# Introduction to Robotics Lab 4 - Forward Kinematics

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## Lab Report

# Task 4.1

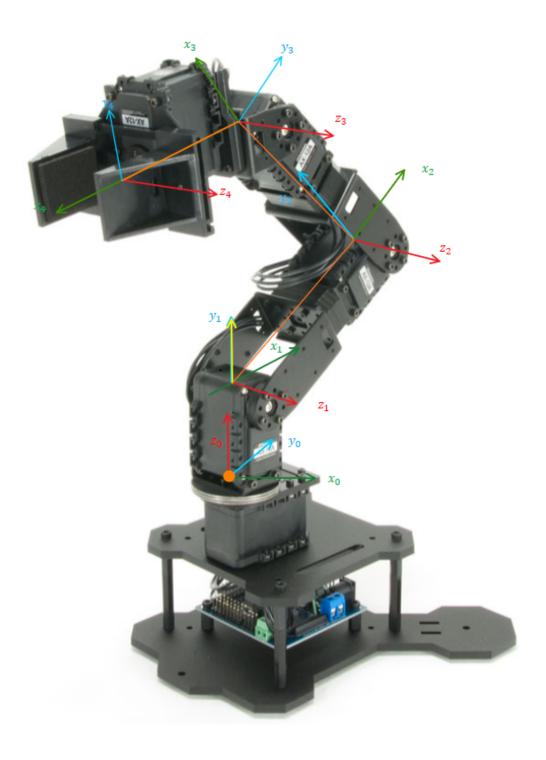


Figure 1: Frame Assignment Based on DH convention

Task 4.2

Link No.	$a_i \text{ (mm)}$	$\alpha_i$ (radians)	$d_i  (\mathrm{mm})$	$\theta_i$ (radians)
1	0	$rac{\pi}{2}$	54	$ heta_1$
2	108	0	0	$\theta_2$
3	108	0	0	$\theta_3$
4	76	0	0	$\theta_4$

Table 1: Table of DH parameters

### Part (a)

The following code generates the intermediate homogenous transformations  ${}^{0}T_{1}$ ,  ${}^{1}T_{2}$ ,  ${}^{2}T_{3}$  and  ${}^{3}T_{4}$ .

```
syms('theta_1', 'theta_2', 'theta_3', 'theta_4', 'alpha_1', 'alpha_2', 'alpha_3', ...
                 'alpha_4', 'a_1', 'a_2', 'a_3', 'a_4', 'd_1', 'd_2', 'd_3', 'd_4');
syms('T_01', 'T_12', 'T_23', 'T_34', 'T_04')
T_01 = [\cos(\theta_1), -\sin(\theta_1) * \cos(\theta_1), \sin(\theta_1), \sin(\theta_1) * \sin(\theta_1), \sin(\theta_1), \sin(\theta_1), \cos(\theta_1)]
                 cos(theta_1);
                                         sin(theta_1), cos(theta_1)*cos(alpha_1), -cos(theta_1)*sin(alpha_1), a_1 * ...
                                                          sin(theta_1);
                                         0, sin(alpha_1), cos(alpha_1), d_1;
                                         0 0 0 1]
T_12 = [\cos(\theta_1) \cdot \sin(\theta_2) \cdot \cos(\theta_1) \cdot \sin(\theta_2) \cdot \sin(\theta_1) \cdot \sin(\theta_2) \cdot \sin(\theta_1) \cdot \sin(\theta_2) \cdot \sin(\theta_1) \cdot \sin(
                 cos(theta_2);
                                         sin(theta_2), cos(theta_2)*cos(alpha_2), -cos(theta_2)*sin(alpha_2), a_2 * \dots
                                                          sin(theta_2);
                                         0, sin(alpha_2), cos(alpha_2), d_2;
                                         0 0 0 11
T_23 = [\cos(\theta_3), -\sin(\theta_3) * \cos(\theta_3), \sin(\theta_3), \sin(\theta_3) * \sin(\theta_3) * \sin(\theta_3), a_3 * \dots]
                 cos(theta_3);
                                         sin(theta_3), cos(theta_3)*cos(alpha_3), -cos(theta_3)*sin(alpha_3), a_3*...
                                                          sin(theta_3);
                                         0, sin(alpha_3), cos(alpha_3), d_3;
                                         0 0 0 1]
T_34 = [\cos(\theta_4), -\sin(\theta_4) \cdot \cos(\theta_4), \sin(\theta_4), \sin(\theta_4) \cdot \sin(\theta_4)]
                cos(theta_4);
                                         sin(theta_4), cos(theta_4)*cos(alpha_4), -cos(theta_4)*sin(alpha_4), a_4*...
                                                          sin(theta_4);
                                         0, sin(alpha_4), cos(alpha_4), d_4;
                                         0 0 0 1]
```

