

Partitioned Nonlinear Structural Analysis of Wind Turbines using BeamDyn



Qi Wang, Michael A. Sprague
Jason Jonkman, Bonnie Jonkman

National Renewable Energy Laboratory

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Background

- ▶ Previous beam model used in FAST (v7.0 and ElastoDyn module of v8.0)
 - Euler-Bernoulli beam model with shortening effect
 - Two degree-of-freedom (No torsion, shear, and axial DoFs)
 - Assumed-mode method (Two bending modes in one direction)
- ▶ Beam models used in other wind turbine tools
 - Multibody-formulation
 - Linear beam models
 - Constraints introduced between linear beams to describe large deflections and rotations
 - Finite element method
- ▶ Partitioned Analysis
 - FAST modularization framework
 - Tight coupling
 - Loose coupling

Objective

- ▶ Objective: create efficient high-fidelity beam models for wind turbine blade analysis
 - Based on Geometrically Exact Beam Theory (GEBT)
 - Advanced numerical techniques for implementation
 - Achieve the speed of computational design without significant loss of accuracy comparing to the ultimate accuracy obtained by 3D nonlinear FEA
 - Compatible with the FAST modularization framework
 - Verification and Validation



NWTC static and dynamic blade tests showing typical large, elastic deflections.

Approach

- ▶ Implementation
 - Geometrically Exact Beam Theory (GEBT)

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 - Mixed implementation (Yu and Blair, 2012; Wang et al., 2013)
- Legendre Spectral Finite Element (LSFE) (Patera, 1984)

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 - A p -version high-order finite element
 - Successfully applied to simulation of fluid dynamics, geophysics, elastodynamics
 - Limited usage in structural dynamics
- FAST Modularization Framework (Jonkman, 2013; Sprague et al., 2015)
 - Loose coupling
 - Predictor-correction

► BeamDyn, an alternative of ElastoDyn in FAST for blades

► Governing Equation

$$\begin{aligned}\dot{\underline{h}} - \underline{F}' &= \underline{f} \\ \dot{\underline{g}} + \ddot{\underline{u}}\underline{h} - \underline{M}' - (\tilde{x}'_0 + \tilde{u}')\underline{E} &= \underline{m}\end{aligned}$$

► Constitutive Equation

$$\begin{aligned}\begin{Bmatrix} \underline{h} \\ \underline{g} \end{Bmatrix} &= \underline{\underline{\mathcal{M}}} \begin{Bmatrix} \dot{\underline{u}} \\ \underline{\omega} \end{Bmatrix} \\ \begin{Bmatrix} \underline{F} \\ \underline{M} \end{Bmatrix} &= \underline{\underline{\mathcal{C}}} \begin{Bmatrix} \underline{\epsilon} \\ \underline{\kappa} \end{Bmatrix}\end{aligned}$$

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- Timoshenko-like beam model

► Strain Measures

$$\begin{Bmatrix} \underline{\epsilon} \\ \underline{\kappa} \end{Bmatrix} = \begin{Bmatrix} \underline{x}'_0 + \underline{u}' - (\underline{R} \underline{R}_0) \bar{l}_1 \\ \underline{k} \end{Bmatrix}$$

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- Timoshenko-like beam model
- Geometrically exact: deformed beam geometry is represented exactly

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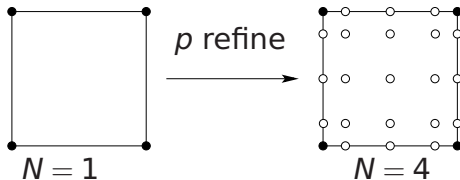
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- $\underline{\underline{M}}$ and $\underline{\underline{C}}$ are 6×6 sectional mass and stiffness matrices, respectively
- Elastic couplings are captured
- Timoshenko-like beam model
- Geometrically exact: deformed beam geometry is represented exactly
- Small strains

