

Worked Solutions to Tutorial Sheet 4

D Neglect Saturation.

With no current

$$\Phi_{\text{per turn}} = 0.625 \text{ mWb}$$

$$\Phi = BA = 0.625 \text{ mWb}$$

$$B = \frac{0.625 \times 10^{-3}}{2500 \times 10^{-6}} = 0.25 \text{ T}$$

When the coil is aiding the magnet, it needs to produce $1.6 - 0.25 = 1.35 \text{ T}$!

Total effective airgap seen by the coil

$$l_{\text{eff}} = 5 + 3 = 8 \text{ mm}$$

$$B = \frac{NI\mu_0}{l_{\text{eff}}} \Rightarrow I = \frac{l_{\text{eff}} B}{N\mu_0}$$

For 1.35 T , 100 turns, $\mu_0 = 4\pi \times 10^{-7}$

$$\underline{\underline{I = 8.6 \text{ A}}}$$

When opposing the magnet the coil needs to produce 1.85 T .

$$\Rightarrow \underline{\underline{I = 11.8 \text{ A}}}$$

②.

$$\text{At } 20^\circ : L = \frac{\Delta \psi}{\Delta I} = \frac{0.4}{0.5} = 0.8 \text{ H.}$$

$$\text{At } 60^\circ \quad L = \frac{\Delta \psi}{\Delta I} = \frac{0.4}{0.5} = 0.8 \text{ H.}$$

=

The torque produced by a machine is proportional to the rate of change of flux-linkage with rotor angle, and not the absolute magnitude of flux-linkage

a) 8000 rpm.

$$\omega = \frac{8000 \times 2\pi}{60} = 837 \text{ rad/s}$$

Peak flux linkage on open circuit ($i_f = I = 0$) is 1.18 Wb.

$$\psi = 1.18 \sin \theta$$

$$\frac{d\psi}{d\theta} = 1.18 \cos \theta$$

$$\left. \frac{d\psi}{d\theta} \right|_{\text{peak}} = 1.18 \leftarrow \text{for } \cos \theta = 1 \text{ i.e. at } \theta = 0^\circ$$

$$e_{\text{peak}} = \frac{d\psi}{d\theta} \cdot \frac{d\theta}{dt} = 1.18 \times 837$$
$$= 988 \text{ V}$$

Since the e.m.f is sinusoidal; $r_{ms} = \frac{988}{\sqrt{2}}$

$$E_{rms} = 700V$$

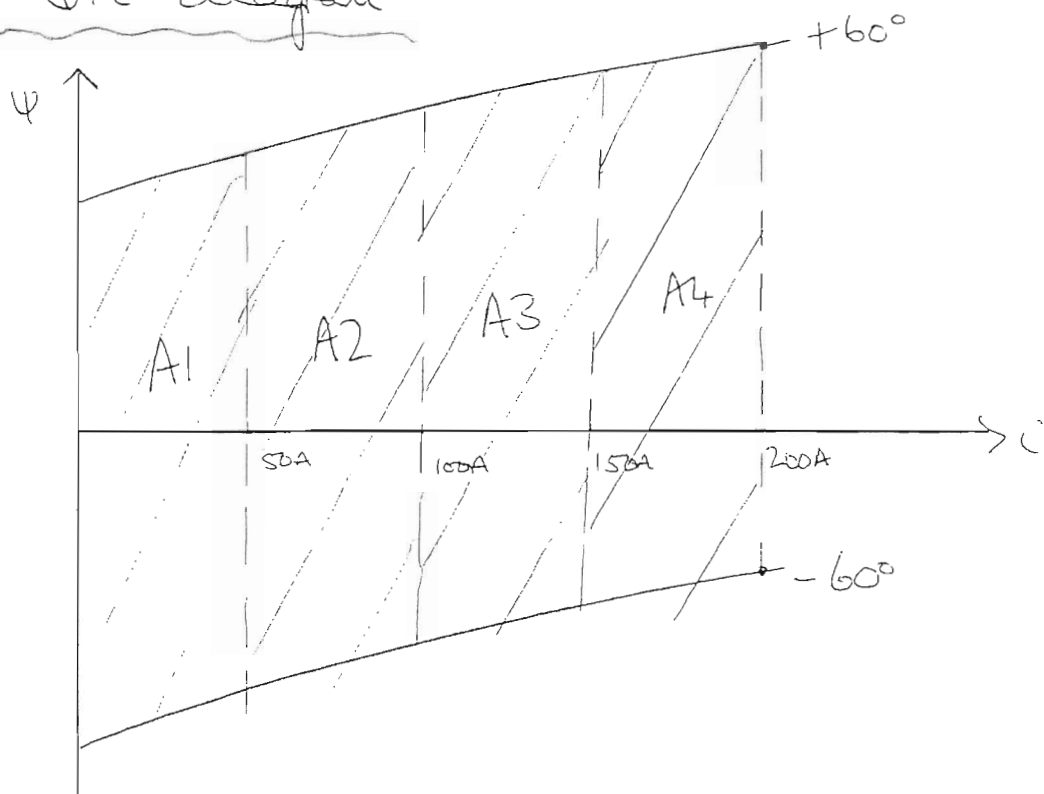
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③ a 12 teeth (i.e $1\frac{1}{2}$ teeth per pole).

