

AC (time varying) circuits

- obey the same rules as dc circuits but there are extra things to take into account.

Components

- capacitors — potential energy stores
— inductors.

↓
usually consist of two plates separated by a "dielectric"

↓
governed by a relationship

$$I = C \frac{dV}{dt}$$

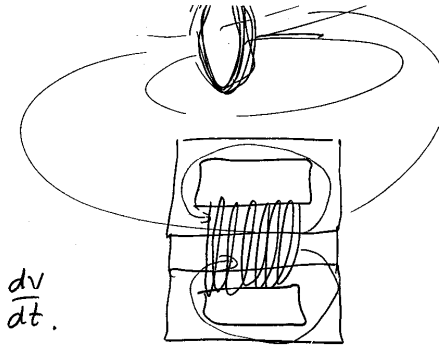
$$Q = CV$$

$$Q = \int I dt \rightarrow I = \frac{dQ}{dt}$$

$$CV = \int I dt$$

$$\text{or } V = \frac{1}{C} \int I dt \rightarrow \frac{dV}{dt} = \frac{I}{C}$$

$$\text{Energy stored} = \frac{1}{2} CV^2$$

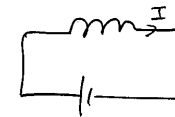
InductorsInductors

$$I = C \frac{dV}{dt}$$

$$V = L \frac{dI}{dt}$$

$$I = \frac{1}{L} \int V dt$$

$$V = \frac{1}{C} \int I dt$$



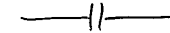
Stored energy in an inductor

$$\text{is } \frac{1}{2} LI^2$$

$$\frac{1}{2} CV^2$$

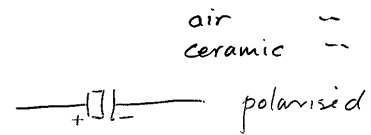
Symbolic representations

capacitor



non-polarised capacitor

plastic dielectric
mica dielectric



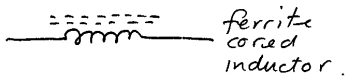
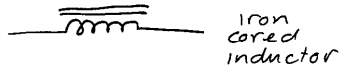
inductors

$$I = C \frac{dv}{dt}$$

$$V = L \frac{dI}{dt}$$



CIVIL



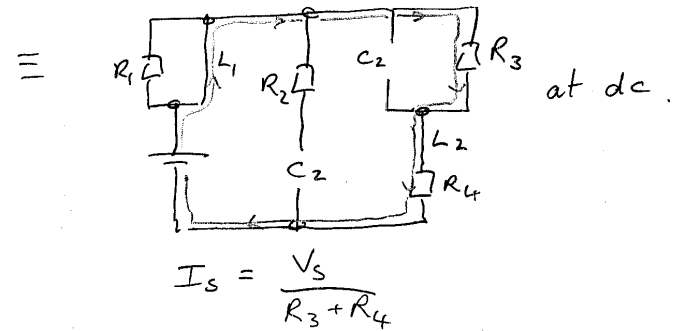
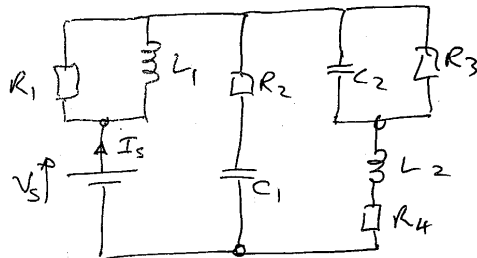
Behaviour of C + L at dc

at dc (ie 0Hz)

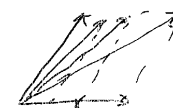
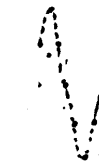
$\frac{dI}{dt} = 0$ everywhere in the ckt

$\frac{dV}{dt} = 0$ everywhere in the ckt.

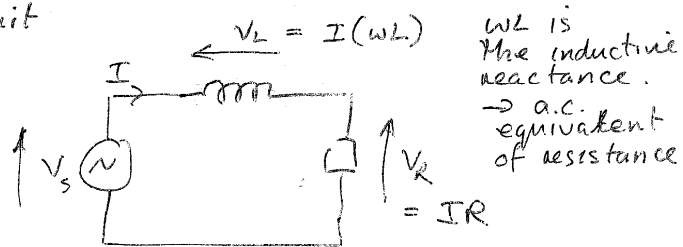
So



Representing ac voltages & currents.



Applying vector ideas to a circuit



need to express V_L in terms of I

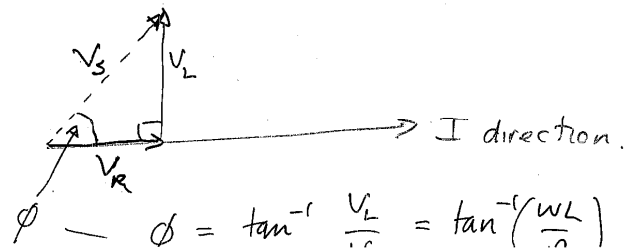
$$V_L = L \frac{dI}{dt}$$

so if I drives L and I is $I_p \sin \omega t$

$$V_L = L I_p \omega \cos \omega t$$

this is the magnitude of V_L

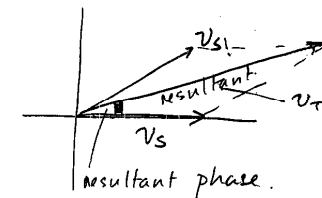
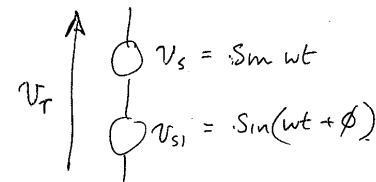
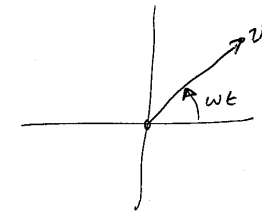
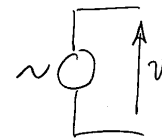
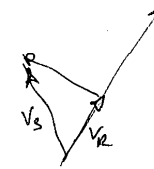
to draw a vector diagram - use I as a reference direction because it is common to all components.



