

reference: Microwave Engineering

Date -
29.02.24

— David M. Pozar
4th ed

microwave frequency $[300 \text{ MHz} - 300 \text{ GHz}]$
— $[3 \text{ GHz} - 300 \text{ GHz}]$

wavelength — $[1 \text{ m} - 1 \text{ mm}]$
— $[3 \text{ GHz} - 30 \text{ GHz}]$

* why are microwave frequencies are in much interest

— advantages:

— Bandwidth and capacity

— Antenna size.

suppose,
we need to transmit 4 kHz voice signal through a wireless link.

lets assume that we have ^{two} wireless system to choose from one, operating at 500 MHz and the second at 4 GHz ; each with a 10% bandwidth around its capacity.

$$\text{Number of channels} = \frac{\text{operating frequency} \times \text{percent BW}}{\text{BW per channel}}$$
$$= \frac{0.5 \text{ GHz} \times 0.1}{4 \text{ kHz}} = 12,500$$

BW = Bandwidth

$$\therefore \text{Number of channels} = \frac{4 \text{ GHz} \times 0.1}{4 \text{ kHz}} = 100,000$$

frequency \uparrow capacity \uparrow

Another adv-

small size antenna वाताहत रहन frequency माफात
रह, [article - 1.1 (table)]
- Higher Bandwidth. fig - 1.1 (Band name)

circuit Theory VS EM field theory

SDHz का frequency - device - AC current

Microwave device - structure बढ़, | Em field
wavelength छोटे, (microwave का सिग्नल)

lumped parameter - structure का लम्बाई
wave length बढ़,

distributed parameter - structure का मापना
wave length छोटे, प्रतिष्ठित current/voltage माप

* General electric circuit - Transistor, FET, MOSFET

* Microwave circuit element - Diode, Tunnel
diode, varactor diode.

* Distributed " " - Isolator, circulator, attenuator

* Klystron Oscillator - microwave

Magnetron "

TWT "

* Antenna converter.

→ compare between electrical circuit and microwave circuit.

→ frequency तब कि जब transmission line or wavelength का की परिवर्तन आता है?

→ microwave heating की बहुत generate करता

Adv- of Antenna size (smaller)

— frequency $f = 300 \text{ MHz}$

$$\lambda = c/f$$
$$= \frac{3 \times 10^8}{300 \times 10^6} = 1 \text{ m}$$

Beamwidth = 100°

$$\text{Diameter } D = 140 \times \frac{\lambda}{B}$$
$$= 140 \times \frac{1}{100}$$
$$= 1.4'$$

[marconny antenna
आकार का होता है]

Second scenario

$f = 30 \text{ GHz}$

$$\lambda = c/f = \frac{3 \times 10^8}{30 \times 10^9} = 0.01$$

$$D = 140 \times \frac{0.01}{100}$$
$$= 0.014'$$

—Application of microwave (Art-1.1-Page-3)

* Microwave Engineering - कौनसा signal generate करेगा,

Lab-01

07.03.21

Ex-01: study of microwave Laboratory components

Lumped parameter

70
— Lab test — 30
— II Report — 20
— Quiz — 20

30
attendance — 10
viva — 20

Front page to Ex. Name लिखें,

— Objective इसका शुरू

1.
2.
3.

— Theoretical background

— Apparatus required

— Experimental set up: circuit with procedure

— Experimental data

— Result analysis

— Discussion [देखें] fulfill रहा किना

Test Bench [Nris 9000]

* several application of microwave Engineering

difficulties:

1. voltage is not well defined [electrical small circuit
ଏହା ଦୁଇଟି ବସ୍ତୁ ମଧ୍ୟରେ ଥିବା
voltage ପାଇଁ]
2. more expensive components
3. one must carefully choose lumped circuit elements
4. To transmit electrical signals from one position to another.