The above code gave the following output:

$${}^{0}T_{1} = \begin{pmatrix} \cos(\theta_{1}) & -\cos(\alpha_{1})\sin(\theta_{1}) & \sin(\alpha_{1})\sin(\theta_{1}) & a_{1}\cos(\theta_{1}) \\ \sin(\theta_{1}) & \cos(\alpha_{1})\cos(\theta_{1}) & -\sin(\alpha_{1})\cos(\theta_{1}) & a_{1}\sin(\theta_{1}) \\ 0 & \sin(\alpha_{1}) & \cos(\alpha_{1}) & d_{1} \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^{1}T_{2} = \begin{pmatrix} \cos(\theta_{2}) & -\cos(\alpha_{2})\sin(\theta_{2}) & \sin(\alpha_{2})\sin(\theta_{2}) & a_{2}\cos(\theta_{2}) \\ \sin(\theta_{2}) & \cos(\alpha_{2})\cos(\theta_{2}) & -\sin(\alpha_{2})\cos(\theta_{2}) & a_{2}\sin(\theta_{2}) \\ 0 & \sin(\alpha_{2}) & \cos(\alpha_{2}) & d_{2} \\ 0 & 0 & 1 \end{pmatrix}$$

$${}^{2}T_{3} = \begin{pmatrix} \cos(\theta_{1}) & -\cos(\alpha_{1})\sin(\theta_{1}) & \sin(\alpha_{1})\sin(\theta_{1}) & a_{1}\cos(\theta_{1}) \\ \sin(\theta_{1}) & \cos(\alpha_{1})\cos(\theta_{1}) & -\sin(\alpha_{1})\cos(\theta_{1}) & a_{1}\sin(\theta_{1}) \\ 0 & \sin(\alpha_{1}) & \cos(\alpha_{1})\cos(\theta_{1}) & a_{1}\sin(\theta_{1}) \\ 0 & 0 & 1 \end{pmatrix}$$

$${}^{3}T_{4} = \begin{pmatrix} \cos(\theta_{4}) & -\cos(\alpha_{4})\sin(\theta_{4}) & \sin(\alpha_{4})\sin(\theta_{4}) & a_{4}\cos(\theta_{4}) \\ \sin(\theta_{4}) & \cos(\alpha_{4})\cos(\theta_{4}) & -\sin(\alpha_{4})\cos(\theta_{4}) & a_{4}\sin(\theta_{4}) \\ 0 & \sin(\alpha_{4}) & \cos(\alpha_{4}) & \cos(\alpha_{4}) & d_{4} \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

#### Part (b)

Finally, we can find the resultant matrix by running the following line of code:

 $T_04 = simplify(T_01*T_12*T_23*T_34)$ 

This gives the required transformation  ${}^{0}T_{4}$  which is:

```
A_{11} = -\sin\theta_4 \,\sigma_1 - \cos\theta_4 \,\sigma_5
  A_{12} = \sin \alpha_4 \,\sigma_3 + \cos \alpha_4 \,\sin \theta_4 \,\sigma_5 - \cos \alpha_4 \,\cos \theta_4 \,\sigma_1
  A_{13} = \cos \alpha_4 \, \sigma_3 - \sin \alpha_4 \, \sin \theta_4 \, \sigma_5 + \sin \alpha_4 \, \cos \theta_4 \, \sigma_1
  A_{14}=a_1\cos\theta_1+d_4\sigma_3+d_3\sigma_{10}+a_2\cos\theta_1\cos\theta_2-a_4\sin\theta_4\sigma_1+d_2\sin\alpha_1\sin\theta_1-a_3\sin\theta_3\sigma_{12}-a_4\cos\theta_4\sigma_5+a_3\cos\theta_3\sigma_{13}-a_2\cos\alpha_1\sin\theta_1\sin\theta_2+a_1\cos\theta_1+a_2\sin\theta_1+a_2\sin\theta_2+a_1\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\cos\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_2\sin\theta_1+a_
 A_{21} = -\cos\theta_4 \,\sigma_6 - \sin\theta_4 \,\sigma_2
 A_{22} = \sin \alpha_4 \, \sigma_4 + \cos \alpha_4 \, \sin \theta_4 \, \sigma_6 - \cos \alpha_4 \, \cos \theta_4 \, \sigma_2
  A_{23} = \cos \alpha_4 \, \sigma_4 - \sin \alpha_4 \, \sin \theta_4 \, \sigma_6 + \sin \alpha_4 \, \cos \theta_4 \, \sigma_2
  A_{24} = d_4 \ \sigma_4 - d_3 \ \sigma_{11} + a_1 \ \sin\theta_1 - a_4 \ \sin\theta_4 \ \sigma_2 - d_2 \ \sin\alpha_1 \ \cos\theta_1 - a_3 \ \sin\theta_3 \ \sigma_{14} + a_2 \ \cos\theta_2 \ \sin\theta_1 - a_4 \ \cos\theta_4 \ \sigma_6 + a_3 \ \cos\theta_3 \ \sigma_{15} + a_2 \ \cos\alpha_1 \ \cos\theta_1 \ \sin\theta_2 + a_3 \ \cos\theta_3 \ \sigma_{15} + a_4 \ \cos\theta_4 \ \sigma_6 + a_5 \ \cos\theta_4 \ \sigma_6 + 
 A_{31} = \sin \theta_4 \, \sigma_7 + \cos \theta_4 \, \sigma_9
  A_{32} = \sin \alpha_4 \sigma_8 + \cos \alpha_4 \cos \theta_4 \sigma_7 - \cos \alpha_4 \sin \theta_4 \sigma_9
 A_{33} = \cos\alpha_4 \,\sigma_8 - \sin\alpha_4 \,\cos\theta_4 \,\sigma_7 + \sin\alpha_4 \,\sin\theta_4 \,\sigma_9
  \sigma_1 = \cos \alpha_3 \sin \theta_3 \sigma_{13} - \sin \alpha_3 \sigma_{10} + \cos \alpha_3 \cos \theta_3 \sigma_{12}
 \sigma_2 = \sin \alpha_3 \, \sigma_{11} + \cos \alpha_3 \, \sin \theta_3 \, \sigma_{15} + \cos \alpha_3 \, \cos \theta_3 \, \sigma_{14}
 \sigma_3 = \cos\alpha_3 \,\sigma_{10} + \sin\alpha_3 \,\sin\theta_3 \,\sigma_{13} + \sin\alpha_3 \,\cos\theta_3 \,\sigma_{12}
 \sigma_4 = \sin \alpha_3 \sin \theta_3 \sigma_{15} - \cos \alpha_3 \sigma_{11} + \sin \alpha_3 \cos \theta_3 \sigma_{14}
 \sigma_5 = \sin \theta_3 \; \sigma_{12} - \cos \theta_3 \; \sigma_{13}
 \sigma_6 = \sin \theta_3 \; \sigma_{14} - \cos \theta_3 \; \sigma_{15}
 \sigma_7 = \sin \alpha_3 \, \sigma_{16} + \cos \alpha_3 \, \cos \theta_3 \, \sigma_{17} - \cos \alpha_3 \, \sin \alpha_1 \, \sin \theta_2 \, \sin \theta_3
 \sigma_8 = \cos \alpha_3 \, \sigma_{16} - \sin \alpha_3 \, \cos \theta_3 \, \sigma_{17} + \sin \alpha_1 \, \sin \alpha_3 \, \sin \theta_2 \, \sin \theta_3
 \sigma_9 = \sin \theta_3 \; \sigma_{17} + \sin \alpha_1 \; \cos \theta_3 \; \sin \theta_2
 \sigma_{10} = \cos\alpha_2\,\sin\alpha_1\,\sin\theta_1 + \sin\alpha_2\,\cos\theta_1\,\sin\theta_2 + \cos\alpha_1\,\sin\alpha_2\,\cos\theta_2\,\sin\theta_1
\sigma_{11} = \cos\alpha_2\,\sin\alpha_1\,\cos\theta_1 - \sin\alpha_2\,\sin\theta_1\,\sin\theta_2 + \cos\alpha_1\,\sin\alpha_2\,\cos\theta_1\,\cos\theta_2
 \sigma_{12} = \cos\alpha_2\,\cos\theta_1\,\sin\theta_2 - \sin\alpha_1\,\sin\alpha_2\,\sin\theta_1 + \cos\alpha_1\,\cos\alpha_2\,\cos\theta_2\,\sin\theta_1
 \sigma_{13} = \cos \theta_1 \, \cos \theta_2 - \cos \alpha_1 \, \sin \theta_1 \, \sin \theta_2
 \sigma_{14} = \sin\alpha_1\,\sin\alpha_2\,\cos\theta_1 + \cos\alpha_2\,\sin\theta_1\,\sin\theta_2 - \cos\alpha_1\,\cos\alpha_2\,\cos\theta_1\,\cos\theta_2
 \sigma_{15} = \cos \theta_2 \, \sin \theta_1 + \cos \alpha_1 \, \cos \theta_1 \, \sin \theta_2
 \sigma_{16} = \cos \alpha_1 \, \cos \alpha_2 - \sin \alpha_1 \, \sin \alpha_2 \, \cos \theta_2
```