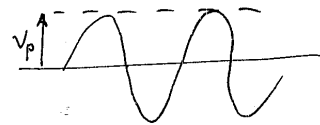
$$\phi - \phi = \tan^{-1} \frac{V_L}{V_R} = \tan^{-1} \left(\frac{\omega L}{R} \right)$$

$$\begin{aligned} V_s^2 &= V_L^2 + V_R^2 \\ &= I^2 \omega^2 L^2 + I^2 R^2 \\ &= I^2 (\omega^2 L^2 + R^2) \end{aligned}$$

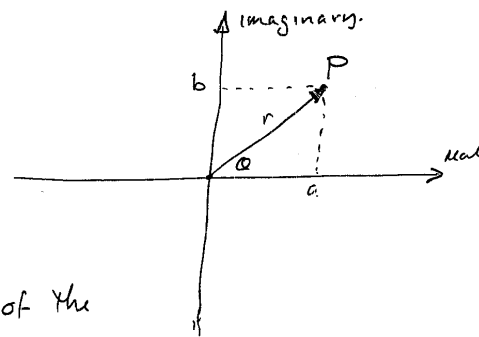
$$\frac{V_s}{I} = |Z| = \sqrt{\omega^2 L^2 + R^2}$$



for a sinusoid $V = V_p \sin(\omega t + \phi)$
 ↑
 amplitude



Complex number representation of a.c.



coordinates of the point P are

$a + jb \Rightarrow$ Cartesian representation

$$r = \sqrt{a^2 + b^2}$$

$$\phi = \tan^{-1} b/a$$

if $\phi = \omega t$, P would rotate in an anti-clockwise direction at a rate of ω rad s^{-1}

an alternative expression of the position of P is $r e^{j\phi} \Rightarrow$ polar representation

Complex numbers are easy to manipulate if

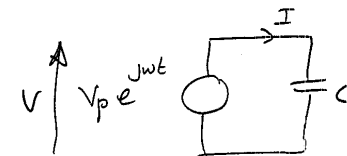
the appropriate form is used.

→ addition and subtraction are best done in cartesian ($a + jb$) form

→ multiplication & division are best done in polar form.

The rotating ac phasor is

$$V_p e^{j\omega t}$$



$$I = C \frac{dV}{dt} = C V_p \omega j e^{j\omega t}$$

$$Z_C = \frac{V}{I} = \frac{V_p e^{j\omega t}}{j C V_p \omega e^{j\omega t}}$$

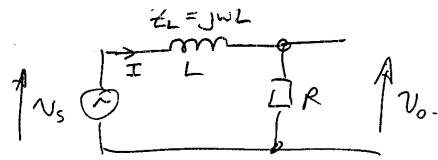
$$= \frac{1}{j\omega C} = -\frac{j}{\omega C} = -j X_C$$

Similarly for an inductor

$$Z_L = j\omega L = j X_L$$

Using "j" on circuits

$$Z_L = j\omega L$$

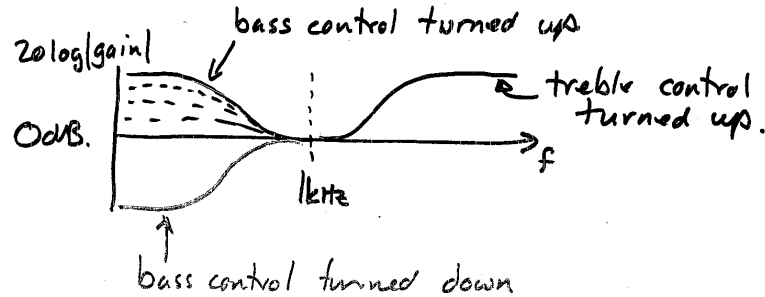


$$I = \frac{v_s}{Z_L + R} = \frac{v_s}{j\omega L + R}$$

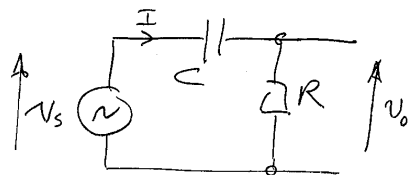
$$\therefore v_o = IR = \frac{v_s R}{j\omega L + R} = \frac{v_s}{1 + j\omega L/R}$$

$$\text{ie } \frac{v_o}{v_i} = \frac{1}{1 + j\omega L/R}$$

$$\left| \frac{v_o}{v_i} \right| = \frac{1}{\sqrt{1 + (\omega L/R)^2}} \quad \angle \left(\frac{v_o}{v_i} \right) = -\tan^{-1} \left(\frac{\omega L/R}{1} \right)$$



The CR circuit

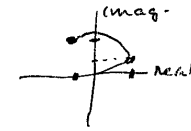


$$Z_c = \frac{1}{j\omega C}$$

Impedance of circuit from v_s 's point of view

$$Z = Z_c + R$$

$$I = \frac{v_s}{Z}$$



$$v_o = IR = \frac{v_s R}{Z} = v_s \frac{R}{Z_c + R} = v_s \frac{R}{\frac{1}{j\omega C} + R}$$

$$= v_s \frac{j\omega CR}{1 + j\omega CR}$$

CR = time constant of the ckt.

$$C = \frac{Q}{V} = \frac{It}{V} = \frac{\text{Amps} \times \text{Time}}{\text{Volts}}$$

$$R = \frac{\text{Volts}}{\text{Amps}}$$

$$CR = \frac{\text{Amps} \times \text{Time}}{\text{Volts}} \times \frac{\text{Volts}}{\text{Amps}} = \text{Time}$$

lets define a frequency domain constant

— say ω_0 or ω_c

$$\text{such that } \omega_0 \text{ (or } \omega_c \text{ or } \dots) = \frac{1}{CR}$$

$$\therefore \frac{v_o}{v_i} = \frac{j\omega/\omega_0}{1 + j\omega/\omega_0} = \frac{j f/f_0}{1 + j f/f_0}$$

$20 \log \left| \frac{v_o}{v_s} \right|$ as a function of f .

