

## Microwave Engineering

- David M Pozar 4th Edition

100 MHz  $\rightarrow$  ~~ultra~~ and 300 GHz  $\rightarrow$  Microwave

3 GHz  $\rightarrow$  ~~radio~~  $\rightarrow$  ~~microwave~~  $\rightarrow$   $10\text{ cm} - 1\text{ mm}$  ~~size~~  $\rightarrow$  ~~parasitic~~

Visible wave length (700-440 nm)

$\hookrightarrow$  Remote  $\rightarrow$  Infrared

\* Why are microwave frequencies of interest?

$\hookrightarrow$  Higher Bandwidth

$\Rightarrow$  1. Bandwidth, capacity

$3 - 3400 / 3.4 \text{ Hz}$

$\leq 3.4 \rightarrow$  Normal

We need to transmit 4KHz voice signal through a wireless link.

One operating at 500 MHz and second at 4 GHz, each with a 10% bandwidth around its center frequency.

500 MHz

Number of channels =  $\frac{\text{Operating frequency} * \text{percent BW}}{\text{BW per channel}}$

$$= \frac{0.5 \text{ GHz} \times 0.1}{4 \text{ KHz}} = 12500$$

4 GHz

$$\text{Number of channels} = \frac{4 \text{ GHz} \times 0.1}{4 \text{ kHz}} = 100,000$$

Operating frequency increases  $\rightarrow$  capacity increases

→  
BW

~~Antenna size~~

## 2. Antenna size

frequency  $\lambda_{RF} \rightarrow$  wavelength  $\lambda_{EM}$

1.1 table

→ 1st 2 page theory

Figure - 1.1 → Approximate Band

940

\* Current theory vs EM Field theory

Structure size, smaller wavelength  $\lambda_{RF}$

50 Hz → AC circuit → Maximum 60 Hz

↪ KCL, KVL

↪ Lumped-parameter circuit components

wavelength  $\lambda \leq 2\pi$ , structure  $\lambda \ll 2\pi$ ,

↪ Linear, nonlinear

↪ EM Field theory

↪ distributed-parameter circuit components

\* Lumped, distributed parameter circuit components ( $\lambda_{RF}$ ,  $\lambda_{EM}$ )

Transistor, Diode,

\* Transition from Lumped to distributed

↪ Tunnel diode

\* General electric circuit - Transistor, FET, MOSFET

\* Microwave- Diode, Tunnel diode, Variable diode

\* Microwave Circuit - Insulator, Circulator, Attenuator

Klystron oscillator → Microwave

Magnator " "

frequency  $\lambda_{\text{far}}$   $\rightarrow$  wavelength  $\lambda_{\text{near}}$   $\rightarrow$  what is the meaning?

1.1 table

→ 1st 2 page Theory

Figure - 1.1  $\rightarrow$  Approximate Band

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Structure size smaller wavelength  $\text{GHz}$

↪ KCL, KVL

50 Hz → AC circuit → Maximum 60 Hz

↪ Lumped-parameter circuit  
with no components

wavelength  $\gg$  structure, structure  $\gg$  circuit,  $\rightarrow$

↪ Linear, nonlinear

↪ EM Field theory

↪ distributed-parameter circuit components

\* Lumped, distributed parameter circuit components ( $\text{capacitor}$ ,  $\text{inductor}$ )

Diode, D, J, P, T, R, L, C, S, M, A, Z, H, G, B, D, F, G, H, J, K, L, M, N, P, Q, R, S, T, U, V, W, X, Y, Z

\* Transition from Lumped to distributed

↪ Tunnel diode

Plistone

\* General electric circuit - Transistor, FET, MOSFET

Channel Block

\* Microwave - Diode, Tunnel diode, Variable diode

Wav. use

\* Microwave Circuit - Insulator, Circulator, Attenuator

Klystron oscillator → Microwave

Magnator

## Antenna Conversion

- \* Compare between electrical circuit and Microwave circuit
- \* Microwave heating to generate ESR?

