## **EEE123 Problem Sheet Solutions**

## **Rectifiers and Smoothing**

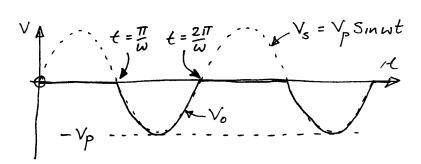
QI (1) The at.

1s a

half wave

Mectifier with a

negative output.



- (11) Vs is always given as an r.m.s. quantity. Vopk = -Vr.m.s.  $\sqrt{2} = -9\sqrt{2} = -12.73 \text{ V}$ . [note that this assumes that the 0.7V diode drop] Is negligible.
- (111) Voave = Vopk (for a half wave rectified sinusoid) = - 4.05 V

If you don't know that  $V_{onve} = \frac{V_{opk}}{II}$  for a half wave nectified sinusoid, you should know how to work it out. You need to work out the area under the waveform and divide it by the periodic time....  $V_{AVE} = \frac{1}{I} \int_{II}^{V} S_{II} wt dt = \frac{1}{(2III)_{W}} \int_{II}^{2III_{W}} V_{p} S_{mwt} dt$   $= \frac{W}{2II} \left[ -\frac{V_{p}}{V} Coswt \right]_{III_{W}}^{2III_{W}} = -\frac{V_{p}}{2II} \left[ 1 - (-1) \right] = -\frac{V_{p}}{II}$ note that the result is negative because the area under the curve for the chosen limits is negative. If the integration limit had been  $II_{W}$  to  $O_{V}$  the answer would have been  $+ V_{p}/I_{II}$ .

(IV) The r.m.s (root mean square) value of a sinusoid is  $VP/\sqrt{2}$  so the mean squared value is  $VP^2/2$ . A half wave signal will have half the mean squared value of a full sinusoid so the half wave mean squared (ms) value is  $VP^2/4$ .

The r.m.s. value of the wantform of part (1) is therefore VP/2 = 6.36V

If you cannot follow the argument above, you can evaluate:

evaluate: 
$$V_p^2 S_m^2 wt dt$$

The trigument doord, god evaluate:

 $V_p^2 S_m^2 wt dt$ 

The to get the same answer.

- (v) If you know the r.m.s voltage across a resistor, working out power chssipation in the resistor is straightforward....  $P_{D} = \frac{V_{rms}^{2}}{R} = \frac{6.36}{100} = \frac{405 \text{ mW.}}{100} = \frac{1000 \text{ mW.}}{100}$
- (VI) If the transformer has an effective series resistance of lon, the voltage across R can be found by potential division of the ideal transformer output voltage ...

(VII) The new power dissipated in R is  $\frac{\sqrt{rms(new)}}{p} = \left(\frac{11.75}{2}\right)^2 \cdot \frac{1}{100} = 335 \text{ mW}.$ 

You could also have taken the view here that the idea Vrms of part (10) - 6.36V - 18 acting on R + The los internal resistance so the power dissipated in this total resistance is

\[ \frac{6.36^2}{1100} = 367.7 \text{ mW}. \]

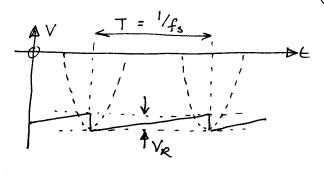
Ten elevenths of this power is being dissipated in R giving Po = 335 \text{ mW}.

## 92

assume:

- (a) IL & constant
- (b) capacitor charges instantaneously at each we half cycle peak.

(c) 0.7V is negligible.



Ripple behaviour governed by  $I_L = C \frac{dV_0}{dt}$  and since  $I_L = const$ ,  $\frac{dV_0}{dt}$  is the slope of the straight line,  $V_{R/T}$ 

$$I_L = \frac{\sqrt{pk}}{R} = C \frac{\sqrt{R}}{T} = C \frac{\sqrt{R}}{\sqrt{f_s}} = C \sqrt{R} f_s$$

or  $C = \frac{\sqrt{pk}}{R \sqrt{R} f_s} \approx \frac{8500 nF}{R \sqrt{R} f_s} (8.5 mF)$ 

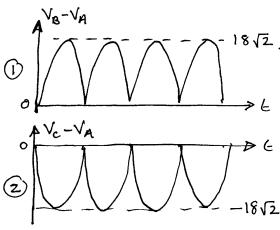
The power new dissipated in R is  $\frac{V_{DL}^2}{R}$   $V_{DL} = V_p - \frac{V_{R/2}}{2} \rightarrow ie$ , the average value of  $V_0$ . = 12.73 - 0.15 Thus  $P_D = 1.58 \, \text{W}$ .