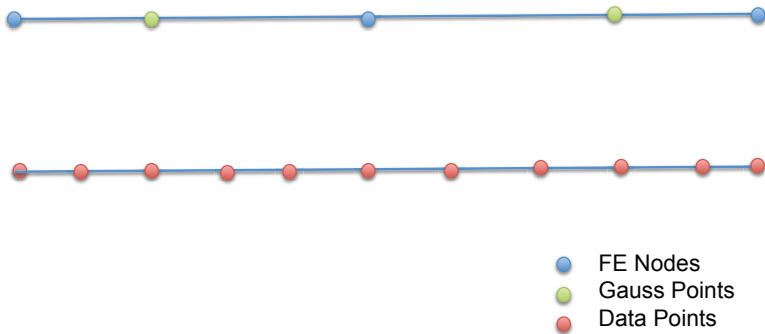
Legendre Spectral Finite Elements

- ▶ LSFE methods combine the geometric flexibility of the FE method with the accuracy of global spectral methods.
 - Solution improved through increased basis polynomial order (p -refinement)
 - LSFEs employ Lagrangian interpolant shape functions with nodes at Gauss-Lobatto-Legendre (GLL) points
 - *Exponential* convergence rates for sufficiently smooth solutions



Numerical Integration

- ▶ FE Node, Integration Point, and Data Point



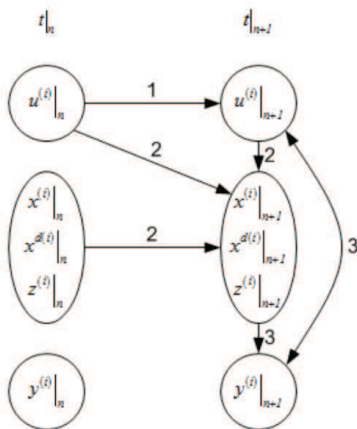
- ▶ Gauss Integration
- ▶ Trapezoidal-Rule Integration

$$\int_a^b f(x)dx \approx \frac{1}{2} \sum_{k=1}^N (x_{k+1} - x_k) [f(x_{k+1}) + f(x_k)]$$

Partitioned Analysis

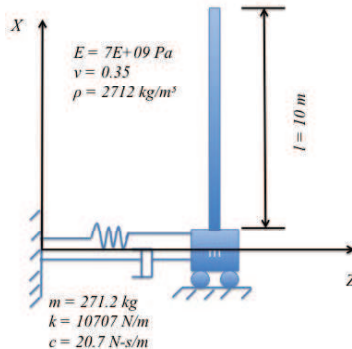
► Module Coupling Algorithm

1. Prediction by extrapolating based on known values.
2. Update states.
3. Global input-output solve. Range from a simple transfer of information to a full nonlinear-system solve.
4. Correction. Either accept the current solutions or repeat 2 and 3.



Example 1: Partitioned Analysis

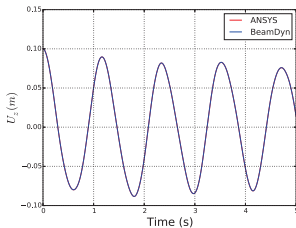
► Beam-Spring-Damper-Mass System



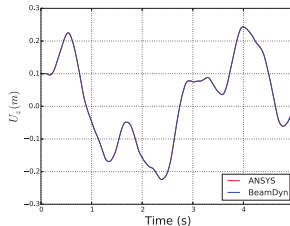
- Time integrator for SDM: Adams-Bashforth-Moulton (ABM4)
- Time integrator for beam: Generalized- α
- Initial condition solution from $U_Z = 0.1 \text{ m}$.
- Benchmark: ANSYS 60 BEAM188 elements; 10^{-5} s time increment

Example 1: Partitioned Analysis

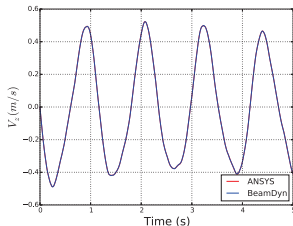
► Root Displacement



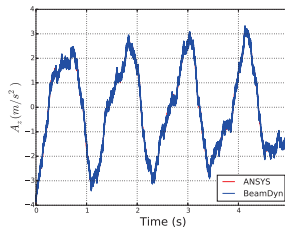
► Tip Displacement



► Root Velocity

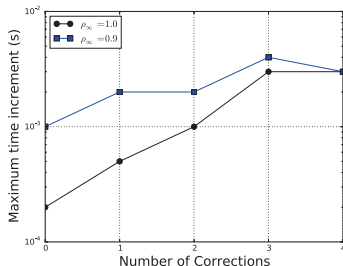


► Root Acceleration



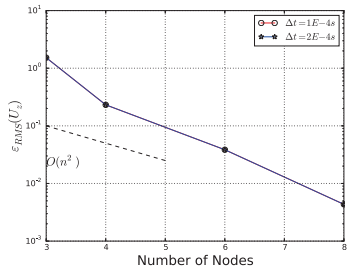
Example 1: Partitioned Analysis

► Stability



- Corrections and numerical damping help maximum allowable time step size
- RMS Error