Transmission line / Wave line that signal passes through wave is

### \* Advantages of MW:

1. capacity / BW (refer)
2. Antenna size (refer)

→

1. Antenna gain is proportional to Beam Width (refer)
- 2.
- 3.

Diameter  $\varnothing$  1.2 m

### \* Transmission Line at wavelength 225 m frequency (refer 225,

frequency,  $f = 300 \text{ MHz}$

$$t = \frac{c}{f}$$

$$= \frac{3 \times 10^8}{300 \times 10^6} =$$

$$= 1 \text{ m}$$

Bandwidth = 100°

$$\text{Diameter, } D = 140 \times \frac{\lambda}{B}$$
$$= 140 \times \frac{1}{100}$$
$$= 1.4$$

\* Microwave antenna 30 GHz  
problem

Second scenario,

$$f = 30 \text{ GHz}$$

$$\lambda = \frac{c}{f}$$
$$= \frac{3 \times 10^8}{30 \times 10^9} = 0.01$$

$$D = 140 \times \frac{0.01}{100}$$
$$= 0.014$$

- \* Microwave Engineering 30 GHz signal generate error?
- \* Microwave Engineering Application  $\rightarrow$  32  $\rightarrow$  325 Page

H.W  $\rightarrow$  1-4 page

Experiment No.1:Study of Microwave laboratory Components

Block diagram (P.S)

Lab report

Experiment No. 1

Microwave Test Bench Services

Nvis 9000 Series

Next experiment no

Date \_\_\_\_\_

Report \_\_\_\_\_

Lump parameter circuits

↳ Circulator, Attenuator, Isolator

Microwave Components

RF Component Test and their test 225

↳ Frequency and bandwidth measurement

Slot in section → 3 to 20 dB

Supply, power, matched termination

Match, Attenuation, component

Report: → 20

Lab test → 30 → Experiment theory

Filter and resonant

VNA test

Lab quiz → 20 → Short question

Attendance → 10

Viva → 20 → Lab + theory

Front page → Ex. Name

2nd , → Objectives (200 words) → Point 100 words

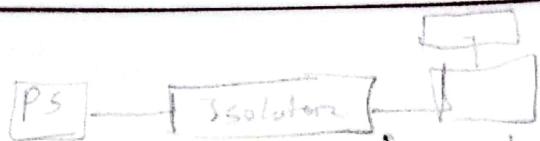
3. Theory4. Apparatus required

Block diagram

→ Ex-1 227 m/s

315 Ex. 21.3 with 3 m/s

5. Experimental Setup6. DataAnalysis7. Ans Result



## 8. Dissent-Discussion : Error (not yet)

Wet sand test condition  
wet sand test

## 2. Objectives:

→ Principal operation

### 3. Theoretical Background:

## 25. theory

### 1. Frequency

## 2. Maximum bias voltage

### 3. Power Output

Waveguides:

## \* Application of Microwaves

↳ softell. (31376B 2572B)

W - best marked - 3

← which will absorb it

Adm. disorder.

1. Voltage is not well defined. Chap 11 3

## 2. Expensive components

Electrically large  $\rightarrow$  starting point a voltage, 'way point'  $\Rightarrow$  voltage diff. 28

small  $\rightarrow$  ~~large~~  $\rightarrow$  same

3.

## 4. special wires

↳ wave guides

ME.

Maxwell's Equation  $\Rightarrow 4\pi T$

Book -1.2

## Solution of different eqn

$$\nabla \times \vec{E} = \frac{\partial \vec{B}}{\partial t} - \vec{A} \quad \rightarrow \text{effective current density} = 0$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} + \vec{j}$$

$$\nabla \cdot \bar{D} = 0$$

1758

$$\mathbf{r} \cdot \mathbf{B} = 0$$

Max Egn Adr.