## Part (c)

Position of End-Effector Frame = 
$${}^{0}O_{4} = \begin{bmatrix} A_{14} \\ A_{24} \\ A_{34} \end{bmatrix}$$
  
Orientation of End-Effector Frame =  ${}^{0}R_{4} = \begin{bmatrix} A_{11} & A_{12} & A_{13} \\ A_{21} & A_{22} & A_{23} \\ A_{31} & A_{32} & A_{33} \end{bmatrix}$ 

Where, the entries  $A_{ij}$  are as specified in part (b).

 $\sigma_{17} = \cos \alpha_1 \sin \alpha_2 + \cos \alpha_2 \sin \alpha_1 \cos \theta_2$ 

## **Task 4.4**

The required MATLAB function for forward kinematics is given below:

```
function [x, y, z, R, theta, phi] = findPincher(jointAngles)
    0.5000*cos(jointAngles(1) + jointAngles(2) + jointAngles(3) + jointAngles(4)) + ...
       0.5000*cos(jointAngles(2) - jointAngles(1) + jointAngles(3) + jointAngles(4)), - ...
       0.5000*sin(jointAngles(2) - jointAngles(1) + jointAngles(3) + jointAngles(4)) - ...
       0.5000*sin(jointAngles(1) + jointAngles(2) + jointAngles(3) + jointAngles(4)), ...
       sin(jointAngles(1)), 5.4000*cos(jointAngles(1) - jointAngles(2)) + ...
       5.4000*cos(jointAngles(1) + jointAngles(2) + jointAngles(3)) + ...
       5.4000*cos(jointAngles(2) - jointAngles(1) + jointAngles(3)) + ...
       3.8000*cos(jointAngles(1) + jointAngles(2) + jointAngles(3) + jointAngles(4)) + ...
       5.4000*cos(jointAngles(1) + jointAngles(2)) + 3.8000*cos(jointAngles(2) - ...
       jointAngles(1) + jointAngles(3) + jointAngles(4));
    0.5000*sin(jointAngles(1) + jointAngles(2) + jointAngles(3) + jointAngles(4)) - ...
       0.5000*sin(jointAngles(2) - jointAngles(1) + jointAngles(3) + jointAngles(4)),
       0.5000*cos(jointAngles(1) + jointAngles(2) + jointAngles(3) + jointAngles(4)) - ...
       0.5000*cos(jointAngles(2) - jointAngles(1) + jointAngles(3) + jointAngles(4)), ...
       -cos(jointAngles(1)), 5.4000*sin(jointAngles(1) - jointAngles(2)) - ...
       3.8000*sin(jointAngles(2) - jointAngles(1) + jointAngles(3) + jointAngles(4)) + ...
       5.4000*sin(jointAngles(1) + jointAngles(2) + jointAngles(3)) - ...
       5.4000*sin(jointAngles(2) - jointAngles(1) + jointAngles(3)) + ...
       3.8000*sin(jointAngles(1) + jointAngles(2) + jointAngles(3) + jointAngles(4)) + ...
       5.4000*sin(jointAngles(1) + jointAngles(2));
    sin(jointAngles(2) + jointAngles(3) + jointAngles(4)), ...
       cos(jointAngles(2) + jointAngles(3) + jointAngles(4)),
                                                                6.1232e-17, ...
       7.6000*sin(jointAngles(2) + jointAngles(3) + jointAngles(4)) + ...
       10.8000*sin(jointAngles(2) + jointAngles(3)) + 10.8000*sin(jointAngles(2)) + 5.4000;
    0, ...
       0,
                     0, ...
    ];
x = T(1, 4);
y = T(2, 4);
z = T(3, 4);
R = T(1:3,1:3);
theta = jointAngles(1);
phi = sum(jointAngles(2:4));
end
```