$$\left| \frac{v_o}{v_s} \right| = \frac{f/f_0}{\sqrt{1 + (f/f_0)^2}}$$

$$= \frac{1}{\sqrt{\left(\frac{f_0}{f}\right)^2 + 1}}$$

$$20 \log \left| \frac{v_o}{v_s} \right| = 20 \log \left[\frac{f/f_0}{\sqrt{1 + (f/f_0)^2}} \right]$$

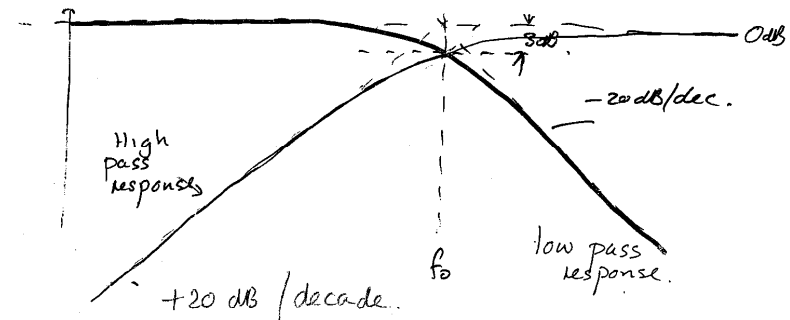
$$= 20 \log \frac{f}{f_0} + 20 \log \left[\frac{1}{\sqrt{1 + (f/f_0)^2}} \right]$$

$$f \ll f_0 \quad \frac{1}{\sqrt{1 + (f/f_0)^2}} \Rightarrow \frac{1}{\sqrt{1}} \Rightarrow 0 \text{ dB.}$$

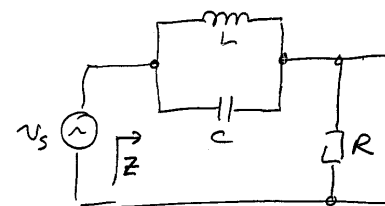
$\text{since } (f/f_0)^2 \ll 1$

$$f = f_0 \quad \frac{1}{\sqrt{1 + 1}} = \frac{1}{\sqrt{2}} \Rightarrow -3 \text{ dB.}$$

$$f \gg f_0 \quad \frac{1}{\sqrt{\frac{f_0^2}{f^2} + 1}} \quad \text{since } \left(\frac{f}{f_0}\right)^2 \gg 1 \quad \frac{v_o}{v_s} \approx \frac{f_0}{f}$$



Another cct from the lab.....



$$Z_1 \parallel Z_2 = \frac{Z_1 Z_2}{Z_1 + Z_2}$$

$$Z = (Z_L \parallel Z_C) + R$$

$$= \frac{j\omega L / j\omega C}{j\omega L + \frac{1}{j\omega C}} + R$$

$$Z_L = j\omega L$$

$$Z_C = \frac{1}{j\omega C}$$

$$= \frac{j\omega L}{j\omega L \cdot j\omega C + 1} + R$$

$$= \frac{j\omega L + R(1 + j^2 \omega^2 LC)}{1 + j^2 \omega^2 LC}$$

but $j^2 = -1$

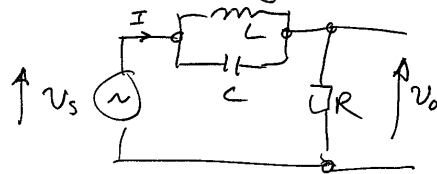
$$= \frac{j\omega L + R - \omega^2 LC R}{1 - \omega^2 LC}$$

$$= \frac{j\omega L + R - \omega^2 LC}{1 - \omega^2 LC}$$

$$= R \left(\frac{j\omega L/R + 1 - \omega^2 LC}{1 - \omega^2 LC} \right)$$

$$|Z| = \frac{R}{1 - \omega^2 LC} \left[(1 - \omega^2 LC)^2 + \frac{\omega^2 L^2}{R^2} \right]^{1/2}$$

To work out gain



$$I = \frac{v_s}{Z} \quad \therefore v_o = I \cdot R$$

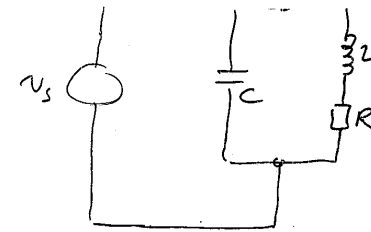
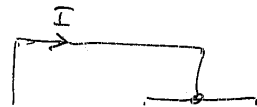
$$= \frac{v_s R}{Z}$$

$$\frac{v_o}{v_s} = \frac{R}{Z} = \frac{R}{R \left(\frac{j\omega L/R + 1 - \omega^2 LC}{1 - \omega^2 LC} \right)}$$

$$= \frac{1 - \omega^2 LC}{j\omega L/R + 1 - \omega^2 LC}$$

What happens if L has some resistance?

What is $\frac{v_s}{I}$



$$Z = Z_c \parallel (R + Z_L)$$

$$= \frac{1}{j\omega C} \parallel (R + j\omega L)$$

$$= \frac{\frac{1}{j\omega C} \cdot (R + j\omega L)}{\frac{1}{j\omega C} + R + j\omega L} \times \frac{j\omega C}{j\omega C}$$

$$= \frac{R + j\omega L}{1 + j\omega CR + j^2 \omega^2 LC}$$

$$= \frac{R + j\omega L}{1 - \omega^2 LC + j\omega CR}$$

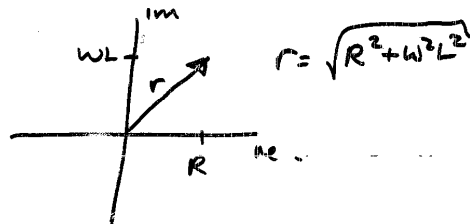
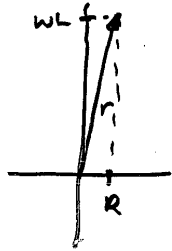
$$I = \frac{V_B - V_A}{R}$$

$$I = \frac{V_A - V_B}{R}$$

$$|Z| = \frac{|R + j\omega L|}{|1 - \omega^2 LC + j\omega CR|}$$

$$= \frac{\sqrt{R^2 + \omega^2 L^2}}{\sqrt{1 - \omega^2 LC + \omega^2 C^2 R^2}}$$

$$= \frac{\sqrt{R^2 + \omega^2 L^2}}{\sqrt{(1 - \omega^2 LC)^2 + \omega^2 CR^2}}$$



$$\angle Z = \tan^{-1} \frac{\omega L}{R} - \tan^{-1} \frac{\omega CR}{1 - \omega^2 LC}$$

Power in ac circuits (page 14).

