

# EEE118: Electronic Devices and Circuits

## Lecture XI

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## Review

- Introduced the bipolar transistor.
- Briefly discussed two numbering systems for active devices.
- Considered the four modes of operation of a BJT.
- Looked at examples of the input, output and transfer characteristics of a BJT.
- Developed a large signal model for a BJT which can be used to solve switching problems.
- Noted some of the limitations of the model in the saturation
  - $h_{FE}$  dependent on  $I_C$
  - $V_{BE(sat)}$  dependent on  $I_C$
  - $V_{CE(sat)}$  dependent on  $I_C$
- Developed a large signal model of a MOSFET.
- Briefly observed some differences between MOSFET and BJT characteristics.

# Outline

- 1 Review
- 2 Switches
- 3 Switch Types
  - Mechanical Switches
  - Electro-Mechanical Switches
  - Electronic Switches
- 4 MOSFET and BJT Switches
  - Output Characteristics
- 5 Power Dissipation
- 6 MOSFET Switches
- 7 BJT Switches
- 8 Bear

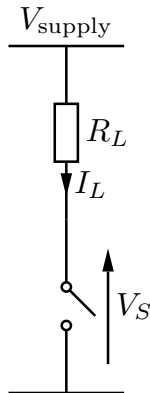
# An Ideal Switch

When “on”  $I_L = \frac{V_{supply}}{R_L}$

When “off”  $I_L = 0$

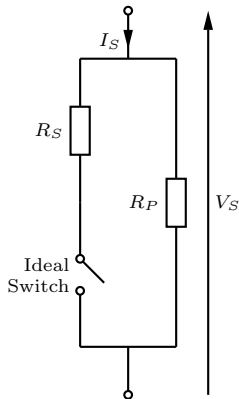
When “on”  $V_S = 0$

When “off”  $V_S = V_{supply}$



The product of  $V_S$  and  $I_L$  is zero in both switch states so no power is dissipated in the switch.  $I_L$  - the on state current - is determined by the external circuit not the switch.

## A Real Switch

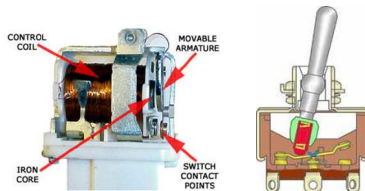


Real switches have some series resistance and some leakage current in the “off state”. In most cases,  $R_P$ , which represents the “off” state leakage can be neglected.  $R_S$  usually has to be considered because it is responsible for the power loss ( $I^2 R$ ) in the switch. For a real switch,

$$I_S = \frac{V_{supply}}{R_L + R_S} \quad (1)$$

## Mechanical Switches

- Mechanical force brings together two metal contacts.
- Easily designed for currents in the range  $10^{-3}$  to  $10^7$  A
- Very low contact resistance ( $R_S$ )
- Very low leakage (high  $R_P$ )
- Requires the application of mechanical force for to operate. Elasticity and inertia limits the switching rate to a few hundred Hz.
- The need for mechanical force requires some kind of linkage between the switch and the operator.



## Electro-Mechanical Switches

- Similar to mechanical switches except that the mechanical force is provided by an electro-magnet.
- Electro-magnet drive scheme offers possibility of remote operation.
- Advantages of mechanical contacts are maintained i.e. low loss.
- Most small toggle switches are rated for  $\sim 10^5$  mechanical operations and  $10^6$  electrical operations but it depends on the application. A particular kilovac<sup>1</sup> carrying 500 A at 600 V has a *rated* lifetime is about 25 switching cycles. Switching no current it is rated for  $10^6$  cycles.

Note that in both these switch types the switch contacts are usually insulated from the control linkages or electromagnet.

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<sup>1</sup>P/N: EV200AAANA see <http://relays.te.com/> or Farnell: 9913971

## Electronic Switches

- Many different types (BJT, MOSFET, JFET, Valve, Triac, Thyristor, “Solid State Relay (SSR)” ...)
- Interested here in MOSFET and BJT.
- Electronic switches can change state very quickly c.f mechanical switches  $> 10^9$  operations *per second* in a modern PC.
- Most mechanical switches would not last 1/1000th of this number of operations!
- Losses in electrical switches considerably greater than mechanical switches.
- The control input is electrically connected to one of the main current path terminals. (Emitter or Source) is common to input network and to output network).
- Most electronic switches support current flow in one direction only (not SSR, it is a compound device).

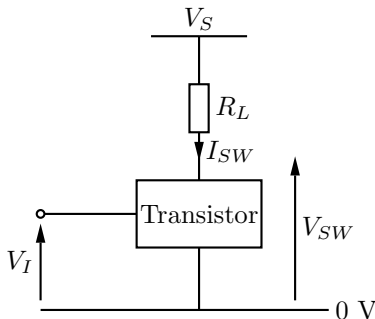


## MOSFET and BJT Switches

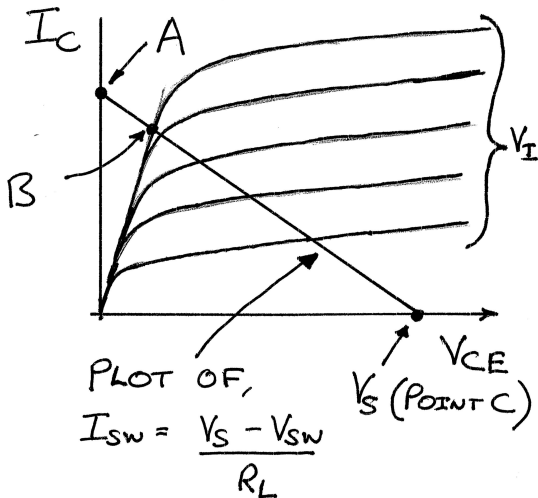
The connection of the control input to the controlled output and the single direction of current flow is inconvenient, however the advantages of electrical switches are so great that designers have developed a number of ways around these problems.

