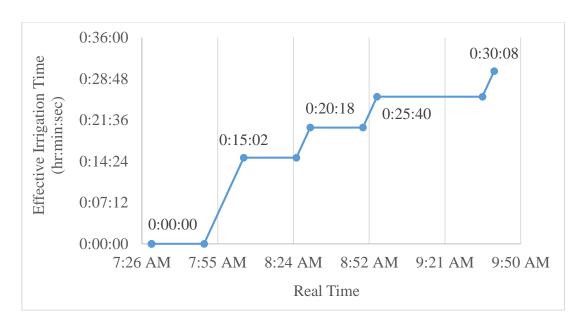


Figure 47. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on April $15^{\rm th}~2015$

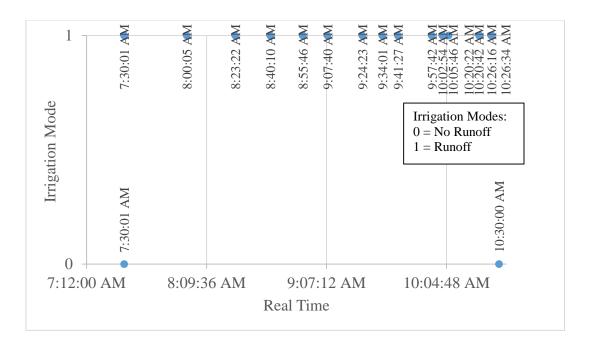


Figure 48. The Runoff Status of Plot 4 (Cubic Float Prototype) on April 15th 2015

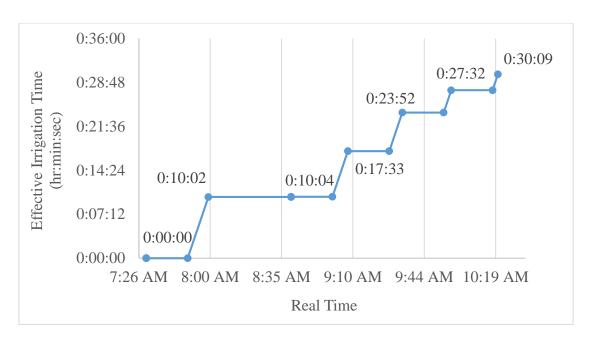


Figure 49. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on April 15th 2015

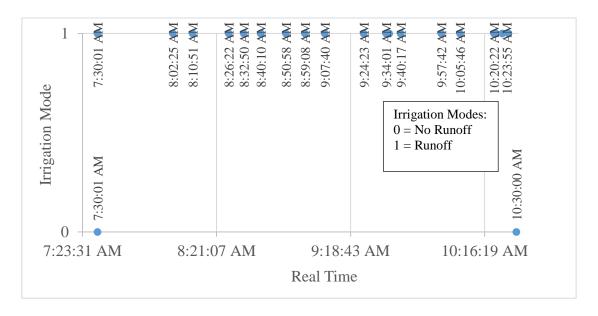


Figure 50. The Runoff Status of Plot 5 (Cubic Float Prototype) on April 15th 2015

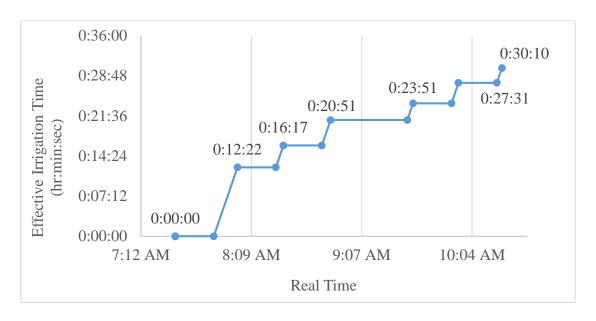


Figure 51. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on April $15^{\rm th}~2015$

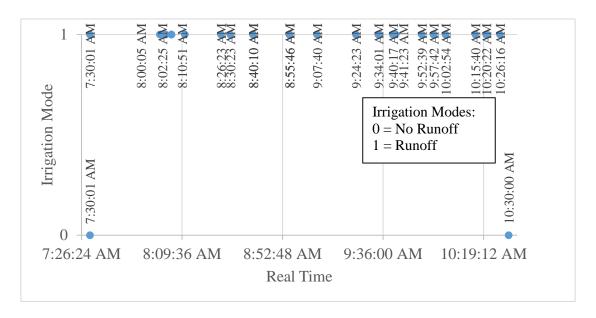


Figure 52. The Runoff Status of Plot 6 (Conductivity Prototype) on April 15th 2015

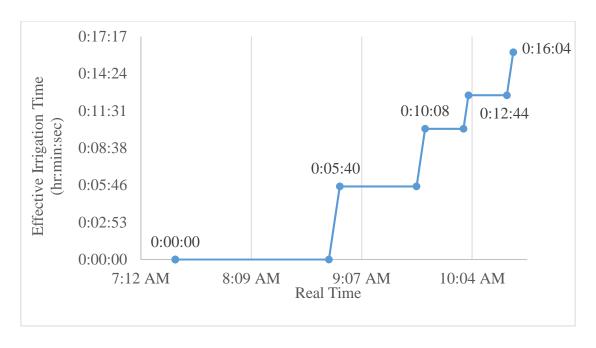


Figure 53. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on April $15^{\rm th}~2015$

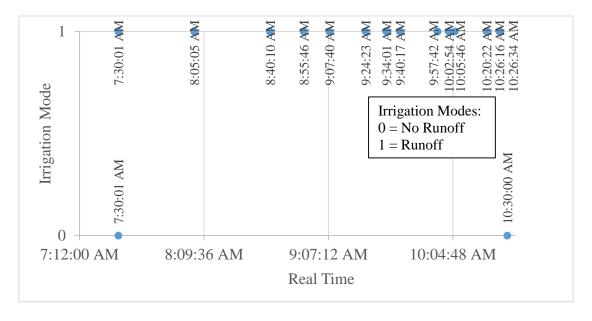


Figure 54. The Runoff Status of Plot 7 (Control) on April 15th 2015

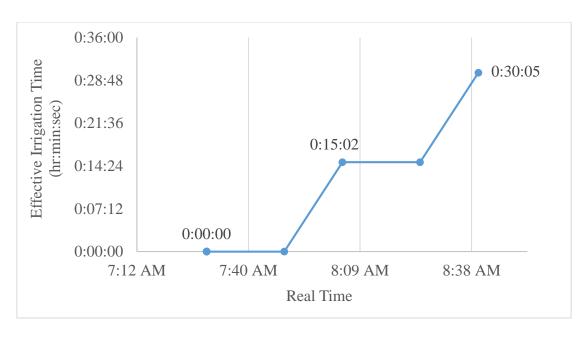


Figure 55. The Effective Irrigation Time of Plot 7 (Control) on April 15th 2015

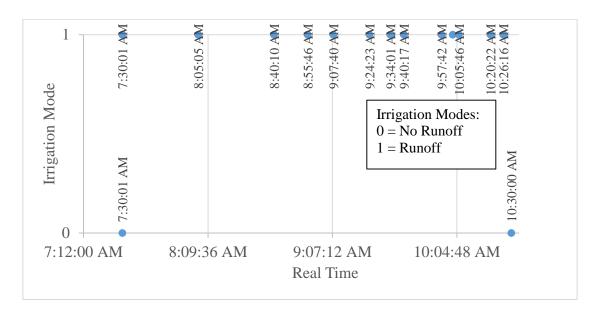


Figure 56. The Runoff Status of Plot 8 (Control) on April 15th 2015

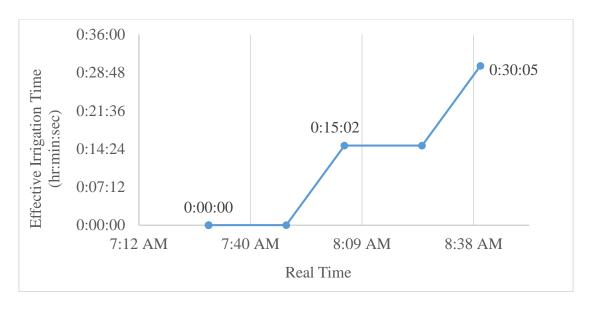


Figure 57. The Effective Irrigation Time of Plot 8 (Control) on April 15th 2015

Based on the irrigation results, the cubic float prototypes and the conductivity prototypes have shown the capability of detecting runoff and fulfilling the complete cycle-soaking. Also, all the prototypes have more accumulated WT than the control plots, allowing more time for water absorption. However, the pause at the beginnings of each irrigation cycle as shown in the figures and during the irrigation of the control plots shows the interruption of irrigation which was triggered by noise and interference as it was the case for the tests conducted on April 8th. The noise-related problem was eliminated by analyzing the runoff signal over a 5 minute period using the data analysis software. The software basically was able to calculate the average value of the runoff signal, and if its value exceeded 4.5 volts, then the runoff was assumed to take place.

4.2.3 Qualitative Field Testing Results for June 16th 2015

Two cubic float prototypes, one conductivity prototype, one paddle wheel prototype and two control plots without irrigation runoff sensors have been tested. The irrigation specifications for the tests are shown in Table 12.

Table 12. Irrigation Specifications of Test on June 16th 2015

| Start Time | 8:00 AM |
|---------------------------------|--|
| Effective Irrigation Time (EIT) | 1 hour |
| Wait Time (WT) | 20 minutes |
| # of Tested Plot | 2 (Conductivity Prototype), 3 (Paddle Wheel Prototype), 4 (Cubic Float Prototype), 5 (Cubic Float Prototype), 7 (Control Plot), 8 (Control Plot) |

The results of the irrigation are shown in Figure 58 - 69.

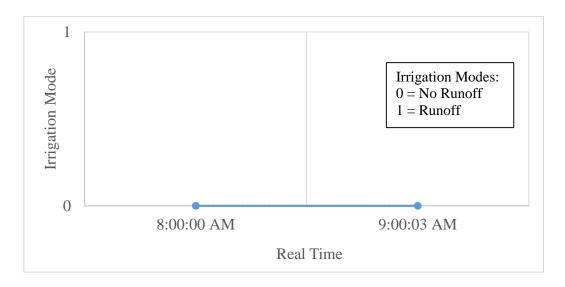


Figure 58. The Runoff Status of Plot 2 (Conductivity Prototype) on June 16th 2015

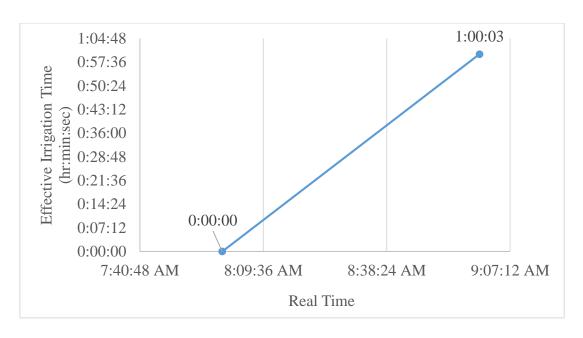


Figure 59. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on June $16^{\text{th}}\,2015$

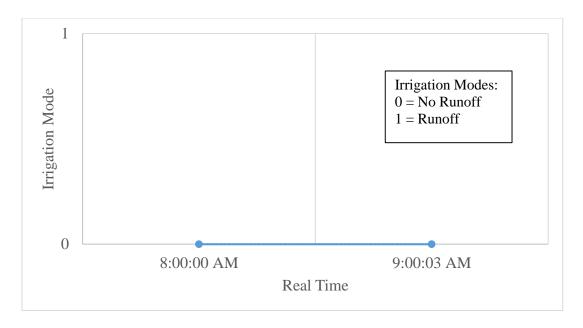


Figure 60. The Runoff Status of Plot 3 (Paddle Wheel Prototype) on June 16th 2015

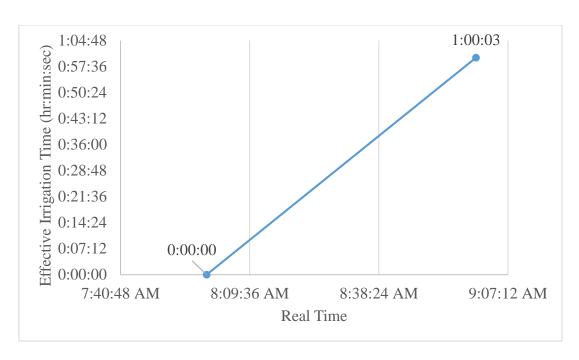


Figure 61. The Effective Irrigation Time of Plot 3 (Paddle Wheel Prototype) on June $16^{\rm th}~2015$

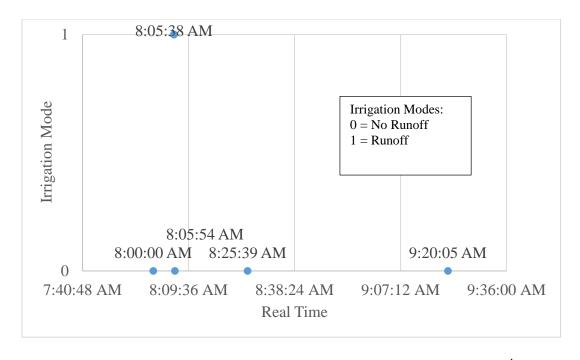


Figure 62. The Runoff Status of Plot 4 (Cubic Float Prototype) on June 16th 2015

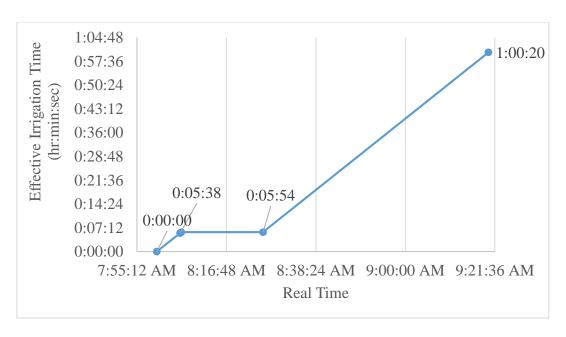


Figure 63. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on June $16^{\rm th}~2015$

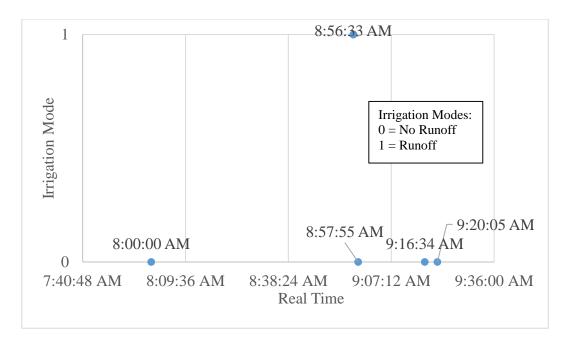


Figure 64. The Runoff Status of Plot 5 (Cubic Float Prototype) on June 16th 2015

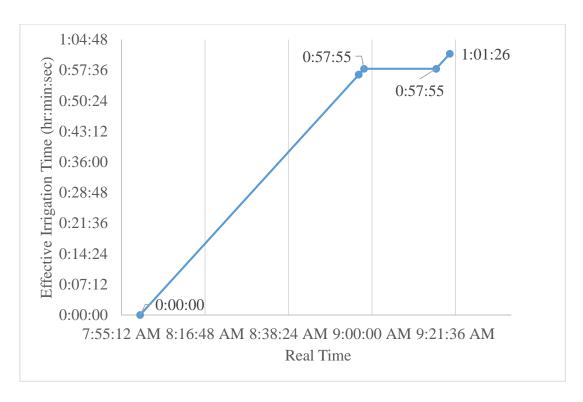


Figure 65. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on June $16^{\rm th}~2015$

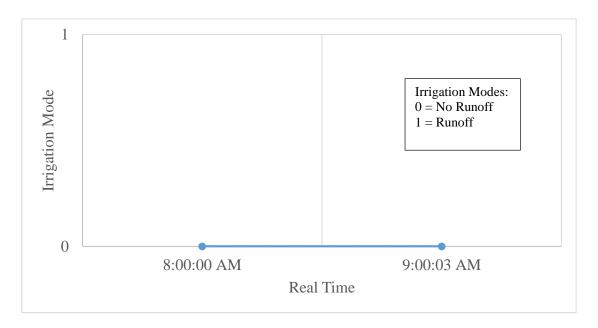


Figure 66. The Runoff Status of Plot 7 (Control) on June 16^{th} 2015

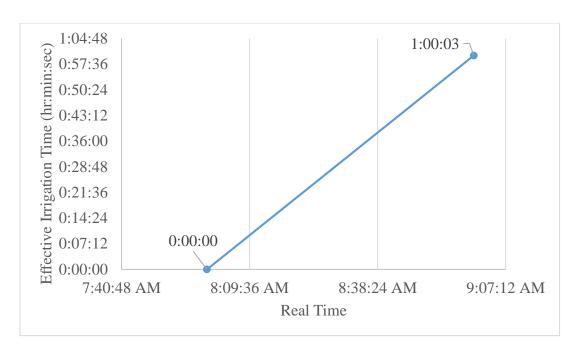


Figure 67. The Effective Irrigation Time of Plot 7 (Control) on June 16th 2015

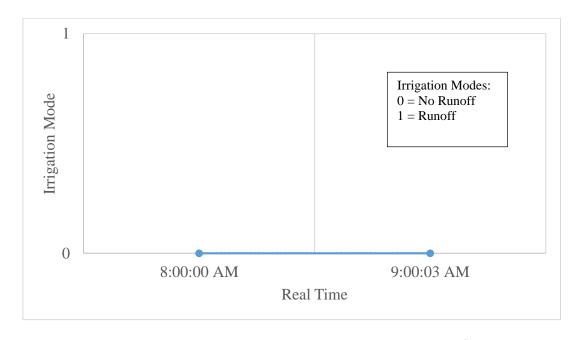


Figure 68. The Runoff Status of Plot 8 (Control) on June 16^{th} 2015

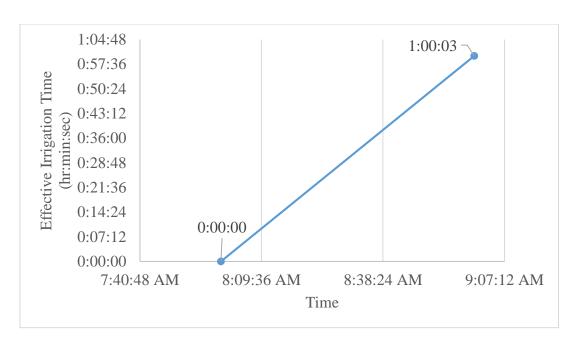


Figure 69. The Effective Irrigation Time of Plot 8 (Control) on June 16th 2015

Only the cubic float prototypes have been activated by the runoff which led to a pause of the irrigation cycle as expected. The paddle wheel prototype and the conductivity prototype have not been activated and thus plots 2, 3 and the two control plots have the same effective irrigation time. The conductivity prototype had clogging issue during the test, while the paddle wheel prototype has been water-damaged. However, no evidence of the noise and interference has been noticed compared to the former two tests. Therefore, the implemented software based criterion for identify noise versus signal is adequate for field implementation.