The problem is that $V + I$ are functions of time.

Only makes sense to talk of power in waveform environments where shapes are periodic — i.e. one cycle is the same as the next.

For power the relationship that never lets you down is

$$P = \frac{1}{T} \int_0^T V(t) I(t) dt.$$

where T is the periodic time of

a periodic waveform.

so if $V(t) = V_p \sin \omega t$
and $I(t) = I_p \sin \omega t$

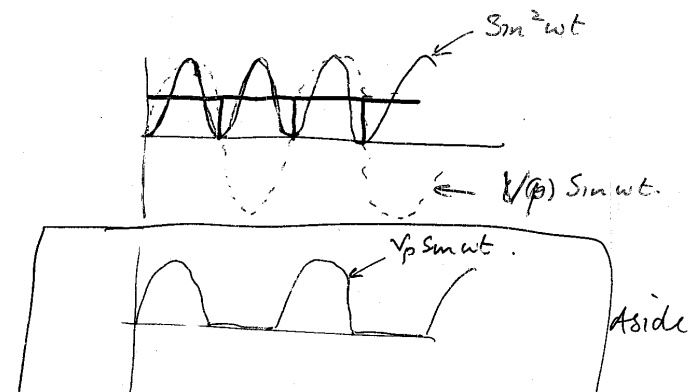
$$P = \frac{1}{T} \int_0^T V_p \sin \omega t \times I_p \sin \omega t dt$$

$$= \frac{1}{T} \int_0^T \frac{V_p^2}{R} \sin^2 \omega t dt$$

$$= \frac{1}{T} \int_0^T I_p^2 R \sin^2 \omega t dt.$$

$$= \frac{1}{T} \int_0^T \frac{V_p^2}{R} \left(\frac{1 - \cos 2\omega t}{2} \right) dt.$$

$$= \frac{1}{T} \frac{V_p^2}{2R} \int_0^T (1 - \cos 2\omega t) dt.$$



$$\omega = 2\pi f = \frac{2\pi}{T} \quad \text{or} \quad T = \frac{2\pi}{\omega}$$

$$\quad \text{or} \quad \frac{T}{2} = \frac{\pi}{\omega}$$

$$P = \frac{1}{T} \frac{V_p^2}{2R} \int_0^{\pi/\omega} (1 - \cos 2\omega t) dt$$

$$= \frac{V_p^2 \omega}{2R\pi} \left[t - \frac{1}{2\omega} \sin 2\omega t \right]_0^{\pi/\omega}$$

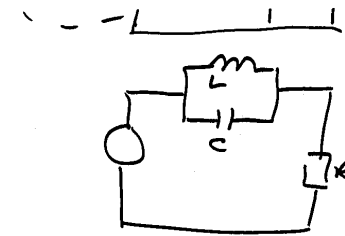
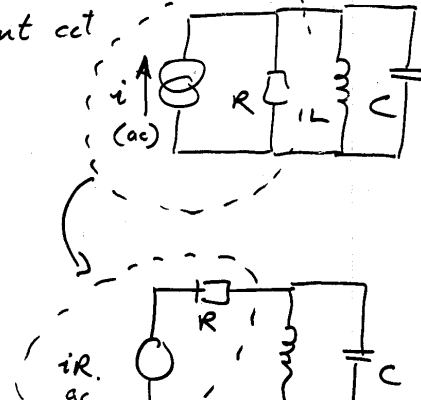
$$= \frac{V_p^2 \omega}{2R\pi} \left[\frac{\pi}{\omega} - 0 - \frac{1}{2\omega} \sin \frac{2\omega\pi}{\omega} + \frac{1}{2\omega} \sin 0 \right]$$

$$= \frac{V_p^2 \omega \pi}{2R\pi \omega} = \frac{1}{R} \left(\frac{V_p^2}{2} \right)$$

mean squared voltage

ASIDE

classic // resonant cct



mean squared voltage is often square rooted to give an equivalent voltage with units of volts. This is V_{rms} → the root-mean-square voltage.

$$\sqrt{V(t)^2} = \text{RMS voltage}$$

Phase difference

$$V_s = V_p \sin \omega t$$

$$I = I_p \sin(\omega t + \phi)$$

$$\frac{V_p}{I_p} = |Z|$$

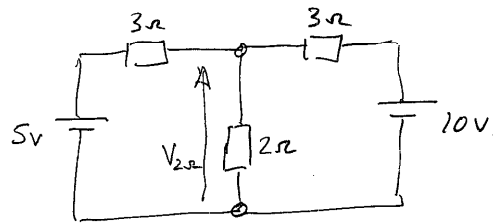
$$P = \frac{1}{T} \int_0^T V_s(t) I(t) dt = \frac{1}{T} \int_0^T V_p \sin \omega t I_p \sin(\omega t + \phi) dt$$

gives

$$P = \frac{V_p I_p}{2} \cos \phi = \frac{V_p^2}{2} \cos \phi = \frac{V_{rms}^2}{2} \cos \phi$$

$$P = \frac{V_p I_p}{2} \cos \phi = \frac{V_p}{2|Z|} \cos \phi = \frac{V_{rms}^2}{|Z|} \cos \phi$$

$$= \frac{I_p^2 |Z|}{2} \cos \phi$$



What is the power dissipated in the 2Ω resistor?