You might legitimately argue that if the 0.7V chode drop can be neglected, then so can VR/2 at a mere \$6.0.15V. Such an argument is fine (in this case) and would give a Pb = 1.62W. If the ripple voltage was 3V, though, ignoring it would be on the border of unreasonable.

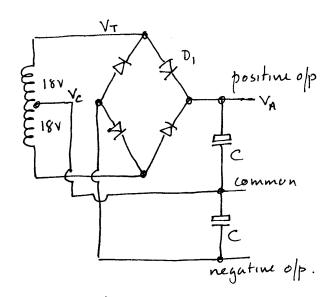
Q3 The outputs are as shown

(b) 
$$(V_A-V_c)_{ph} = -(-18\sqrt{2})$$
  
=  $18\sqrt{2}$ .

(c) 
$$(V_c - V_B)_{plc} = -18\sqrt{2} - 18\sqrt{2}$$
  
= -36\sqrt{2}



Q4 (1)



(11) using the same approximations as in 62 but recognising that IL is given explicitly and the circuit is full wave (ie the charging interval is 1/2fs)

$$I_{L} = C \frac{dV_{0}}{dt} = \frac{CV_{R}}{\frac{1}{2}f_{s}} = 2f_{s}CV_{R}.$$

This gives 
$$C = \frac{IL}{2f_s V_R} = \frac{2}{2.50.1} = \frac{20 \text{ mF}}{}$$

Since the tre + - we outputs have the same load conditions, this value of C applies to both.

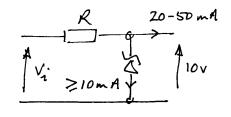
(iii) A variety of answers are acceptable here depending on assumptions made ... These must be stated if used. The answer given is based on

Vode =  $\sqrt{pk} - 0.7 - \sqrt{k/2} = 24.3.V$ If you choose to neglect the 0.7V or the  $\sqrt{k/2}$ or both — all reasonable approximations in this case, you would get marginally higher answers.

(IV) Consider D<sub>1</sub>. When V<sub>T</sub> is at its +ve peak w.r.t.  $V_c$ , D<sub>1</sub> conducts and C is charged to almost  $18\sqrt{2}$  V. V<sub>T</sub> Then falls until at the peak of the next half cycle it =  $-18\sqrt{2}$ . But V<sub>A</sub> is still  $\approx +18\sqrt{2}$  so the peak reverse voltage across D<sub>1</sub> is  $2 \times 18\sqrt{2} \approx 51$ V.

Q5. (1) 10 V (should be obvious!)

(11) A range of answers is possible here depending on the assumptions made in determining the output voltage from Q4.



The answer given here uses the instantaneous minimum value of Vo taking drade drop and ripple into account...

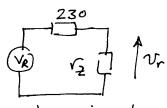
 $R_{\text{max}} = \frac{V_{\text{imin}} - V_0}{I_{\text{Lmax}} + I_{\text{Zmin}}} = \frac{(18\sqrt{2} - 0.7 - 1) - 10}{50\text{mA} + 10\text{mA}}$ = 230 s

If you neglected the 0.7 and VR, R = 258.
Ignoring one or the other gives an answer between 230 n + 258 n

- (111) If the load is disconnectied, all 60mt will flow through the Zener chode:
  PD = 10v × 60mA = 600 mW
- (IV) This answer will be shightly dependent on your assumptions about Vi and your value of R. The answer given assumes an average of Vi of 25V (ie the 0.7V drop is ignored)  $P_{D} = \frac{25 \times 25}{230} = 2.72 \text{ W}$
- (v) Under normal conditions

PD(zener) = 10v × 40mA = 400mW. (note that the minimum IL condition represents the worst case normal operation for the Zener). PD nes. = 15<sup>2</sup>/230 = 980mW. (this value depends on R and Vi assumptions)

(vi)  $V_r = V_R \frac{C_2}{230 + C_2}$   $V_r = 10 \text{ mV}$   $V_R = 1 \text{ V}$  yr = 1 W yr = 1 Wyr = 1 W



ripple egniv cct.