4.2.4 Qualitative Field Testing Results for June 24th 2015

Two cubic float prototypes, two conductivity prototypes and two control plots without irrigation runoff sensors have been tested. The irrigation specifications have been listed, as shown in Table 13.

Table 13. Irrigation Specifications of Test on June 24th 2015

| Start Time | 8:00 AM | |
|---------------------------------|-----------------------------|--|
| Effective Irrigation Time (EIT) | 1 hour | |
| Wait Time (WT) | 20 minutes | |
| | 2 (Conductivity Prototype), | |
| | 4 (Cubic Float Prototype), | |
| # of Tested Plot | 5 (Cubic Float Prototype), | |
| # of Tested Flot | 6 (Conductivity Prototype), | |
| | 7 (Control Plot), | |
| | 8 (Control Plot) | |

The results of the irrigation are shown in Figure 70 - 81.

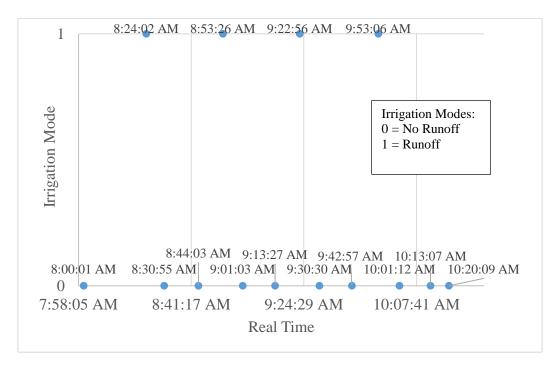


Figure 70. The Runoff Status of Plot 2 (Conductivity Prototype) on June 24th 2015

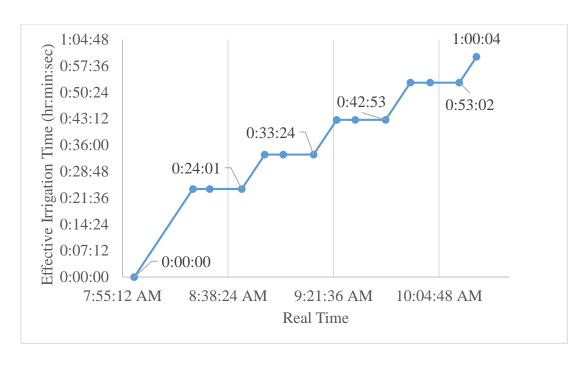


Figure 71. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on June 24^{th} 2015

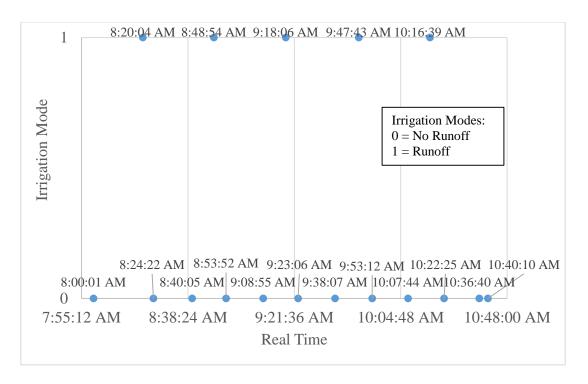


Figure 72. The Runoff Status of Plot 4 (Cubic Float Prototype) on June 24th 2015

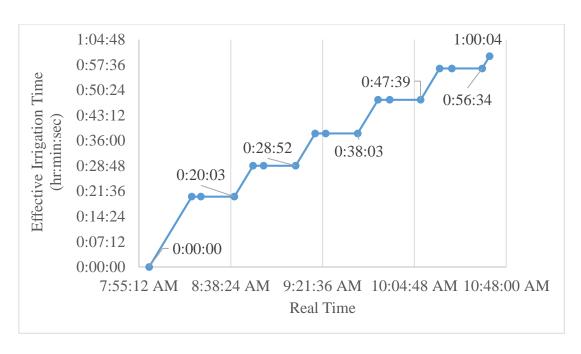


Figure 73. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on June $24^{th}\ 2015$

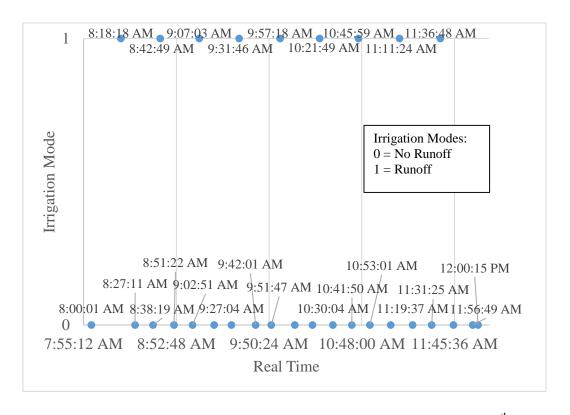


Figure 74. The Runoff Status of Plot 5 (Cubic Float Prototype) on June 24th 2015

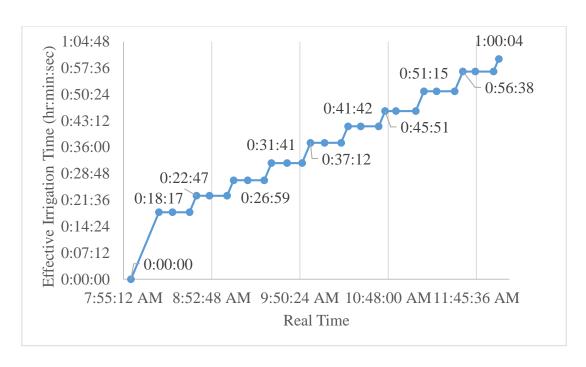


Figure 75. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on June 24th 2015

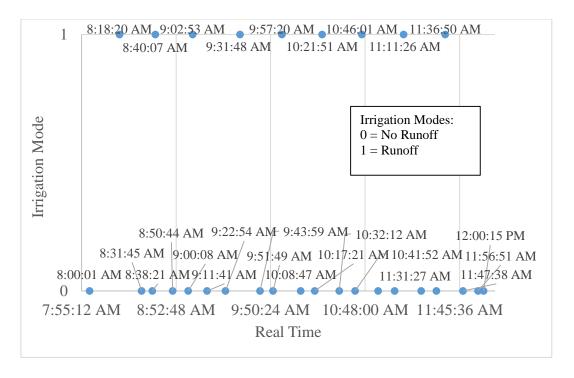


Figure 76. The Runoff Status of Plot 6 (Conductivity Prototype) on June 24th 2015

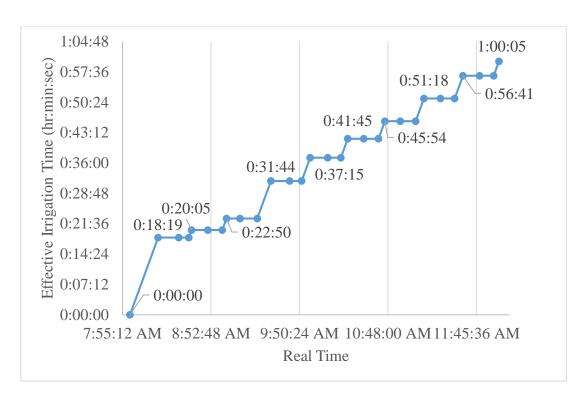


Figure 77. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on June $24^{th}\ 2015$

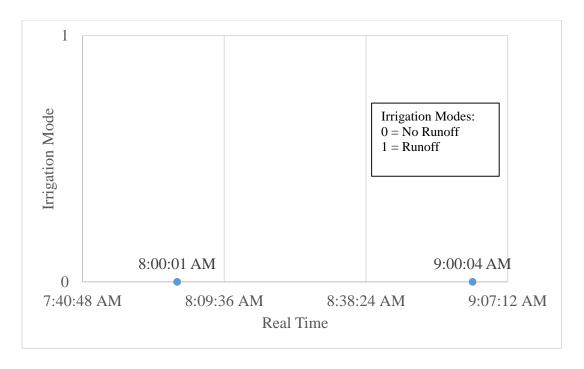


Figure 78. The Runoff Status of Plot 7 (Control) on June 24th 2015

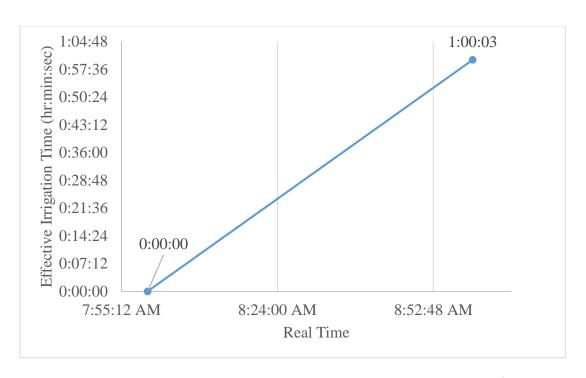


Figure 79. The Effective Irrigation Time of Plot 7 (Control) on June 24th 2015

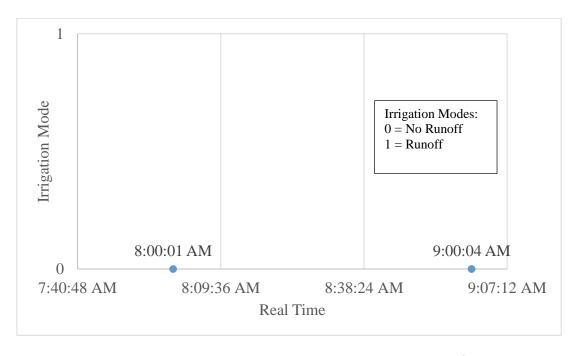


Figure 80. The Runoff Status of Plot 8 (Control) on June 24th 2015

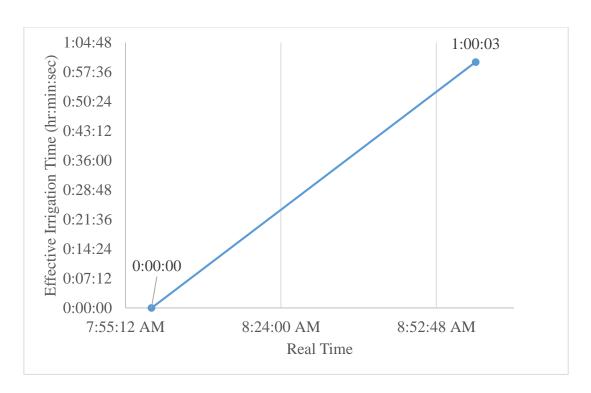


Figure 81. The Effective Irrigation Time of Plot 8 (Control) on June 24th 2015

Both the cubic float prototypes and the conductivity prototypes have shown the capability of detecting runoff and fulfilling the complete cycle-soaking. In the meantime, the cubic float prototypes have exhibited to be more sensitive than the conductivity prototype, allowing more WT during the irrigation cycle.

4.2.5 Qualitative Field Testing Results for June 30th 2015

Two cubic float prototypes, two conductivity prototypes and two control plots without irrigation runoff sensors have been tested. The irrigation specifications have been listed, as shown in Table 14.

Table 14. Irrigation Specifications of Test on June 30th 2015

| Start Time | 8:00 AM |
|---------------------------------|-----------------------------|
| Effective Irrigation Time (EIT) | 1 hour |
| Wait Time (WT) | 20 minutes |
| # of Tested Plot | 2 (Conductivity Prototype), |
| | 4 (Cubic Float Prototype), |
| | 5 (Cubic Float Prototype), |
| | 6 (Conductivity Prototype), |
| | 7 (Control Plot), |
| | 8 (Control Plot) |

The results of the irrigation are shown in Figure 82 - 93.

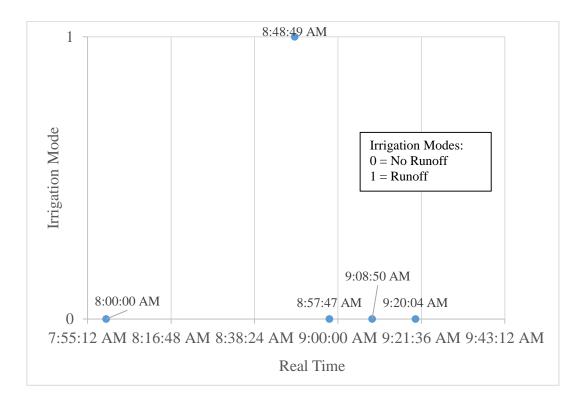


Figure 82. The Runoff Status of Plot 2 (Conductivity Prototype) on June 30th 2015

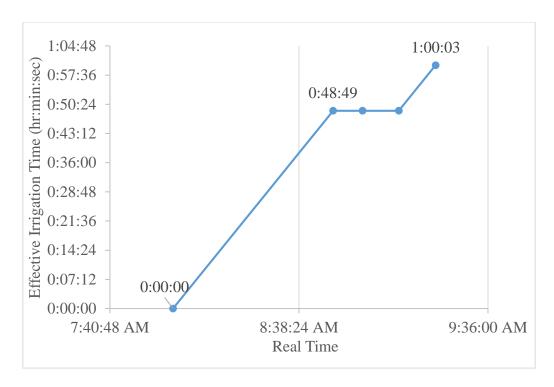


Figure 83. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on June $30^{\rm th}~2015$

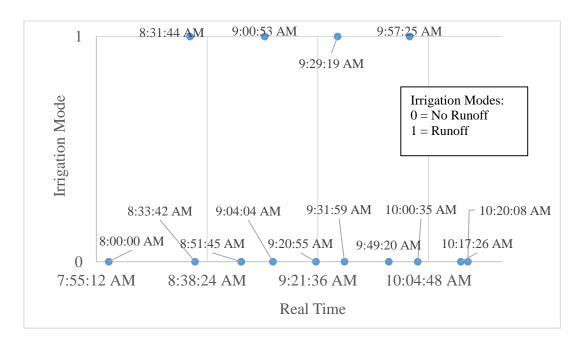


Figure 84. The Runoff Status of Plot 4 (Cubic Float Prototype) on June 30^{th} 2015

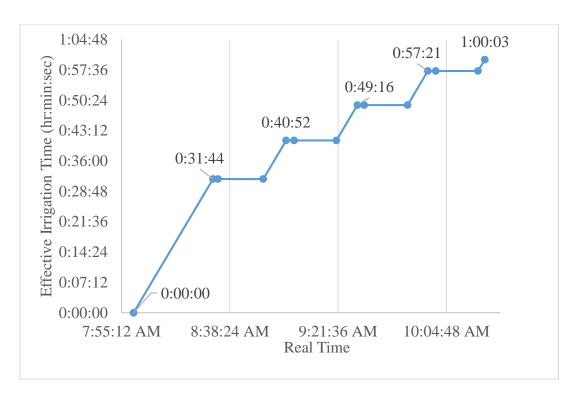


Figure 85. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on June $30^{\rm th}~2015$