Some people have used superposition

$$V_{2r} \text{ due to } 5V = 5 \times \frac{2||3}{3+2||3} = \frac{5 \times 6/5}{2/5}$$

$$= \frac{6 \times 5}{2/5} = \frac{10}{7} V$$

$$\text{So } P_{2r} \text{ due to } 5V = \left(\frac{10}{7}\right)^2 / R = \frac{100}{2 \times 49} \approx 1W$$

$$V_{2r} \text{ due to } 10V = 10 \times \frac{2||3}{3+2||3} = \frac{20}{7} V$$

$$P_{2r} \text{ due to } 10V = \frac{400}{2 \times 49} \approx 4W$$

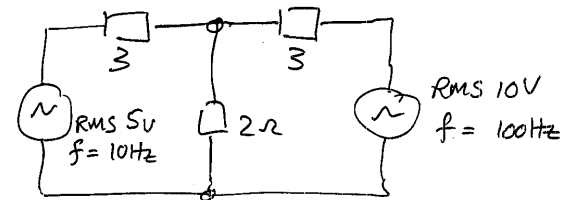
$$P = \frac{1}{2} (V_1 + V_2)^2$$

Some people said $P_{2r} = \frac{(V_{2r/5V} + V_{2r/10V})^2}{R}$

$$= \frac{\left(\frac{30}{7}\right)^2 \times \frac{1}{2}}{2 \times 49}$$

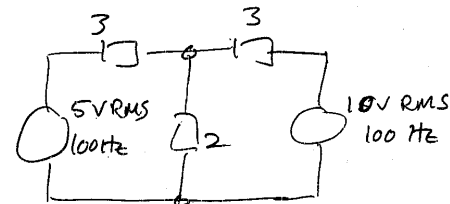
$$= \frac{900}{2 \times 49} \approx 9W \checkmark$$

Now consider a different problem



$$\left. \begin{array}{l} P_{2r} \text{ due to } 5V_{100Hz} \approx 1W \\ P_{2r} \text{ due to } 10V_{100Hz} \approx 4W \end{array} \right\} P_{Tot} \approx 5W$$

If voltages are added first
 $P_{2r} = 9W$.



Same result as the d.c. source case.

The mean squared value of

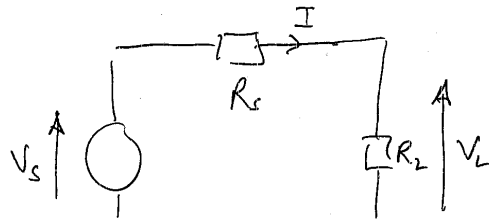
Consider a sum of two ac voltage sources.

$$\begin{aligned}\overline{(V_1 + V_2)^2} &= \overline{V_1^2 + 2V_1V_2 + V_2^2} \\ &= \overline{V_1^2} + \overline{V_2^2} + \overline{2V_1V_2}\end{aligned}$$

— one dc + one ac voltage

$$\begin{aligned}\overline{(V_1 + V_p \sin \omega t)^2} &= \overline{V_1^2} + \overline{V_p^2 \sin^2 \omega t} + \overline{2V_1 V_p \sin \omega t} \\ &\quad \quad \quad \nearrow \\ &\quad \quad \quad \underline{2V_{p1} V_{p2} \sin \omega_1 t \sin \omega_2 t.}\end{aligned}$$

Maximum Power Transfer.



want to find the value of R_L that will maximise transfer of power from V_s to R_L .

$$I = \frac{V_s}{R_s + R_L}$$

$$V_L = IR_L = \frac{V_s}{R_s + R_L} \cdot R_L$$

P_L = power transferred to R_L

$$\begin{aligned}P_L &= \frac{V_L^2}{R_L} = \frac{V_s^2 R_L^2}{(R_s + R_L)^2 R_L} \\ &= \frac{V_s^2 R_L}{(R_s + R_L)^2}\end{aligned}$$

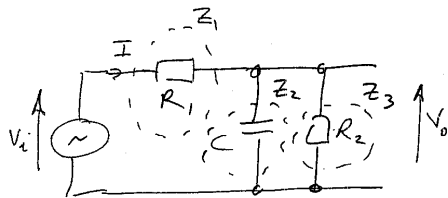
now we need to differentiate P_L w.r.t R_L to find max P_L

alternatively look for a minimum in $\frac{1}{P_L}$

$$\begin{aligned}\frac{d}{dR_L} \left(\frac{1}{P_L} \right) &= \frac{d}{dR_L} \left(\frac{(R_s + R_L)^2}{V_s^2 R_L} \right) \\ &= \frac{d}{dR_L} \left(\frac{R_s^2 + 2R_s R_L + R_L^2}{V_s^2 R_L} \right)\end{aligned}$$

$$\begin{aligned}
 & \frac{V_s^2 R_L}{dR_L} \\
 & = \frac{1}{V_s^2} d \left(\frac{R_s^2}{R_L} + 2R_s + R_L \right) \\
 & \quad \frac{dR_L}{dR_L} \\
 & 0 = \frac{1}{V_s^2} \left[-R_s^2 R_L^{-2} + 0 + 1 \right] \\
 & 0 = \frac{1}{V_s^2} \left[-\frac{R_s^2}{R_L^2} + 1 \right] \\
 & R_s^2 = R_L^2 \text{ for min in } \frac{1}{P_L} \text{ or} \\
 & \text{or } R_s = R_L \text{ max in } P_L.
 \end{aligned}$$

Start with an R-C circuit



What impedance does V_i see (ie what is $\frac{V_i}{I}$)

What is $\frac{V_o}{V_i}$?

$$\begin{aligned}
 Z &= \frac{V_i}{I} = Z_1 + Z_2 \parallel Z_3 \\
 &= R_1 + \frac{Z_2 Z_3}{Z_2 + Z_3} = R_1 + \frac{\frac{1}{j\omega C} R_2}{\frac{1}{j\omega C} + R_2}
 \end{aligned}$$

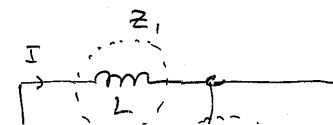
$$\begin{aligned}
 &= R_1 + \frac{R_2}{1 + j\omega C R_2} \\
 &= \frac{R_1 + j\omega C R_1 R_2 + R_2}{1 + j\omega C R_2} = \frac{(R_1 + R_2) + j\omega C R_1 R_2}{1 + j\omega C R_2} \\
 &= (R_1 + R_2) \frac{(1 + j\omega C \frac{R_1 R_2}{R_1 + R_2})}{1 + j\omega C R_2}
 \end{aligned}$$

