

Partitioned nonlinear structural analysis of wind turbines using BeamDyn

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In this paper, we present the numerical implementation of BeamDyn, a finite element beam solver based on geometrically exact beam theory (GEBT), and its coupling to different partitions in the FAST modularization framework. The theory is being reviewed first. Then the coupling algorithm and numerical integration scheme specifically designed for wind turbine analysis are introduced. The implicit loose coupling method for BeamDyn coupling is used where nonlinear input-output relations are solved by Newton-Raphson method. Finally, numerical examples are provided to validate both the beam solver and the coupling algorithm.

I. Introduction

Recently, NREL has developed BeamDyn, a nonlinear structural dynamics module for composite wind turbine blade analysis in the FAST modularization framework. This work is motivated by a fact that composite materials have been introduced into the wind energy industry which makes manufacturing of much lighter, larger wind turbine blade a possibility. However, the use of composites also introduces some difficulties in the design and analysis stage. For example, the coupling behavior that exists in composite materials can hardly be captured by the conventional theories which are usually based on isotropic assumptions. Moreover, as the increasing size of the wind turbines, the deformations of the blades cannot be assumed to be linear anymore. This beam solver, BeamDyn, is implemented based on the geometrically exact beam theory (GEBT), which is a beam-deformation model useful in efficient analysis of highly flexible composite structures. GEBT was first proposed by Reissner¹ and then extended to three-dimensional (3D) beams by Simo² and Simo and Vu-Quoc³. Readers are referred to Hodges⁴, in which comprehensive derivations and discussions on nonlinear composite-beam theories can be found. The numerical tool in BeamDyn to discretize the space domain is the Legendre spectral finite elements (LSFE), which is a p -type high-order element that combines the accuracy of global spectral methods with the geometric modeling flexibility of h -type finite elements (FEs). More details on BeamDyn can be found in Wang et al.⁵.

FAST is the flagship multi-physics engineering tool developed at the National Renewable Energy Laboratory (NREL) for analyzing both land-based and offshore wind turbines under realistic operating conditions. The previous beam model in FAST was not capable of predictive analysis of highly flexible, composite wind turbine blades. FAST has been reformulated under a new modularized framework that provides a rigorous means by which various mathematical systems are implemented in distinct modules. The restructuring of FAST greatly enhanced flexibility and expandability to enable further developments of functionality without the need to recode established modules. These modules are interconnected to solve for the globally coupled dynamic responses of wind turbines and wind plants^{6,7}. In previous work, this framework is extended to handle the non-matching spatial grids at interfaces and non-matching temporal meshes that allow module solutions to advance with different time increments and different time integrators.⁸

In this paper, the formulation of the beam theory is firstly reviewed. Then the coupling algorithm of BeamDyn with other modules is presented. Numerical integration scheme that specifically implemented for wind turbine analysis is also introduced. Numerical examples are provided to validate the proposed beam solver and its coupling algorithm when it is running in a couple-to-FAST mode.

II. Geometrically Exact Beam Theory

This section briefly reviews the geometrically exact beam theory. Further details on the content of this section can be found in many other papers and textbooks^{4,9,10}. Figure 1 shows a beam in its initial undeformed and deformed states. A reference frame \mathbf{b}_i is introduced along the beam axis for the undeformed state and a frame \mathbf{B}_i is introduced along each point of the deformed beam axis. The curvilinear coordinate x_1 defines the intrinsic parameterization of

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the reference line. In this paper, matrix notation is used to denote vectorial or vectorial-like quantities. For example,

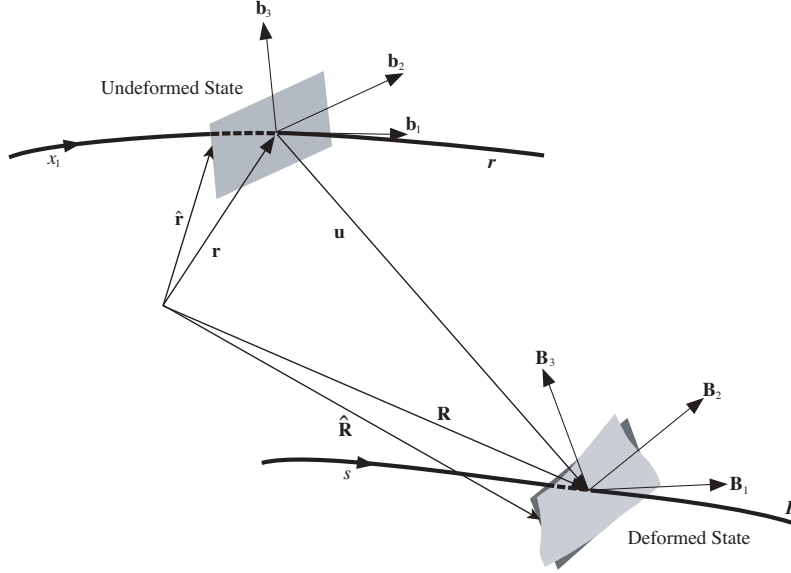


Figure 1: A beam deformation schematic.

an underline denotes a vector \underline{u} , a bar denotes unit vector \bar{n} , and a double underline denotes a tensor $\underline{\underline{A}}$. Note that sometimes the underlines only denote the dimension of the corresponding matrix. The governing equations of motion for geometrically exact beam theory can be written as⁹

$$\dot{\underline{h}} - \underline{F}' = \underline{f} \quad (1)$$

$$\dot{\underline{g}} + \tilde{\underline{u}}\underline{h} - \underline{M}' + (\tilde{x}'_0 + \tilde{u}')^T \underline{F} = \underline{m} \quad (2)$$

where \underline{h} and \underline{g} are the linear and angular momenta resolved in the inertial coordinate system, respectively; \underline{F} and \underline{M} are the beam's sectional force and moment resultants, respectively; \underline{u} is the one-dimensional (1D) displacement of a point on the reference line; \underline{x}_0 is the position vector of a point along the beam's reference line; and \underline{f} and \underline{m} are the distributed force and moment applied to the beam structure. The notation $(\bullet)'$ indicates a derivative with respect to beam axis x_1 and $(\dot{\bullet})$ indicates a derivative with respect to time. The tilde operator $(\tilde{\bullet})$ defines a skew-symmetric tensor corresponding to the given vector. In the literature, it is also termed as “cross-product matrix”. For example,

$$\tilde{n} = \begin{bmatrix} 0 & -n_3 & n_2 \\ n_3 & 0 & -n_1 \\ -n_2 & n_1 & 0 \end{bmatrix}$$