► Accuracy



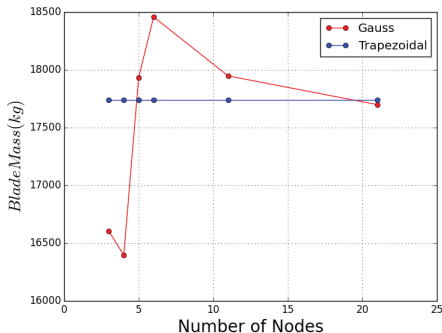
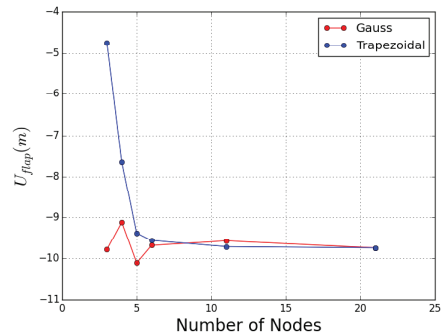
$$\epsilon_{RMS} = \sqrt{\frac{\sum_{k=0}^{n_{max}} [U_z^k - U_b(t^k)]^2}{\sum_{k=0}^{n_{max}} [U_b(t^k)]^2}}$$

Example 2: NREL 5-MW Wind Turbine

- ▶ NREL 5-MW Wind Turbine
 - 61.5m long with initial twist
 - 49 cross-sectional stations
 - Blade modeled with a SINGLE element

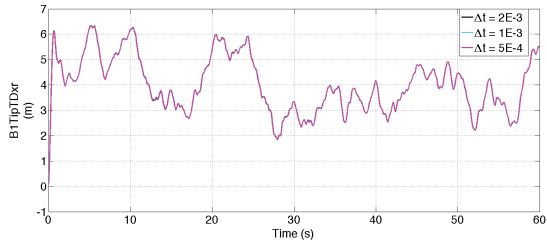
Tip Displacement

▶ Blade Mass

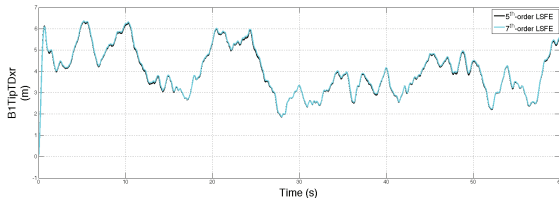


Example 2: NREL 5-MW Wind Turbine

► Time Discretization

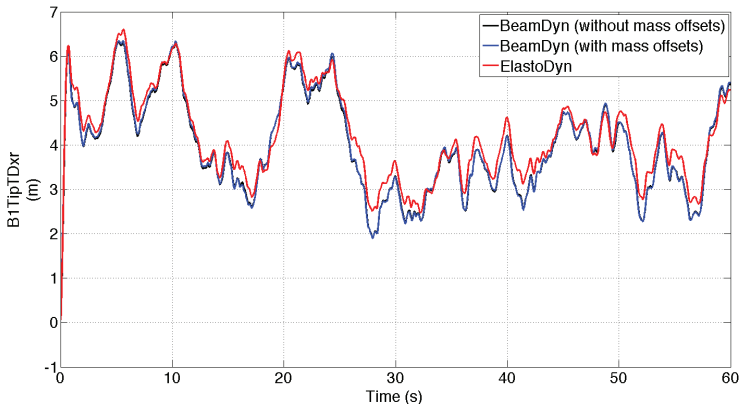


► Space Discretization



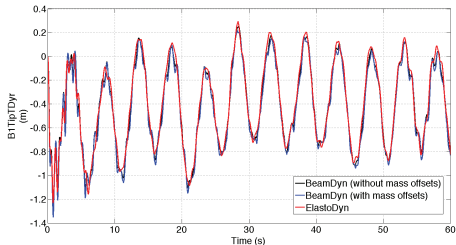
Example 2: NREL 5-MW Wind Turbine

- ▶ Aero-Servo-Elastic Coupled Analysis
- ▶ Mean Wind Speed 12 m/s^2 with Turbulence
- ▶ Test Case 26 in FAST Archive
- ▶ Tip Displacement U_{flap}