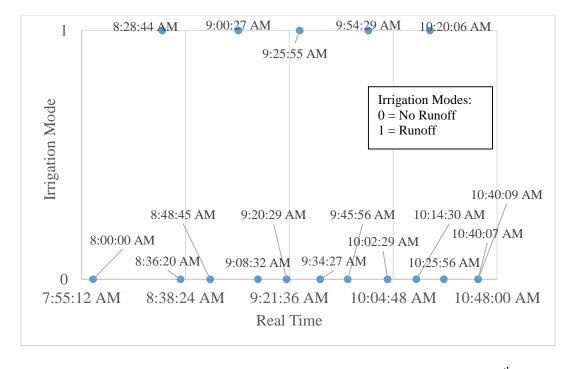


Figure 86. The Runoff Status of Plot 5 (Cubic Float Prototype) on June 30th 2015

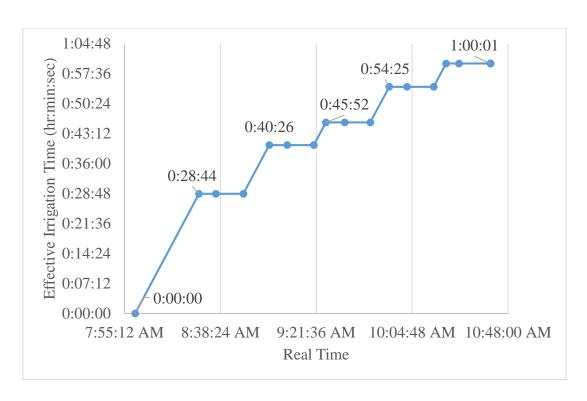


Figure 87. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on June $30^{\rm th}~2015$

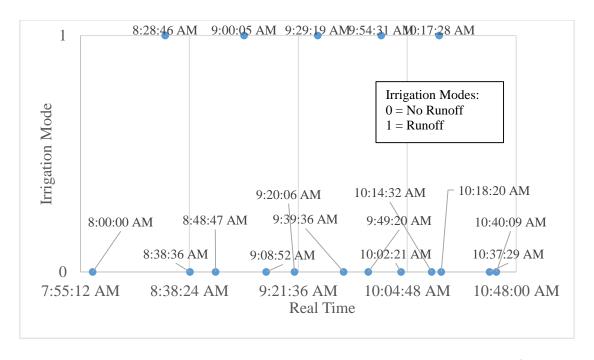


Figure 88. The Runoff Status of Plot 6 (Conductivity Prototype) on June 30th 2015

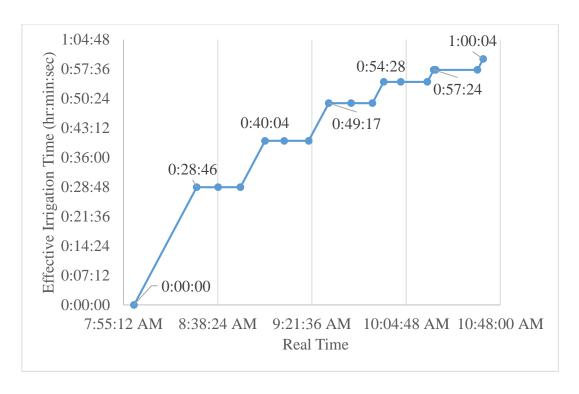


Figure 89. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on June $30^{\rm th}~2015$

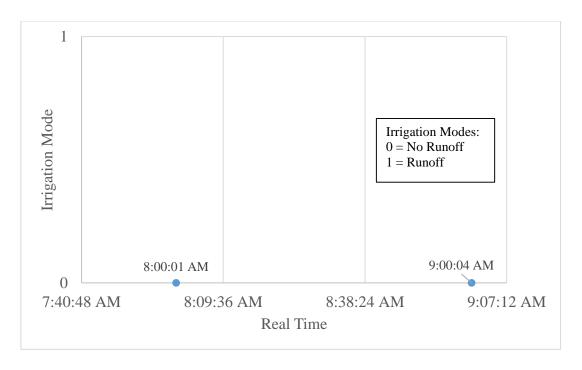


Figure 90. The Runoff Status of Plot 7 (Control) on June 30th 2015

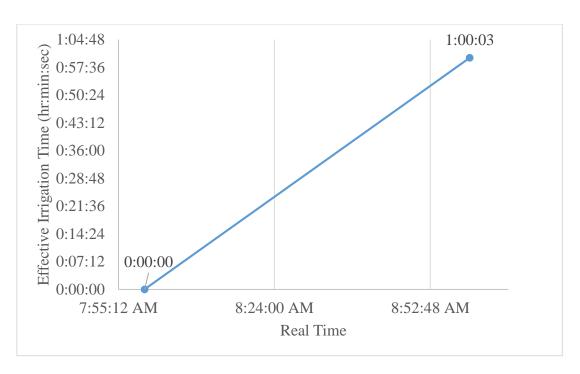


Figure 91. The Effective Irrigation Time of Plot 7 (Control) on June 30th 2015

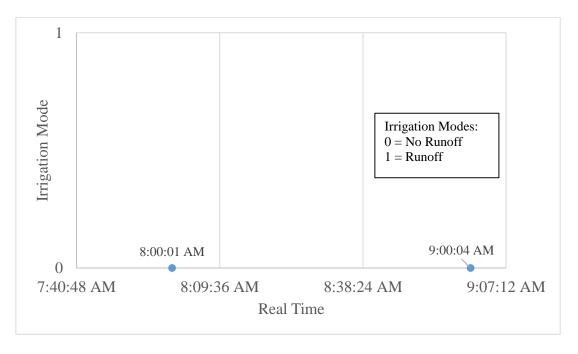


Figure 92. The Runoff Status of Plot 8 (Control) on June 30^{th} 2015

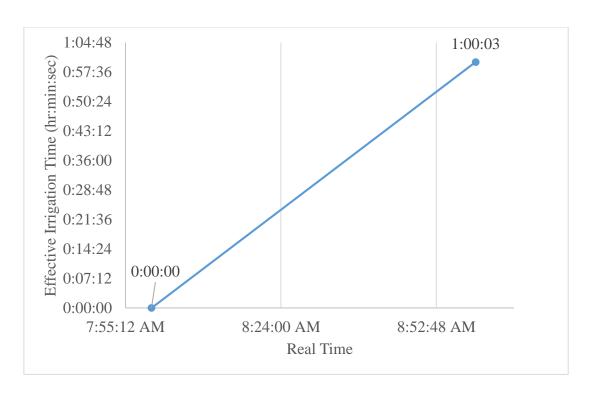


Figure 93. The Effective Irrigation Time of Plot 8 (Control) on June 30th 2015

Based on the testing results, both the cubic float prototypes and the conductivity prototypes have successfully detected runoff and paused the irrigation cycle. Similar to the former tests, the cubic float prototypes have exhibited to be more sensitive than the conductivity prototype, allowing more WT during the irrigation cycle.

4.2.6 Qualitative Field Testing Results for July 11th 2015

Two cubic float prototypes, two conductivity prototypes, one elbow float prototype and one control plot without irrigation runoff sensors have been tested. The irrigation specifications have been listed, as shown in Table 15.

Table 15. Irrigation Specifications of Test on July 11th 2015

| Start Time | 8:00 AM |
|---------------------------------|-----------------------------|
| Effective Irrigation Time (EIT) | 1 hour |
| Wait Time (WT) | 20 minutes |
| # of Tested Plot | 2 (Conductivity Prototype), |
| | 4 (Cubic Float Prototype), |
| | 5 (Cubic Float Prototype), |
| | 6 (Conductivity Prototype), |
| | 7 (Control Plot), |
| | 9 (Elbow Float Plot) |

The results of the irrigation are shown in Figure 94 - 105.

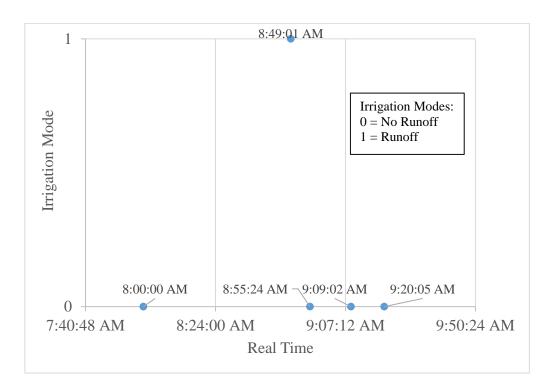


Figure 94. The Runoff Status of Plot 2 (Conductivity Prototype) on July 11th 2015

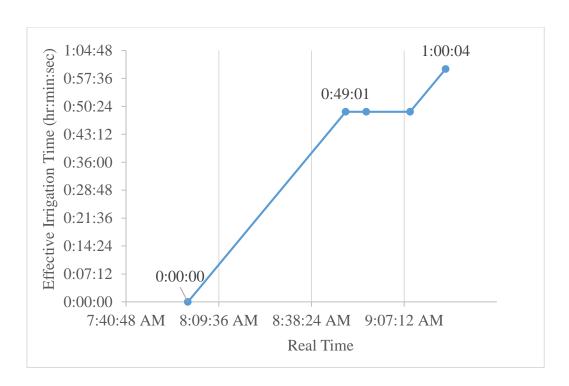


Figure 95. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on July $11^{\rm th}~2015$

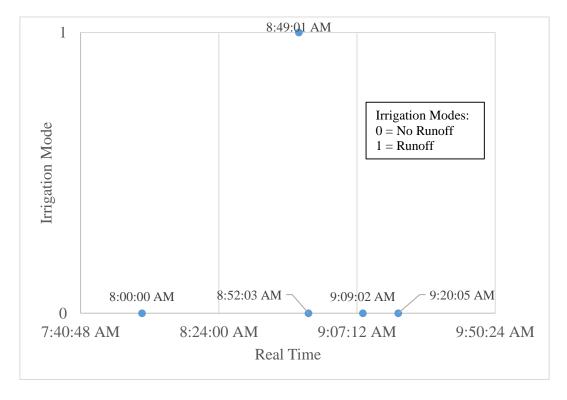


Figure 96. The Runoff Status of Plot 4 (Cubic Float Prototype) on July 11th 2015

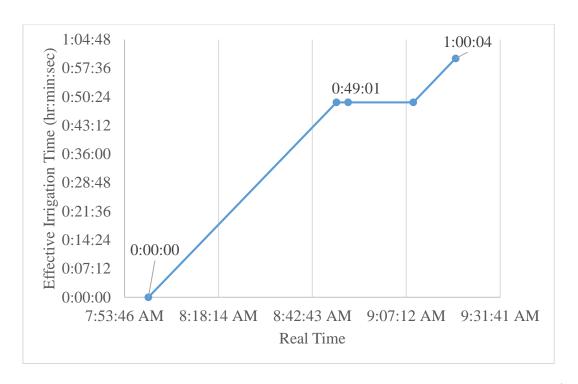


Figure 97. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on July 11th 2015

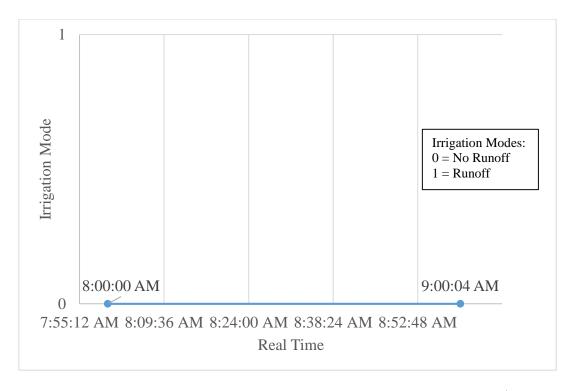


Figure 98. The Runoff Status of Plot 5 (Cubic Float Prototype) on July 11th 2015

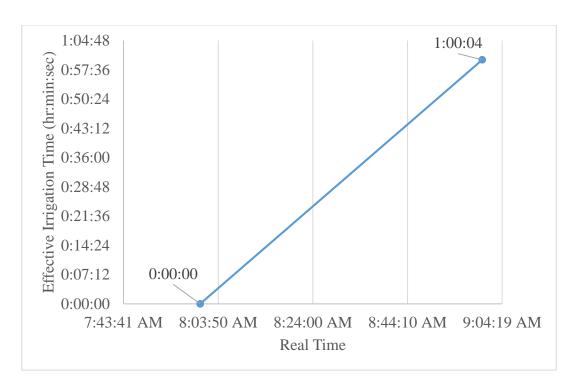


Figure 99. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on July 11th 2015

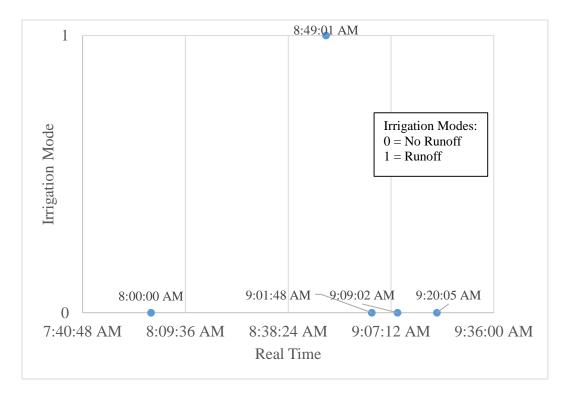


Figure 100. The Runoff Status of Plot 6 (Conductivity Prototype) on July 11th 2015

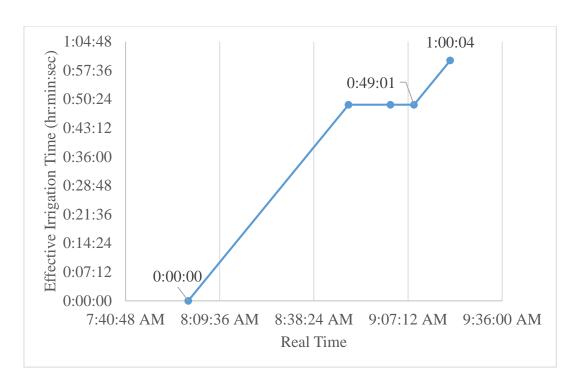


Figure 101. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on July $11^{\rm th}~2015$

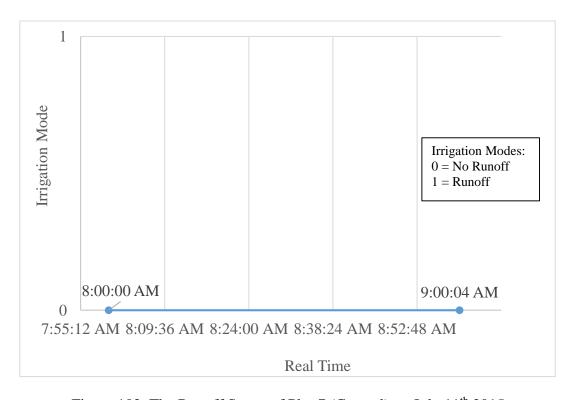


Figure 102. The Runoff Status of Plot 7 (Control) on July 11th 2015

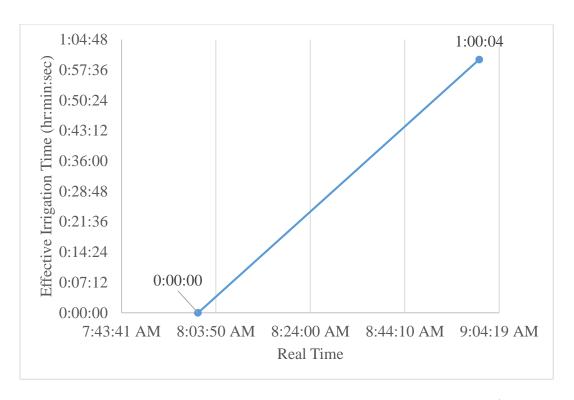


Figure 103. The Effective Irrigation Time of Plot 7 (Control) on July 11th 2015

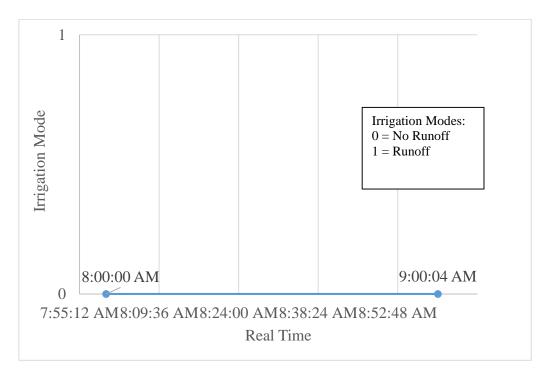


Figure 104. The Runoff Status of Plot 9 (Elbow Float Prototype) on July 11^{th} 2015

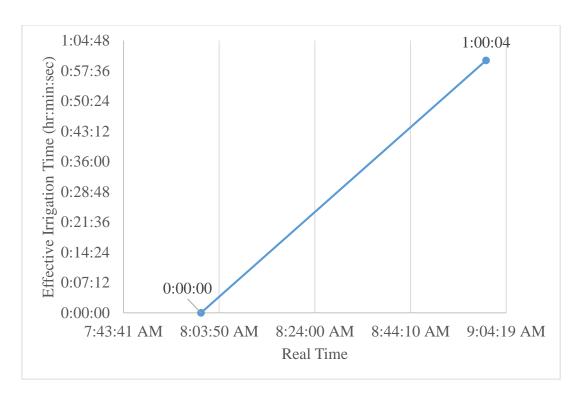


Figure 105. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on July $11^{\rm th}~2015$

During the tests, only one cubic float prototype and two conductivity prototypes have paused irrigation based on detecting runoff. The other plots started to have runoff after irrigation stopped. The dry and hot weather on that day may be responsible for the results.