The constitutive equations relate the velocities to the momenta and the 1D strain measures to the sectional resultants as

$$\begin{Bmatrix} \underline{h} \\ \underline{g} \end{Bmatrix} = \underline{\underline{M}} \begin{Bmatrix} \underline{\dot{u}} \\ \underline{\omega} \end{Bmatrix} \quad (3)$$

$$\begin{Bmatrix} \underline{F} \\ \underline{M} \end{Bmatrix} = \underline{\underline{C}} \begin{Bmatrix} \underline{\epsilon} \\ \underline{\kappa} \end{Bmatrix} \quad (4)$$

where $\underline{\underline{M}}$ and $\underline{\underline{C}}$ are the 6×6 sectional mass and stiffness matrices, respectively (note that they are not really tensors); $\underline{\epsilon}$ and $\underline{\kappa}$ are the 1D strains and curvatures, respectively; and, $\underline{\omega}$ is the angular velocity vector that is defined by the rotation tensor \underline{R} as $\underline{\omega} = \text{axial}(\dot{\underline{R}} \underline{R}^T)$. The axial vector \underline{a} associated with a second-order tensor $\underline{\underline{A}}$ is denoted $\underline{a} = \text{axial}(\underline{\underline{A}})$ and its components are defined as

$$\underline{a} = \text{axial}(\underline{\underline{A}}) = \begin{Bmatrix} a_1 \\ a_2 \\ a_3 \end{Bmatrix} = \frac{1}{2} \begin{Bmatrix} A_{32} - A_{23} \\ A_{13} - A_{31} \\ A_{21} - A_{12} \end{Bmatrix} \quad (5)$$

The 1D strain measures are defined as

$$\begin{Bmatrix} \underline{\epsilon} \\ \underline{\kappa} \end{Bmatrix} = \begin{Bmatrix} \underline{x}'_0 + \underline{u}' - (\underline{R} \underline{R}_0) \bar{i}_1 \\ \underline{k} \end{Bmatrix} \quad (6)$$

where $\underline{k} = axial[(\underline{RR}_0)'(\underline{RR}_0)^T]$ is the sectional curvature vector resolved in the inertial basis and \bar{e}_1 is the unit vector along x_1 direction in the inertial basis. Note that these three sets of equations, including equations of motion Eq. (1) and (2), constitutive equations Eq. (3) and (4), and kinematical equations Eq. (6), provide a full mathematical description of elasticity problems.

For a displacement-based finite-element implementation, there are six degrees of freedom at each node: three displacement components and three rotation components. Here, \underline{q} denotes the elemental displacement array as $\underline{q}^T = [\underline{u}^T \ \underline{p}^T]$ where \underline{u} is the displacement and \underline{p} is the rotation-parameter vector. The acceleration array can thus be defined as $\underline{a}^T = [\underline{\ddot{u}}^T \ \underline{\dot{\omega}}^T]$. For nonlinear finite-element analysis, the discretized forms of displacement, velocity, and acceleration are written as

$$\underline{q}(x_1) = \underline{N} \hat{\underline{q}} \quad \underline{q}^T = [\underline{u}^T \ \underline{p}^T] \quad (7)$$

$$\underline{v}(x_1) = \underline{N} \hat{\underline{v}} \quad \underline{v}^T = [\underline{\dot{u}}^T \ \underline{\dot{\omega}}^T] \quad (8)$$

$$\underline{a}(x_1) = \underline{N} \hat{\underline{a}} \quad \underline{a}^T = [\underline{\ddot{u}}^T \ \underline{\dot{\omega}}^T] \quad (9)$$

where \underline{N} is the shape function matrix and (\cdot) denotes a column matrix of nodal values.

III. Implicit Coupling Algorithm

For clarification, “implicit” here refers to a module that needs information from other modules before the solution can be time-advanced; the modules are thus tied together in a linear or nonlinear system that must be solved for time advancement. Specifically to the BeamDyn module, which is used to represent a blade in the wind turbine system, the inputs are the root motion including displacements/rotations, linear and angular velocities, and linear and angular accelerations; and the outputs are the root reaction forces and moments transferred to the hub. The inputs and outputs can be written as

$$\mathbf{u}_{BD} = [\underline{q} \ \underline{v} \ \underline{a}]^T \quad (10)$$

$$\mathbf{y}_{BD} = [\underline{f} \ \underline{m}]^T \quad (11)$$

The inputs and outputs of the module that being coupled to BeamDyn have the form

$$\mathbf{u}_O = [\underline{f} \ \underline{m}]^T \quad (12)$$

$$\mathbf{y}_O = [\underline{q} \ \underline{v} \ \underline{a}]^T \quad (13)$$

The input-output equations can be written as

$$\mathbf{U}_1 : \mathbf{u}_{BD} - \mathbf{y}_O(\mathbf{u}_O, t) = 0 \quad (14)$$

$$\mathbf{U}_2 : \mathbf{u}_O - \mathbf{y}_{BD}(\mathbf{u}_{BD}, t) = 0 \quad (15)$$

Newton-Raphson method is adopted here to solve this nonlinear system:

$$\begin{bmatrix} \frac{\partial \mathbf{U}_1}{\partial \mathbf{u}_{BD}} & \frac{\partial \mathbf{U}_1}{\partial \mathbf{u}_O} \\ \frac{\partial \mathbf{U}_2}{\partial \mathbf{u}_{BD}} & \frac{\partial \mathbf{U}_2}{\partial \mathbf{u}_O} \end{bmatrix} \begin{Bmatrix} \Delta \mathbf{u}_{BD} \\ \Delta \mathbf{u}_O \end{Bmatrix} = - \begin{Bmatrix} \mathbf{U}_1 \\ \mathbf{U}_2 \end{Bmatrix} \quad (16)$$

The Jacobian matrix \mathbf{J} on the left-hand-side is computed numerically using the forward differences formulae

$$\mathbf{J}_{ij} = \frac{1}{\epsilon_j} [\mathbf{U}_i(\mathbf{u} + \epsilon_j \mathbf{e}_j) - \mathbf{U}_i(\mathbf{u})] \quad (17)$$

where \mathbf{e}_j is the unit vector in the \mathbf{u}_j direction and ϵ_j represents a small increment.