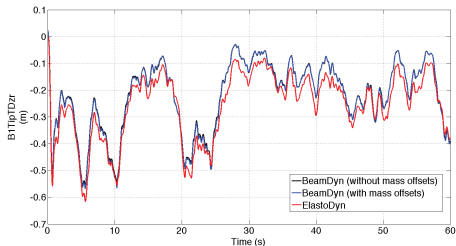


Example 2: NREL 5-MW Wind Turbine

► Tip Displacement U_{edge}

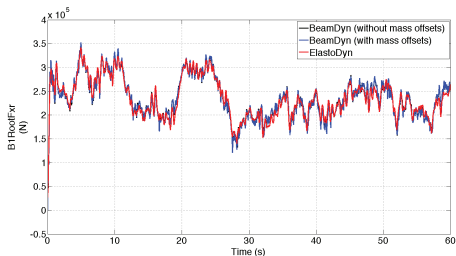


► Tip Displacement U_{axial}

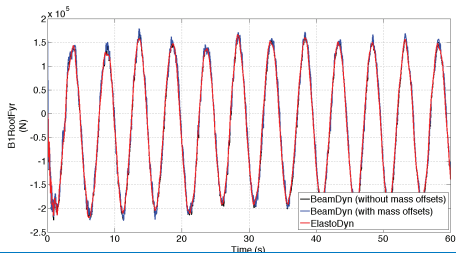


Example 2: NREL 5-MW Wind Turbine

► Root Reaction Force F_{flap}

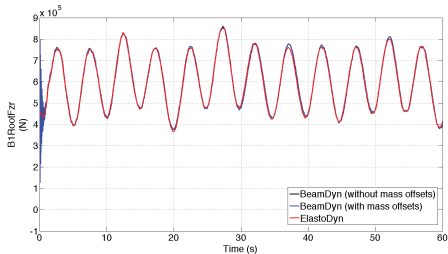


► Root Reaction Force F_{edge}

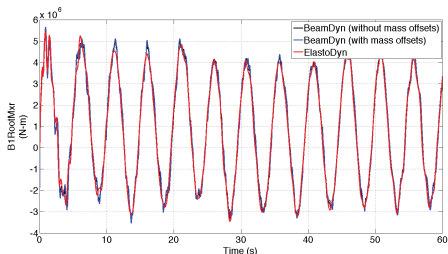


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► Root Reaction Force F_{axial}

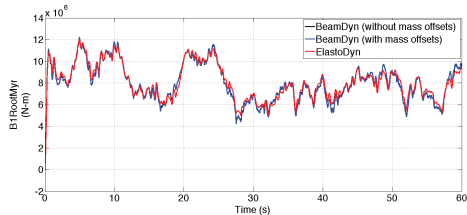


► Root Reaction Moment M_{edge}

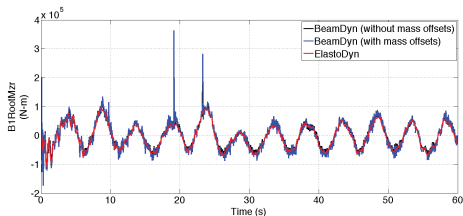


Example 2: NREL 5-MW Wind Turbine

► Root Reaction Moment M_{flap}



► Root Reaction Torque M_{pitch}



Summary

► Conclusion

- Based on **geometrically exact beam theory**, BeamDyn is capable of dealing with **geometric nonlinear** beam problems with arbitrary magnitude of displacements and rotations for both static and dynamic analyses
- Along with a preprocessor like PreComp or VABS, BeamDyn takes **full elastic coupling effects** into account
- Spectral Finite Elements and new Trapezoidal-Rule quadrature have been adopted in the implementation of BeamDyn. These new techniques further improved the efficiency and accuracy.
- BeamDyn is implemented following the programming requirements (data structures and interfaces) of the **FAST modularization framework**. The module coupling algorithm has been implemented and verified through numerical examples.
- BeamDyn optionally replaces previous blade model of FAST when high-fidelity modeling of aero-elastically tailored blades is required.
- More verification and validation results in "FAST v8 Verification and Validation for a MW-Scale Wind Turbine with Aeroelastically Tailored Blades", Guntur, S. et al.

Questions?

Acknowledgments

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