4.2.7 Qualitative Field Testing Results for July 14th 2015

Two cubic float prototypes, two conductivity prototypes, one elbow float prototype and one control plot without irrigation runoff sensors have been tested. The irrigation specifications have been listed, as shown in Table 16.

Table 16. Irrigation Specifications of Test on July 14th 2015

| Start Time | 8:00 AM |
|---------------------------------|-----------------------------|
| Effective Irrigation Time (EIT) | 1.5 hour |
| Wait Time (WT) | 20 minutes |
| # of Tested Plot | 2 (Conductivity Prototype), |
| | 4 (Cubic Float Prototype), |
| | 5 (Cubic Float Prototype), |
| | 6 (Conductivity Prototype), |
| | 7 (Control Plot), |
| | 9 (Elbow Float Plot) |

The results of the irrigation are shown in Figure 106 - 117.

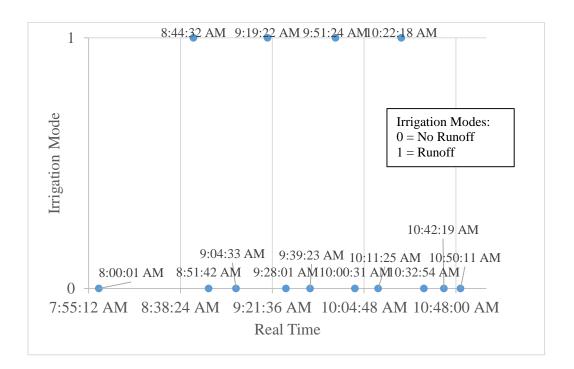


Figure 106. The Runoff Status of Plot 2 (Conductivity Prototype) on July 14th 2015

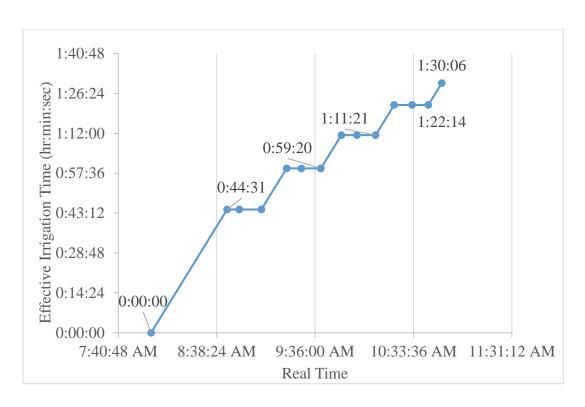


Figure 107. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on July $14^{\rm th}~2015$

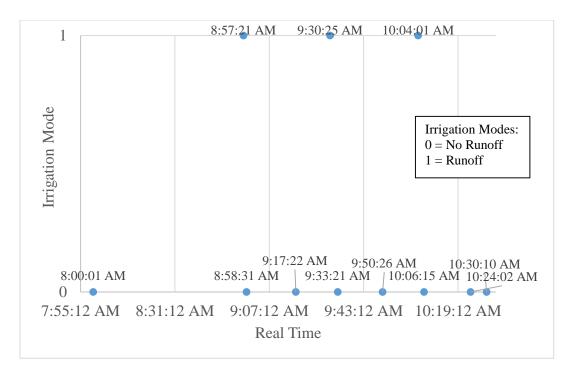


Figure 108. The Runoff Status of Plot 4 (Cubic Float Prototype) on July 14th 2015

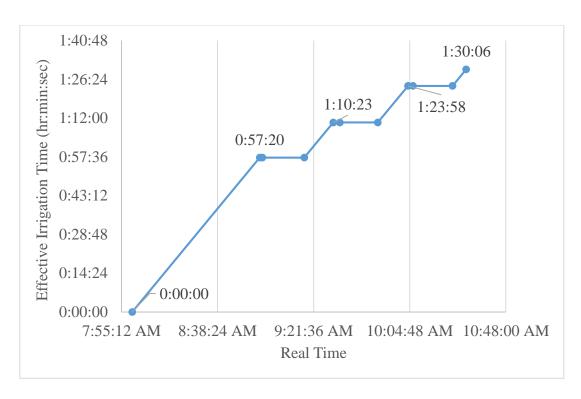


Figure 109. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on July $14^{\rm th}~2015$

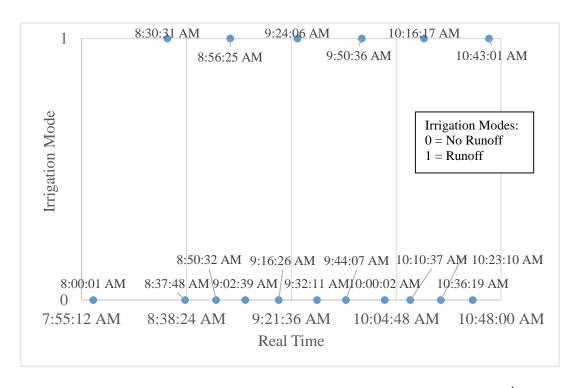


Figure 110. The Runoff Status of Plot 5 (Cubic Float Prototype) on July 14th 2015

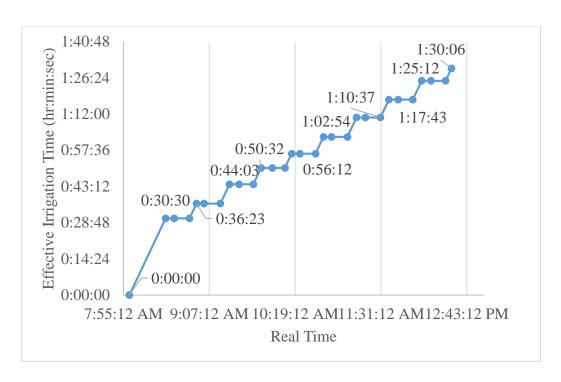


Figure 111. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on July 14th 2015

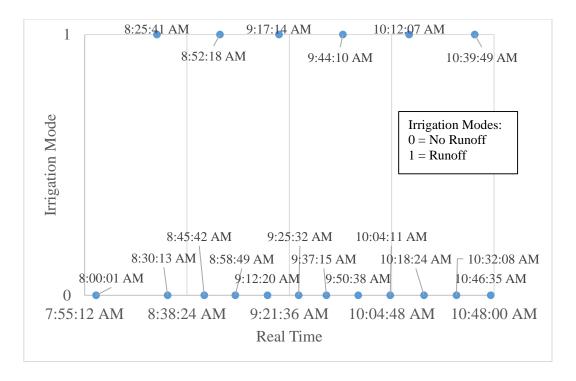


Figure 112. The Runoff Status of Plot 6 (Conductivity Prototype) on July 14th 2015

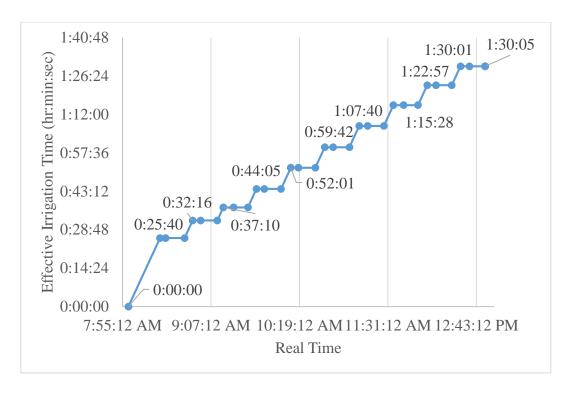


Figure 113. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on July $14^{th}\ 2015$

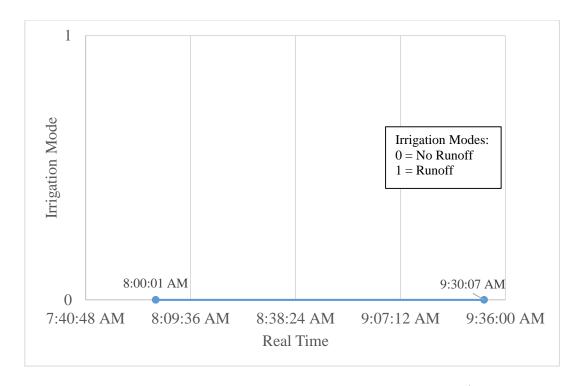


Figure 114. The Runoff Status of Plot 7 (Control) on July 14th 2015

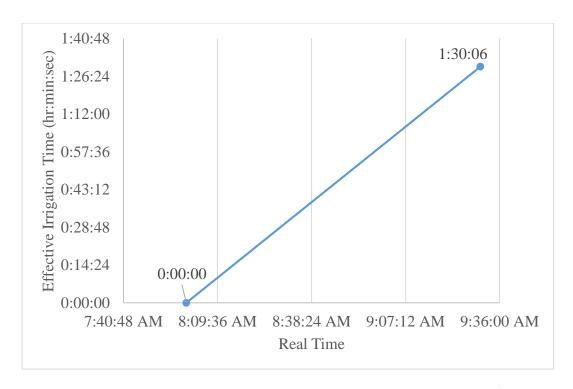


Figure 115. The Effective Irrigation Time of Plot 7 (Control) on July 14th 2015

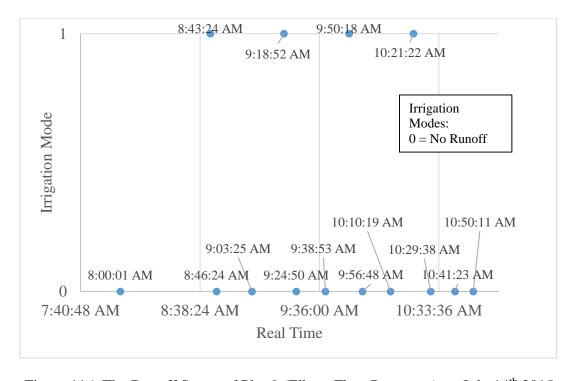


Figure 116. The Runoff Status of Plot 9 (Elbow Float Prototype) on July 14th 2015

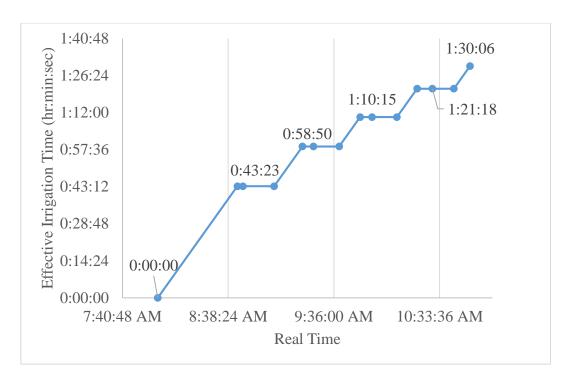


Figure 117. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on July 14th 2015

Based on the testing results, both the conductivity prototypes, the cubic float prototypes and the elbow float prototype have detected runoff and paused the irrigation. During these tests, the conductivity prototypes and the cubic float prototypes have shown similar sensitivity to runoff, which is higher than the elbow float prototype.

4.2.8 Qualitative Field Testing Results for July 21st 2015

Two cubic float prototypes, two conductivity prototypes, one elbow float prototype and one control plot without irrigation runoff sensors have been tested. The irrigation specifications have been listed, as shown in Table 17.

Table 17. Irrigation Specifications of Test on July 21st 2015

| Start Time | 8:00 AM |
|---------------------------------|-----------------------------|
| Effective Irrigation Time (EIT) | 1.5 hour |
| Wait Time (WT) | 20 minutes |
| # of Tested Plot | 2 (Conductivity Prototype), |
| | 4 (Cubic Float Prototype), |
| | 5 (Cubic Float Prototype), |
| | 6 (Conductivity Prototype), |
| | 7 (Control Plot), |
| | 9 (Elbow Float Plot) |

The results of the irrigation are shown in Figure 118 - 129.

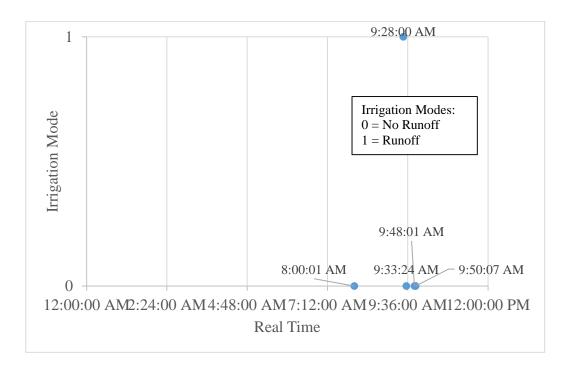


Figure 118. The Runoff Status of Plot 2 (Conductivity Prototype) on July 21st 2015

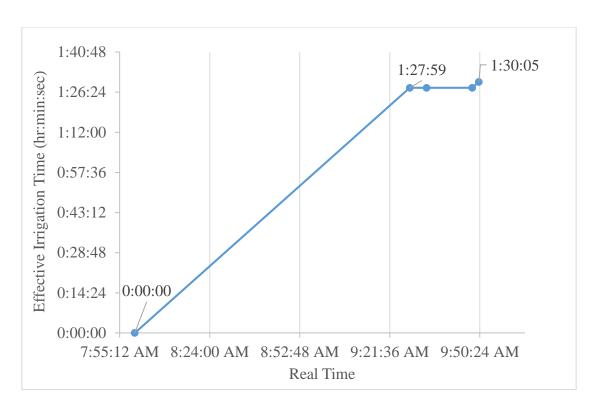


Figure 119. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on July $21^{\rm st}$ 2015

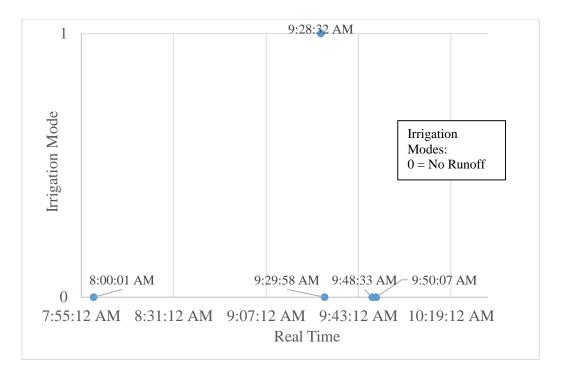


Figure 120. The Runoff Status of Plot 4 (Cubic Float Prototype) on July 21st 2015

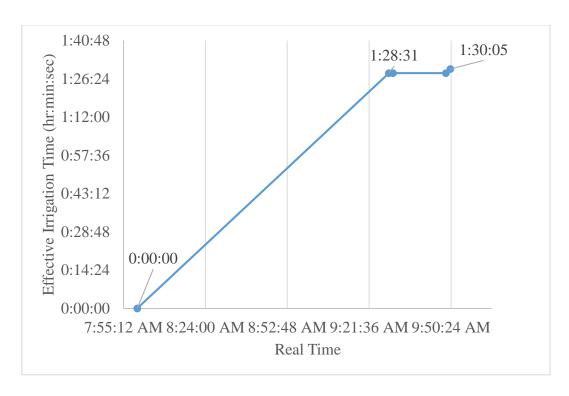


Figure 121. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on July $21^{\rm st}$ 2015

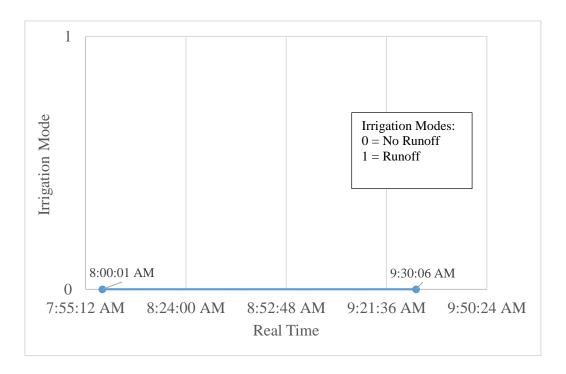


Figure 122. The Runoff Status of Plot 5 (Cubic Float Prototype) on July 21st 2015

