

# Applied Signal Processing

## Lecture 8

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- Multirate Processing
  - Up-sampling
  - Interpolation
  - Down-sampling
  - Decimation
  - Rate changes
  - Modulation - Demodulation

## Motivations

- Rate changes to match different standards
- Oversampling
  - Use sample-rate higher than required Nyquist-rate at signal acquisition
  - Signal reconstruction at a rate higher than Nyquist-rate
- Handle signals in frequency divided channels
- Efficient processing of band pass signals by using downsampling

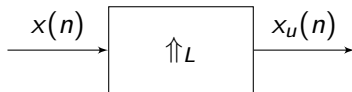
Use the delay operator  $z^{-1}$  to denote filtering:

$$H(z) = \sum_{k=-\infty}^{\infty} h(k)z^{-k}$$

$\Rightarrow$

$$y(n) = H(z)x(n) = \sum_{k=-\infty}^{\infty} h(k)x(n-k)$$

since  $z^{-k}x(n) = x(n-k)$ .



We define *up-sampling* with factor  $L$

$$x_u(n) \triangleq \begin{cases} x(n/L), & n = 0, \pm L, \pm 2L, \dots \\ 0, & \text{otherwise} \end{cases}$$

The signal  $x_u$  have sampling frequency  $\omega_{s_u} = L\omega_s$  and sampling interval  $\Delta t_u = \Delta t/L$  where  $\omega_s$  and  $\Delta t$  correspond to the signal  $x(n)$ .

We use the short-form notation

$$x_u(n) = \uparrow_L[x(n)]$$

$$\begin{aligned}X_u(\omega) &= \sum_{n=-\infty}^{\infty} x_u(n) e^{-j\omega n \Delta t_u} = [m = n/L \text{ and } \Delta t_u = \Delta t/L] \\&= \sum_{m=-\infty}^{\infty} x(m) e^{-j\omega L m \Delta t/L} = [n = m] \\&= \sum_{n=-\infty}^{\infty} x(n) e^{-j\omega n \Delta t} = X(\omega)\end{aligned}$$

where  $\omega$  is un-normalized, i.e. rad/s.

### DTFT up-sampling

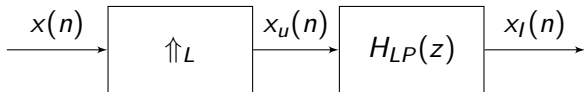
$$X_u(\omega) = X(\omega)$$

The DTFT is *unchanged* after up-sampling. The new sampling frequency is  $L$  times higher.

Since  $X(\omega)$  is periodic with period  $\omega_s$  the identity

$$X_u(\omega) = X(\omega)$$

imply that  $x_u(\omega)$  will have  $L - 1$  extra images of the original DTFT from  $\omega_s$  to  $L\omega_s = \omega_{s_u}$ .



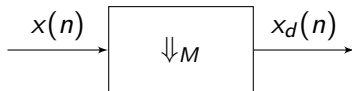
The combined operation of up-sampling and LP filtering is known as *interpolation*.

The LP-filter will remove the extra images introduced by interpolation. To get the desired behaviour the LP filter should (ideally) have the specifications.

$$H(\omega) = \begin{cases} 1, & \text{for } |\omega| \leq \frac{\omega_s}{2L} \\ 0, & \text{otherwise} \end{cases}$$

The result  $X_I(n)$  will be a signal which resembles the shape of  $x(n)$  but will have a factor  $L$  more samples.





We define *down-sampling* with factor  $M$  as

$$x_d(n) \triangleq \Downarrow_M[x(n)] \triangleq x(Mn), \quad n = 0, \pm 1, \pm 2, \dots$$

The signal  $x_d$  have sampling frequency  $\omega_{s_d} = \omega_s/M$  and sampling interval  $\Delta t_d = M\Delta t$  where  $\omega_s$  and  $\Delta t$  correspond to the signal  $x(n)$ .

We use the short-form notation

$$x_u(n) = \Downarrow_M[x(n)]$$

Clearly the down-sampling is an operation which potentially reduce/distort the information in the signal. In the DTFT domain we have

## DTFT for down-sampling

$$X_d(\omega) = \frac{1}{M} \sum_{k=0}^{M-1} X\left(\omega + \frac{\omega_s k}{M}\right).$$

where  $\omega$  is un-normalized, i.e. rad/s.

