

# Solutions to Tutorial Sheet 2

1.

$\vec{J} = \nabla \times \vec{H}$  and in Cartesian co-ordinates

$$\nabla \times \vec{H} = \begin{vmatrix} \mathbf{e}_x & \mathbf{e}_y & \mathbf{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ H_x & H_y & H_z \end{vmatrix} = \begin{vmatrix} \mathbf{e}_x & \mathbf{e}_y & \mathbf{e}_z \\ 3 & 7y & 2x \end{vmatrix} = -2 \mathbf{e}_y$$

## 2. Solution 1

From Application of Ampere's law to the path shown below:

$$I = \oint \vec{H} \cdot d\vec{l} = \int H_1 dl_1 + \int H_2 dl_2 + \int H_3 dl_3 + \int H_4 dl_4$$

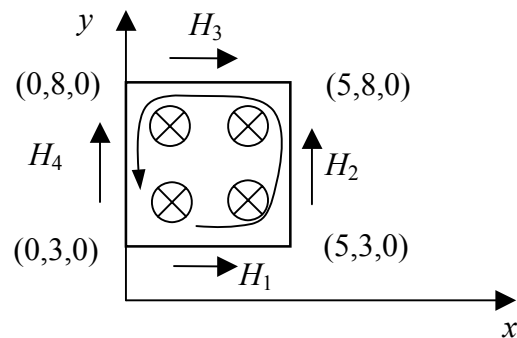
But  $\vec{H}$  has only  $x$  components, thus

$$H_2 = H_4 = 0;$$

$$H_1(x, y=3) = 81 \mathbf{e}_x$$

$$H_3(x, y=8) = 1536 \mathbf{e}_x$$

$$\begin{aligned} I &= \oint \vec{H} \cdot d\vec{l} = \int H_1 dl_1 + \int H_3 dl_3 \\ &= 81 \times 5 - 1536 \times 5 = -7275 \text{ (A)} \end{aligned}$$



The negative sign indicates that the current flows in the opposite direction of the  $z$  axis

## Solution 2

Using

$$\vec{J} = \nabla \times \vec{H} = \begin{vmatrix} \mathbf{e}_x & \mathbf{e}_y & \mathbf{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ H_x & H_y & H_z \end{vmatrix} = \begin{vmatrix} \mathbf{e}_x & \mathbf{e}_y & \mathbf{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ 3y^3 & 0 & 0 \end{vmatrix} = -9y^2 \mathbf{e}_x$$

The total current is the integration of the current density over the square region:

$$I = \iint_S \vec{J} \cdot d\vec{s} = \int_0^5 dx \int_3^8 -9y^2 dy = -5(3y^3) \Big|_3^8 = -7275 \text{ (A)}$$

3. From the definition

$$\begin{aligned} \vec{B} = \nabla \times \vec{A} &= \begin{vmatrix} \mathbf{e}_x & \mathbf{e}_y & \mathbf{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ A_x & A_y & A_z \end{vmatrix} = \begin{vmatrix} \mathbf{e}_x & \mathbf{e}_y & \mathbf{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ xyz & 4xy & 7 \end{vmatrix} = xy \mathbf{e}_y + (4y - xz) \mathbf{e}_z \\ &= 6 \mathbf{e}_y - 14 \mathbf{e}_z \end{aligned}$$

4. Again using

$$\vec{J} = \nabla \times \vec{H} = \begin{vmatrix} \vec{e}_x & \vec{e}_y & \vec{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ H_x & H_y & H_z \end{vmatrix} = \begin{vmatrix} \vec{e}_x & \vec{e}_y & \vec{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ 7y & 7x & 7xy \end{vmatrix} = 7x \vec{e}_x - 7y \vec{e}_y$$

Thus, at (2, 1, 0)  $\vec{J} = 14 \vec{e}_x - 7 \vec{e}_y$

And at (0, 0, 0)  $\vec{J} = \vec{0}$

5.

$$\begin{aligned} \nabla \cdot (\nabla \times \vec{F}) &= \frac{\partial}{\partial x} \left[ \frac{\partial F_z}{\partial y} - \frac{\partial F_y}{\partial z} \right] + \frac{\partial}{\partial y} \left[ \frac{\partial F_x}{\partial z} - \frac{\partial F_z}{\partial x} \right] + \frac{\partial}{\partial z} \left[ \frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right] \\ &= \frac{\partial^2 F_z}{\partial x \partial y} - \frac{\partial^2 F_y}{\partial x \partial z} + \frac{\partial^2 F_x}{\partial y \partial z} - \frac{\partial^2 F_z}{\partial y \partial x} + \frac{\partial^2 F_y}{\partial z \partial x} - \frac{\partial^2 F_x}{\partial z \partial y} = 0 \end{aligned}$$