## ↳ wave phenomena (524)

$E$  = Electric field  $\rightarrow \text{V/m}$

$H$  = Magnetic field  $\rightarrow \text{Nm}$

$D$  = Electric flux density  $\rightarrow$

$B$  = Magnetic  $\rightarrow$  units  $\text{Wb/m}^2$

$A = I \text{ m}$  Current density  $\rightarrow$  units  $\text{A/m}^2$

$J$  = Electric  $\rightarrow$  units  $\text{A/m}^2$

$P = \dots$  Charge  $\rightarrow$  units  $\text{C}$

Free space,

$$\bar{B} = \mu_0 \bar{H}$$

$$\bar{D} = \epsilon_0 \bar{E} \quad D = \epsilon_0 \bar{E}$$

$$\nabla \cdot \nabla \times \bar{H} = -\frac{\partial}{\partial t} (\nabla \cdot \bar{D}) + \nabla^2 P$$

$$\Rightarrow 0 = \frac{\partial P}{\partial t} + \nabla \cdot J$$

$$\nabla \cdot J + \frac{\partial P}{\partial t} = 0$$

Harmonic oscillations  $\rightarrow$

\*

$$\oint_C \bar{E} \cdot d\bar{l} = -\frac{\partial}{\partial t} \int_S \bar{B} \cdot d\bar{s} - \int_S \bar{H} \cdot d\bar{s}$$

$$P = \frac{\partial \phi}{\partial t} = 5 \text{ V}$$

$$E = 4 \text{ V}$$

$$B = 8 \text{ V}$$

Eqn-1

$$\frac{\partial}{\partial t} \rightarrow j\omega$$

↑  
Frequency

Time domain

$$\nabla \times \bar{E} = -j\omega \bar{B} - \bar{F}$$

$$\nabla \times \bar{H} = j\omega \bar{D} + \bar{G}$$

$$\nabla \cdot \bar{D} = 0$$

$$\nabla \cdot \bar{B} = 0$$

Another representation:

$$\bar{E}(x, y, z, t) = \bar{E}(x, y, z) \cdot e^{j\omega t + \phi}$$

$$E(x, y, z, t) = \operatorname{Re} [\bar{E}(x, y, z) e^{j\omega t}]$$

$$\nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t} - \bar{F}$$

$$\nabla \times \bar{E}(x, y, z, t) = -\frac{\partial \bar{B}}{\partial t}(x, y, z, t) - \bar{F}(x, y, z, t)$$

$$\nabla \times E(x, y, z) e^{j\omega t} = -\frac{\partial \bar{B}}{\partial t} \bar{B}(x, y, z) e^{j\omega t} - \bar{F}(x, y, z) e^{j\omega t}$$

$$e^{j\omega t} [\nabla \times E(x, y, z)] = -\bar{B}(x, y, z) (\frac{1}{j} \omega \cdot e^{j\omega t}) - \bar{F}(x, y, z) e^{j\omega t}$$

Sol:  $\nabla \times E(x, y, z) = -j\omega \bar{B}(x, y, z) - \bar{F}(x, y, z)$

\* Importance of Max. eqn: Micro. Eng.  $\rightarrow$  ~~Applications~~  
 $\hookrightarrow$  Wave  $\&$  characteristics

\* Different notations of Max. eqn.

\* Ant. 1-2

H.W.  $\rightarrow$  1-3 Ant.

Lab report-2

Ex. No-2

## Precautions:

(i) Keep all the knobs in minimum position before going to switch 'ON' the power supply of VSWR/Klystron power supplies.

Note: For klystron power supply "HT" should be 'OFF' before switching 'ON' the main supply.

(ii) Beam knob should be completely in anticlockwise direction and repeller voltage knob should be completely clockwise direction.

(iii) Switch on the main supply and give some warm up time to get current/accurate reading.

(iv) After the completion of experiment, before going to switch off the mains keep all the knobs in minimum position (i.e.) as those are in rule 1.

\* If the main supply failed in the middle of the experiment, come to 1st condition (i.e.) keep all the knobs in minimum position and switch off main switch, go to another experiment.

(v) Don't increase the repeller voltage more than  $-70V$ : (i.e) it should be between  $-70V$  to  $-270V$ .

### Ex No- 2:

Study of the characteristics of Klystron Tube and to determine its electronic tuning range.