IV. Trapezoidal Quadrature

The numerical analysis of wind turbine blade features a large number of cross-sectional data along the blade, usually ranging from dozens to more than one hundred stations. A typical practice in dealing with those cross-sectional data is interpolating a subset of the data to the quadrature point, for example, Gauss point. However, there are two drawbacks of this method. One is that it is very difficult to include all the data given the large number of cross sections used in wind turbine modeling. The widely used NREL 5-MW reference wind turbine blade, for example, provides 49 stations along the blade axis. If linearly discretizing this blade, 48 first-order finite elements, with two end points align with two adjacent stations, are needed to make sure that all the cross-sectional data being used in the simulation. The other drawback is that there is no rigorous way to interpolate the station data to the quadrature points.

Given the discussion above, we implemented a new trapezoidal quadrature into BeamDyn, see Eq. 18.

$$\int_a^b f(x)dx \approx \frac{1}{2} \sum_{k=1}^N (x_{k+1} - x_k) [f(x_{k+1}) + f(x_k)] \quad (18)$$

where N is the total number of intervals. Generally, this is a over-integration scheme by assuming that each station point is a quadrature point regardless of the number of the finite element nodes. Based on this assumption, all the cross-sectional data are included in the calculation and no interpolation is needed since the quadrature points are exactly located on the cross-sectional station points.

V. Numerical Examples

A. Example 1: Partitioned Analysis

This example validates and examines the accuracy and numerical behavior of the proposed coupling algorithm. A beam attaches its root to a spring-mass-damper system, which is a simplified blade-hub system, see Figure 2. The beam

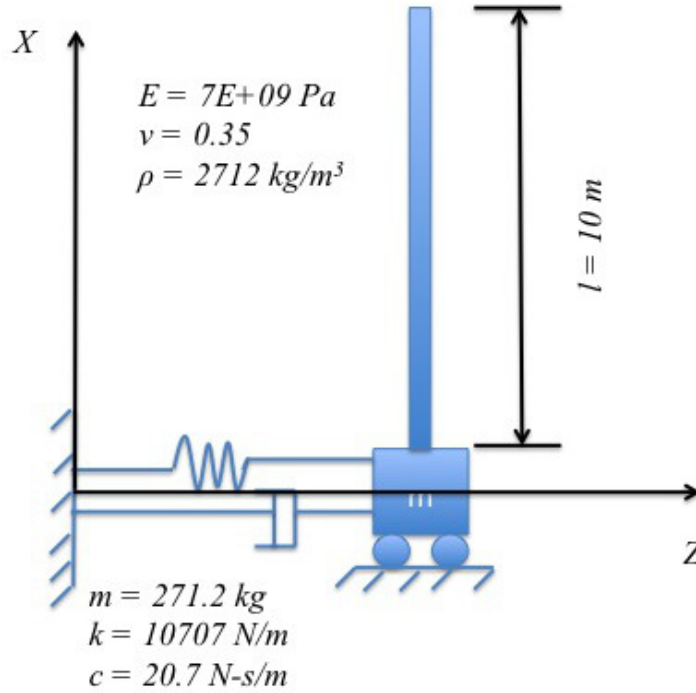


Figure 2: Sketch of a beam attaching to a spring-mass-damper system.

is modeled by BeamDyn and the time integrator for the spring-damper-mass system is Adams-Bashforth-Moulton (ABM4). The material properties, coordinate system, and geometric parameters can be found in Figure 2. The dimensions of the cross-section of the beam is $0.1m \times 0.1m$. The natural frequency of the lumped-mass-spring-damper system is $6.28rad/s$ and the first five natural frequencies for the cantilevered beam are 0.26, 1.72, 5.78, 22.62, and 24.21 in the same unit, respectively. The first five natural frequencies of the coupled system, obtained by ANSYS modal analysis, are 0.25, 0.85, 1.80, 4.76, and $9.34rad/s$, respectively.

In the present study, the system is at stationary at beginning but we apply a initial displacement of $0.1m$ along Z axis. We firstly studied the stability of the proposed coupling algorithm. In the stability analysis, the beam is discretized by a single fifth-order LSFE. Figure 3 shows the maximum stable time step sizes obtained by numerical experiment against the number of predictor-correction times. It can be seen that the predictor-correction scheme helps increasing the maximum stable time increments. Moreover, by introducing numerical damping in the BeamDyn module, the maximum stable time increments also increase for most cases.