* Maxwell Equation [Art-1.2]

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} - \vec{M} \quad \text{--- (i)}$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} + \vec{J} \quad \text{--- (ii)}$$

$$\nabla \cdot \vec{D} = \rho \quad \text{--- (iii)}$$

$$\nabla \cdot \vec{B} = 0 \quad \text{--- (iv)}$$

* Adv of Maxwell Equation

$$\vec{B} = \mu_0 \vec{H}$$

$$\vec{D} = \epsilon_0 \vec{E}$$

(1) $\nabla \cdot \nabla \times \vec{H} = \frac{\partial}{\partial t} (\nabla \cdot \vec{D}) + \nabla \cdot \vec{J}$

$$\Rightarrow 0 = \frac{\partial \rho}{\partial t} + \nabla \cdot \vec{J}$$

$$\nabla \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0$$

\vec{M} - magnetic current density

\vec{J} - Electric current density

\vec{E} - electric field

\vec{H} - magnetic "

\vec{D} = electric flux density

ρ = electric charge density.

$\mu_0 = 4\pi \times 10^{-7}$ henry

ϵ_0 = permittivity

* Ampere's Law

* Stokes theory

$$\oint_C \vec{E} \cdot d\vec{s} = - \frac{\partial}{\partial t} \int_S \vec{B} \cdot d\vec{s} - \int_S \vec{M} \cdot d\vec{s}$$

$$\oint_C \vec{H} \cdot d\vec{l} = \frac{\partial}{\partial t} \int_S \vec{D} \cdot d\vec{s} + \int_S \vec{J} \cdot d\vec{s} = \frac{\partial}{\partial t} \int_S \vec{D} \cdot d\vec{s} + I$$

$\frac{\partial}{\partial t} \rightarrow j\omega$
 \downarrow
 time domain $\quad \downarrow$ frequency domain

$$-\nabla \times \vec{E} = -j\omega \vec{B} - \vec{M}$$

$$-\nabla \times \vec{H} = j\omega \vec{D} + \vec{J}$$

$$-\nabla \cdot \vec{D} = \rho$$

$$-\nabla \cdot \vec{B} = 0$$

$$\vec{E}(x, y, z, t) = \text{Re} [\vec{E}(x, y, z) e^{j\omega t}]$$

$$\nabla \times \vec{E} = \frac{-\partial \vec{B}}{\partial t} - \vec{M}$$

$$\nabla \times \vec{E}(x, y, z, t) = \frac{-\partial \vec{B}}{\partial t}(x, y, z, t) - \vec{M}(x, y, z, t)$$

$$\nabla \times \vec{E}(x, y, z) e^{j\omega t} = \frac{-\partial}{\partial t} \vec{B}(x, y, z) e^{j\omega t} - \vec{M}(x, y, z) e^{j\omega t}$$

$$e^{j\omega t} [\nabla \times \vec{E}(x, y, z)] = -\vec{B}(x, y, z) (j\omega \cdot e^{j\omega t}) - \vec{M}(x, y, z) e^{j\omega t}$$

$$\nabla \times \vec{E}(x, y, z) = -j\omega \vec{B}(x, y, z) - \vec{M}(x, y, z)$$

Home work

- The importance of Maxwell equation
- Microwave is equation or not a equation, what wave is and its use.
- Different notation of Maxwell equation or, what that equation is or represent what.

Art - [1.2, 1.3 - fields in media and...]

Micro lab - 2

Precaution

- I. Main power supply knob minimum position or 25, RT should be 'OFF' before switching 'ON' the main supply.
- II. Beam knob should be anticlockwise and repeller voltage knob should be clockwise.
- III. Switch on the main supply and some warm up time to get current.
- IV. Fans use for 25 to make the power supply cool down.

v. ON and off button press કરવા માટે knob minimum position (અડધા પર),

VI. Don't increase the repeller voltage more than $-70V$. It should be between $-70V$ to $-290V$

Ex-2:

Study of the characteristics of kryston tube and to determine its electronic tuning range.