Procedure  
L01 no 20

Modulation  $512\text{KHz}$  signal mix or  $\rightarrow$  Faraday grid

Maximum to minimum:

### Apparatus required:

1. Klystron power supply

2. Klystron tube with Klystron mount

3. Isolator

4. Frequency meter

5. Variable attenuator

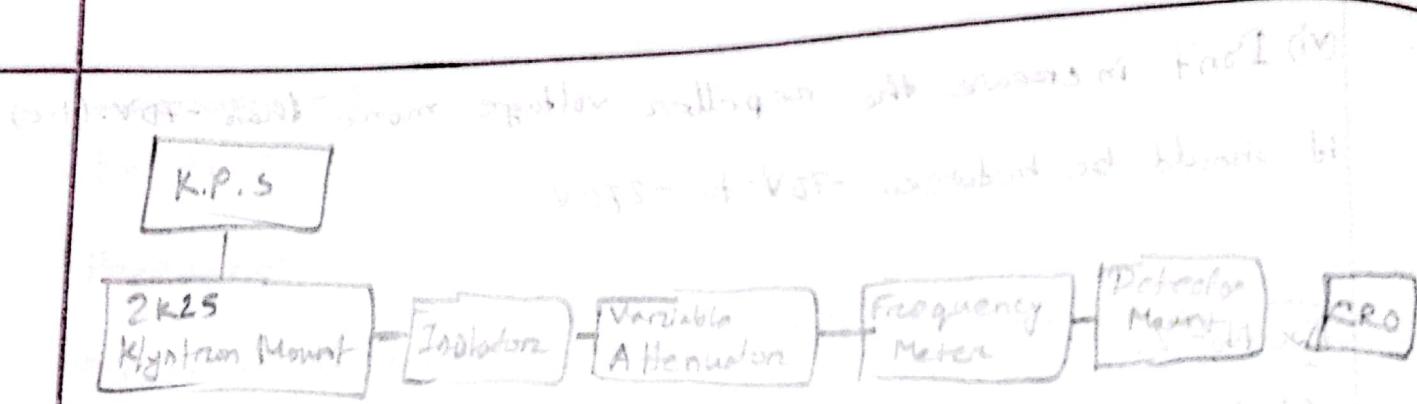
### Theory: $\rightarrow$ Principal of operation

Square wave operation  $\rightarrow$   $475$

Carrier  $u$   $\rightarrow$   $u \sin \omega t$

current  $i$   $\rightarrow$   $i = I_0 \sin \omega t$

resonant frequency  $\omega_0 = \sqrt{\frac{2\pi}{L}}$

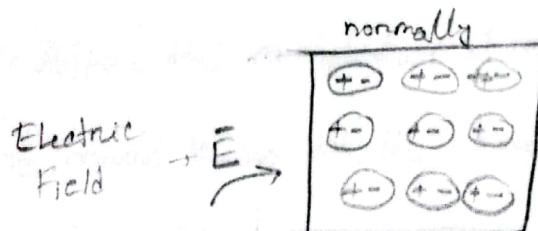


21-3-24

Sec-3

### Art. 1.3: Fields in media

Piece of electronic material



Any piece of dielectric material has dipoles that are randomly distributed. When an electric field is passed through this material polarization occurs.

$$D = \epsilon \cdot E + P_e \quad [ \because P_e = \text{electric polarization} ]$$

In linear medium,  $\rho_e \bar{P}_e = \epsilon_0 \chi_e \bar{E}$  [ :  $\chi_e$  = electric susceptibility ]

$$D = \epsilon_0 \bar{E} + \epsilon_0 \chi_e \bar{E} = \epsilon_0 (1 + \chi_e) \bar{E} = \epsilon \bar{E}$$

$$E = E' - jE'' = E_0(1 + x_e)$$

Imaginary part of Dielectric loss Represented by  
 $\downarrow$   
Dipole moment  $\propto$

The imaginary part  $(j\epsilon'')$  represents loss in the medium due to damping of the vibrating dipole moments.

In material with conductivity  $\sigma$ , a conduction current will exist.