For validation purpose, we analyzed this case in ANSYS using 20 BEAM188 element and the time step size is set to $1E-05$. With this well-refined mesh in both time and spectral domains, the ANSYS solution is used as benchmark in the following comparisons. The root and tip displacements of the beam can be found in Figure 4. The beam is discretized in BeamDyn by a single 5th-order element. The time increment in BeamDyn for these results is $2E-05$

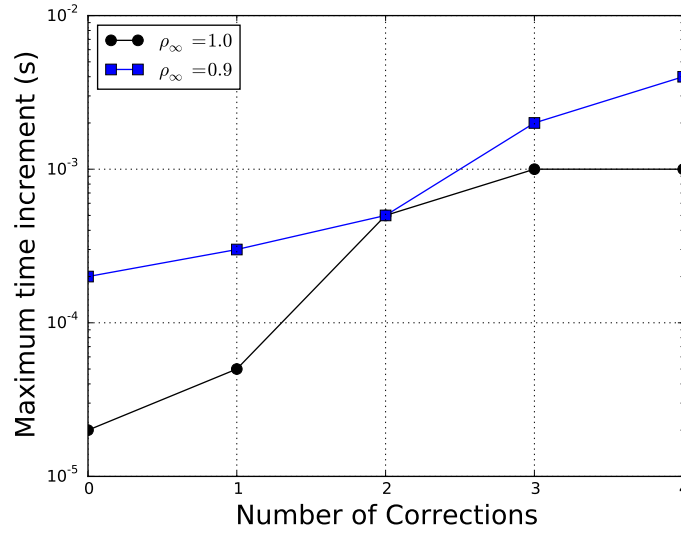


Figure 3: Maximum stable time increments increase as increasing number of predictor-correction times. Numerical damping introduced in BeamDyn module also helps increasing the maximum stable time increments. It is noted that in the generalized- α time integrator that is implemented in BeamDyn, $\rho_\infty = 1.0$ represents no numerical damping (Newmark scheme); while maximum numerical damping are allowed by setting $\rho_\infty = 0.0$.

to resolve all the frequencies. Good agreements can be observed between the benchmark solution and the BeamDyn results. The root velocity and accelerations are also compared between current model and ANSYS benchmark solution

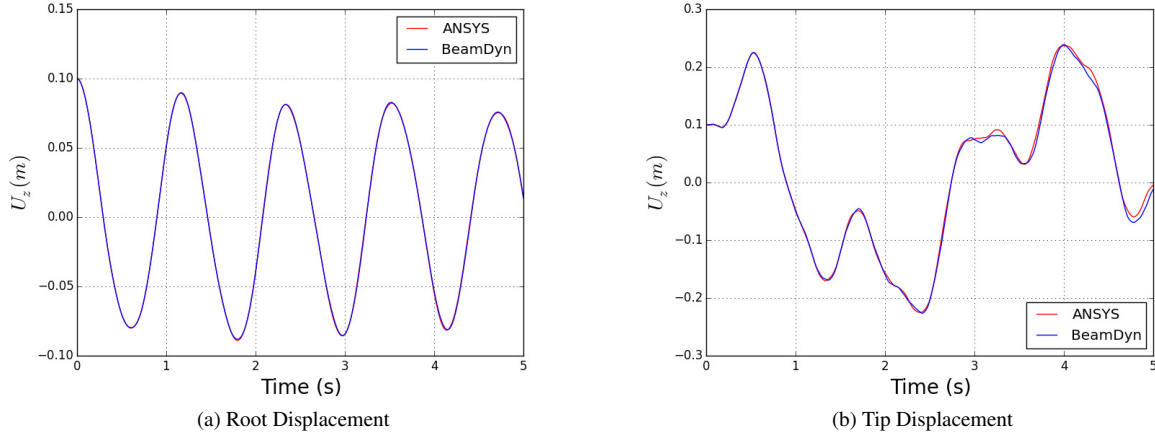


Figure 4: Comparisons of root and tip displacements between ANSYS and BeamDyn results

in Figure 5. Again, good agreements are found in those quantities. It is noted that high-frequency fluctuations can be observed in the acceleration plot of BeamDyn results. We believe that the fluctuation is the constraint on the time step size and numerical damping damps some of these out thus in turn helps increasing the time step size as shown in Figure 3. Introducing numerical damping into the coupling algorithm could be a solution to further reduce such high frequency behavior and thus allow larger time step size in the future.

Next we studied the numerical performance of BeamDyn. The accuracy and efficiency of the present results of the coupled system were examined by the root-mean-square (RMS) errors, which aggregates the magnitudes of the errors in predictions for various times into a single measure of predictive performance. The error was calculated using

$$\varepsilon_{RMS} = \sqrt{\frac{\sum_{k=0}^{n_{max}} [U_z^k - U_b(t^k)]^2}{\sum_{k=0}^{n_{max}} [U_b(t^k)]^2}} \quad (19)$$

where $U_b(t)$ is the benchmark solution given by ANSYS. Figure 6 shows the RMS error of the tip displacements along Z direction as a function of total number of nodes for three different time increment sizes and number of predictor-

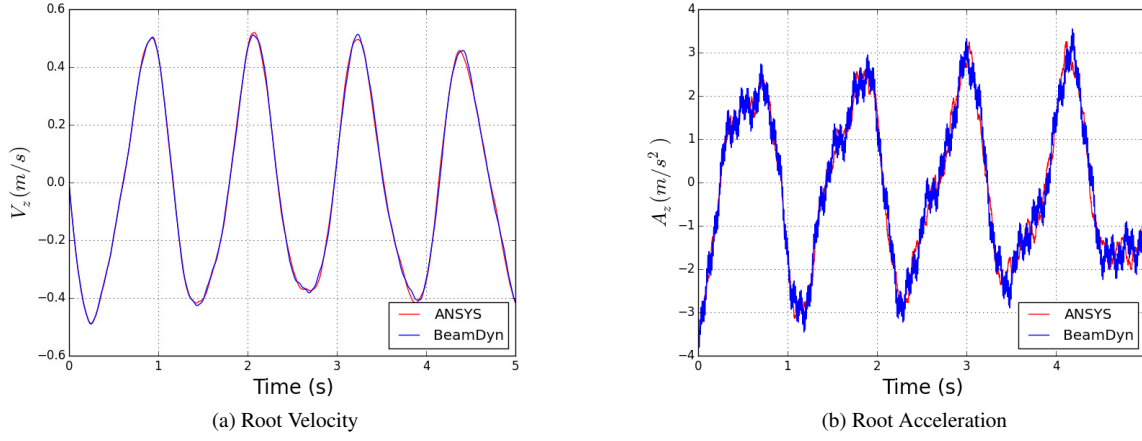


Figure 5: Comparisons of root velocity and acceleration between ANSYS and BeamDyn results

correction times. The time increments for Case 1, Case 2, and Case 3 are $2E-5$, $5E-4$, and $1E-3$, respectively; and the number of corrections for the three cases are 0 (no correction), 2, and 3, respectively. It can be concluded that