The device is placed into the circuit (right). In which  $V_S$  is the supply voltage,  $V_I$  is the control voltage and  $V_{SW}$  is the voltage across the switch.  $V_{SW}$  and  $I_{SW}$  are related by

$$I_{SW} = \frac{V_S - V_{SW}}{R_L} \quad (2)$$



There is also a second relationship between  $V_{SW}$  and  $I_{SW}$  defined by the output characteristics of the transistor.



# Notes on the Output Characteristic

- The switch is controlled by  $V_I$  (which is equal to  $V_{BE}$  in this example).
- Point C is the “off state” point.
- Point B is the real “on state” point.
- Point A is the ideal on state point.
- As  $V_I$  is increased,  $I_C$  will increase and  $V_{CE}$  will decrease until point B is reached.
- The dots on the diagram can be thought of as several different operating points but they are not quiescent conditions as the changes are large compared to the non-linearity of the transistor characteristics.

## Notes on the Output Characteristic II

- The operating point moves across a non-linear portion of the characteristics (it's a large signal problem)
- The locus - the path - of the operating point across the output characteristics is called the "load line". It is defined by the load resistance and the supply voltage ( $V_S$ ).
- The load line is straight - no surprise - it represents a resistance as a function of  $V$  and  $I$ ... Ohm's law.
- In the region between B and C there is a significant  $V / I$  product.
- The designer must keep the transistor at point B or point C and move between them as fast as possible.

## Power Dissipation

- The ZTX653 (from Lecture 10) can dissipate 1 W.
- And can carry 2 A...
- At up to 100 V ( $V_{CE}$ ).
- So it can control 200 W in the load.
- The instantaneous power in the transistor mid-way between B and C would be 50 W.
- Which is sufficient to blow the transistor to pieces.

The designer must ensure the transistor switches quickly to keep the average energy in any switching cycle below the permissible limit. More on this in “EEE340: Analogue and Switching Circuits” now called “EEE223: Energy Management and Conversion”.

## MOSFET Switches

- From Lecture 10 the MOSFET behaves like a resistance when “on” (linear region) i.e. at point B.
- Manufacturers specify  $R_{DS(on)}$ .
- $I_D$  is given by,

$$I_D = \frac{V_S}{R_L + R_{DS(on)}} \quad (3)$$

when in the “on” state

- $I_D = 0$  in the “off” state.
- The effect of  $R_{DS(on)}$  on load power is small (1 – 2% drop).
- The effect on the transistor is

$$P = I_{D(on)}^2 R_{DS(on)} \quad (4)$$

which may be significant.

## MOSFET Switches II

- To ensure the MOSFET is fully “on” the datasheet should be consulted or output characteristics obtained by experiment. A  $V_{GS}$  of 7 – 10V will probably be sufficient to switch the transistor under most circumstances.
- Since the gate is insulated from the source and drain, no current is required to maintain the gate drive voltage (MOSFETs have no equivalent of  $I_B$ ).
- Note that the gate has capacitance associated with it and this capacitance complicates transient drive conditions. More in “EEE340: Analogue and Switching Circuits” now called “EEE223: Energy Management and Conversion”.

## BJT Switches

- When a BJT is fully “on” (i.e. at Point B) the voltage across it is  $V_{CE(sat)}$  - the saturated on state voltage drop.
- $V_{CE(sat)}$  is approximately constant for a constant value of  $h_{FE}$
- The value of  $h_{FE}$  depends on the particular transistor.

$$I_{C(on)} = \frac{V_S - V_{CE(sat)}}{R_L} \quad (5)$$

- $I_{C(off)} = 0$  because the leakage is small.
- To be sure the BJT is fully on, the designer must ensure there is sufficient base current available.
- The base current is determined by

$$I_B = \frac{I_C}{h_{FE}} \quad (6)$$



## BJT Switch Design Process

First estimate  $I_C$ ,

$$I_C \approx \frac{V_S}{R_L} \text{ if } V_S \gg V_{CE(sat)} \quad (7)$$

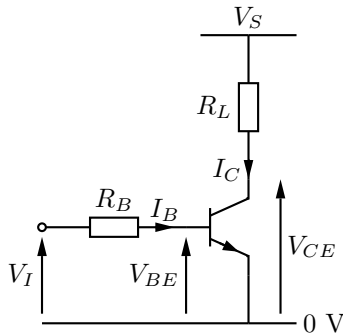
then calculate the required base current,

$$\therefore \min I_B = \frac{I_C}{h_{FE}} = \frac{V_S}{h_{FE} R_L} \quad (8)$$

$I_B$  is controlled by

$$I_B = \frac{V_I - V_{BE}}{R_B} \quad (9)$$

Where  $V_I$  is the input voltage and  $V_{BE}$  is the voltage associated with the forward biased base emitter junction (0.7 V). Usually it is necessary to make  $I_B$  several times the minimum value to make the transistor switch properly under all circumstances.



## Review

- Discussed an ideal switch
- Considered the non-idealities of a switch
- Looked at three classes of 'switch'
- Considered how the switching action of a transistor is represented on the output characteristics.
- Introduced the idea of a 'load line'
- Considered power dissipation in the "on" state
- Provided design equations for MOS and BJT switches

Next time: Design (problem sheet style) example for transistor switch, methods for using electronic switches with AC and switching inductive loads.