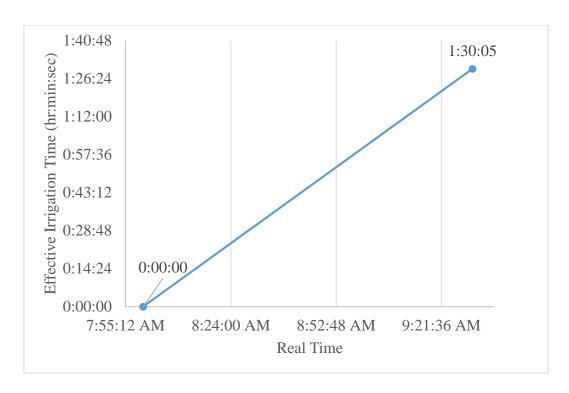


Figure 123. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on July $21^{\rm st}~2015$

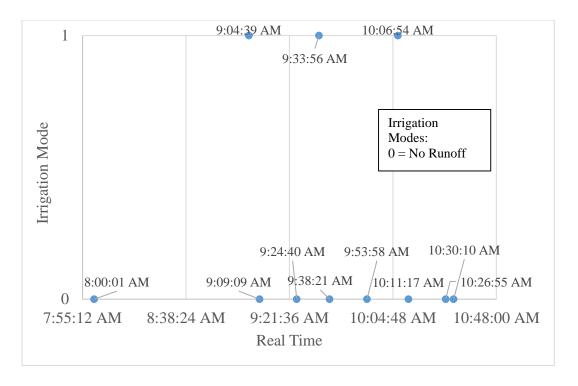


Figure 124. The Runoff Status of Plot 6 (Conductivity Prototype) on July 21st 2015

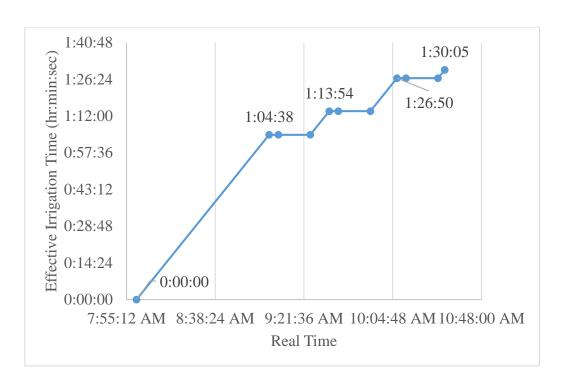


Figure 125. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on July $21^{\rm st}\ 2015$

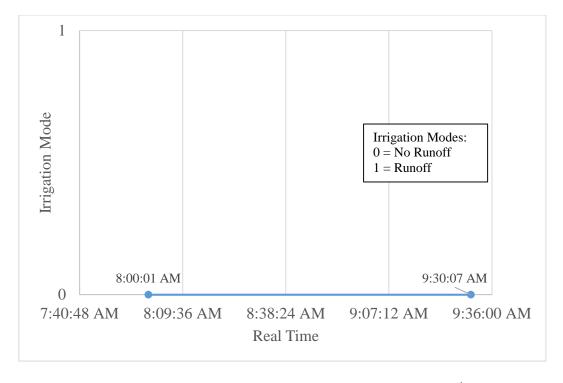


Figure 126. The Runoff Status of Plot 7 (Control) on July 21st 2015

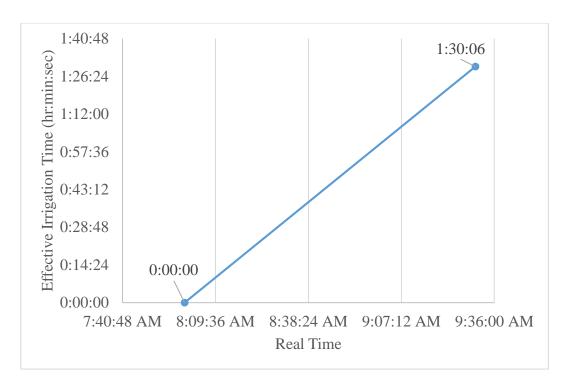


Figure 127. The Effective Irrigation Time of Plot 7 (Control) on July 21st 2015

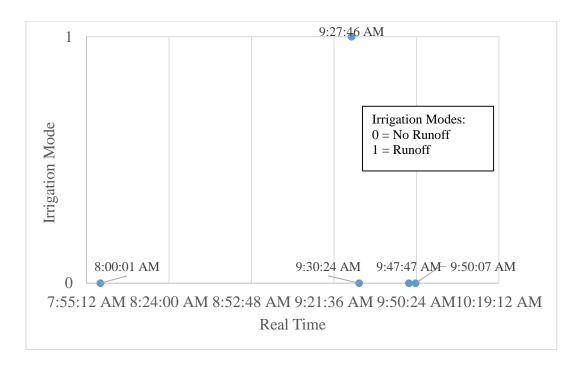


Figure 128. The Runoff Status of Plot 9 (Elbow Float Prototype) on July 21st 2015

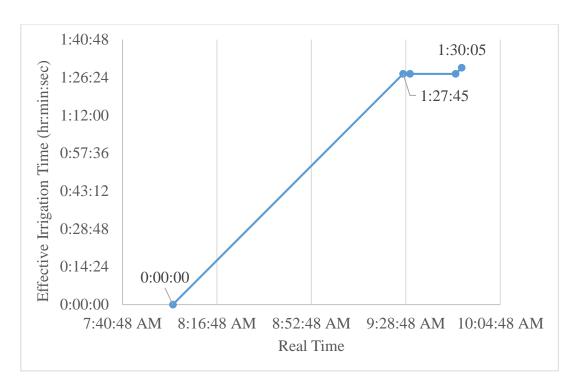


Figure 129. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on July $21^{\rm st}$ 2015

From the testing results, only one cubic float prototype has not been activated by runoff during the test during the 30 minute of irrigation. However, it has detected runoff just after the irrigation stopped. Most irrigation runoff sensor prototypes have detected runoff when approaching the end of the irrigation with plot 4 (cubic float prototype) as an exception, which showed the higher sensitivity of this prototype.

4.2.9 Qualitative Field Testing Results for Aug 4th 2015

Two cubic float prototypes, two conductivity prototypes, one elbow float prototype and one control plot without irrigation runoff sensors have been tested. The irrigation specifications have been listed, as shown in Table 18.

Table 18. Irrigation Specifications of Test on Aug 4th 2015

| Start Time | 8:00 AM |
|---------------------------------|-----------------------------|
| Effective Irrigation Time (EIT) | 1.5 hour |
| Wait Time (WT) | 20 minutes |
| # of Tested Plot | 2 (Conductivity Prototype), |
| | 4 (Cubic Float Prototype), |
| | 5 (Cubic Float Prototype), |
| | 6 (Conductivity Prototype), |
| | 7 (Control Plot), |
| | 9 (Elbow Float Plot) |

The results of the irrigation are shown in Figure 130 - 141.

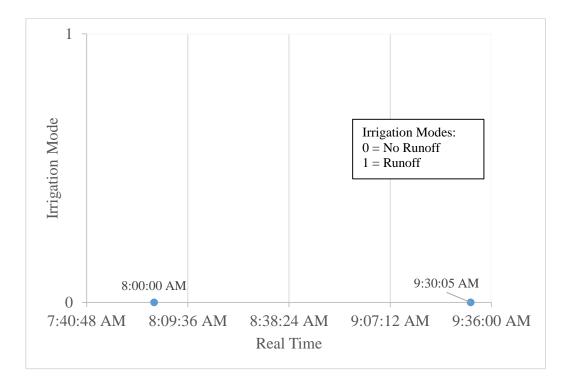


Figure 130. The Runoff Status of Plot 2 (Conductivity Prototype) on Aug 4th 2015

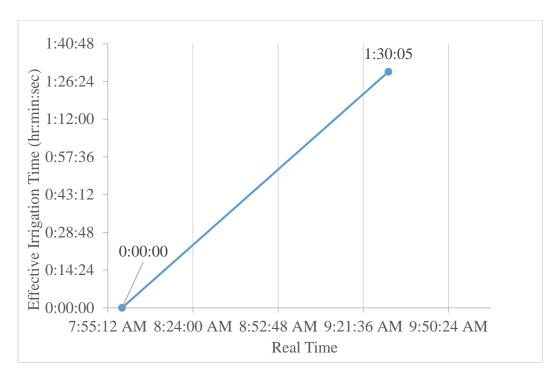


Figure 131. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on Aug 4^{th} 2015

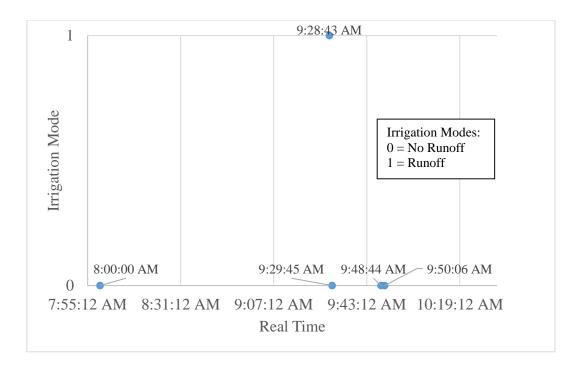


Figure 132. The Runoff Status of Plot 4 (Cubic Float Prototype) on Aug 4^{th} 2015

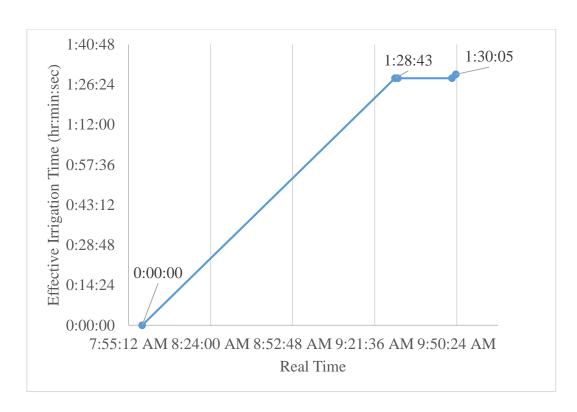


Figure 133. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on Aug 4th 2015

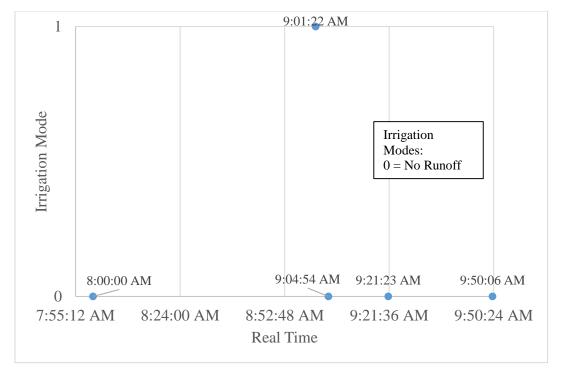


Figure 134. The Runoff Status of Plot 5 (Cubic Float Prototype) on Aug 4^{th} 2015 144

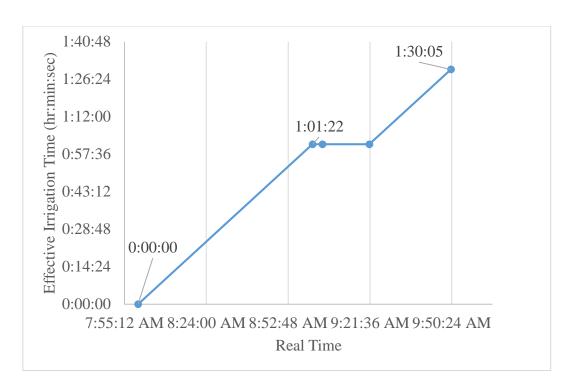


Figure 135. The Effective Irrigation Time of Plot 5 (Cubic Float Prototype) on Aug 4th 2015

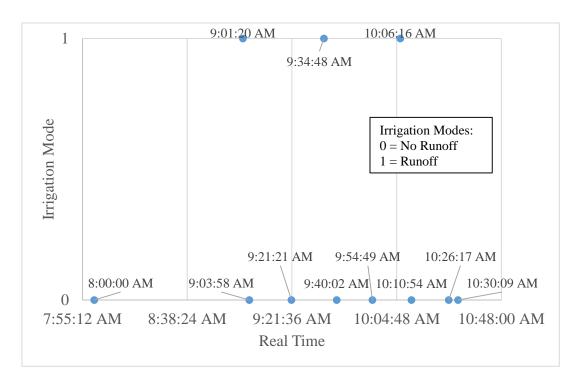


Figure 136. The Runoff Status of Plot 6 (Conductivity Prototype) on Aug 4th 2015

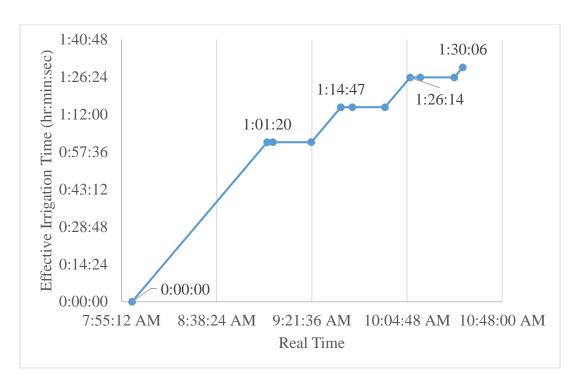


Figure 137. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on Aug 4^{th} 2015

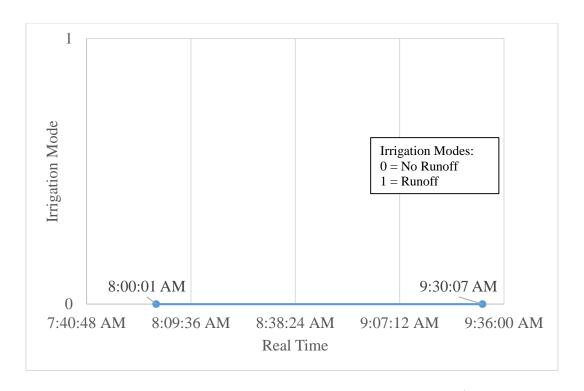


Figure 138. The Runoff Status of Plot 7 (Control) on Aug 4th 2015

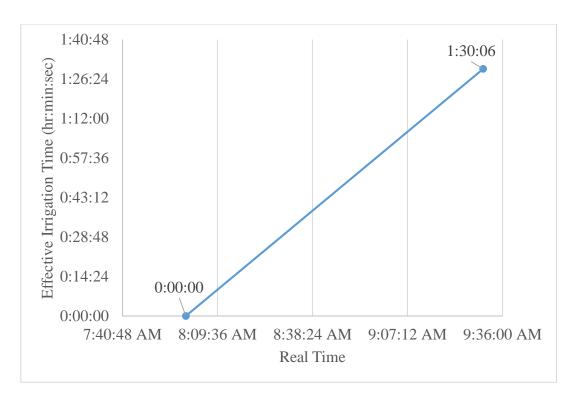


Figure 139. The Effective Irrigation Time of Plot 7 (Control) on Aug 4th 2015

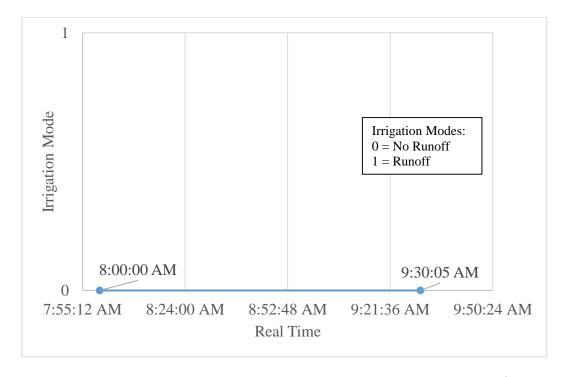


Figure 140. The Runoff Status of Plot 9 (Elbow Float Prototype) on Aug 4th 2015

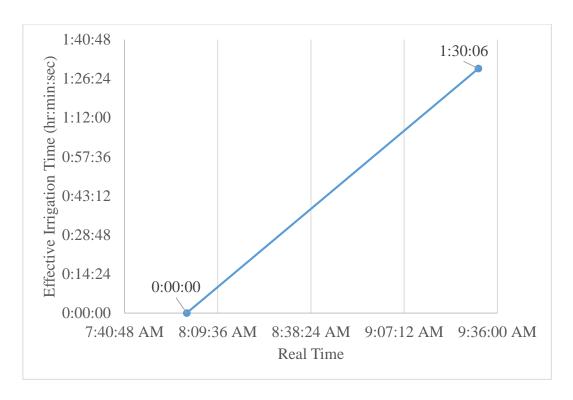


Figure 141. The Effective Irrigation Time of Plot 9 (Elbow Float Prototype) on Aug 4th 2015

Based on the irrigation results, one conductivity prototype and one elbow float prototype have not detected runoff and did not pause the irrigation cycle. The malfunctioning conductivity prototype was found to be clogged by debris while the vertical float sensor in the elbow float prototype has been found broken. The conductivity prototype was fixed once it was cleaned to remove the debris that was clogging it.