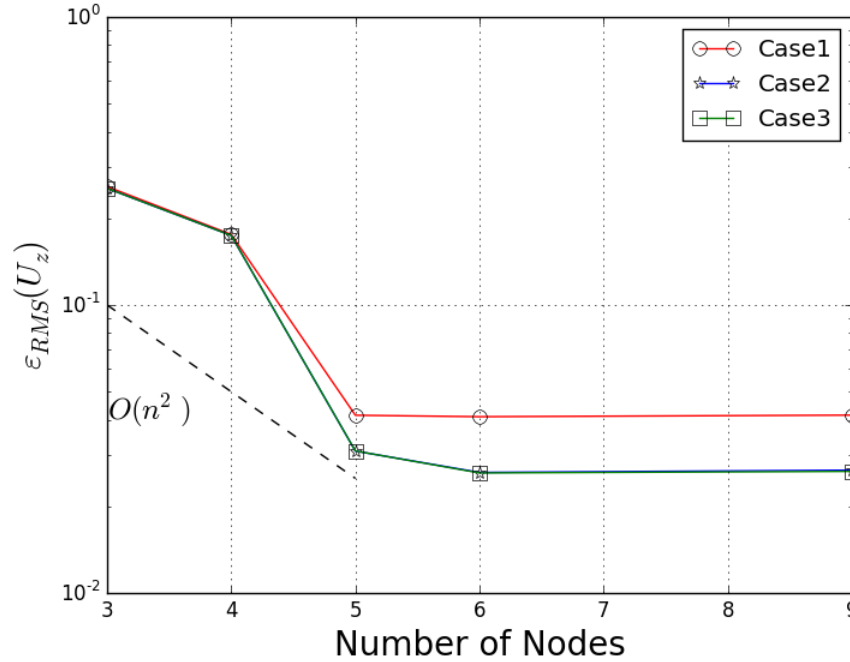


Figure 6: Normalized RMS error of U_z histories as a function of total number of nodes for three different time increments and number of corrections. The dashed line shows ideal second-order convergence.

although other factors have been introduced into the simulation, exponential convergence rate which is a feature of LSFs in space discretization can be observed. 5^{th} -order element (six nodes) being used in this case is a reasonable choice for a converged analysis. Moreover, results obtained by corrections are more accurate than those with smaller time increments but no correction.

B. Example 2: NREL 5-MW Wind Turbine

The second example is a coupled analysis of NREL 5-MW reference wind turbine system. The three blades are modeled by BeamDyn while the scheme discussed in this paper were implemented to couple BeamDyn to FAST.

Firstly we examines the numerical performance of two different quadrature methods, Gauss and trapezoidal quadratures, on this realistic blade analysis. A static cantilevered blade under a uniformly distributed force of mag-

nitude $1E + 04$ along the flap direction were analyzed. Figure 7 shows the results. Monotonous convergence can be observed for the trapezoidal quadrature results with increasing number of nodes; while the convergence curve for the Gauss quadrature was very jagged, depending on which stations being chosen and how these data being interpolated to the Gauss point. This can be even clearly observed from the mass calculation, see Figure 8: the constant mass by trapezoidal quadrature which includes all the cross-sectional data regardless of the finite element discretization; and the mass calculated by Gauss quadrature is more like a serendipity.

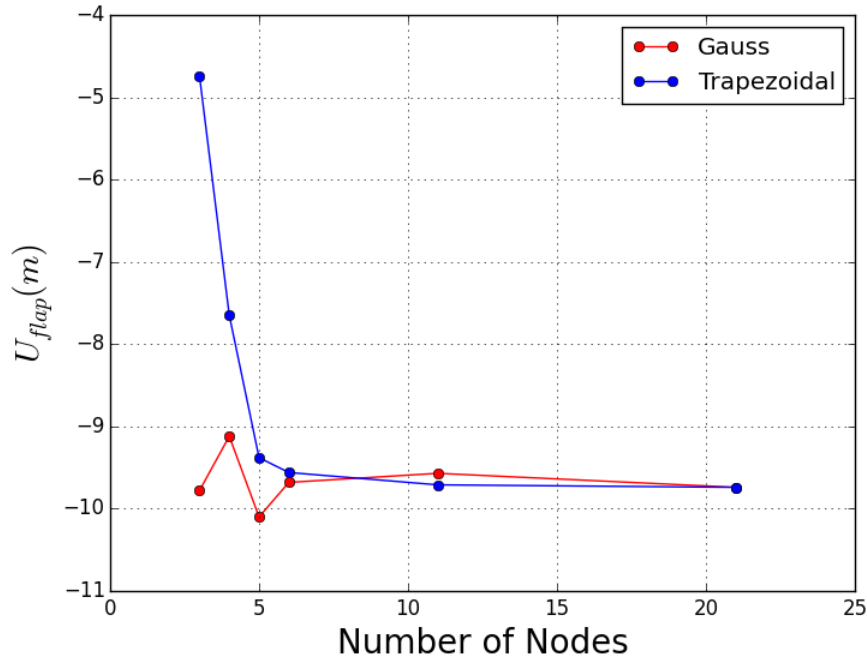


Figure 7: Tip deflections of a cantilevered NREL 5-MW blade under uniformly distributed load by Gauss and trapezoidal quadratures.

Next the stabilities of BeamDyn in stand-alone and couple-to-FAST modes are studied. Figure 9 shows the maximum time step size versus the number of nodes. In the stand-alone mode, we are using FAST as the driver but turning off all the coupling options so that the blade is free rotating under gravity. For the coupled-to-FAST case, we conducted a fully-coupled wind turbine analysis under mean wind speed of 12 m/s^2 with turbulence, which is a certification test case in FAST package.

The convergence of the time integrator is also evaluate using the RMS error defined in Eq (19). Again, a free spinning case which uses FAST as a driver code is studied for the convergence, see Figure 10. The blade is discretized by a single fifth-order element and the benchmark solution is obtained by a time step size of 0.001 seconds. Second order convergence rate can be observed in the plot.