From Maxwell curl equation for  $\vec{H}$  becomes,  $\nabla \times \vec{H} = \mu_0 \vec{D} + \vec{J}$

$$\begin{aligned}
 E &= E' - jE'' \\
 &= j\omega D + \sigma \bar{E} \\
 &= j\omega G \bar{E} + \sigma \bar{E} \\
 &\rightarrow \text{H} \quad = j\omega C' \bar{E} + (w\epsilon'' + \sigma) \bar{E} \\
 &= j\omega (E' - jE'' - j\frac{\sigma}{\omega}) \bar{E} \\
 &= j\omega \epsilon_0 \epsilon_r (1 - j \tan \theta) \bar{E}
 \end{aligned}$$

Where,  $\tan \delta = \frac{\omega E'' + \sigma}{\omega E'}$  represents loss tangent

Two types of Loss,  $\rightarrow$

1. Conductor loss ( $\sigma$ )

2. Dielectric loss ( $\tan \delta$ )

Conductor loss;

$$\tan \delta = \frac{\sigma}{\omega \epsilon}$$

Anisotropic material,  $\tan \delta$  is not the same as  $\epsilon$ .

The direction ~~of~~ of polarization is not the same as  $\vec{E}$ .

Ex: crystals      }       $\rightarrow$  ferrites - magnetic anisotropic material:  $\vec{E}$

ionized gas      }      electric anisotropic

electrolytes

electric anisotropic

material

$$\vec{P}_c, \vec{B} \rightarrow \vec{U} \vec{P} \vec{B}$$

$$\vec{P}_n, \vec{H}$$

Electric field  $\vec{E}$  and magnetic field  $\vec{B}$  are perpendicular to each other.

Electric field  $\vec{E}$  and magnetic field  $\vec{B}$  are perpendicular to each other.

$$\mathbf{D} = \mathbf{C} \mathbf{E}$$

PM  $\rightarrow$  Break

$$\text{Electrodes} \quad \begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \begin{bmatrix} \epsilon_{xx} & \epsilon_{xy} & \epsilon_{xz} \\ \epsilon_{yx} & \epsilon_{yy} & \epsilon_{yz} \\ \epsilon_{zx} & \epsilon_{zy} & \epsilon_{zz} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}$$

Similarly,

Magnetics

$$\begin{bmatrix} B_x \\ B_y \\ B_z \end{bmatrix} = \begin{bmatrix} \mu_{xx} & \mu_{xy} & \mu_{xz} \\ \mu_{yx} & \mu_{yy} & \mu_{yz} \\ \mu_{zx} & \mu_{zy} & \mu_{zz} \end{bmatrix} \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix} = [\mu] \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix}$$

Ex: Anisotropic materials

$$\epsilon = \epsilon_0 \begin{bmatrix} 2 & -2j & 0 \\ 2j & 3 & 0 \\ 0 & 0 & 4 \end{bmatrix}$$

$$\mathbf{E} = 2\hat{x} + 3\hat{y} + 4\hat{z} \quad \text{what is } \mathbf{D} = ?$$

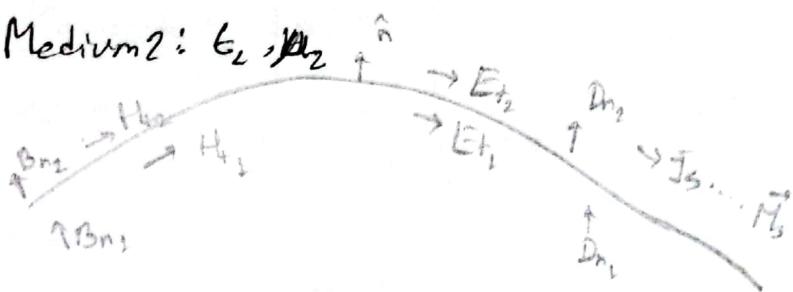
$\Rightarrow$

$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \epsilon \begin{bmatrix} 2 & -2j & 0 \\ 2j & 3 & 0 \\ 0 & 0 & 4 \end{bmatrix} \begin{bmatrix} 2 \\ 3 \\ 4 \end{bmatrix}$$

$$= \begin{bmatrix} 2 - 6j \\ 4j + 9 \\ 0 + 0 + 16 \end{bmatrix}$$

Boundary condition.