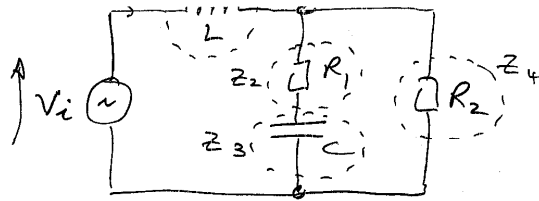
What about $\frac{V_o}{V_i}$?

$$I = \frac{V_i}{Z}$$

$$V_o = I \cdot Z_2 \parallel Z_3 = I \frac{R_2}{1 + j\omega C R_2}$$

$$\begin{aligned}
 \frac{V_o}{V_i} &= \frac{Z_2 \parallel Z_3}{Z} = \frac{\frac{R_2}{1 + j\omega C R_2}}{(R_1 + R_2) \frac{(1 + j\omega C \frac{R_1 R_2}{R_1 + R_2})}{1 + j\omega C R_2}} \\
 &= \frac{R_2}{(R_1 + R_2)} \cdot \frac{1}{1 + j\omega C \frac{R_1 R_2}{R_1 + R_2}} \\
 &= k \cdot \frac{1}{1 + j \frac{f}{f_0}} \\
 &\text{where } k = \frac{R_2}{R_1 + R_2} \\
 &\text{and } f_0 = \frac{1}{2\pi C (R_1 \parallel R_2)}
 \end{aligned}$$





What does Z look like as far as V_i is concerned.

$$Z_T = \frac{V_i}{I} = Z_1 + [Z_4 \parallel (Z_2 + Z_3)]$$

let $j\omega = s$.

$$Z_1 = j\omega L \Rightarrow sL \quad Z_2 = R_1 \quad Z_3 = \frac{1}{j\omega C} \Rightarrow \frac{1}{sC}$$

$$Z_4 = R_2$$

$$\begin{aligned} \therefore Z_T &= sL + \frac{Z_4(Z_2 + Z_3)}{Z_4 + Z_2 + Z_3} \\ &= sL + \frac{R_2(R_1 + \frac{1}{sC})}{R_2 + R_1 + \frac{1}{sC}} \quad \text{multiply top + bottom by } sC \\ &= sL + \frac{R_2(sCR_1 + 1)}{sC(R_2 + R_1) + 1} \\ &= \frac{s^2LC(R_2 + R_1) + sL + R_2sCR_1 + R_2}{1 + sC(R_2 + R_1)} \\ &= \frac{R_2 + s(L + CR_1R_2) + s^2LC(R_2 + R_1)}{1 + sC(R_2 + R_1)} \end{aligned}$$

putting $s = j\omega$

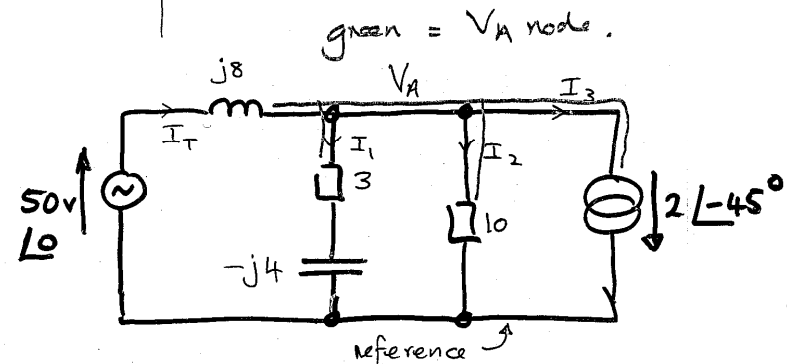
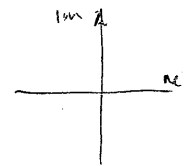
$$= \frac{R_2 - \omega^2LC(R_2 + R_1) + j\omega(L + CR_1R_2)}{1 + j\omega C(R_1 + R_2)}$$

$$= \frac{R_2 - \omega^2LC(R_2 + R_1) + j\omega(L + CR_1R_2)}{1 + j\omega C(R_1 + R_2)}$$

$$|Z| = \frac{|V|}{|I|} = \frac{V_p}{I_p} = \frac{V_{rms}}{I_{rms}}$$

$$|Z| = \left[\frac{[R_2 - \omega^2LC(R_2 + R_1)]^2 + \omega^2(L + CR_1R_2)^2}{[1 + \omega^2C^2(R_1 + R_2)^2]} \right]^{1/2}$$

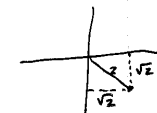
$$\phi(z) = \tan^{-1} \frac{\omega(L + CR_1R_2)}{R_2 - \omega^2LC(R_2 + R_1)} - \tan^{-1} \frac{\omega C(R_1 + R_2)}{1}$$



What is V_A (with respect to the reference).

Sum currents at V_A node

$$I_T = I_1 + I_2 + I_3$$



$$\frac{50 - V_A}{j8} = \frac{V_A}{3 + (-j4)} + \frac{V_A}{10} + 2 \angle -45^\circ$$

$$\frac{50 - V_A}{j8} = \frac{V_A}{3 - j4} + \frac{V_A}{10} + \sqrt{2} - j\sqrt{2}$$

$$\frac{-50j + jV_A}{8} = \frac{V_A(3 + j4)}{\underbrace{3^2 + 4^2}_{=25}} + \frac{V_A}{10} + \sqrt{2} - j\sqrt{2}$$

$$-50 \cdot 25j + 25jV_A = 24V_A + 32jV_A + 20V_A + 200\sqrt{2} - 200j\sqrt{2}$$

$$-1250j + 200\sqrt{2}j - 200\sqrt{2} = V_A [24 + 20 + j(32 - 25)]$$

$$-967j - 283 = V_A [44 + j(7)]$$

$$V_A = \frac{-967j - 283}{44 + j7} = \frac{1008 \angle 73.7^\circ - 180^\circ}{44 \cdot 03 \angle 9.04^\circ}$$

$$= \frac{1008 \angle -106.3^\circ}{44 \angle 9^\circ}$$

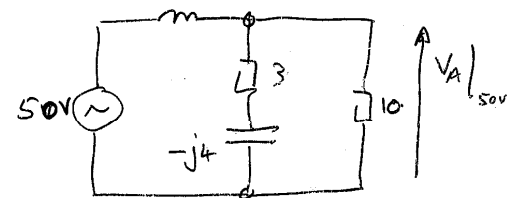
$$V_A = \frac{1008}{44} \angle -106.3^\circ - 9^\circ$$

$$= 22.9 \angle -115.3^\circ$$

Lets try using superposition.