Finally we studied the performance of BeamDyn in the fully coupled FAST analysis. Figures 11 and ?? show the tip flap displacement histories under different time and space discretizations. Note that all the quantities studied here are resolved in the body-attached blade reference coordinate system following the IEC standard, where X direction towards the suction side of the airfoil, Y direction towards the trailing edge, and Z direction towards the blade tip from root. It can be observed that for this case, reasonable results can be obtained by the $2E - 3s$ time increment and a single fifth-order element.

The tip displacements of blade 1 are shown in Figure 13. We compared the results obtained by BeamDyn with those obtained by ElastoDyn for this case. Results are plotted from fifth seconds to remove the initial effects. Good agreements can be observed. It is noted that due to the Trapeze effect and centrifugal force considered in BeamDyn, the mean value the the axial displacement in Figure 13c by BeamDyn is different from ElastoDyn. Figure 14 shows the root reaction forces calculated by BeamDyn and ElastoDyn. Again, reasonable agreement can be found in these quantities.

VI. Conclusion

In this paper, we examined the beam theory and the coupling algorithm for partitioned mechanical system analysis. The full set of governing equations for BeamDyn are reviewed and the coupling schemes between BeamDyn and other

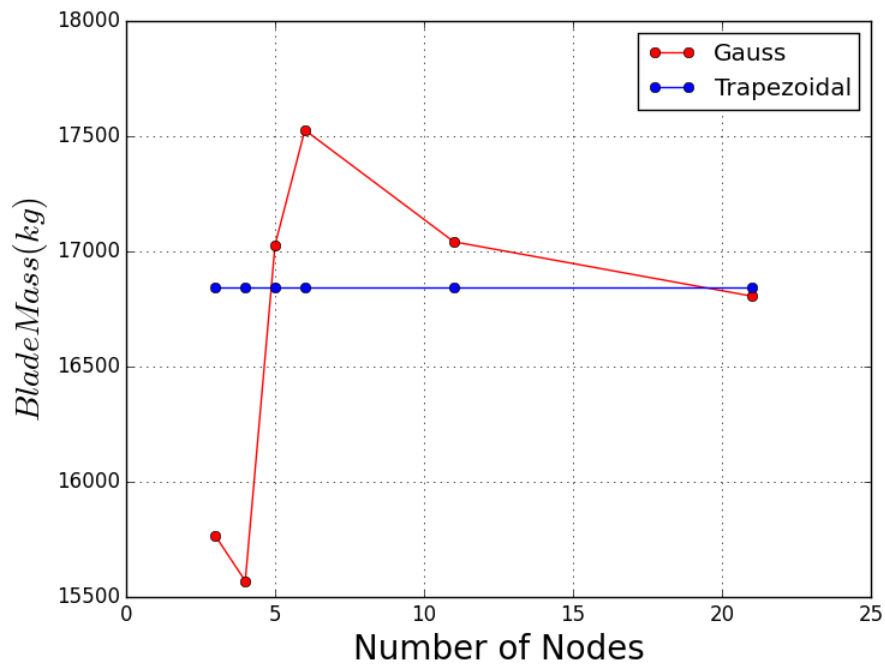


Figure 8: Total blade mass of a NREL 5-MW reference blade calculated by Gauss and trapezoidal quadratures.

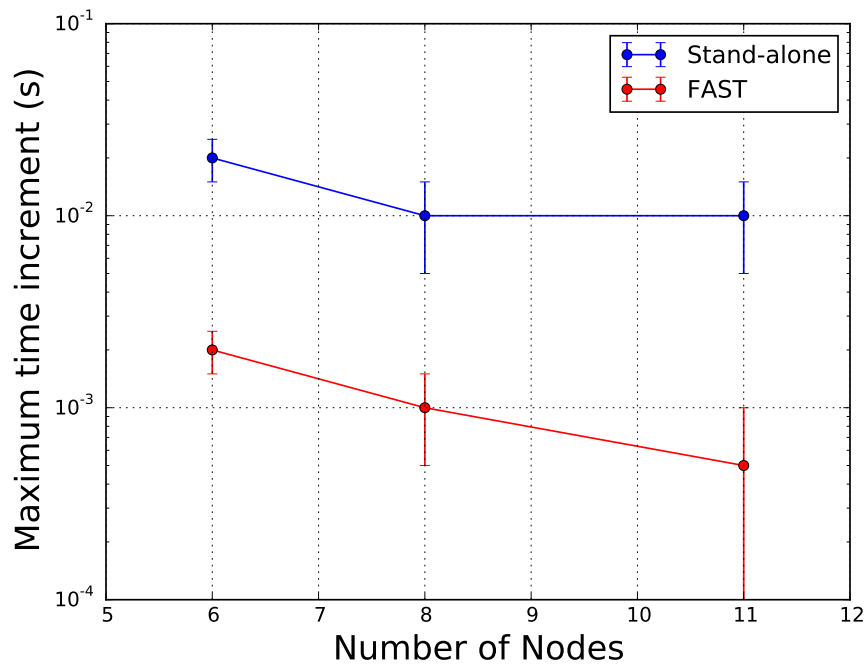


Figure 9: Maximum stable time increments vs number of FE nodes.

