

Q1

Part a

Causality is a system where the output depends on present or previous inputs 1 mark

A system where the output ONLY depends on the present inputs is memoryless. 1 mark

. (0.5 marks for memory correct, 0.5 marks for causal correct)

i) No memory, causal

ii) Memory, non causal

iii) Memory, causal

Part b.

$$y(t) = t^3 * t * t$$

$$y(t) = (t^3 * t) * t$$

$$(t^3 * t) = \int_0^t \tau^3 (t - \tau) d\tau \quad \leftarrow \quad \boxed{1 \text{ mark}}$$

$$(t^3 * t) = t \int_0^t \tau^3 d\tau - \int_0^t \tau^4 d\tau$$

$$(t^3 * t) = \frac{t^5}{20} \quad \leftarrow \quad \boxed{1 \text{ mark}}$$

$$y(t) = \frac{t^5}{20} * t = \frac{1}{20} \int_0^t \tau^5 (t - \tau) d\tau = \frac{1}{20} \left[t \int_0^t \tau^5 d\tau - \int_0^t \tau^6 d\tau \right] \quad \leftarrow \quad \boxed{1 \text{ mark}}$$

$$y(t) = \frac{t^7}{840} \quad \leftarrow \quad \boxed{1 \text{ mark}}$$

Part c

$$a_0 = \frac{1}{T} \int_{-0.1T}^{0.9T} f(t) dt = \frac{1}{T} \left[\int_{-0.1T}^{0.1T} A dt - \int_{0.1T}^{0.9T} A dt \right] \quad 1 \text{ Mark}$$

$$a_0 = \frac{A}{T} [0.2T - 0.8T] = -0.6A$$

The function is even hence bn=0. 1 mark

$$a_n = 2 * \frac{2}{T} \int_0^{T/2} f(t) \cos(n\omega_0 t) dt$$

$$a_n = \frac{4A}{T} \left[\int_0^{0.1T} \cos(n\omega_0 t) dt - \int_{0.1T}^{0.5T} \cos(n\omega_0 t) dt \right]$$

2 marks

$$a_n = \frac{4A}{n\omega_0 T} [\sin(0.2n\pi) - (\sin(0.5n\pi) - \sin(0.2n\pi))]$$

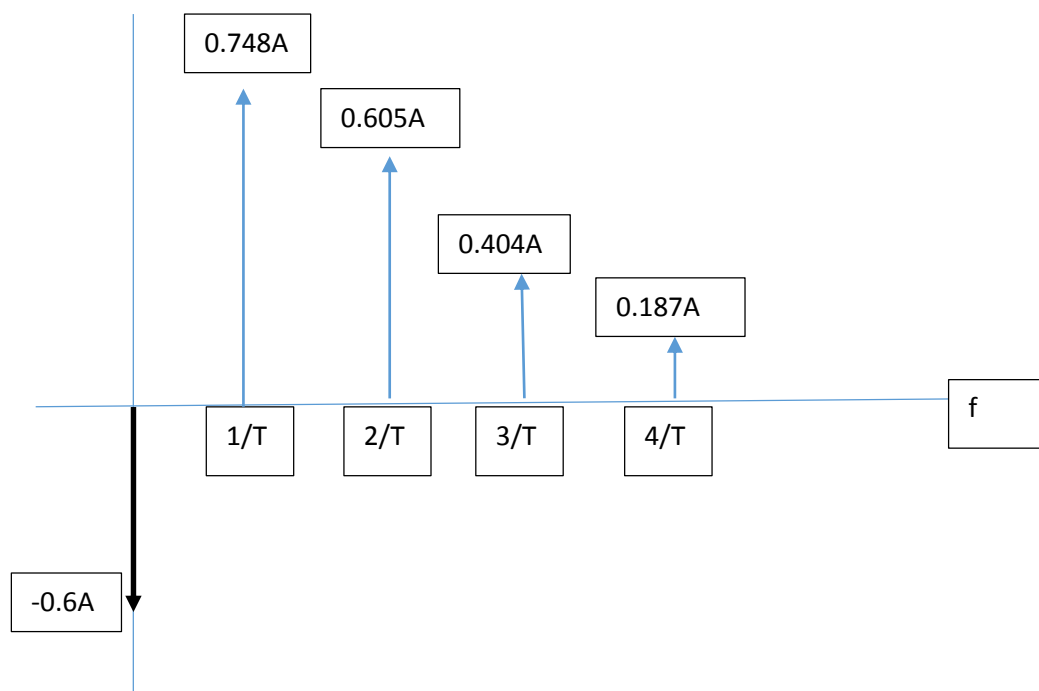
2 marks

$$a_n = \frac{4A}{n\pi} \sin(0.2n\pi)$$

Hence,

$$f(t) = -0.6A + \frac{4A}{\pi} \sum_{n=1}^{\infty} \frac{\sin(0.2n\pi)}{n} \cos(n\omega_0 t) \quad 1 \text{ mark}$$