- modulation કરતાં signal નો કોઈ માપદંડ નથી, માત્ર સ્થિતિ જોઈ શકાય છે,
- front panel control

objective

— Apparatus required

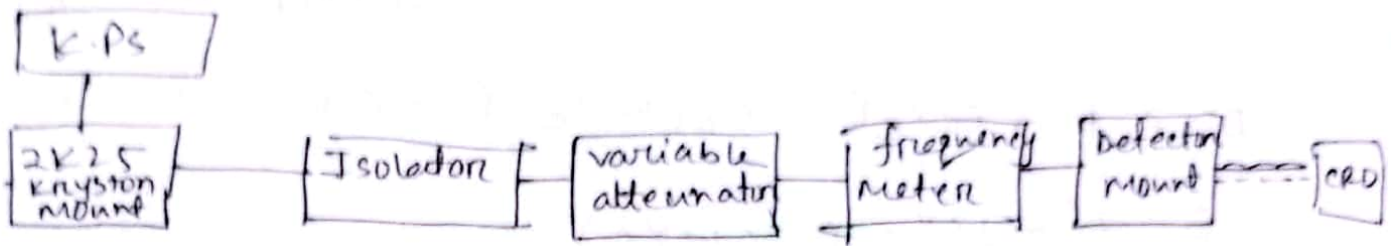
1. kryston power supply
2. kryston tube with kryston mount
3. Isolator
4. Frequency meter
5. variable attenuator
6. detector mount.

Theory—

Principle of operation.

—square wave operation

Experimental setup

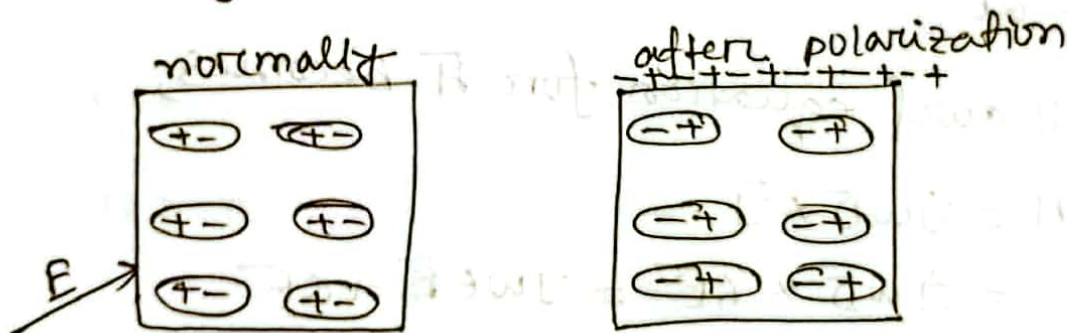


Lecture-3

21.03.24

Art-1.3 [fields in media]

Piece of dielectric material



Any piece of dielectric material has dipoles that are randomly distributed. When an electric field is passed through this material polarization occurs.

$$D = \epsilon_0 \bar{E} + \bar{P}_e \quad [\because \bar{P}_e = \text{electric polarization}]$$

In Linear medium,

$$\bar{P}_e = \epsilon_0 \chi_e \bar{E} \quad [\because \chi_e = \text{electric susceptibility}]$$

$$\bar{D} = \epsilon_0 \bar{E} + \epsilon_0 \chi_e \bar{E} = \epsilon_0 (1 + \chi_e) \bar{E} = \epsilon \bar{E}$$

$$\epsilon = \epsilon' - j\epsilon'' = \epsilon_0 (1 + \chi_e)$$

The imaginary part of $(j\epsilon'')$ represents loss in the medium due to damping of the vibrating dipole moments

In material with conductivity σ , a conduction current will exist.

$$\bar{J} = \sigma \bar{E}$$

From Maxwell curl equation for \bar{H} becomes;

$$\nabla \times \bar{H} = j\omega \bar{D} + \bar{J}$$

$$= j\omega \bar{D} + \sigma \bar{E} = j\omega \epsilon \bar{E} + \sigma \bar{E}$$

$$= j\omega \epsilon' \bar{E} + (\omega \epsilon'' + \sigma) \bar{E}$$

$$= j\omega (\epsilon' - j\epsilon'' - j\frac{\sigma}{\omega}) \bar{E}$$

$$= j\omega \epsilon_0 \epsilon_r (1 - j \tan \delta) \bar{E}$$

where, $\tan \delta = \frac{\omega \epsilon'' + \sigma}{\omega \epsilon'}$ represents loss tangent.