4.2.10 Qualitative Field Testing Results for Aug 25th 2015

One cubic float prototypes, two conductivity prototypes and two control plots without irrigation runoff sensors have been tested. The irrigation specifications have been listed, as shown in Table 19.

Table 19. Irrigation Specifications of Test on Aug 25th 2015

| Start Time | 8:00 AM |
|---------------------------------|-----------------------------|
| Effective Irrigation Time (EIT) | 1.5 hour |
| Wait Time (WT) | 20 minutes |
| | 2 (Conductivity Prototype), |
| | 4 (Cubic Float Prototype), |
| # of Tested Plot | 6 (Conductivity Prototype), |
| | 7 (Control Plot), |
| | 8 (Control Plot) |

The results of the irrigation are shown in Figure 142 - 151.

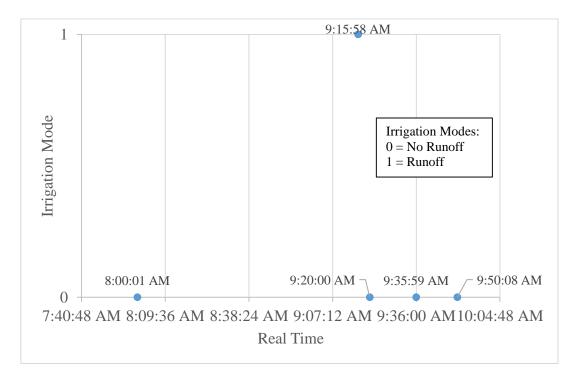


Figure 142. The Runoff Status of Plot 2 (Conductivity Prototype) on Aug 25th 2015

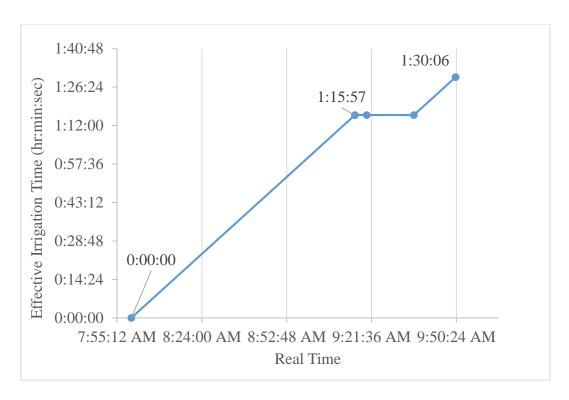


Figure 143. The Effective Irrigation Time of Plot 2 (Conductivity Prototype) on Aug $25^{\rm th}~2015$

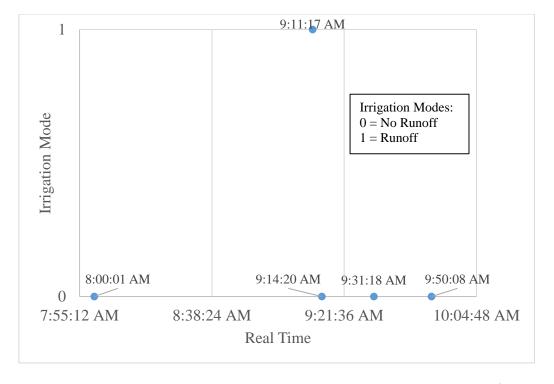


Figure 144. The Runoff Status of Plot 4 (Cubic Float Prototype) on Aug 25th 2015 150

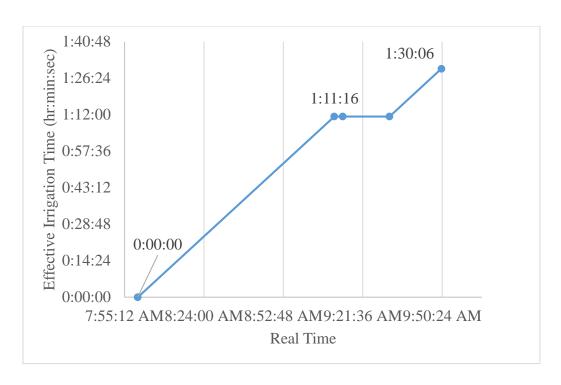


Figure 145. The Effective Irrigation Time of Plot 4 (Cubic Float Prototype) on Aug $25^{\rm th}~2015$

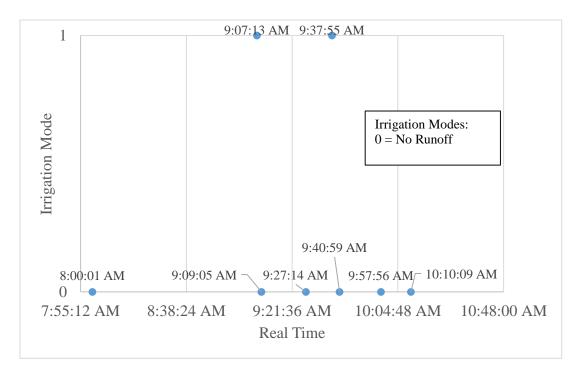


Figure 146. The Runoff Status of Plot 6 (Conductivity Prototype) on Aug 25th 2015

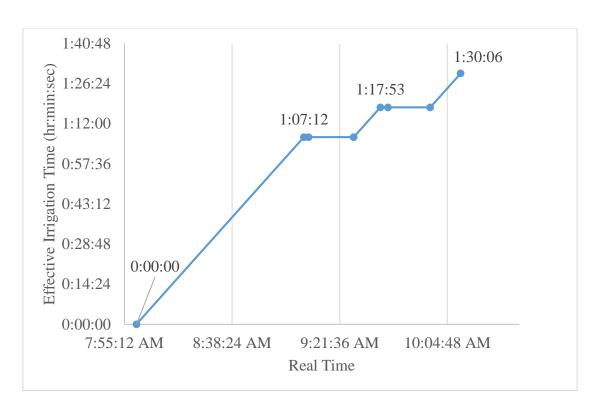


Figure 147. The Effective Irrigation Time of Plot 6 (Conductivity Prototype) on Aug 25th 2015

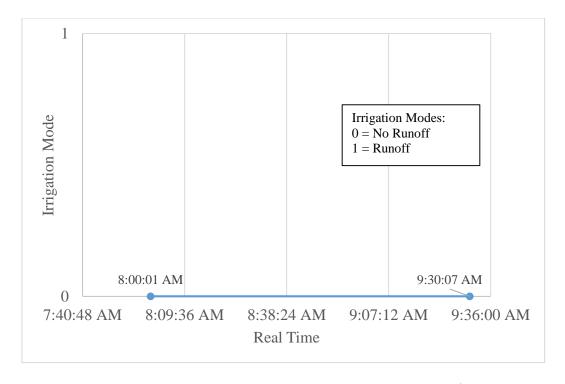


Figure 148. The Runoff Status of Plot 7 (Control) on Aug 25th 2015 152

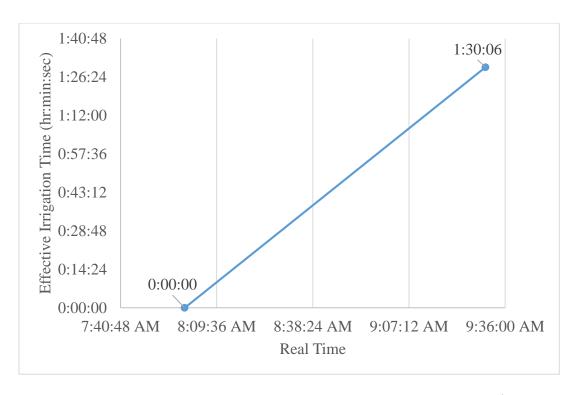


Figure 149. The Effective Irrigation Time of Plot 7 (Control) on Aug 25th 2015

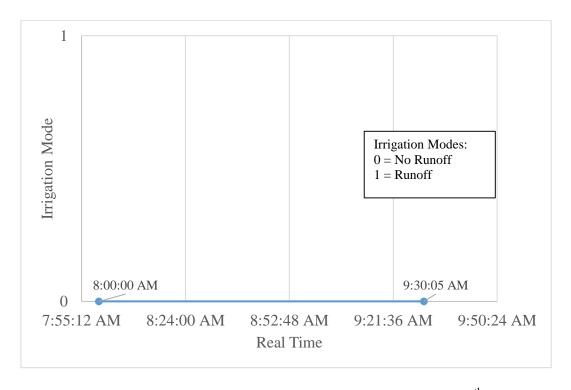


Figure 150. The Runoff Status of Plot 8 (Control Plot) on Aug 25th 2015

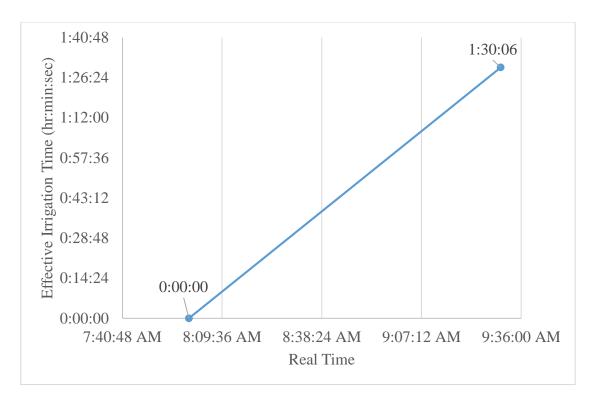


Figure 151. The Effective Irrigation Time of Plot 8 (Control Plot) on Aug 25th 2015

From the irrigation results, both prototypes have successfully detected runoff and paused the irrigation as prescribed.

4.2.11 Qualitative Field Testing Result Analysis

Based on the irrigation results for the ten qualitative field tests shown above, the performance of the different prototypes has been evaluated taking into account functionality and reliability. Table 20 shows relevant data of all the tested prototypes for comparison purposes.

Table 20. Analysis and Comparison of the Performance of the Irrigation Runoff
Sensors during Qualitative Field Testing

| Prototype | Plot # | Times of Being Tested | Times of Successful Tests | Success Rate (Successful test/Total | Longest Working Time without Breaking Down | Comments |
|--------------------------|--------------------------|--------------------------|------------------------------|--|--|---|
| Paddle Wheel | 1 N/A N/A N/A N/A Paddle | | N/A | The paddle wheel prototypes have encountered various problems preventing them from working | | |
| Prototype | 3 | 1 | 0 | 0 | N/A | properly. Plot 1 never worked while plot 3 kept having clogging issues and water-damage. |
| | 4 | 9 | 9 | 100% | 15 Weeks | The cubic float prototypes could work for a long time without |
| Cubic Float Prototype | 5 | 9 | 9 | 100% | 16 Weeks | maintenance. During the 4-month testing period, no problem has been detected. |
| Elbow Float Prototype | 9 | 4 | 3 | 75% | 3 Weeks | The elbow float prototype has had a problem of clogging and thus needed a maintenance biweekly. The vertical float sensor finally broke down after 3 weeks. |

| Prototype | Plot # | Times of Being Tested | Times of Successful Tests | Success Rate (Successful test/Total number of tests) | Longest Working Time without Breaking Down | Comments |
|---------------------------|--------|--------------------------|------------------------------|--|--|---|
| | 2 | 9 | 7 | 77.8% | 8 Weeks | The conductivity prototypes have had problems of rusting and clogging, which needed biweekly maintenance. The |
| Conductivity Prototype | 6 | 9 | 9 | 100% | 16 Weeks | conductivity prototypes have also shown the capability of working reliably and properly for a long time with appropriate maintenance. |

Taken the performance of different prototypes into consideration, the cubic float prototype and the conductivity prototype have been selected for the quantitative field testing phase.

4.3 Quantitative Field Testing Results of Cubic Float and Conductivity Prototypes

The cubic float prototype and the conductivity prototype have been selected out of the four prototypes for the quantitative field testing based on their performance during the qualitative field testing phase. During quantitative field testing, each plot has been irrigated for 30 minutes including the control plot. The amount of irrigation water and the runoff of water have been calculated by the water meters in the field.

Then the amount of runoff of the irrigation sensor plot and the control plot have been compared to show the capability of reducing runoff.

4.3.1 Quantitative Field Testing Results for Sept 17th 2015

A conductivity prototype has been installed in plot 15 while a control plot (plot 18) was used during each test for comparison purposes. The irrigation specifications have been listed, as shown in Table 21.

Table 21. Irrigation Specifications of Test on Sept 17th 2015

| Start Time | 8:00 AM | | |
|---------------------------------|------------------------------|--|--|
| Effective Irrigation Time (EIT) | 30 minutes | | |
| Wait Time (WT) | 20 minutes | | |
| # of Tested Plot | 15 (Conductivity Prototype), | | |
| # 01 Tested Plot | 18 (Control) | | |

The results are shown in Figures 152 - 156.

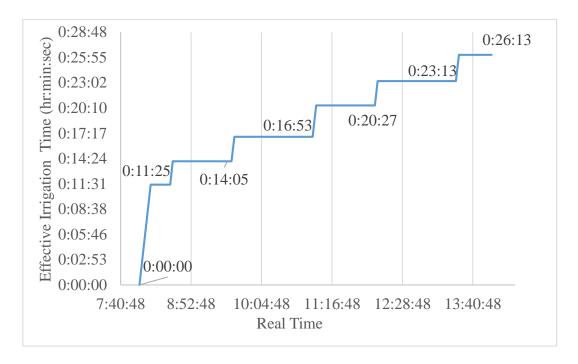


Figure 152. Plot 15 (Conductivity Prototype) Irrigation Results on Sept 17th 2015

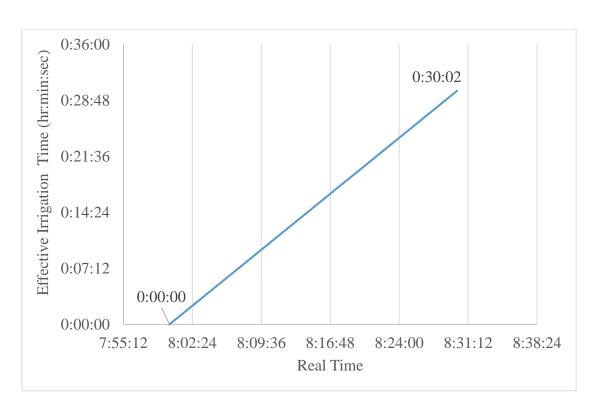


Figure 153. Plot 18 (Control) Irrigation Results on Sept 17th 2015

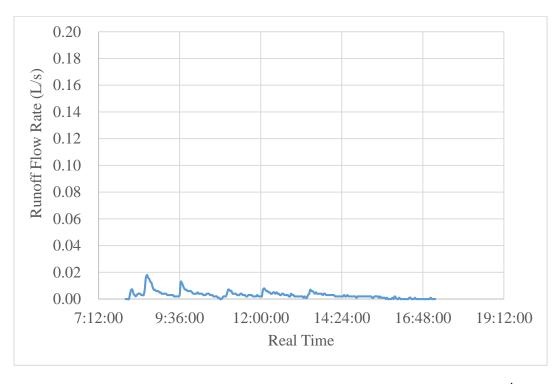


Figure 154. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 17^{th} 2015

(Scale: 0 to 0.2 L/s)

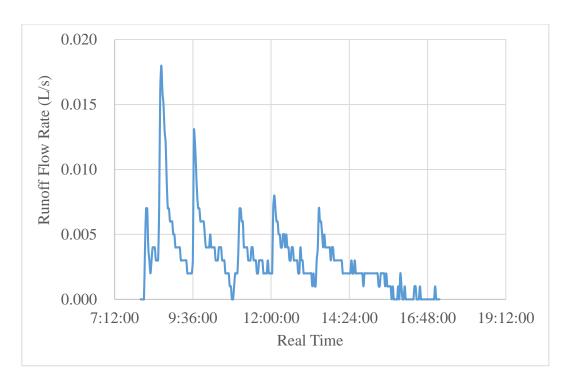


Figure 155. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 17th 2015 (Scale: 0 to 0.02 L/s)

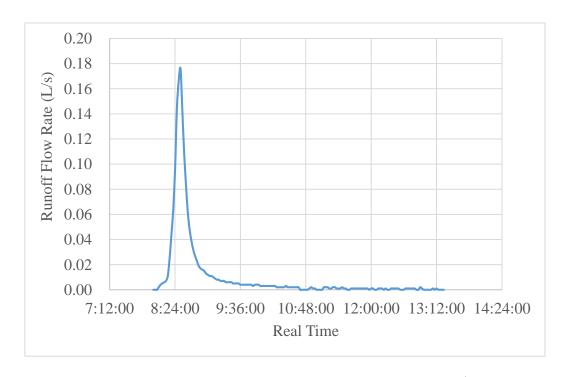


Figure 156. Runoff Flow Rate of Plot 18 (Control) on Sept 17th 2015

(Scale: 0 to 0.2 L/s)

The total amount of the used water, runoff and the water absorbed by the field are listed in Table 22.