6.

$$\begin{aligned} \nabla \times (\nabla \varphi) &= \nabla \times \left\{ \frac{\partial \varphi}{\partial x} \vec{e}_x + \frac{\partial \varphi}{\partial y} \vec{e}_y + \frac{\partial \varphi}{\partial z} \vec{e}_z \right\} = \begin{vmatrix} \vec{e}_x & \vec{e}_y & \vec{e}_z \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ \frac{\partial \varphi}{\partial x} & \frac{\partial \varphi}{\partial y} & \frac{\partial \varphi}{\partial z} \end{vmatrix} \\ &= \left( \frac{\partial^2 \varphi}{\partial y \partial z} - \frac{\partial^2 \varphi}{\partial z \partial y} \right) \vec{e}_x + \left( \frac{\partial^2 \varphi}{\partial z \partial x} - \frac{\partial^2 \varphi}{\partial x \partial z} \right) \vec{e}_y + \left( \frac{\partial^2 \varphi}{\partial x \partial y} - \frac{\partial^2 \varphi}{\partial y \partial x} \right) \vec{e}_z = 0 \end{aligned}$$

7.

$$H_{x2} - H_{x1} = J = (0.32 - 21.6) \cos(2\pi x / 6.3) = -21.28 \cos(2\pi x / 6.3)$$

$$\text{At } x = 3 \quad J = -21.25$$

Since flux density  $B$  is usually limited to a few Tesla in any materials whilst the permeability of iron could be a few thousand times greater than that in air, from  $H = B/\mu$ , the larger the permeability, the smaller the magnetic field intensity. Thus, it is likely that region 2 with lower  $H_{x2}$  contains iron.

8. This is virtually the same problem as *Example 1* in section 3.6. However, the magnetic field solutions needs to be considered in both regions ( $y \geq 0$  and  $y < 0$ ) and in finding the solutions, scalar magnetic potential  $\varphi$  will be used.

$$\vec{H} = -\nabla \varphi$$

and it satisfies the Laplace's equation:

$$\nabla^2 \varphi = 0$$

Also due to the symmetry,  $\phi$  will be independent of  $z$ , thus

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = 0$$

$$H_x = -\frac{\partial \phi}{\partial x} \quad ; \quad H_y = -\frac{\partial \phi}{\partial y}$$

Assume solution takes the form:

$$\phi(x, y) = F(x) \bullet G(y)$$

Where  $F$  is a function of  $x$  only, and  $G$  is a function of  $y$  only. Thus:

$$G \frac{d^2 F}{dx^2} + F \frac{d^2 G}{dy^2} = 0$$

Dividing both sides by  $\{-F(x)G(y)\}$  gives:

$$-\frac{1}{F} \frac{d^2 F}{dx^2} = \frac{1}{G} \frac{d^2 G}{dy^2} = k^2$$

The standard solutions are:

$$F(x) = C_1 \sin(kx) + C_2 \cos(kx)$$

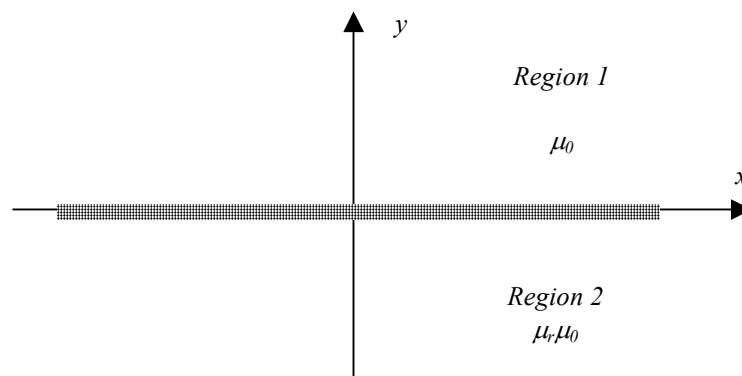
$$G(y) = C_3 e^{ky} + C_4 e^{-ky}$$

where  $C_1, C_2, C_3$  and  $C_4$  are constants to be determined. Hence:

$$\phi(x, y) = \{C_1 \sin(kx) + C_2 \cos(kx)\} \{C_3 e^{ky} + C_4 e^{-ky}\}$$

Since the excitation (field source) has the form of  $J_m \sin(px)$ , we would expect  $H$  (or  $-\frac{\partial \phi}{\partial x}$ ) variation with  $x$  of the same form as the excitation. Thus:

$$k = p \text{ and } C_1 = 0$$



The solution for regions 1 and 2 are given by:

Region 1,  $y \geq 0$ ,  $\phi_1(x,y)$  must be finite as  $y \rightarrow \infty$ . This implies  $C_3 = 0$ . Now  $\phi$  is further simplified to:

$$\phi_1(x,y) = K_1 (\cos px) e^{-py}$$

Region 2,  $y < 0$ ,  $\phi_2(x,y)$  must be finite as  $y \rightarrow -\infty$ . This implies  $C_4 = 0$ , and  $\phi$  is further simplified to:

$$\phi_2(x,y) = K_2 (\cos px) e^{py}$$

Use the boundary condition at  $y = 0$ :

$$B_{y1}|_{y=0} = B_{y2}|_{y=0}$$

$$H_{x2}|_{y=0} - H_{x1}|_{y=0} = J_m \sin(px)$$

$$H_{x1} = -\frac{\partial \phi_1}{\partial x} = K_1 p \sin(px) e^{-py}$$

$$H_{y1} = -\frac{\partial \phi_1}{\partial y} = K_1 p \cos(px) e^{-py}$$

$$H_{x2} = -\frac{\partial \phi_2}{\partial x} = K_2 p \sin(px) e^{py}$$

$$H_{y2} = -\frac{\partial \phi_2}{\partial y} = -K_2 p \cos(px) e^{py}$$

At  $y = 0$

$$B_{y1} = \mu_0 H_{y1} = \mu_0 K_1 p \cos(px) = B_{y2} = \mu_0 \mu_r H_{y2} = -\mu_0 \mu_r K_2 p \cos(px)$$

or

$$K_1 + \mu_r K_2 = 0$$

$$H_{x2} - H_{x1} = K_2 p \sin(px) - K_1 p \sin(px) = J_m \sin(px)$$

or

$$K_2 - K_1 = J_m / p$$

$$\therefore K_2 = \frac{J_m}{p(1 + \mu_r)} \quad ; \quad K_1 = -\frac{\mu_r J_m}{p(1 + \mu_r)}$$

and

$$\phi_1(x,y) = \frac{-\mu_r J_m}{p(1 + \mu_r)} \cos(px) e^{-py}$$

$$\phi_2(x,y) = \frac{J_m}{p(1 + \mu_r)} \cos(px) e^{py}$$

At any point (x, y) in regions 1 and 2, the x and y components of  $\mathbf{B}$  are given by:

$$\begin{aligned}
B_{x1} &= -\mu_0 \frac{\partial \varphi_1}{\partial x} = \frac{-\mu_0 \mu_r J_m}{(1 + \mu_r)} \sin(px) e^{-py} \\
B_{y1} &= -\mu_0 \frac{\partial \varphi_2}{\partial y} = \frac{-\mu_0 \mu_r J_m}{(1 + \mu_r)} \cos(px) e^{-py} \\
H_{x2} &= -\frac{\partial \varphi_2}{\partial x} = \frac{J_m}{(1 + \mu_r)} \sin(px) e^{py} \\
H_{y2} &= -\frac{\partial \varphi_2}{\partial y} = \frac{-J_m}{(1 + \mu_r)} \cos(px) e^{py} \\
B_{x2} &= \mu_0 \mu_r H_{x2} = \frac{\mu_0 \mu_r J_m}{(1 + \mu_r)} \sin(px) e^{py} \\
B_{y2} &= \mu_0 \mu_r H_{y2} = \frac{-\mu_0 \mu_r J_m}{(1 + \mu_r)} \cos(px) e^{py}
\end{aligned}$$

It should be noted that if the relative permeability  $\mu_r$  in region 2 is very large, which is often the case with ferromagnetic materials such as silicon steel,  $(\mu_r + 1) \gg 1$ ,  $H_{y2} \ll H_{y1}$ , and  $H_{y2}$  can be approximate to zero, which leads to the same result with the vector magnetic potential approach in the lecture note pp. 3-9 ~ 3-10.

