



The
University
Of
Sheffield.

DEPARTMENT OF ELECTRONIC AND ELECTRICAL ENGINEERING

Spring Semester 2015-16 (2.0 hours)

EEE305 Machine Design

Answer **THREE** questions. **No marks will be awarded for solutions to a fourth question.** Solutions will be considered in the order that they are presented in the answer book. Trial answers will be ignored if they are clearly crossed out. **The numbers given after each section of a question indicate the relative weighting of that section.**

1. The major dimensions and parameters of a radial field, 12-slot, 10-pole surface mounted permanent magnet machine shown in Figure 1 are listed in TABLE 1. By specifying appropriate approximations, answer the following questions.
 - a. Assuming the permanent magnets are full arc (180°) and $\mu_r = 1$, calculate the magnetic loading B and list possible ways to increase the magnetic loading B . (6)
 - b. If the allowable peak no-load lamination flux density is 2 T, choose a suitable stator tooth width (t_w) and comment on the result. (4)
 - c. For the same peak no-load lamination flux density stated in Q1.b, choose a suitable stator yoke thickness (d_c) and comment on the result. (4)
 - d. Calculate the electric loading Q if the total Ampere-Turns for the 3-phase windings are $NI = 1000A$. List the limiting factors for increase in electrical loading Q . (4)
 - e. Calculate the electromagnetic torque using the previously obtained electrical loading Q and magnetic loading B . (2)

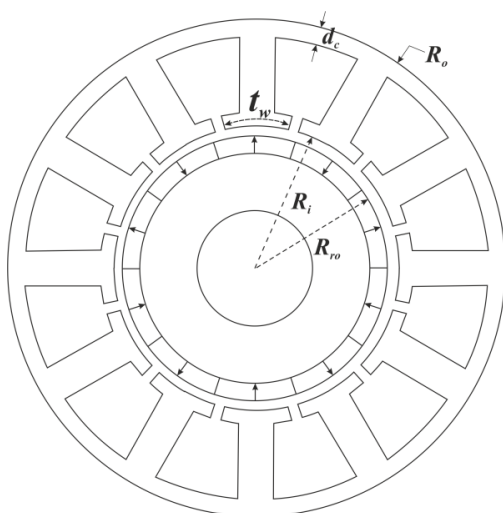


Figure 1

TABLE 1

Slot number (N_s)	12
Pole number ($2p$)	10
Stator outer radius (R_o)	50 mm
Stator inner radius (R_i)	28.5 mm
Active axial length (L_a)	50 mm
Air-gap length (L_g)	1 mm
Rotor outer radius (R_{ro})	27.5 mm
Magnet thickness (L_m)	3 mm
Magnet remanence (Br)	1.2 T

2. A 4-pole surface mounted permanent magnet machine has 15 stator slots (N_s) and the following dimensions:

Rotor outside diameter (D) = 30 mm

Rotor active length (L) = 80 mm

Stator slot area (A_s) = 30 mm²/slot

Magnet pole arc (α) = 140° (elec.)

Effective airgap (l_g) = 1.0 mm

Magnet recoil permeability (μ_r) = 1.1

The magnet material has the B-H characteristic shown in Figure 2.

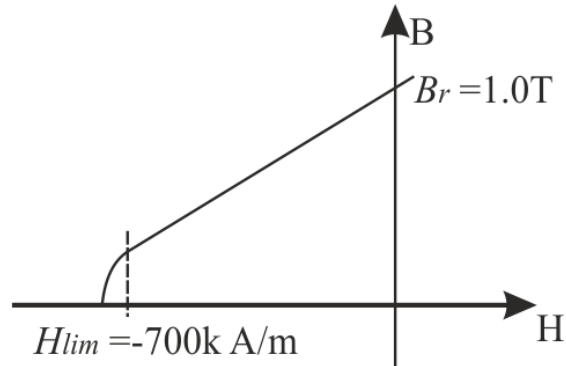


Figure 2

- a. If the winding has a current density of $J = 8 \text{ A/mm}^2$ and a packing factor of 0.5, calculate the magnet thickness required to obtain a power output of 600 W at 5000 rpm. (6)
- b. List possible ways to improve the open-circuit airgap flux density. (3)
- c. Check whether the magnet will be demagnetised at three times the full-load torque. (6)
- d. Sketch the difference between reversible and irreversible demagnetizations. (3)
- e. Explain the influence of temperature on the irreversible demagnetization for both Ferrite and NdFeB permanent magnets. (2)

3. a. Derive general expressions for the winding pitch-factor, K_p , and the distribution-factor, K_d , for both fundamental and n-th EMF harmonic components. (6)
- b. By employing coil vectors, determine the coil connections that yield a maximum winding factor for a 3-phase, 12-slot, 14-pole permanent magnet machine with double layer, concentrated windings. (4)
- c. Repeat Q3.b for a 3-phase, 12-slot, 14-pole permanent magnet machine with single layer, concentrated windings. (3)
- d. Explain the main advantages and disadvantages of a single layer winding. (4)
- e. Describe the main differences between concentrated winding and distributed winding and explain their merits and disadvantages. (3)

4. a. Derive an expression for the slot leakage inductance per-unit length, for a slot shown in Figure 3 (a) with N number of turns, specifying any assumptions which need to be made. Please note full marks will not be given if appropriate assumptions are not specified.

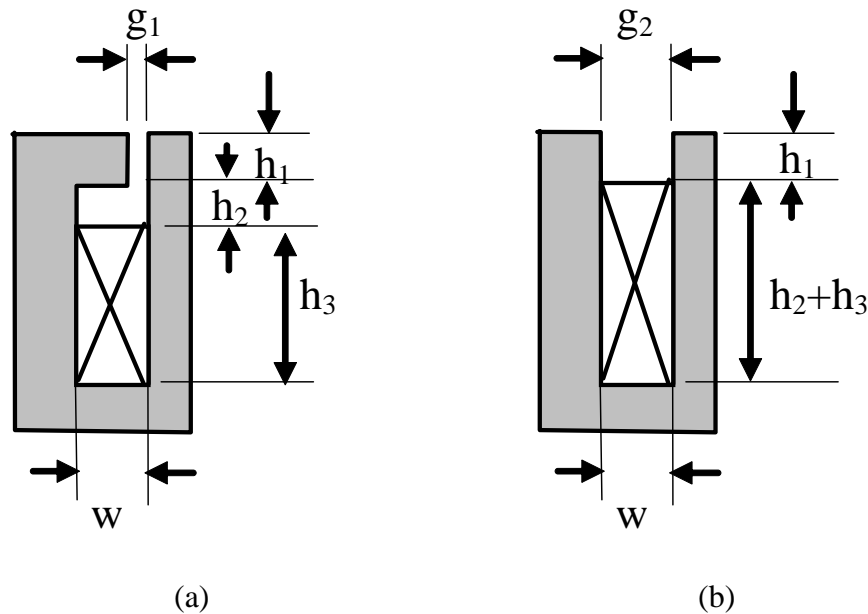


Figure 3

- b. For large wind power generators and hydroelectric generators, it is often preferred to employ open slots, as shown in Figure 3(b). Calculate the difference in winding slot-leakage inductances between Figures 3(a) and 3(b). (6)
- c. State the advantages and disadvantages of the slot configurations shown in Figures 3(a) and 3(b). (4)
- d. List possible ways to increase winding inductances and state their limitations. (6)

GJL/JBW