The following code was added below in the given PincherModel.m file which generates 5 random configurations for the robot.

```
for i = 1:5
    disp(strcat('Random Configuration Number: ', num2str(i)));
    config = randomConfiguration(robot);
    disp("Our Calculations:");
    config_Arr = [0, 0, 0, 0];
    config_Arr(1) = getfield(config, {1}, 'JointPosition');
```

```
config_Arr(2) = getfield(config, {2}, 'JointPosition');
    config_Arr(3) = getfield(config, {3}, 'JointPosition');
    config_Arr(4) = getfield(config, {4}, 'JointPosition');
    [x, y, z, R, theta, phi] = findPincher(config_Arr)
    figure;
    show(robot, config);
    % Determine the pose of end-effector in provided configuration
    poseNow = getTransform(robot, config, "body4");
    % Display position and orientation of end-effector
    disp('The position of end-effector is:');
    disp('');
    disp(['X: ', num2str(poseNow(1,4))]);
    disp('');
    disp(['Y: ', num2str(poseNow(2,4))]);
    disp('');
    disp(['Z: ', num2str(poseNow(3,4))]);
    disp(' ');
    disp(['R: ']);
    poseNow(1:3,1:3)
    disp(' ');
    disp('The orientation angle is given with respect to the x-axis of joint 2:');
   disp('');
    poseNow01 = getTransform(robot, config, "body1");
   R14 = poseNow01(1:3,1:3)'*poseNow(1:3,1:3);
    angle = rad2deg(atan2(R14(2,1),R14(1,1)));
    disp(['Angle: ',num2str(angle), ' degrees.']);
end
```

We get the following calculated and obtained values for our 5 different configurations:

No.	Obtained					Calculated									
INO.	x	y	z		R			x	y	z			R		
1	23.4303	18.3029	262.3922		$egin{array}{ccc} 0.3047 & 0.726 \\ 0.2383 & 0.568 \\ 0.9222 & -0.38 \\ \end{array}$	1 0.7877		23.404	18.303	262.392		0.3047 0.2383 0.9222	0.7264 $0.5681$ $-0.3868$	$     \begin{bmatrix}     -0.6160 \\     0.7877 \\     0.0     \end{bmatrix} $	
2	50.9604	32.7114	70.9767			49 0.8415		50.96	32.711	70.977		$\begin{bmatrix} -0.2543 \\ -0.1633 \\ 0.9532 \end{bmatrix}$	0.8022 $0.5149$ $0.3022$		
3	153.9145	-60.8438	120.451		$     \begin{array}{rrr}       -0.5925 & -0.7 \\       0.2342 & 0.28 \\       0.7708 & -0.6     \end{array} $	-0.93	6	153.914	-60.844	120.451		-0.5925 $0.2342$ $0.7708$	-0.7168 $0.2834$ $-0.6371$	-0.3676 $-0.9300$ $0.0$	
4	-120.9881	-13.7822	57.0917			75 -0.9936		-120.988	-13.782	57.092		$\begin{bmatrix} 0.9639 \\ 0.1098 \\ 0.2428 \end{bmatrix}$	-0.2412 $-0.0275$ $0.9701$	$     \begin{bmatrix}       0.1132 \\       -0.9936 \\       0.0     \end{bmatrix} $	
5	-11.8649	-202.9725	18.4770			70 0.0584		-11.865	-202.972	184.770		$     \begin{bmatrix}       -0.0380 \\       -0.6507 \\       0.7583     \end{bmatrix} $	0.0443 0.7570 0.6519	$ \begin{array}{c} -0.9983 \\ 0.0584 \\ 0.0 \end{array} $	

Table 2: Calculated and Obtained [x, y, z, R] for 5 Random Robot Configurations

Where the values of x, y, z are in mm. We see that both the Calculated and Obtained values are the same.