9. This question is very similar to example 2 in section 3.6, except for the boundary conditions

(a) Boundary conditions at  $r = R_2$ :

$$H_{\theta 2} = J \cos \theta$$

Interface conditions at  $r = R_1$ :

$$H_{\theta 1} = H_{\theta 2} \quad ; \quad B_{r1} = B_{r2}$$

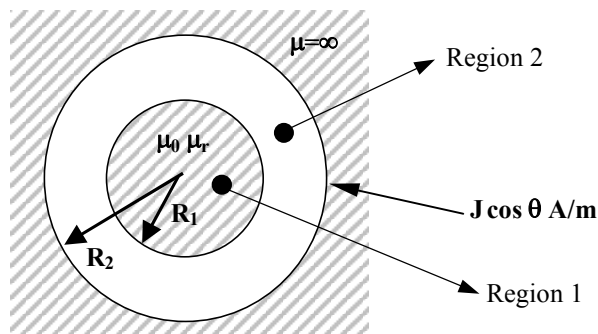
(b) Field Solution

Use the scalar magnetic potential, the general solution for Laplace's equation for both regions is

$$\varphi = (K_1 \sin k\theta + K_2 \cos k\theta) (K_3 r^k + K_4 r^{-k})$$

Since the source of field varies as  $J \cos \theta$ , and  $H_\theta = \frac{-1}{r} \frac{\partial \varphi}{\partial \theta}$

Set  $k = 1$  and  $K_2 = 0$ . The solutions for regions 1 and 2 are given:



In **region (1)**:  $r < R_1$

$$\varphi_1 = (C_1 r + C_2 r^{-1}) \sin \theta$$

In **region (2)**:  $r > R_1$

$$\varphi_2 = (C_3 r + C_4 r^{-1}) \sin \theta$$

To find the 4 unknown constants, 4 boundary/interface conditions are applied

### **Boundary Conditions**

(i) At  $r = 0$ ,  $\varphi_1 = 0$ ,  $\therefore C_2 = 0$   
 $\therefore \varphi_1 = C_1 r \sin \theta$

(ii) At  $r = R_2$ ,  
 $H_{\theta 2} = J \cos \theta$  **Note:**  $H_{\theta} = -\nabla \varphi|_{r=R_2} = -\frac{1}{r} \frac{\partial \varphi}{\partial \theta}$

$$\therefore -(C_3 + C_4 \frac{1}{R_2^2}) \cos \theta = J \cos \theta$$

$$\therefore -(C_3 + C_4 \frac{1}{R_2^2}) = J \quad (1)$$

(iii) At  $r = R_1$   $B_{r1} = B_{r2}$   $B_r = -\mu \frac{\partial \varphi}{\partial r}$

$$\therefore -\mu_0 \mu_r \frac{\partial \varphi_1}{\partial r} = -\mu_0 \frac{\partial \varphi_2}{\partial r}$$

$$\therefore -\mu_0 \mu_r C_1 \sin \theta = (-\mu_0 C_3 + \mu_0 C_4 R_1^{-2}) \sin \theta$$

$$\therefore -\mu_r C_1 = -C_3 + C_4 R_1^{-2} \quad (2)$$

(iv) At  $r = R_1$ ,  $H_{\theta 1} = H_{\theta 2}$   $H_{\theta} = \frac{-1}{r} \frac{\partial \varphi}{\partial \theta}$

$$\therefore \frac{C_1}{R_1} \cos \theta = C_3 \frac{R_1}{R_1} \cos \theta + \frac{C_4}{R_1^2} \cos \theta$$

$$\therefore C_1 = C_3 + \frac{C_4}{R_1^2} \quad (3)$$

Solving for  $C_1$ ,  $C_3$  and  $C_4$

$$C_1 = \frac{-2(1 + \mu_r)J}{(1 - \mu_r)R_1^2 \left[ \frac{1 + \mu_r}{R_1^2} + \frac{1 - \mu_r}{R_2^2} \right]}$$

$$C_3 = \frac{-(1 + \mu_r)J}{R_1^2 \left[ \frac{1 + \mu_r}{R_1^2} + \frac{1 - \mu_r}{R_2^2} \right]}$$

$$C_4 = \frac{-(1 - \mu_r)J}{\left[ \frac{1 + \mu_r}{R_1^2} + \frac{1 - \mu_r}{R_2^2} \right]}$$

Finally,

$$\varphi_2 = (C_3 r + C_4 r^{-1}) \sin \theta$$

$$\varphi_2 = \frac{-J}{\left[ \frac{1 + \mu_r}{R_1^2} + \frac{1 - \mu_r}{R_2^2} \right]} \left( \left[ \frac{(1 + \mu_r)r}{R_1^2} \right] + \left[ \frac{(1 - \mu_r)}{r} \right] \right) \sin \theta$$

**Note: A useful method to verify your solution is to check if it satisfies the boundary/interface conditions**