Two types of loss

- conduction loss (σ)
- Di-electric loss ($\sigma \epsilon''$)

$$\text{conductor loss, } \tan \delta = \frac{\sigma}{\omega \epsilon'}$$

Anisotropic material:

The direction of polarization is not the same as E .

example:

crystals
ionized gas

electric
anisotropic
material

example:

ferrites — magnetic
Anisotropic
material

P_e = electric polarization

P_m = magnetic "

E = Electric "

H = magnetic "

P_e, E
Direction similar —
Isotropic
|| not similar —
Anisotropic

$$\text{Electric } \begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \begin{bmatrix} \epsilon_{xx} & \epsilon_{xy} & \epsilon_{xz} \\ \epsilon_{yx} & \epsilon_{yy} & \epsilon_{yz} \\ \epsilon_{zx} & \epsilon_{zy} & \epsilon_{zz} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} = [\epsilon] \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}$$

$$\boxed{D = \epsilon E}$$

$$\boxed{B = \mu H}$$

Similarly,

magnetic,

$$\begin{bmatrix} B_x \\ B_y \\ B_z \end{bmatrix} = \begin{bmatrix} \mu_{xx} & \mu_{xy} & \mu_{xz} \\ \mu_{yx} & \mu_{yy} & \mu_{yz} \\ \mu_{zx} & \mu_{zy} & \mu_{zz} \end{bmatrix} \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix} = [\mu] \begin{bmatrix} H_x \\ H_y \\ H_z \end{bmatrix}$$

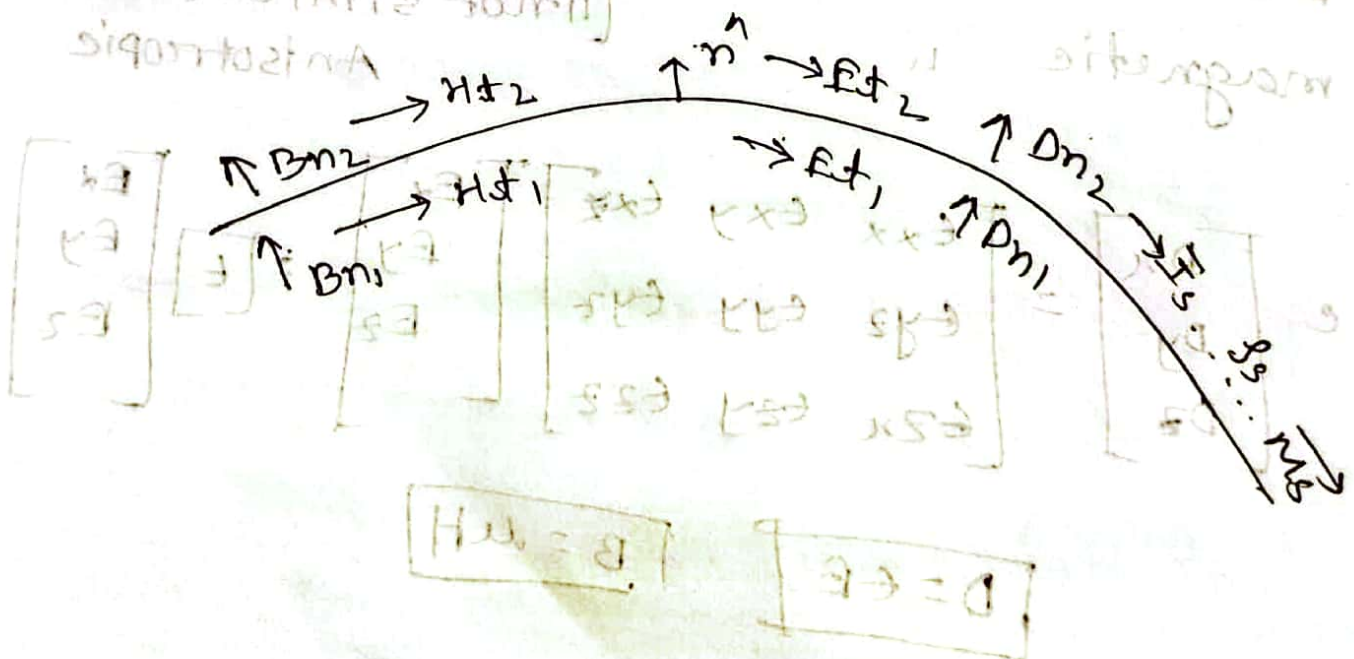
Example :