b At 90° , $200A$.

$$L = \frac{\Delta\psi}{\Delta I} = \frac{0.02}{50} = 400\mu H.$$

c * Plot ψ/i diagram



Calculate the areas A_1, A_2, A_3 & A_4 by applying simple trapezium integration

For SOA.

$$T = \frac{A_1}{\frac{120 \times \pi}{180}} \times PP = 4 \times 186 = 744 \text{ Nm}$$

↑
convert to rads

For ZOA.

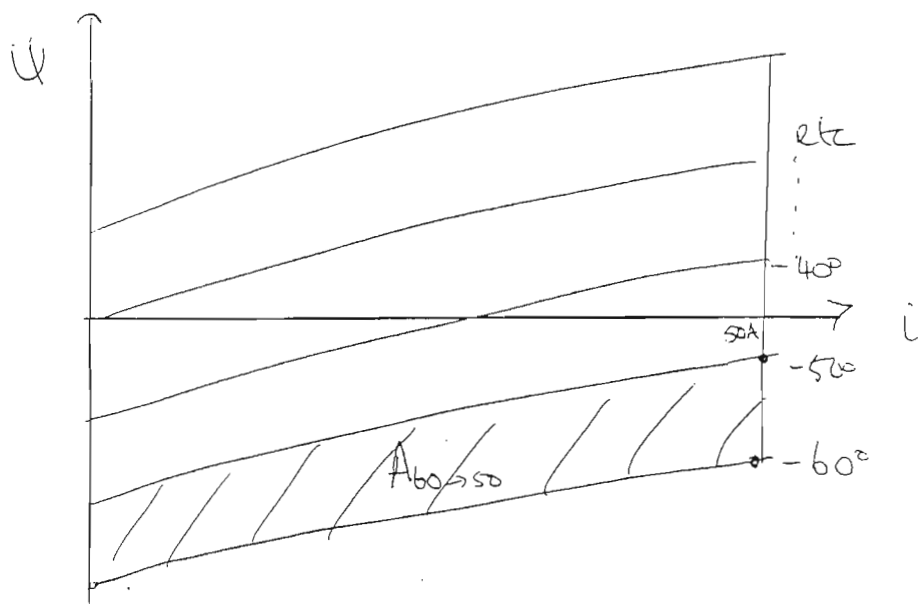
$$T = \frac{(A_1 + A_2 + A_3 + A_4)}{\frac{120 \times \pi}{180}} PP = 2852 \text{ Nm}$$

Repeat the same process for the -80° to 140° interval; values derived graphically are approximate

$$T_{SOA} = 696 \text{ Nm}$$

$$T_{ZOA} = 2772 \text{ Nm}$$

3). Plot a ψ/i diagram.