Consider expressing the down-sampled signal in terms of the inverse DTFT of the original signal:

$$\begin{aligned}
 x_d(n) &= x(nM) = \frac{1}{\omega_s} \int_0^{\omega_s} X(\omega) e^{j\omega n M \Delta t} d\omega = [\Delta t_d = M \Delta t] \\
 &= \frac{1}{\omega_s} \sum_{k=0}^{M-1} \int_{\omega_s k/M}^{\omega_s (k+1)/M} X(\omega) e^{j\omega n \Delta t_d} d\omega = [\omega = \lambda + \omega_s k/M] \\
 &= \frac{1}{\omega_s/M} \int_0^{\omega_s/M} \underbrace{\frac{1}{M} \sum_{k=0}^{M-1} X\left(\lambda + \frac{\omega_s k}{M}\right)}_{X_d(\lambda)} e^{j\lambda n \Delta t_d} d\lambda.
 \end{aligned}$$

Since the last expression is the inverse DTFT of  $x_d$  we have shown that

$$X_d(\omega) = \frac{1}{M} \sum_{k=0}^{M-1} X\left(\omega + \frac{\omega_s k}{M}\right).$$

By inspection of the result

$$X_d(\omega) = \frac{1}{M} \sum_{k=0}^{M-1} X\left(\omega + \frac{\omega_s k}{M}\right).$$

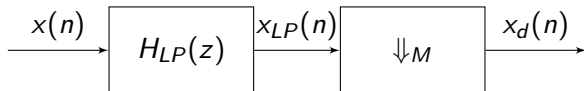
we can conclude the following theorem:

## Nyquist theorem for down-sampling

If  $X(\omega) = 0$ , for  $|\omega| \geq \frac{\omega_s}{2M}$ ,

then  $X(\omega) = M X_d(\omega)$ , for  $|\omega| < \frac{\omega_s}{2M}$  where  $\omega_{sd} = \omega_s/M$

If the signal  $x(n)$  is sufficiently band-limited, the down-sampling does not cause aliasing. Conversely if  $X(\omega)$  is non-zero for a frequency band larger than  $\omega_{sd}$ , aliasing will occur.



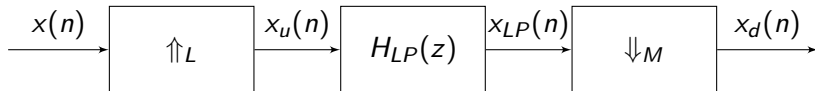
The combined operation of LP-filtering and down-sampling is known as *decimation*.

The LP-filter will bandlimit the signal to avoid aliasing. To get the desired behaviour the LP filter should (ideally) have the specification.

$$H_{LP}(\omega) = \begin{cases} 1, & \text{for } |\omega| \leq \frac{\omega_s}{2M} \\ 0, & \text{otherwise} \end{cases}$$

The result  $x_d(n)$  will be a signal which resembles the shape of  $x_{LP}(n)$  but will have a factor  $M$  less samples.

The interpolation and decimation methods can be combined to perform a fractional rate change. Assume we want to create a signal with the new rate  $\omega'_s = \frac{L}{M}\omega_s$ .

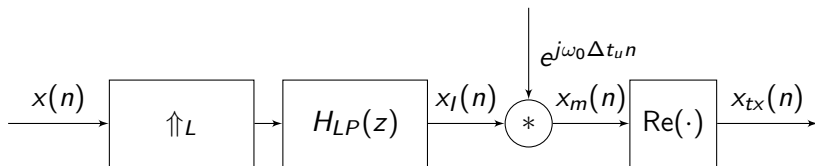


To avoid aliasing in the down-sampling stage the filter should satisfy

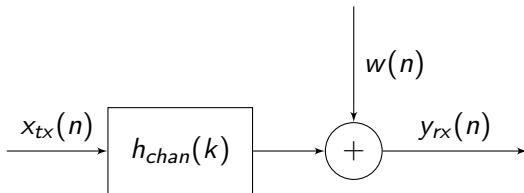
$$H_{LP}(\omega) = \begin{cases} 1, & \text{for } |\omega| \leq \frac{\omega'_s}{2} \\ 0, & \text{otherwise} \end{cases}$$

Can we shift the order of the up-sampler and down-sampler?

On the transmitter side:



- $x(n)$  complex base band signal
- $x_I(n)$  interpolated base band signal
- $x_m(n)$  modulated complex signal with center frequency  $\omega_0$
- $x_{tx}(n)$  real valued modulated signal.
- $\Delta t_u = L\Delta t$

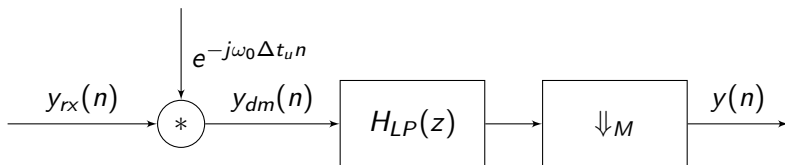


- $x_{tx}(n)$  transmitted real valued signal
- $y_{rx}(n)$  received real valued signal
- $w(n)$  noise signal

$$Y_{rx}(\omega) = H_{chan}(\omega)X_{tx}(\omega) + W(\omega)$$



On the receiver side:



- $y_{rx}(n)$  received real valued signal
- $y_{dm}(n)$  demodulated complex signal
- $y(n)$  complex decimated base band signal
- Here  $M = L$  to match the transmitter.