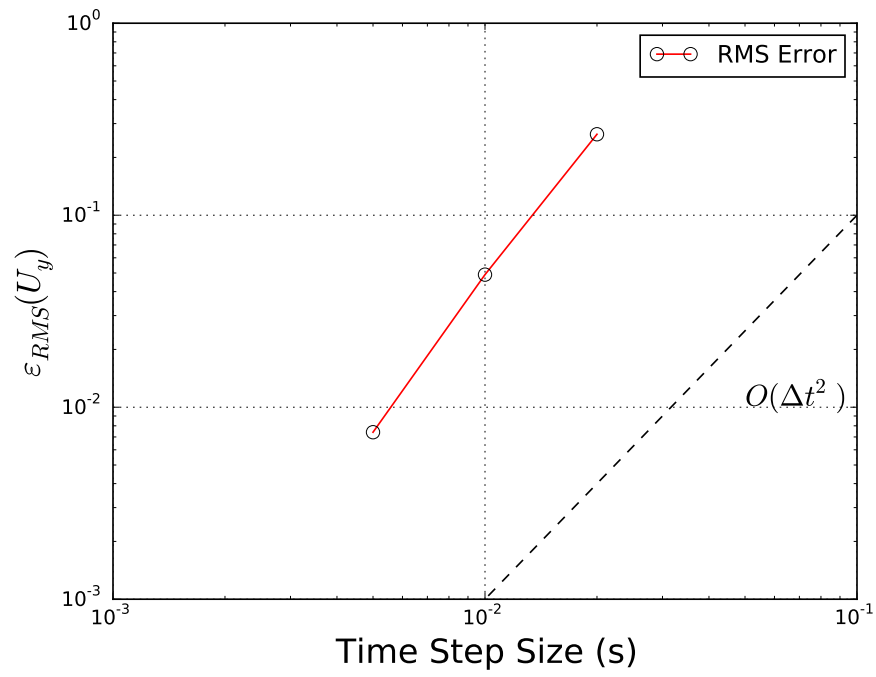


Figure 10: RMS error of tip edge displacement vs. time step size.

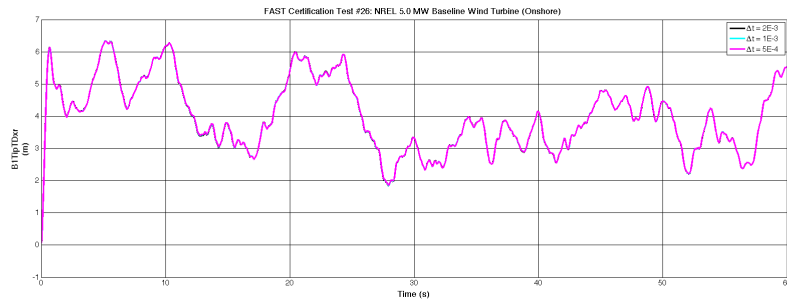


Figure 11: Blade tip deflection histories along flap direction obtained using different time increments.

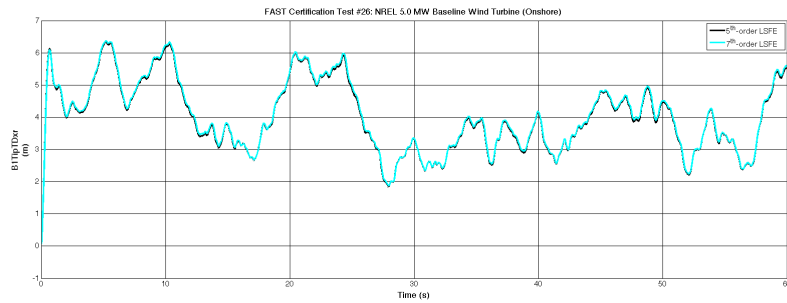
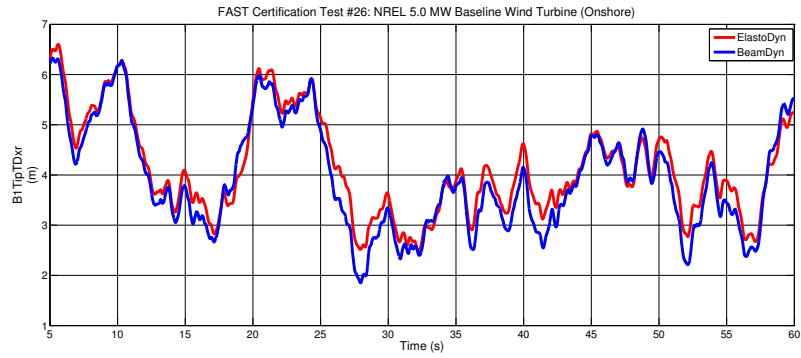
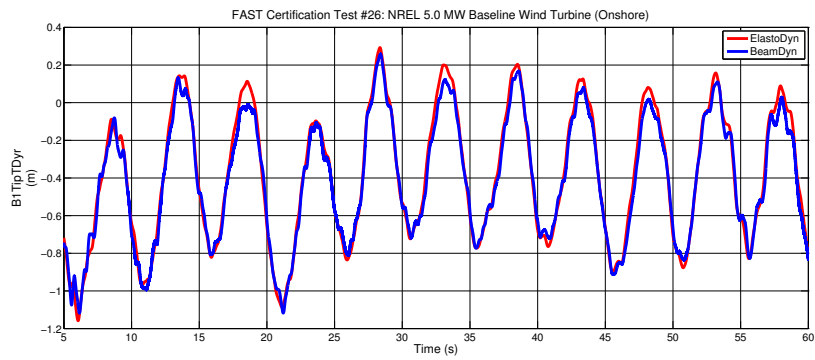


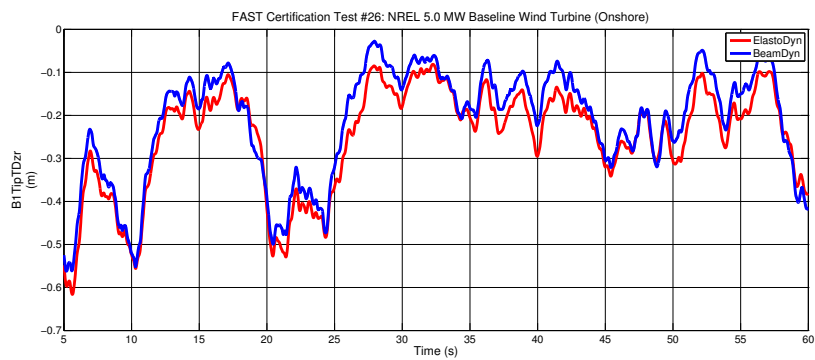
Figure 12: Blade tip deflection histories along flap direction obtained using different elements.