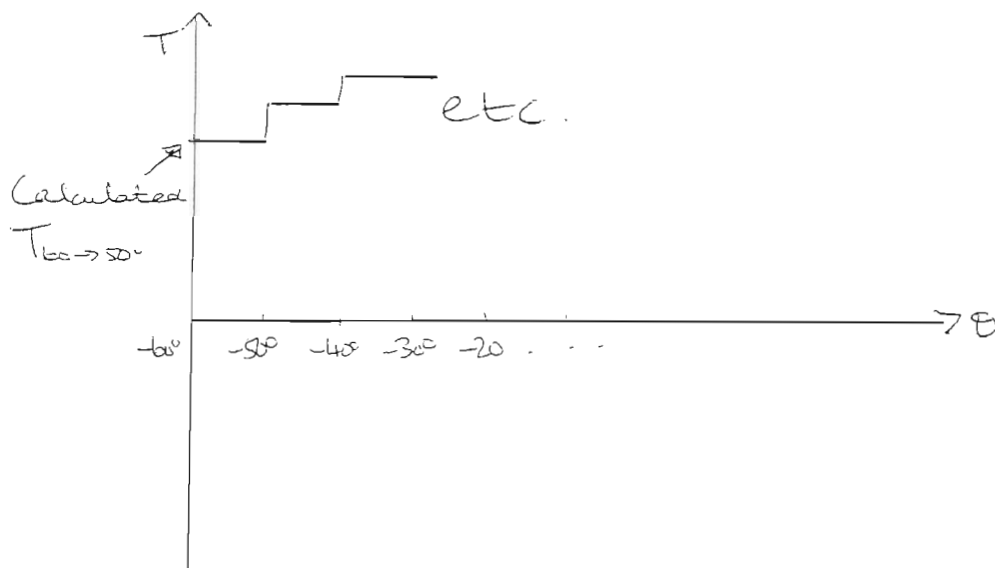


Calculate $A_{60 \rightarrow 50}$

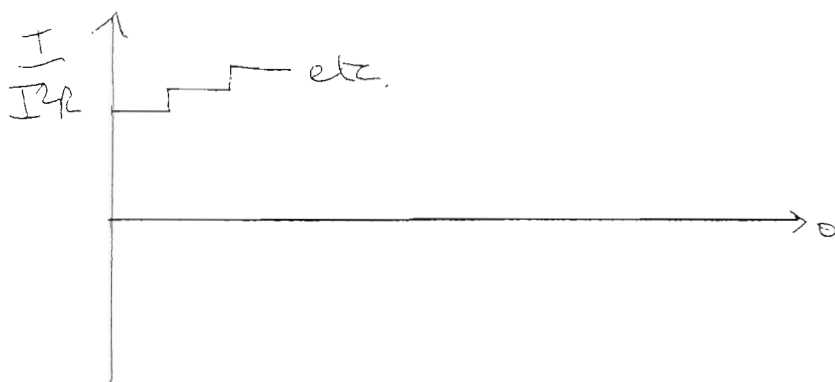
The average torque over this 10° interval is given by

$$T_{\frac{60}{50}} = \frac{A_{60 \rightarrow 50} \times PP}{10 \times \frac{\pi}{180}}$$

Calculate for each interval and plot as a graph



②. Plot same graph as before but divide by $I^2 R$ ($R = 1 \Omega$) (will give same shape, but demonstrates the variation in efficiency over the interval).



f) Supply with more sinusoidally shaped current

g) Max at 0°
Min at 90°

h) Higher torque per amp and hence efficiency.
Lower $\cos \phi$ loss
Higher inductance \rightarrow lower PWM frequency.

i) Aerospace, Motorsport
i.e. any application where weight is more important than efficiency.