$j8$

← partial cct for 50v source.



V_A due to 50v

$$= 50 \frac{10 \parallel (3 - j4)}{j8 + 10 \parallel (3 - j4)}$$

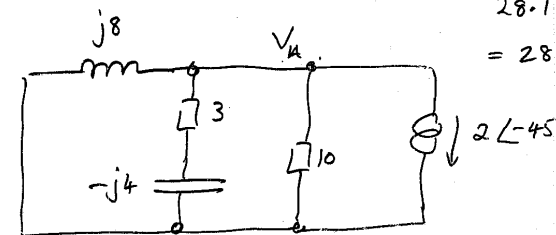
$$= 50 \frac{10(3 - j4)}{10 + 3 - j4} \frac{10(3 - j4)}{j8 + \frac{10(3 - j4)}{10 + 3 - j4}}$$

$$= 50 \frac{10(3 - j4)}{j8(10 + 3 - j4) + 10(3 - j4)}$$

$$= \frac{500(3 - j4)}{104j + 32 + 30 - 40j} = \frac{500(3 - j4)}{64j + 62}$$

$$= 500 \cdot 5 \angle -53^\circ / 89 \angle 46^\circ$$

partial circuit for $2 \angle -45^\circ$



$$28.1 \angle -53^\circ - 46^\circ$$

$$= 28.1 \angle -99^\circ$$

Impedance seen by current source looking into the circuit is

$11 \parallel 11 \dots$

$$10 \parallel j8 \parallel (3-j4)$$

$$\therefore \frac{1}{Z_T} = \frac{1}{10} + \frac{1}{3-j4} + \frac{1}{j8}$$

$$= \frac{1}{10} + \frac{3+j4}{25} - \frac{j}{8}$$

$$= \frac{20 + 24 + j32 - j25}{200} = \frac{44 + 7j}{200}$$

$$\therefore Z_T = \frac{200}{44 + 7j}$$

$$V_A = - [2 \angle -45^\circ] \times Z_T = \frac{-\sqrt{2} + j\sqrt{2}}{44 + 7j} \cdot 200$$

$$\approx \left[\frac{2 \angle 135^\circ}{44 \angle 9^\circ} \right] 200$$

$$\left[\frac{1}{22} \angle 135 - 9 \right] 200$$

$$= 9.1 \angle 126^\circ$$

$$V_{A \text{ TOT}} = 28.1 \angle -99^\circ + 9.0 \angle 126^\circ$$

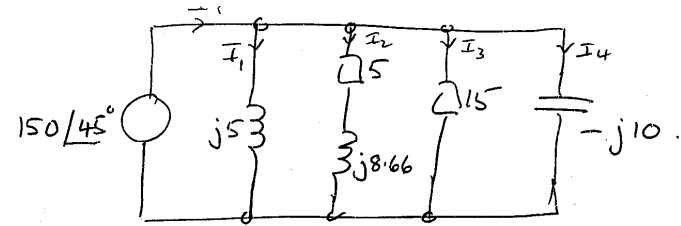
$$\downarrow \qquad \qquad \downarrow$$

$$-4.41 - 27.7j \quad -5.28 + j7.27$$

$$= -9.7 - 20.4j$$

$$= 22.6 \angle -115.4^\circ$$

Another circuit example.



Find total current I_T and cct impedance from source point of view.

method 1

$$\frac{1}{Z} = \frac{1}{j5} + \frac{1}{5 + j8.66} + \frac{1}{15} + \frac{1}{-j10}$$

$$= \frac{-j}{5} + \frac{5 - j8.66}{100} + \frac{1}{15} + \frac{j}{10}$$

$$= \frac{-30j + 5 - j8.66 + 10 + 15j}{150}$$

$$= \frac{-27.99j + 17.5}{150}$$

$$\therefore Z = \frac{150}{17.5 - 27.99j} = \frac{150(17.5 + 27.99j)}{1090}$$

$$= 0.138(17.5 + 27.99j)$$

$$= 0.138 \times 33 \angle 58^\circ$$

$$= 4.55 \angle 58^\circ$$

$$Z = \frac{V}{I_T} \quad I_T = I_1 + I_2 + I_3 + I_4$$

$$T = 150 \angle 45^\circ \quad T = 150 \angle 45^\circ$$

$$I_1 = \frac{150 \angle 45^\circ}{j5} \quad I_2 = \frac{150 \angle 45^\circ}{5 + j8.66}$$

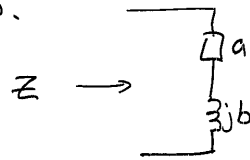
$$I_3 = \frac{150 \angle 45^\circ}{15} \quad I_4 = \frac{150 \angle 45^\circ}{-j10}$$

move the problem back by 45°

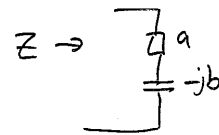
$$I_1 = \frac{150}{j5} \quad I_2 = \frac{150}{5 + j8.66} \quad I_3 = \frac{15}{15}$$

$$I_4 = \frac{150}{-j10}$$

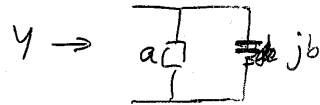
$$Z = a + jb$$



$$\text{if } Z = a - jb$$



$$Y = a + jb$$



$$Y = a - jb$$

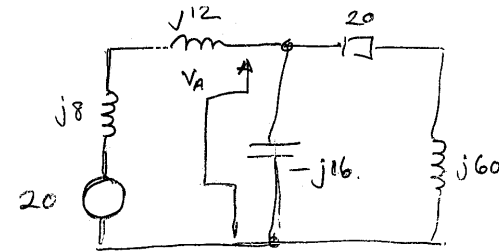


$$Z_L = j\omega L$$

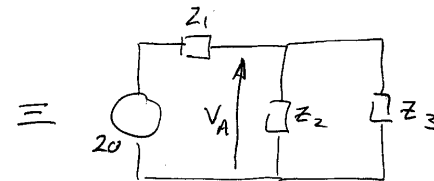
$$Y_L = \frac{1}{j\omega L} = -\frac{j}{\omega L}$$