Table 22. Water Usage and Runoff Analysis of Irrigation on Sept 17th 2015 (TIT)

| | Irrigation Time, IT (hr:min:sec) | Total Amount of Used Water (Gallon) ¹ | Runoff (Gallon) | Water Absorbed by Soil (Gallon) | | % of Runoff Reduction |
|--|--|--|--------------------|---------------------------------------|-------|--------------------------|
| Plot 15 (Conductivity Prototype) | 5:26:32 | 217 | 27.07 | 189.93 | 87.5% | 49.3% |
| Plot 18 (Control) | 0:30:02 | 229 | 53.38 | 175.62 | 76.7% | N/A |

Note: (1) Total amount of water used by Plots 15 and 18 is within 5.2% of each other.

Based on the results shown in Figures ##, ## and ## and Table 22, the conductivity prototype has allowed a shorter effective irrigation time (EIT) when compared to the control plot because total irrigation time (TIT) was been reached before EIT had been reached. However, the conductivity prototype has still led to a 49.29% reduction in runoff and a higher water absorption rate. Moreover, the smaller EIT has shown the capability of the conductivity prototype to prevent over-irrigation by appropriately setting the EIT and TIT. The conductivity prototype has allowed much longer time for the irrigation, which can prevent nutrients and other important lawn components from being flushed by the runoff.

4.3.2 Quantitative Field Testing Results for Sept 19th 2015

A conductivity prototype has been installed in plot 15 while a control plot (plot 18) was used during each test for comparison purposes. The effective irrigation time

has been set to 15 minutes for the first test, with a 15-minute test starting one hour after the end of the first test. The irrigation specifications are listed in Table 23.

Table 23. Irrigation Specifications of Test on Sept 19th 2015

| Start Time | 7:55 AM (1 st Test) 10:50 AM (2 nd Test) |
|---------------------------------|---|
| Effective Irrigation Time (EIT) | 15 minutes for each test |
| Wait Time (WT) | 10 minutes |
| # of Tested Plot | 15 (Conductivity Prototype), 18 (Control) |

The results for the two 15-minute tests are shown in Figures 156 - 163.

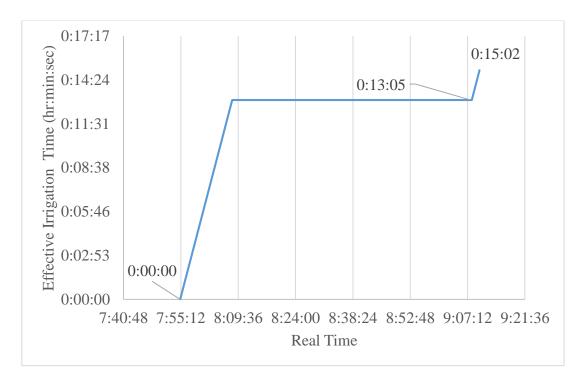


Figure 157. Plot 15 (Conductivity Prototype) Irrigation Results of the First 15-Minute

Test on Sept 19th 2015

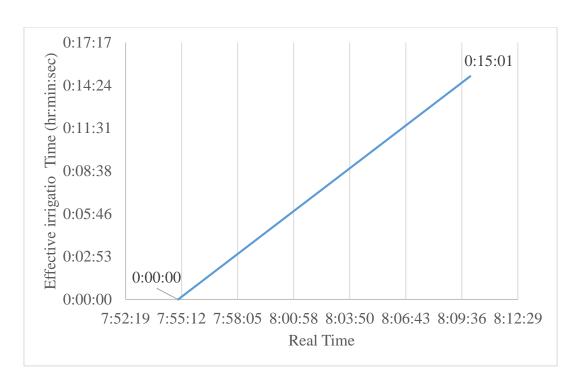


Figure 158. Plot 18 (Control) Irrigation Results of the First 15-Minute Test on Sept 19^{th} 2015

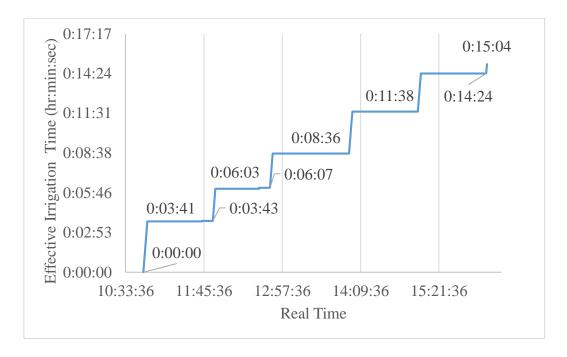


Figure 159. Plot 15 (Conductivity Prototype) Irrigation Results of the Second

15-Minute Test on Sept 19th 2015

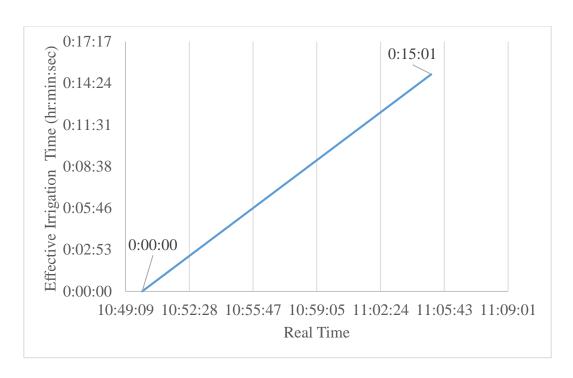


Figure 160. Plot 18 (Control) Irrigation Results of the Second 15-Minute Test on Sept 19th 2015

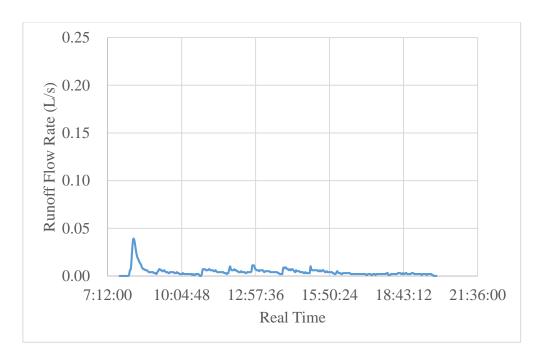


Figure 161. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 19th 2015 (Scale: 0 to 0.25 L/s)

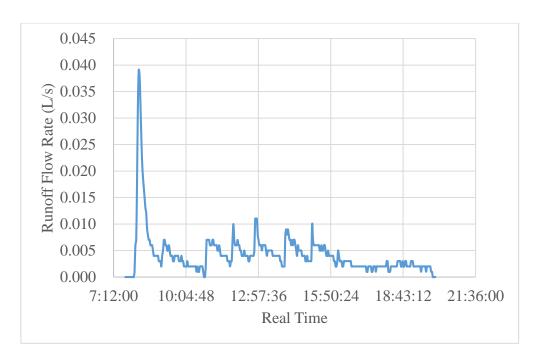


Figure 162. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 19th 2015 (Scale: 0 to 0.045 L/s)

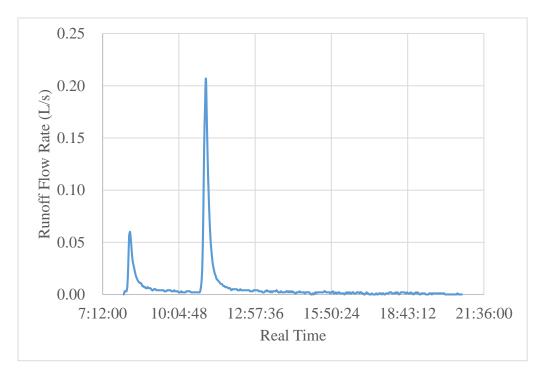


Figure 163. Runoff Flow Rate of Plot 18 (Control) on Sept 19th 2015

(Scale: 0 to 0.25 L/s)

The total amount of the used water, the runoff and the water absorbed by the field for both two tests have been listed. Also, the results of combining the two tests together (Effective irrigation time = 15 + 15 minutes = 30 minutes) have also been listed, as shown in Table 24.

Table 24. Water Usage and Runoff Analysis of Irrigation on Sept 19th 2015

| | | Irrigation Time, IT (hr:min:sec) | Total Amount of Used Water (Gallon) | Runoff (Gallon) | Water Absorbed by Soil (Gallon) | Water Absorption Rate (Water Absorbed/Total Use) | % of Runoff Reduction |
|----------------------------|--|-------------------------------------|--|-----------------|------------------------------------|--|--------------------------|
| First Test (EIT: 15 | Plot 15 (Conductivity Prototype) | 1:15:11 | 120 | 17.23 | 102.77 | 85.6% | 20.78% |
| minutes) ¹ | Plot 18 (Control) | 0:15:01 | 115 | 21.75 | 93.25 | 81.1% | N/A |
| Second Test (EIT: 15 | Plot 15 (Conductivity Prototype) | 5:15:44 | 122 | 33 | 89 | 73.0% | 46.48% |
| minutes) ² | Plot 18 (Control) | 0:15:01 | 116 | 61.66 | 54.34 | 46.8% | N/A |
| Total (EIT: 30 | Plot 15 (Conductivity Prototype) | 6:30:12 | 242 | 50.23 | 191.77 | 79.2% | 39.78% |
| minutes) ³ | Plot 18 (Control) | 0:30:02 | 231 | 83.41 | 147.59 | 63.9% | N/A |

Note:

⁽¹⁾ Total amount of water used by Plots 15 and 18 during the first test is within 4.3% of each other.

⁽²⁾ Total amount of water used by Plots 15 and 18 during the second test is within 4.9% of each other.

⁽³⁾ Total amount of water used by Plots 15 and 18 during the two tests is within 4.8% of each other.

Based on the results, the conductivity prototype and the control plot have allowed similar effective irrigation time, leading to the similar total amount of water being used by each plot. However, the conductivity prototype has resulted in a 20.78% reduction of runoff in the first 15 minutes test, while the reduction rate grows to 46.48% in the second 15 minutes test. When combing the two tests together, the effective irrigation time is 30 minutes and the runoff reduction rate then is 39.78%. Moreover, the tests have also shown that the conductivity prototype has led to a higher runoff reduction rate during the longer irrigation period which helped keep the soil wetter for a longer period of time.

4.3.3 Quantitative Field Testing Results for Sept 21st 2015

A conductivity prototype has been installed in plot 15 while a control plot (plot 18) was used during each test for comparison purposes. The irrigation specifications have been listed, as shown in Table 25.

Table 25. Irrigation Specifications of Test on Sept 21st 2015

| Start Time | 7:20 AM | | |
|---------------------------------|--|--|--|
| Effective Irrigation Time (EIT) | 30 minutes | | |
| Wait Time (WT) | 10 minutes | | |
| # of Tested Plot | 15 (Conductivity Prototype), 18 (Control) | | |

The results have been shown in Figures 162 - 168.

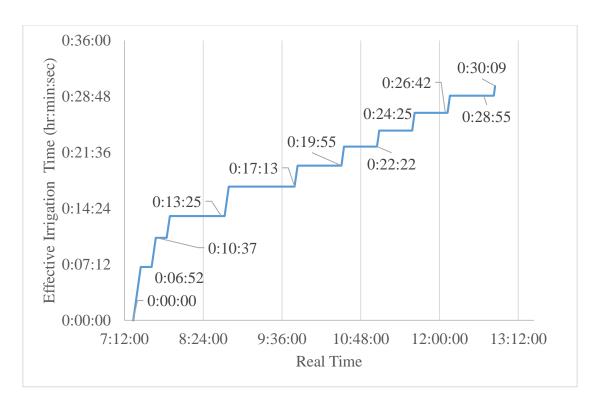


Figure 164. Plot 15 (Conductivity Prototype) Irrigation Results on Sept 21st 2015

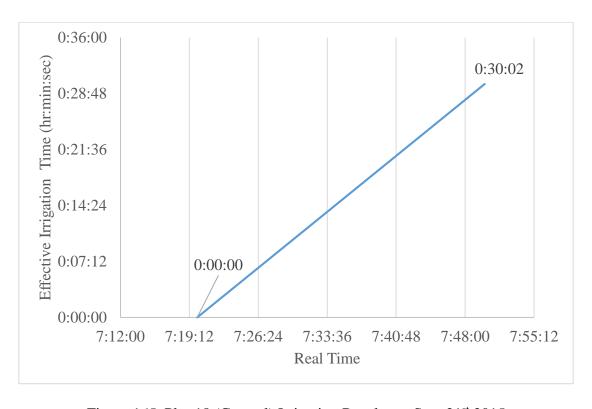


Figure 165. Plot 18 (Control) Irrigation Results on Sept 21st 2015

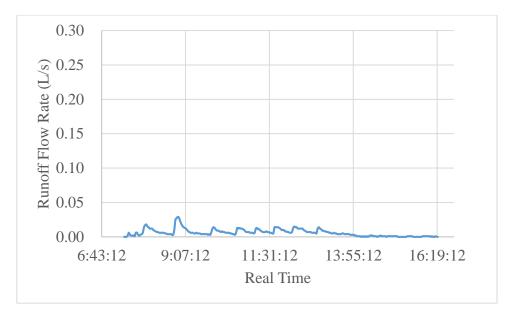


Figure 166. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 21st 2015 (Scale: 0 to 0.3 L/s)

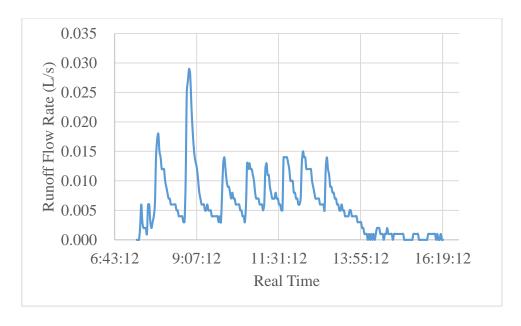


Figure 167. Runoff Flow Rate of Plot 15 (Conductivity Prototype) on Sept 21st 2015 (Scale: 0 to 0.035 L/s)

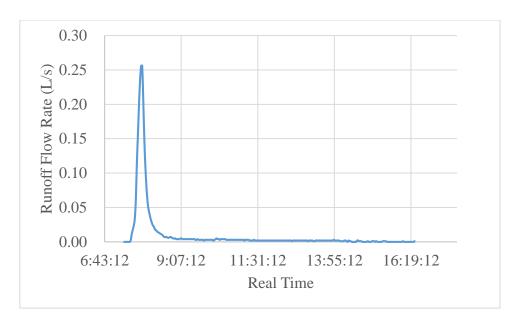


Figure 168. Runoff Flow Rate of Plot 18 (Control) on Sept 21st 2015 (Scale: 0 to 0.3 L/s)

The total amount of the used water, the runoff and the water absorbed by the field have been listed, as shown in Table 26.

Table 26. Water Usage and Runoff Analysis of Irrigation on Sept 21st 2015

| | Irrigation Time, IT (hr:min:sec) | Total Amount of Used Water (Gallon) ¹ | Runoff (Gallon) | Water Absorbed by Soil (Gallon) | Water Absorption Rate (Water Absorbed/Total Use) | % of Runoff Reduction |
|--|-------------------------------------|--|-----------------|------------------------------------|---|--------------------------|
| Plot 15 (Conductivity Prototype) | 5:30:53 | 237 | 51.55 | 185.45 | 78.2% | 41.51% |
| Plot 18 (Control) | 0:30:02 | 231 | 88.13 | 142.87 | 61.8% | N/A |

Note: (1) Total amount of water used by Plots 15 and 18 is within 2.6% of each other.

From the results, both plots have had a 30 minutes effective irrigation. The conductivity prototype have shown the capability of reducing the runoff by 41.51% and leads to a higher water absorption rate. The conductivity prototype has allowed 5 additional hours longer of irrigation, but in a manner that minimizes runoff, which prevents nutrients from being flushed by the runoff.

4.3.4 Quantitative Field Testing Results for Sept 25th 2015

A cubic float prototype has been installed in plot 15 while a control plot (plot 18) was used during each test for comparison purposes. The irrigation specifications have been listed, as shown in Table 27.

Table 27. Irrigation Specifications of Test on Sept 25th 2015

| Start Time | 6:00 AM | |
|---------------------------------|-----------------------------|--|
| Effective Irrigation Time (EIT) | 30 minutes | |
| Wait Time (WT) | 10 minutes | |
| # of Tested Plot | 15 (Cubic Float Prototype), | |
| # 01 Tested Plot | 18 (Control) | |

The results have been shown in Figures 169 - 173.