Anisotropic material, $\epsilon = \epsilon_0 \begin{bmatrix} 1 & -2j & 0 \\ 2j & 3 & 0 \\ 0 & 0 & 4 \end{bmatrix}$

$E = 2\hat{x} + 3\hat{y} + 4\hat{z}$, what is $\bar{D} = ?$

Boundary condition :

medium 2: $\epsilon_2 = \mu_2$



Medium 1: ϵ_1, μ_1

$$\hat{n} \cdot (\vec{D}_2 - \vec{D}_1) = \rho_s$$

$$\hat{n} \cdot \vec{B}_1 = \hat{n} \cdot \vec{B}_2$$

$$(\vec{E}_2 - \vec{E}_1) \times \hat{n} = \vec{M}_s$$

$$\hat{n} \times (\vec{H}_2 - \vec{H}_1) = \vec{J}_s$$

boundary conditions at a dielectric interface,

$$\rho_s = 0$$

$$\vec{J}_s = 0$$

conditions:

$$\left. \begin{aligned} \hat{n} \cdot \vec{D}_1 &= \hat{n} \cdot \vec{D}_2 \\ \hat{n} \cdot \vec{B}_1 &= \hat{n} \cdot \vec{B}_2 \end{aligned} \right\} \begin{array}{l} \text{normal flux density is} \\ \text{continuous} \end{array}$$

$$\left. \begin{aligned} \hat{n} \times \vec{E}_1 &= \hat{n} \times \vec{E}_2 \\ \hat{n} \times \vec{H}_1 &= \hat{n} \times \vec{H}_2 \end{aligned} \right\} \begin{array}{l} \text{Tangential field intensity} \\ \text{is continuous.} \end{array}$$

→ Boundary conditions at the interface with a perfect conductor.

→ Boundary conditions at the interface with a magnetic wall.

1.4

1.4
The wave eqn and basic plane wave solution

- The helmholtz equation

- The helmholtz equation
- plane wave in a lossless medium.

Exp-1.1.

A-1.1
plane waves in a general lossy medium.

plane. " " " good conductor.

Example - 1.2

chap-2

T-line Theory

Whether the simple circuit laws may be used depends on the size of our circuit in relation to the wavelength corresponding to the operating frequency.

$$\lambda = c/f$$

The relation between wave-length and the operating frequency.

- If the size of the circuit (or element) in question is much smaller than the operating wavelength ($\lambda/100$ or smaller), the simple circuit laws apply. In such a case, we say that the elements of the circuit are "Lumped" elements.

- If the size of the circuit question is comparable to that of the operating wavelength ($\sim \lambda/10$ to λ), the simple circuit laws do not apply. In such a case, we say that the elements of the circuit are "distributed" elements.

Lumped: resistor, capacitor

Distributed: T-lines.

Art (2.1)

- TEM fields (Transverse electromagnetic fields)