Medium 2:  $\epsilon_2, \mu_2$



Medium 1:  $\epsilon, \mu$

18.

$$\hat{n} \cdot (\bar{D}_2 - \bar{D}_1) = J_s$$

$$\Rightarrow \hat{n} \cdot \bar{B}_1 = \hat{n} \cdot \bar{B}_2$$

$$\Rightarrow (\bar{E}_2 - \bar{E}_1) \times \hat{n} = \bar{M}_s$$

$$\Rightarrow \hat{n} \times (\bar{H}_2 - \bar{H}_1) = \bar{J}_s$$

Boundary conditions at a dielectric interface,

$$J_s = 0$$

$$J_s = 0$$

Conditions:

$$\hat{n} \cdot \bar{D}_1 = \hat{n} \cdot \bar{D}_2$$

$$\hat{n} \cdot \bar{B}_1 = \hat{n} \cdot \bar{B}_2$$

$$\hat{n} \cdot \bar{E}_1 = \hat{n} \times \bar{E}_2$$

$$\hat{n} \times \bar{H}_1 = \hat{n} \times \bar{H}_2$$

Normal Flux density  
is continuous

Tangential  
Field intensity is continuous

\* At Medium 2:  $\mu_2 > \mu_1$  Dielectric force  $\propto \epsilon_2 \epsilon_1$  where  $\epsilon_2 > \epsilon_1$

H.W) Boundary condition at the interface with a perfect conductor.

→ magnetic wall.

H.W.

22-3-24  
Lec-

1.4. The wave eqn and basic plane wave solution

Study of scattering of waves and waves in a dielectric.

The helmholtz equation:

Plane wave in a lossless medium

at half period as done at physics and Fourier analysis

Ex-1.1

Plane waves reflected and waves set to attenuate

Plane waves in a general lossy medium

Plane waves in a good conductor

Ex-1.2

Study of scattering of waves with loss and lossy

EEB 4308-L1-3

PDF

at half period as done at physics and Fourier analysis

Ch-2

T-Line/Transmission Line

→ propagation delay

\*  $\lambda_{air}$ ,  $\lambda_{water}$  are 325?

↓  $\lambda$  (period) with propagation delay as path length

Whether the simple circuit laws may be used depends on the size of our circuit in relation to the wavelength corresponding to the operating frequency.

Size of circuit is now for a particular dimension  $\lambda$  (path length)

The relation between wavelength and operating frequency

$$\lambda = \frac{c}{f}$$

Lumped element description:

If the size of the circuit (or element) in question is much smaller than the operating wavelength ( $\approx \lambda/100$  or smaller), the simple circuit laws apply. In such a case, we say that the elements of the circuit are "lumped" elements.

If the size of the circuit in question is comparable to that of the operating wavelength ( $\approx \lambda/10$  to  $-\lambda$ ), the simple circuit laws do not apply. In such a case, we say that the elements of the circuit are "distributed" elements.

\* Why do we need transmission line theory?

\* Co-axial cable

\* Parallel Plate

\* Two-wire

\* T-line Current, voltage or wave represent z0,

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\* T-line or current voltage or wave to represent ~~and~~