112

22



find V_A .



$$Z_1 = j20 \cdot [j12 + j8]$$

$$Z_2 = -j16$$

$$Z_3 = 20 + j60$$

$$V_A = \frac{20 \cdot Z_2 \parallel Z_3}{Z_1 + Z_2 \parallel Z_3}$$

$$= 20 \times \frac{-j16(20 + j60)}{-j16 + 20 + j60}$$

$$\frac{j20 + \frac{-j16(20 + j60)}{-j16 + 20 + j60}}{-j16 + 20 + j60}$$

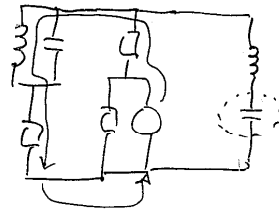
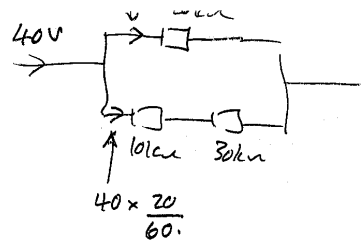
$$= 20 \times \frac{[-j320 - j^2 960]}{j20(-j16 + 20 + j60) - j320 - j^2 960}$$

$$= \frac{20 [-j320 - j^2 960]}{-j^2 320 + 400j + 1200j^2 - 320j - j^2 960}$$

$$j^2 = -1$$

$$\frac{40 \times 40}{60}$$

$$40V \rightarrow \downarrow 20k\Omega$$

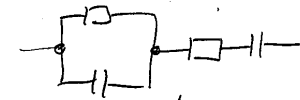


Resonance

Resonance is a property of circuits or systems that contain two or more independent reactances.

→ eg an L and a C
or two Cs separated by
resistors in such a way
that knowledge of

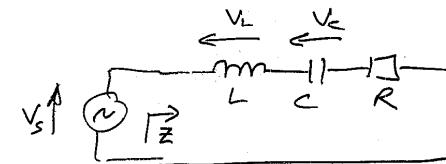
... gives no information about
voltage across the other
or knowledge of current
through one gives no info.
about current through other.



this circuit can be
resonant.

Definition of a resonant condition in
a reactive ckt is when Z is purely
real.

Classic resonant circuits



$$Z = j\omega L + \frac{1}{j\omega C} + R$$

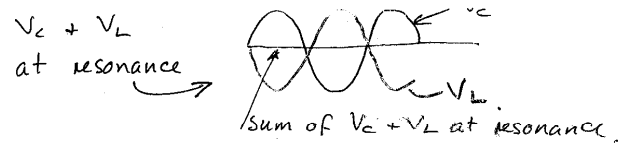
$$= j\left(\omega L - \frac{1}{\omega C}\right) + R$$

ckt resonant when j terms = 0

ie when $(\omega L - \frac{1}{\omega C}) = 0$

$$\text{or } \omega^2 = \frac{1}{LC} \text{ or } \omega = \frac{1}{\sqrt{LC}}$$

... .. V_C



$$Q = \frac{|V_L|}{|V_S|} = \frac{|V_C|}{|V_S|} \text{ at resonance.}$$

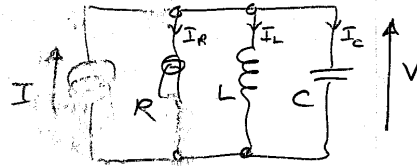
$$\frac{|V_L|}{|V_S|} = \frac{|V_C|}{|V_S|} = \frac{I_{wC}}{I_R} = \frac{1}{WCR}$$

in terms of L $\frac{WL}{R}$

put $W = \frac{1}{\sqrt{LC}}$

$$Q = \frac{1}{CR} = \frac{\sqrt{LC}}{CR} = \frac{1}{R} \sqrt{\frac{L}{C}}$$

Classical parallel resonant ckt



$$\frac{1}{Z} = \frac{1}{R} + \frac{1}{j\omega L} + j\omega C$$

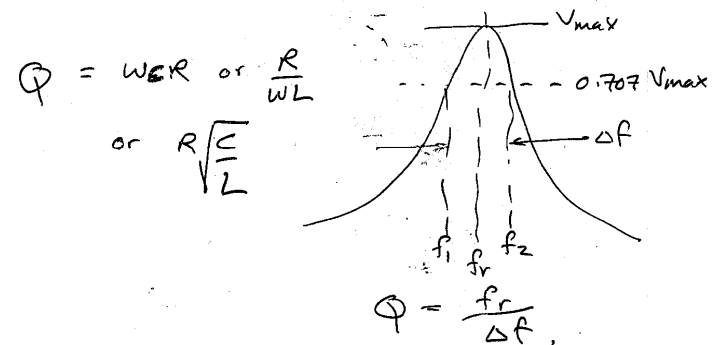
$$= \frac{j\omega L + R + j\omega C \cdot j\omega L \cdot R}{R j\omega L}$$

$$\begin{aligned} Z &= \frac{R j\omega L}{R + j\omega L - \omega^2 LC R} \\ &= \frac{j\omega L}{1 + j\omega \frac{L}{R} - \omega^2 LC} \times \frac{j}{j} \\ &= \frac{-\omega L}{j(1 - \omega^2 LC) - \omega \frac{L}{R}} \\ &= \frac{\omega L}{\omega^2 \frac{L}{R} - j(1 - \omega^2 LC)} \end{aligned}$$

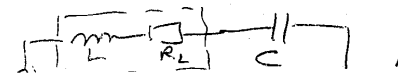
to make Z purely real, equate coefficient of j to zero.

$$1 - \omega^2 LC = 0$$

$$\omega = \frac{1}{\sqrt{LC}}$$



Non ideal behaviour



Non ideal behavior