**Task 4.6** 

Joint ID	DH Joint Angle $(\theta_i)$	Servo Angle $(\psi_i)$	Aligned directions of rotation (Yes/No)
1	$0^o$	$-90^{o}$	Yes
2	$0^o$	$-90^{o}$	Yes
3	00	00	Yes
4	00	00	Yes

Table 3: Linear mapping between servo angles and DH angles

Joint ID	Minimum	ı Joint Angle	Maximum Joint Angle			
	Servo Angle	DH Joint Angle	Servo Angle	DH Joint Angle		
1	$-150^{o}$	$-60^{o}$	$150^{o}$	$240^{o}$		
2	$-150^{o}$	$-60^{o}$	$150^{o}$	$240^{o}$		
3	$-150^{o}$	$-150^{o}$	$150^{o}$	$150^{o}$		
4	$-150^{o}$	$-150^{o}$	$150^{o}$	$150^{o}$		

Table 4: Joint Limits

The following code generates the required figures for identifying the reachable workspace.

```
N = 500;
arr = transpose (0:1/(N-1):1);
theta = [ones(1,N^2); ones(1,N^2); ones(1,N^2); ones(1,N^2)];
min_{theta} = [-60, -60, -150, -150] .* (pi/180);
max_theta = [240, 240, 150, 150] .* (pi/180);
x = ones(1, N^2);
y = ones(1, N^2);
z = ones(1, N^2);
theta(3,:) = \min_{t \in \mathbb{N}} \{x \in \mathbb{N} : x \in \mathbb{N} \} theta(3) -\min_{t \in \mathbb{N}} \{x \in \mathbb{N} : x \in \mathbb{N} \} theta(3) + \max_{t \in \mathbb{N}} \{x \in \mathbb{N} : x \in \mathbb{N} \}
theta(4,:) = min_theta(4) + (max_theta(4)-min_theta(4)) * rand(N^2,1);
theta(1,:) = \min_{t \in \mathbb{N}^2} theta(1) + (\max_{t \in \mathbb{N}^2} theta(1) - \min_{t \in \mathbb{N}^2} theta(1)) * rand(N^2,1);
theta(2,:) = min_theta(2) + (max_theta(2)-min_theta(2)) * rand(N^2,1);
for i = 1:N^2
     [x(i), y(i), z(i)] = findPincher(theta(1:4,i));
end
figure;
scatter3(x, y, z, 10, [0 0 1], 'filled');
[X, Y, Z] = sphere(25);
figure;
hold on;
scatter3(x, y, z, 10, [0 0 1], 'filled');
s = surf(X.*((max(x) - min(x))/2 + 1) + (max(x) - min(x))/2 + min(x), Y.*((max(y) - ...
    \min(y)/2 + 1) + (\max(y) - \min(y))/2 + \min(y), (Z).*((\max(z) - \min(z))/2 + 2) + ...
    (\max(z) - \min(z))/2 + \min(z));
s.FaceAlpha = 0.8;
s.FaceColor = [1 0 1];
```

The following Figure is obtained containing randomized points for our reachable workspace.

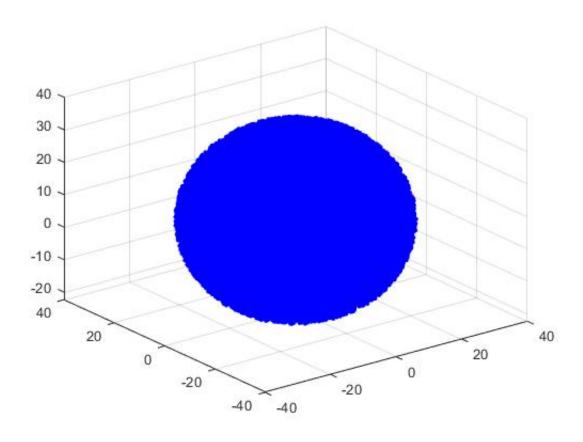


Figure 2: Reachable Workspace

We can see that the reachable workspace estiamtes a sphere. So our workspace can be expressed as a sphere that encloses all the points at which our Robot can move, Such a sphere is shown in the following figure, where a circle encloses all the plotted points.