(a) Flap Displacement



(b) Edge Displacement



(c) Axial Displacement

Figure 13: Comparisons of blade 1 tip displacements between ElastoDyn and BeamDyn results

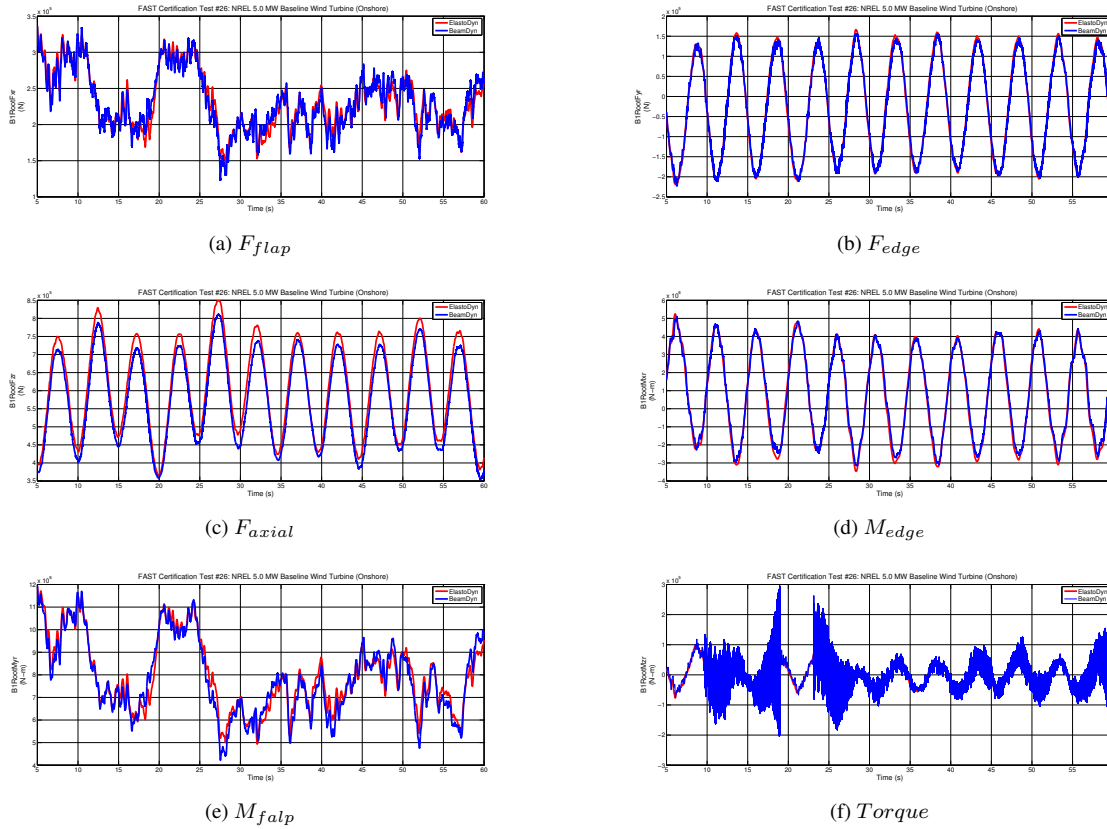


Figure 14: Comparisons of root reaction loads between ElastoDyn and BeamDyn results

mechanical modules are derived. For wind turbine analysis which features a large number of cross-sectional stations along blade axis, we implemented a trapezoidal numerical integration so that all the cross-sectional data, including inertial and stiffness matrices, can be used in the analysis. The users do not need to pick certain stations in a large set of data neither numerically interpolates them, which usually introduces errors. The new integration method, coupling algorithm as well as fully coupled mode have been validated in the numerical examples. The results obtained by trapezoidal quadrature were monotonously converged while those obtained by conventional Gauss integration were randomly converged depending on the stations chosen and interpolation method. In the coupled analysis, exponential convergence rate can be seen in the BeamDyn results, which is a prominent feature of the LSFs. In the full turbine analysis, reasonable agreement between BeamDyn and ElastoDyn results is found. More verification and validation results can be found in

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References

- ¹Reissner, E., "On one-dimensional large-displacement finite-strain beam theory," *Studies in Applied Mathematics LII*, 1973, pp. 87–95.
- ²Simo, J. C., "A finite strain beam formulation. The three-dimensional dynamic problem. Part I," *Computer Methods in Applied Mechanics and Engineering*, Vol. 49, 1985, pp. 55–70.
- ³Simo, J. C. and Vu-Quoc, L., "A three-dimensional finite-strain rod model. Part II," *Computer Methods in Applied Mechanics and Engineering*, Vol. 58, 1986, pp. 79–116.
- ⁴Hodges, D. H., *Nonlinear Composite Beam Theory*, AIAA, 2006.
- ⁵Wang, Q., Sprague, M. A., Jonkman, J., and Johnson, N., "Nonlinear Legendre spectral finite elements for wind turbine blade dynamics," *Proceedings of the 32nd ASME Wind Energy Symposium*, National Harbor, Maryland, January 2014.
- ⁶Jonkman, J. M., "The new modularization framework for the FAST wind turbine CAE tool," *Proceedings of the 51st AIAA Aerospace Sciences Meeting including the New Horizons Forum and Aerospace Exposition*, Grapevine, Texas, January 2013.
- ⁷Jonkman, J. and Jonkman, B., "FAST v8," <https://nwtc.nrel.gov/FAST8>, October 2013, [Online; accessed 29-OCTOBER-2014].

⁸Sprague, M., Jonkman, J., and Jonkman, B., “FAST modular wind turbine CAE tool: non matching spatial and temporal meshes,” *Proceedings of the 32nd ASME Wind Energy Symposium*, National Harbor, Maryland, January 2014.

⁹Bauchau, O. A., *Flexible Multibody Dynamics*, Springer, 2010.

¹⁰Yu, W. and Blair, M., “GEBT: A general-purpose nonlinear analysis tool for composite beams,” *Composite Structures*, Vol. 94, 2012, pp. 2677–2689.