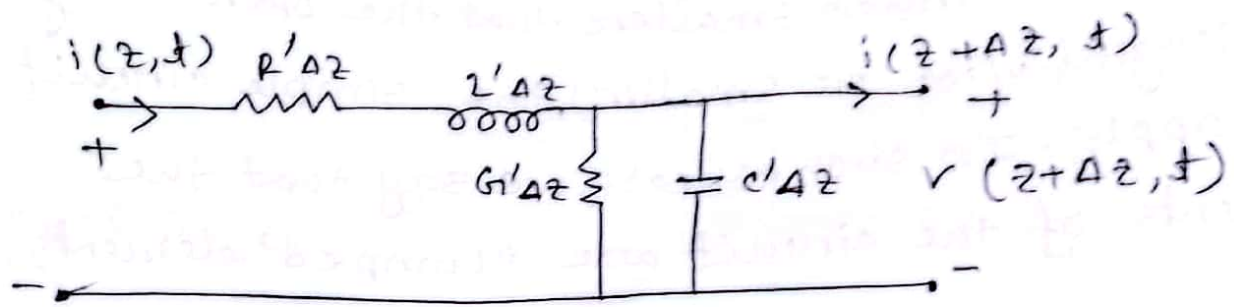
- RLC model

conduction current $\left[\begin{array}{l} R' - \text{series resistance (}\Omega/\text{m)} \\ L' - \text{" inductance (nH/m)} \end{array} \right.$

Displacement current $\left[\begin{array}{l} G' - \text{shunt conductance (S/m)} \\ C' - \text{" capacitance (f/m)} \end{array} \right.$

[R' and G' represent loss in circuit]

Generic equivalent-circuit model:



— After applying KVL, governing equation for

$v(z, t)$:-

$$v(z, t) = v(z + \Delta z, t) + i(z, t)R'\Delta z + L'\Delta z \frac{\partial i(z, t)}{\partial t} \quad \text{--- 1(a)}$$

$$\Delta v = v(z + \Delta z, t) - v(z, t)$$

$$= -i(z, t)R'\Delta z - L'\Delta z \frac{\partial i(z, t)}{\partial t}$$

— for current $i(z, t)$, apply KCL at Node A

$$i(z, t) = i(z + \Delta z, t) + v(z + \Delta z, t)G'\Delta z + C'\Delta z \frac{\partial v(z + \Delta z, t)}{\partial t} \quad \text{--- 1(b)}$$

Divide 1(a) and 1(b) by Δz and taking the limit as $\Delta z \rightarrow 0$

$$\frac{\partial v(z, t)}{\partial z} = -R'i(z, t) - L' \frac{\partial i(z, t)}{\partial t}$$

$$\frac{\partial i(z, t)}{\partial z} = -G'v(z, t) - C' \frac{\partial v(z, t)}{\partial t}$$

These are called 'Telegrapher's equations'
'T-line equations'

$$\frac{\partial V(z)}{\partial z} = -(R + j\omega L) I(z) \quad (2.3a)$$

$$\frac{\partial I(z)}{\partial z} = -(G + j\omega C) V(z) \quad (2.3b)$$

Transmission line parameters are
I and V are,

[Art - 2.1, 2.2, 2.3]

CT-chap-1

chap-2 (2.1, 2.2, 2.3)

Lect-5 (online) 23.04.24

(2.2a) (2.2b) equation

↓

Solution

(2.3a) (2.3b)

Wave propagation on a Transmission line:

$$(2.4a) \quad \frac{d^2 V(z)}{dz^2} - \gamma^2 V(z) = 0$$

$$(2.4b) \quad \frac{d^2 I(z)}{dz^2} - \gamma^2 I(z) = 0$$

$\gamma \rightarrow$ complex
Propagation

$$\gamma = \alpha + j\beta = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$V(z) = V_0^+ e^{-\gamma z} + V_0^- e^{\gamma z} \quad (2.6a)$$

$$I(z) = I_0^+ e^{-\gamma z} + I_0^- e^{\gamma z} \quad (2.6b)$$

সামান্য দিকে যে wave থাকে তা forward voltage/wave - V_0^+

বিপরীত দিকে যাওয়ায় wave - Reflected wave - V_0^-

$$Z_0 = \frac{R + j\omega L}{\gamma} = \sqrt{\frac{R + j\omega L}{G + j\omega C}} \quad (2.7)$$

↓
Characteristic Impedance

The reflection coefficient

$$(2.8) \quad \frac{V_0^+}{I_0^+} = Z_0 \frac{-V_0^-}{I_0^-} \quad \left[\begin{array}{l} \text{direction বাক্য} \\ \text{impedance বাক্য} \\ \text{negative ২য় স্র} \end{array} \right]$$

$$(2.9) \quad V(z, t) = (|V_0^+| \cos(\omega t - \beta z + \phi^+) e^{-\alpha z} + |V_0^-| \cos(\omega t + \beta z + \phi^-) e^{\alpha z})$$

$$(2.11) \quad v_g = \frac{\omega}{\beta} = \lambda f$$

एक transmission line draw करें,

The lossless line [transmission line absolutely lossless लाइन]

$R, G \rightarrow$ lossless लाइन represent करें,

attenuation const zero.