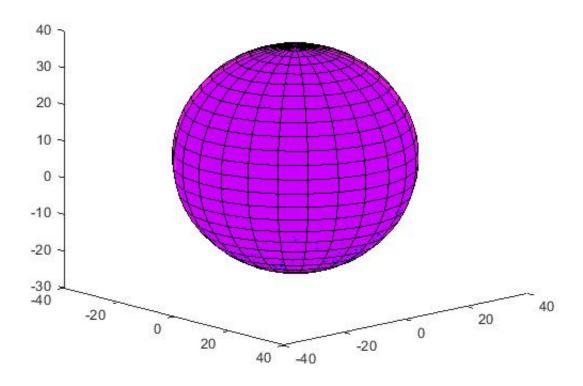


Figure 3: Reachable Workspace (Approximated as a Sphere)

The Projection of the point onto the X-Y plane can be seen in the following figure.

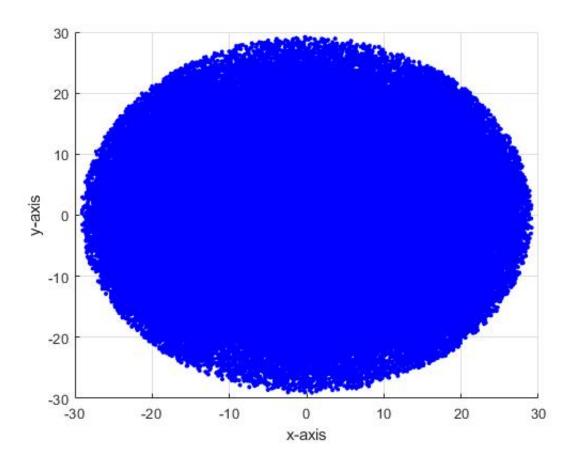


Figure 4: Reachable Workspace (Project on X - Y plane)

The maximum horizontal reach according to our identified workspace is [-30, 30]

## Task 4.8

```
function errorCode = setPosition(jointAngles)
   new_theta = zeros(1,4); % Array for JointAngles Mapped to [-pi, pi]
   errorCode = 0; % 0 -> No error yet
   for i=1:4
       % Mapping each jointangle to [-pi,pi]
       new_theta(i) = mod(jointAngles(i)+pi, 2*pi) - pi;
       % Condition for invalid input angle
       if ~(new_theta(i) <= pi && new_theta(i) >= -pi)
            disp(strcat('Angle ', num2str(i), ' Out of range'));
            % Error code = i -> ith Joint is out of range
            errorCode = i;
       end
   end
   % Passing the Joint Angles to Robot is no Error Occured
   if errorCode == 0
        % Mapping DH angles to Servo Angles
       map\_theta = zeros(1,5);
       map_theta(1) = jointAngles(1) - pi/2;
```

```
map_theta(2) = jointAngles(2) - pi/2;
map_theta(3) = jointAngles(3);
map_theta(4) = jointAngles(4);
% Connecting to Robot and passing the theta information
% to Robot for execution with a certain speed (64 for every joint
% in this case
arb = Arbotix('port', 'COM3', 'nservos', 5)
arb.setpos(map_theta, [64, 64, 64, 64]);
end
end
```

The following code command the robot to move to the 5 selected joint configurations. It also gives the values of [x, y, z, R].

```
thetas = zeros(5,4);
thetas(1,:) = [pi/2, pi/2, pi/2, pi/2];
thetas(2,:) = [-pi/4, pi/4, 0, 0];
thetas(3,:) = [-pi/4, pi/4, pi/2, -pi/2];
thetas(4,:) = [-pi/4, pi/4, -pi/2, pi/2];
thetas(5,:) = [pi/4, 5*pi/6, 0, 0];
for i=5:5
    [x, y, z, R, theta, phi] = findPincher(thetas(i,:))
    setPosition(thetas(i,:));
    pause(5);
end
```

No.	Calculated (cm)			Me	asured	Error (cm)	
110.	x	y	z	$\boldsymbol{x}$	y	z	d
1	0	-10.8	8.6	0	-10.4	8.4	0.447
2	14.6	-14.6	26.04	15	-15	24.8	0.947
3	3.8	-3.8	26.04	3.5	3.4	25.6	0.751
4	14.6	-14.6	10.77	15	-15	10.2	0.803
5	-17.88	-17.88	20	18	-18	19.6	0.434

Table 5: Calculated & Measured End-Effector Positions (with Error)

There are indeed errors in the measurement. The most prominent of them is the human error in measuring the positions because of limitations of instruments and ways to measure the position. Secondly, the torque of the motors also come into play. There are also uncertainties related to Servo Motor Angles which can cause the error.