2 waves  $\rightarrow$  1. Electric, 2. Magnetic

\* T-line  $\rightarrow$  2 br conductors ~~2 wires~~ Always

RLGC Model

Conduction  $\rightarrow$  displacement current

2 conductors

2 conductors

# Conduction current impedance

$$\sqrt{R} = [A/m] \rightarrow \text{Loss component}$$

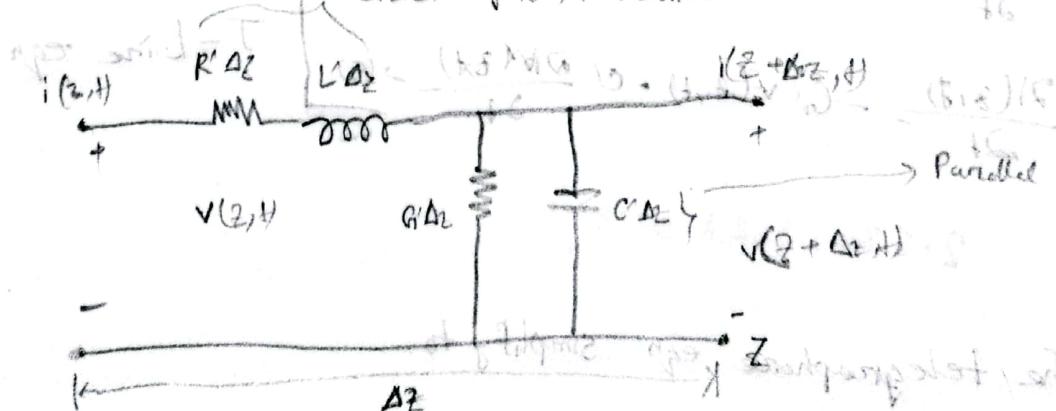
$$L' = [H/m] \rightarrow (A/m) \cdot (A/m) \cdot (H/m) = (A^2 H/m) = \text{NA}^2$$

# Displacement current impedance

$$\sqrt{G} = [S/m]$$

$$C' = [F/m]$$

R G circuit  $\rightarrow$  Loss (or represent ~~loss~~)  $\rightarrow$  Series Register, inductance



$$2\text{-wire T-line} \rightarrow \frac{1}{j\omega C' \Delta z} + \frac{1}{j\omega L' \Delta z} = \frac{1}{j\omega C' \Delta z} + \frac{1}{j\omega L' \Delta z}$$

$$j\omega C' \Delta z + j\omega L' \Delta z = j\omega C' \Delta z + j\omega L' \Delta z$$

→ 4 Dr parameter  $\rightarrow V, I$

T-line  $\rightarrow$  shorting  $V, I$   $\rightarrow$  shorting  $V, I$

$V(z,t), i(z,t) = ?$

After applying KVL  $\rightarrow V(z,t)$

$$V(z,t) = V(z + \Delta z, t) + i(z,t) R' \Delta z + L' \Delta z \frac{\partial i(z,t)}{\partial t}$$

$$\Delta V = V(z + \Delta z, t) - V(z, t) = -i(z,t) R' \Delta z - L' \Delta z \frac{\partial i(z,t)}{\partial t} \rightarrow (1a)$$

After applying KCL  $\rightarrow i(z,t)$

$$i(z,t) = i(z + \Delta z, t) + V(z + \Delta z, t) G' \Delta z + C' \Delta z \frac{\partial V(z + \Delta z, t)}{\partial t}$$

$$\Delta i = i(z + \Delta z, t) - i(z, t) = -V(z + \Delta z, t) G' \Delta z - C' \Delta z \frac{\partial V(z + \Delta z, t)}{\partial t} \rightarrow (1b)$$

Divide (1a) and (1b) by  $\Delta z$  and taking the limit as  $\Delta z$  tends to 0.

$$\Delta z \rightarrow 0$$

$$\cancel{V(z + \Delta z)}$$

$$\frac{\partial V(z, t)}{\partial z} = -R' i(z, t) - L' \frac{\partial i(z, t)}{\partial t} \rightarrow (4) \quad \text{Telegrapher eqn/}$$

$$\frac{\partial i(z, t)}{\partial z} = -G' V(z, t) - C' \frac{\partial V(z, t)}{\partial t} \rightarrow (5) \quad \text{T-Line eqn}$$

2.23a, 2.23 b  $\rightarrow$  eqn

The telegrapher eqn simplify to,

$$\frac{\partial V(z)}{\partial z} = -(R + j\omega L) I(z)$$

$$\frac{\partial I(z)}{\partial z} = -(G + j\omega C) V(z)$$