(2.13)

low loss transmission line :

condition :

Distortion less line (लाइन use करें लाइन लाइन)

Art-2.7

lossy transmission line (low loss distortion)

$$(2.82) \gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

Homework

Ex-2.6 $R/2 = \frac{G}{C}$

Art-2.88

Art-2.7

Ex-2.1

Art
Next class - 2.2 (Field Analysis)

Art - 2.3 - The terminated lossless Transmission Line

2.2 Field Analysis of transmission line.

* telegrapher equation

$$\left. \begin{array}{l} (2.18) \\ (2.19) \\ (2.20) \end{array} \right\} \text{Fig-2.3}$$

Example - 2.1

Table - 2.1

How to calculate the permittance of coaxial cable

Art-2.3 The terminated lossless transmission line

Fig-2.4

$\beta = \text{phase constant}$

* reflected wave

Eq (2.34a) (2.34b)

eq (2.35)

* standing still wave

matched condition

$$\Gamma = 0 \quad \text{or} \quad \Gamma = 0$$

there is no reflected wave,

voltage is min,

max

mismatch condition

$$\Gamma = 1 \quad \text{or} \quad \Gamma = 1$$

V_{max}

V_{min}

max

load is pure resistive

$Z_L = Z_0$ or $Z_L = Z_0$

or, $Z_L \neq Z_0$

(2.37), (2.38) \rightarrow matched loss
Reflection coefficient standing wave ratio,

(2.39)

(2.40a), (2.40b), (2.41)

SWR = min, max ∞

* 2 এর মান ক্ষুদ্রতম মান,

$\lambda/2$, two successive minimum

* SWR এর মান যত্ন না কি কম মান উদ্ভব?

Homework - 2.42

(2.43) (2.44)

lec-7

25-9-24

Minimum impedance মান max voltage ratio,
eq (2.43) (2.44)

* special case

* terminated in short circuit

short circuit,

$$V = 0, I = \infty$$

R_L, Z_L, I_L, V_L [একই স্থান]

(2.45c) Fig-2.6, 2.7

transmission line in open circuit

$$I=0 \quad V=\infty \quad Z_L=\infty$$

eq (2.44), (2.46c) (2.47) (2.48)

$$\downarrow$$
$$Z_{in} = Z_L$$

$$\downarrow$$
$$Z_{in} = \frac{Z_0^2}{Z_L}$$

— Transmission co-efficient

(2.49)

(2.50b) . (2.51) (2.52)

Desire convert NP to

vice-versa

* Smith chart.

lect-8

28-4-24

* construction of Smith chart

* Smith chart parametric Equation

Q2: How this resistance circle created

|| || reactance || ||

* complete the Smith chart

$$Z_L = (300 - j25) \Omega$$

$$Z_0 = 50 \Omega$$

$$Z_L' = (300/50 - j 25/300) \Omega$$

$$= (6 - j0.5) \Omega$$

$\uparrow \quad \uparrow$
R X_L

[measurement error]



માન સામાન્ય હોતી રીત

Exm ૫ માં મમકુર રીત,

lec-9

02-4-24

- How to calculate SWR

* Reflection co-efficient

* angle of reflection

— magnitude

— angle

31.65° → angle

↓
magnitude

Example
(4.2)

load impedance

Ex-2.4

ch-3

Transmission line and

[wave guide

→ high frequency electromagnetic
way to transmit data]

* difference between

waveguide| transmission line |co-axialloss at,
power loss,
expensiveexpensive
or,
TEM wave
to propagate
is not possible,

— Transmission line or? or? or?

waveguide

" "

— can wave can waveguide support
or?

Art-3.1 ↗

[Home work]