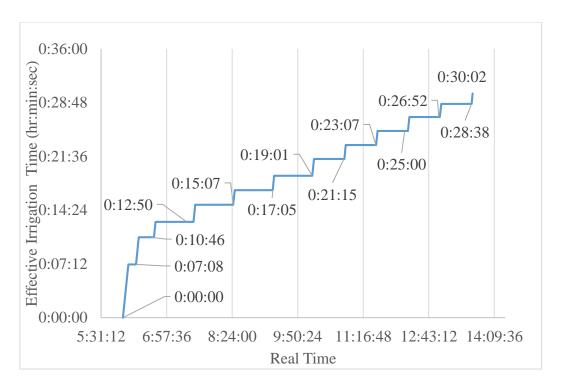


Figure 169. Plot 15 (Conductivity Prototype) Irrigation Results on Sept 25th 2015

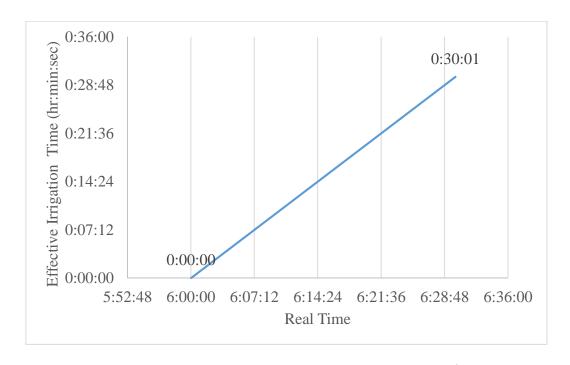


Figure 170. Plot 18 (Control) Irrigation Results on Sept 25th 2015

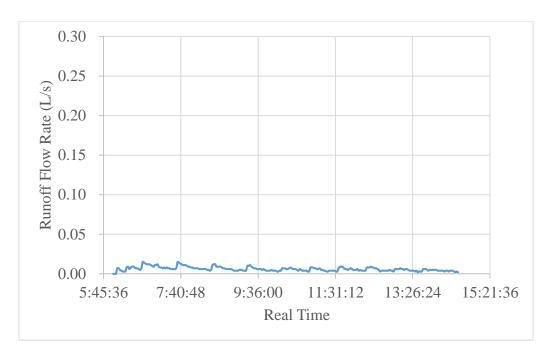


Figure 171. Runoff Flow Rate of Plot 15 (Cubic Float Prototype) on Sept 25th 2015 (Scale: 0 to 0.3 L/s)

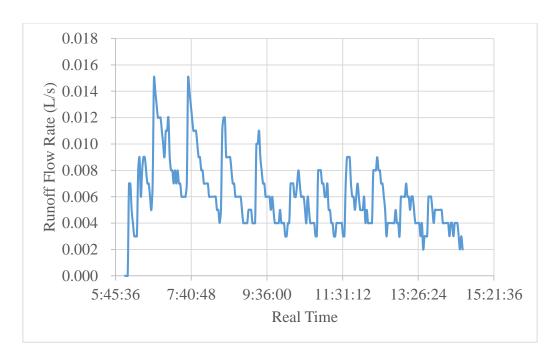


Figure 172. Runoff Flow Rate of Plot 15 (Cubic Float Prototype) on Sept 25th 2015 (Scale: 0 to 0.018 L/s)

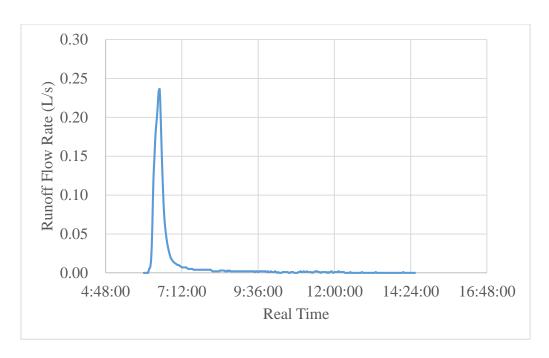


Figure 173. Runoff Flow Rate of Plot 18 (Control) on Sept 25th 2015 (Scale: 0 to 0.3 L/s)

The total amount of the used water, the runoff and the water absorbed by the field have been listed, as shown in Table 28.

Table 28. Water Usage and Runoff Analysis of Irrigation on Sept 17th 2015

| | Irrigation Time, IT (hr:min:sec) | Total Amount of Used Water (Gallon) ¹ | Runoff (Gallon) | Water Absorbed by Soil (Gallon) | Absorption Rate (Water Absorbed/Total | Runoff Reducing Percent |
|--|-------------------------------------|--|-----------------|------------------------------------|---|-------------------------------|
| Plot 15 (Cubic Float Prototype) | 7:41:02 | 241 | 49.8 | 191.2 | 79.3% | 39.83% |
| Plot 18 (Control) | 0:30:01 | 223 | 82.77 | 140.23 | 62.9% | N/A |

Note: (1) Total amount of water used by Plots 15 and 18 is within 8.1% of each other.

Based on the results, both plots have had a 30 minutes of effective irrigation. The cubic float prototype have shown the capability of reducing the runoff by 39.83%, while more water has been allowed to be absorbed by soil. The float prototype has allowed an even longer time for irrigation, compared to the conductivity one. It has also increased the water absorption rate, which is similar to the conductivity prototype.

In general, both prototypes are capable of reducing runoff while increasing the amount of water being absorbed by the plots. However, the cubic float prototype did not experience clogging or rust problems. Furthermore, the electronic system that supports the irrigation and runoff systems were able to perform flawlessly during all the quantitative tests.

5. CONCLUSION

A Landscape Irrigation Runoff Mitigation System (LIRMS) was designed, built and field-tested for minimizing irrigation water losses from residential or commercial landscapes. Four types of irrigation runoff sensors, based on different working principles, were designed and manufactured using common materials and components. Then a central control module capable of receiving signals from sensors and controlling several irrigation valves at the same time was designed, built and tested. Afterwards, the prototypes were installed in the field and hardwired with the central control module along with two control plots that had no runoff sensors installed. The different types were evaluated based on their performance characteristics including the ability of each prototype to work reliably over an extended period of time. The conductivity prototype and the cubic float prototype showed to be stable, reliable and functional. These two types of prototypes were then used in the field for the quantitative field testing phase. The amount of runoff of the prototypes were recorded and compared, leading to the final selection of the irrigation runoff sensor prototype. The conductivity prototype resulted in 40% - 50% reduction in runoff and 10% - 30% increase in water absorption by soil based on a 30 minutes effective irrigation. The cubic float prototype showed the ability of reducing runoff by 40% and allowed greater water absorption.

A web-based interface (i.e. server) was designed and programmer so that irrigation data could be accessed online. Also, a wireless communication module and an autonomous energy system were designed and tested to allow wireless

communication between the irrigation runoff sensors and the control unit which also allowed for energy savings.

The cubic float prototype was tested and used for a longer irrigation time. The conductivity prototype resulted in a higher runoff reduction rate. The main requirements of the devices were met in term of being inexpensive, reliable and durable during the field-testing phase. The Landscape Irrigation Runoff Mitigation System (LIRMS) equipped with the cubic float prototype/conductivity prototype showed the great capability for water conservation.

6. FUTURE WORK

Further studies should focus on investigating different irrigation strategies for runoff reduction, grass quality and economic benefits. Equipped with advanced strategies, the current LIMRS system could greatly improve the irrigation results while preserving lawn quality.

6.1 Reduction of Effective Irrigation Time

Based on the results of the tests during the quantitative field testing phase, it has been shown that more water has been absorbed by the experimental plot (the plot with the irrigation runoff sensor prototype) than the control plot during the same effective irrigation time (EIT). Thus, the effective irrigation time of the experimental plot could be reduced in order to maintain the same quality of the grass as the control plot by reducing the level of water absorption for the same weekly irrigation frequencies. The suggested tests' specifications and changes have been listed, as shown in Table 29.

Table 29. Changes of Specifications between the Experimental and the Control Plots

| | Experimental Group | Control Group |
|-----------------------------------|--------------------|---------------|
| Effective Irrigation Time | EIT < 30 minutes | 30 minutes |
| Weekly Irrigation Frequency (WIF) | 1/Week | 1/Week |
| Amount of Water Absorbed | San | ne |

Further tests should be done to determine the effective irrigation time of the experimental group in order to get the same amount of water absorbed by soil as in the control group.

6.2 Reduction of Irrigation Frequency

In order to maintain the same quality of grass of the experimental and the control plots, the weekly irrigation frequency of the experimental plot can be reduced while the effective irrigation time of every irrigation event remains the same. As a result, the experimental plot will have the same amount of water absorption with the control plot, which can further reduce the total amount of water usage and the runoff. The tests' specifications and changes have been listed, as shown in Table 30.

Table 30. Changes of Specifications between the Experimental and the Control Plots

| | Experimental Group | Control Group |
|-----------------------------------|--------------------|---------------|
| Effective Irrigation Time | 30 minutes | 30 minutes |
| Weekly Irrigation Frequency (WIF) | WIF < 1/Week | 1/Week |
| Amount of Water Absorbed | Same | |

Further tests should be done to determine the irrigation frequency of the experimental group in order to get the same amount of water absorbed by soil as in the control group.

6.3 Self-adjustable LIRMS for minimum runoff

An intelligent controller module with autonomous learning abilities should be considered in the future. The control module should be able to correlate runoff time and

total irrigation time so an optimum EIT can be identified by using historical irrigation data. The intelligent controller should adjust the time between the start of the irrigation (SI) and the time of runoff detection referred as the Runoff Detection Time (RDT), so that the time between detection and disappearance of runoff referred as Runoff Existing Time (RET) can be minimized. The real irrigation time represents the time when the irrigation system is in operation. Several case scenarios are shown in Table 31.

Table 31. Case Scenarios of the LIRMS System with Autonomous Learning Ability

| | Real Irrigation Time | RDT | RET |
|-----------------------|----------------------|------------|-----------|
| 1 st Trial | 30 minutes | 30 minutes | 4 minutes |
| 2 nd Trial | 28 minutes | 40 minutes | 2 minutes |
| 3 rd Trial | 26 minutes | 45 minutes | 1 minute |

The LIMRS system with a new intelligent control module should be installed in the field. For the first irrigation cycle, the system irrigates the field for 30 minutes and then detects runoff. The runoff is assumed to last 4 minutes. Thus the RDT is 30 minutes while the RET is 4 minutes. During the second irrigation case scenario, the LIRMS system should have taught itself to reduce the irrigation time (i.e. to 28 minutes), so runoff occurs after 40 minutes or more from the start of the irrigation. During the third test, the irrigation time is set to be 26 minutes, runoff is assumed to be detected after 45 minutes from the start of the irrigation while the RET is detected to be 1 minute. Optimally, the LIRMS system should keep adjusting RDT and RET, with the ultimate goal of maximizing RDT while minimizing RET. Further water savings are expected with the procedures of autonomous learning, as outlined above.

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APPENDIX A

2-D Mechanical Drawings:

PaddleWheel_2D Drawings.DWG

CubicFloat_2D Drawings.DWG

ElbowFloat_2D Drawings.DWG

Conductivity_2D Drawings.DWG

APPENDIX B

Main Program:

```
#include "Arduino.h"
#include "I2C.h"
#include "RTC.h"
#define byte uint8_t
#define DS1307_ADDRESS 0x68
//char mess[128] = \{0\};
void DateTime::set time(uint8 t sec, uint8 t minu, uint8 t hr, uint8 t wkday, uint8 t dy, uint8 t mon,
uint16 t yr){
   second = sec;
   minute = minu;
   hour = hr;
   weekday = wkday;
   day = dy;
   month = mon;
   year = yr;
}
uint8_t DateTime::dayofweek(const DateTime& A){
return A.weekday;
byte bcdToDec(byte val) {
// Convert binary coded decimal to normal decimal numbers
  return ( (val/16*10) + (val%16) );
}
void DateTime::round_time(){
 year = year + (month + (day + (hour + (minute + (second)/60)/60)/24)/30)/12;
 month = (month + (day + (hour + (minute + (second)/60)/60)/24)/30)\% 12;
 day = (day + (hour + (minute + (second)/60)/60)/24)\%30;
 hour = (hour + (minute + (second)/60)/60)\%24;
 minute = (minute + (second)/60)% 60;
 second = second\%60;
}
void DateTime::current_time(){
  I2c.read(0x68, 0x00, 7);
  second = bcdToDec(I2c.receive());
  minute = bcdToDec(I2c.receive());
  hour = bcdToDec(I2c.receive() & 0b111111); //24 hour time
  weekday = bcdToDec(I2c.receive()); //0-6 -> sunday - Saturday
  day = bcdToDec(I2c.receive());
  month = bcdToDec(I2c.receive());
  year = bcdToDec(I2c.receive());
```

```
void DateTime::print_time(){
  Serial.print(month);
  Serial.print(F("/"));
  Serial.print(day);
  Serial.print(F("/"));
  Serial.print(year);
  Serial.print(F(" "));
  Serial.print(hour);
  Serial.print(F(":"));
  Serial.print(minute);
  Serial.print(F(":"));
  Serial.print(second);
  Serial.println();
void DateTime::logtime(char *time){
  sprintf(time,"%d/%d/%d %d:%d:%d%c",month, day, year, hour, minute, second, \\0');
DateTime DateTime::operator+(const DateTime& A){
  /*const int month_days[] = {31,28,31,30,31,30,31,30,31,30,31}; //Good till 2016 when next leap
year
  DateTime date;
  date.set_time(0,0,0,0,0,0,0);
  date.second = this->second + A.second;
  date.minute = this->minute + A.minute;
  date.hour = this->hour + A.hour;
  date.weekday = this->weekday + A.weekday;
  date.day = this->day + A.day;
  date.month = this->month + A.month;
  date.year = this->year + A.year;
  date.round_time();
  if(date.day >= month_days[date.month])
    date.month+=1;
     date.day/=month_days[date.month];
  return date;*/
  DateTime date;
  date.set_time(0,0,0,0,0,0,0);
  date.second = this->second + A.second;
  date.minute = this->minute + A.minute;
  date.hour = this->hour + A.hour;
  date.round_time();
  return date;
DateTime DateTime::operator-(const DateTime& A){
DateTime right, left;
right.set_time(0, 0, 0, 0, 0, 0, 0);
left.set_time(0, 0, 0, 0, 0, 0, 0);
 // this is left, A is right
  right.hour = A.hour;
  right.minute = A.minute;
  right.second = A.second;
  left.hour = this->hour;
  left.minute = this->minute;
  left.second = this->second;
  if (left.minute < right.minute){</pre>
```

```
left.minute+=60;
      --left.hour;
  if(left.second < right.second){</pre>
      left.second+=60;
      --left.minute;
  }
  right.hour = left.hour - right.hour;
  right.minute = left.minute - right.minute;
  right.second = left.second - right.second;
                            //Return final DateTime
  return right;
boolean DateTime::operator>=(const DateTime& A){
  // "this" is on the left and "A" on the right
  // No need to irrigate for more than 24 hours
  if (this->hour > A.hour) return 1;
  if (this->hour < A.hour) return 0;
  if (this->minute > A.minute) return 1;
  if (this->minute < A.minute) return 0;
  if (this->second > A.second) return 1;
  return 0;
```

SD Card Program:

```
#include <SD.h>
#include "SPI.h"
#include "SDcard.h"
// On the Ethernet Shield, CS is pin 4. Note that even if it's not
// used as the CS pin, the hardware CS pin (10 on most Arduino boards,
// 53 on the Mega) must be left as an output or the SD library
// functions will not work.
const uint8_t SD_CS = 5;
const uint8_t SD_CD = 4;
SDcard::SDcard(){
}
void SDcard::inserted()
  SD_SPI_setup();
  Serial.print(F("Initializing SD card..."));
  // make sure that the default chip select pin is set to
  // output, even if you don't use it:
  // see if the card is present and can be initialized:
  if (!SD.begin(SD_CS)) {
     Serial.println(F("Card failed, or not present"));
     // don't do anything more:
     return;
  Serial.println(F("card initialized."));
```

```
}
void SDcard::SD_SPI_setup(){
  SPI.setClockDivider(4);
  SPI.setBitOrder(MSBFIRST);
  SPI.setDataMode(SPI_MODE3);
                                       // Data mode 0, 3 work
void SDcard::SD_setup(){
   pinMode(SD_CS, OUTPUT); // Chip select
   pinMode(SD_CD, INPUT);
                                 // Chip detect
   pinMode(10, OUTPUT);
                                 // Needed for SD library to work correctly
   digitalWrite(SD_CS, HIGH); // Dectivate SD for setup
   SD_SPI_setup();
}
boolean SDcard::logdata(String dataString, int newline)
  SD_SPI_setup();
                       // Reconfigure SPI settings to be able to read from the card
  // open the file. note that only one file can be open at a time,
  // so you have to close this one before opening another.
  File dataFile = SD.open("datalog.txt", O_CREAT | O_WRITE); //O_CREAT | O_WRITE
  // if the file is available, write to it:
  if (dataFile) {
     if (newline) dataFile.println(dataString);
    else dataFile.print(dataString);
    dataFile.flush();
    dataFile.close();
    // print to the serial port too:
    return true; //Data logged without errors
  // if the file isn't open, pop up an error:
     return false; // Error with logging data
}
SDcard SDc = SDcard();
```