0.5 marks for correct amplitudes, 0.5 marks for correct frequency of each component (no marks for DC component, just shown for completeness)



Q2

a **1 mark each**

Allows for multiplexing

Efficient antenna size

Improves S/N

Allows users to have different carrier frequencies

b

$$C = B \log_2(1 + S / N)$$

$$C = 20 \log_2(1 + 1000) \quad 3 \text{ marks}$$

$$C = 199 \text{ Mbit / s}$$

$$C = \frac{B}{2} \log_2(1 + S / 2N)$$

$$C = 40 \log_2(1 + 500) \quad 3 \text{ marks}$$

$$C = 359 \text{ Mbit / s}$$

c

i) sampling frequency = $2 \times 10 = 20 \text{ kHz}$ (1 mark)

ii) $8 = 2^N$, hence $N = 3$ (2 marks)

iii) Data rate = $3 \times 20 = 60 \text{ bit/s}$ (2 marks)

At $t=0$ the voltage is 5V. Quantisation level 6 : PCM = 101 (1 mark)

At $t=50$ the voltage is 4.3V. Quantisation level 5: PCM = 100 (1 mark)

At $t=100$ the voltage is 3V. Quantisation level 4: PCM = 011 (1 mark)

At $t=150$ the voltage is 2.6V. Quantisation level 4: PCM = 011 (1 mark)

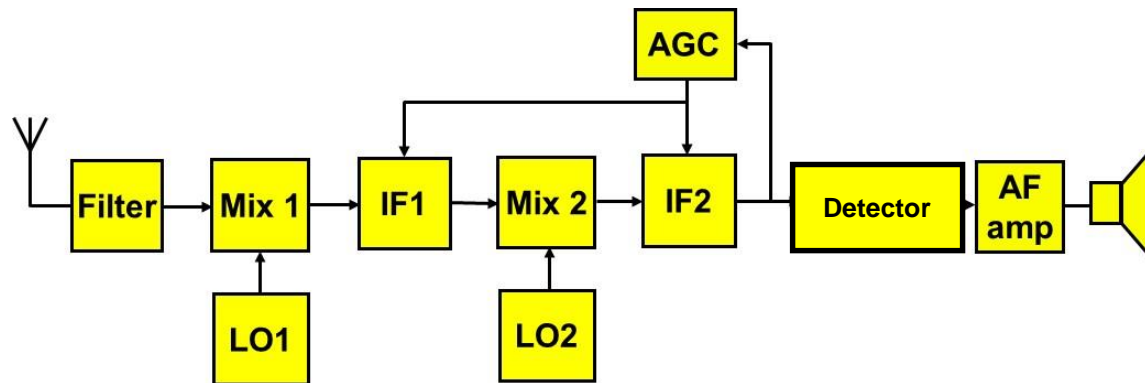
At $t=200$ the voltage is 1.8V. Quantisation level 3: PCM = 010 (1 mark)

Hence total PCM code is

101 100 011 011 010

Q3

a



1 mark is awarded for each of the elements below, 1 mark for correct diagram

- A bandpass filter reduces the effect of image frequencies
- Mixer down covers f_{RF} to the 1st IF
- IF amplifier to required levels
- 2nd mixer converts to final IF
- AGC adjusts the gain to keep the carrier levels constant
- Detector demodulates the signal to receive the baseband information

b

Firstly the parameters we need are below.

$$F_{RF} = 420\text{MHz}$$

$$F_{IF1} = 60\text{MHz}$$

$$F_{IF2} = 0.455\text{MHz}$$

$$F_{LO1} > F_{RF}$$

$$F_{LO2} < F_{IF1}$$

i) $F_{LO1} - 420 = 60$
 $F_{LO1} = 480\text{MHz}$ 1 mark

ii) $60 - F_{LO2} = 0.455$
 $F_{LO2} = 59.545\text{MHz}$ 1 mark

iii) $F_{image1} = 480 + 60 = 540\text{MHz}$ 1 mark

iv) $F_{image1} = 59.545 - 0.455 = 59.09MHz$ 1 mark

$$F_1 \rightarrow 480 - F_1 = 59.09$$

$$F_1 = 420.91$$

v) 2 marks

$$F_2 \rightarrow F_2 - 480 = 59.09$$

$$F_2 = 539.09MHz$$

Part C

i) $F_{RF} - 100 = 0.455$ 1 mark
 $F_{RF} = 100.455MHz$

$$100 - F_{image} = 0.455$$

$$F_{image} = 99.545MHz$$

ii) $IFRR = \sqrt{1 + Q^2 x^2}$ 3 marks

$$x = \frac{F_{image}}{F_{RF}} - \frac{F_{RF}}{F_{image}}$$

$$x = \frac{99.545}{100.455} - \frac{100.455}{99.545} = -0.0182$$

$$IFRR = 1.235 = 1.8dB$$

part D

Could improve by increasing IF or Q factor, practical issues would suggest IF is easier.

Question 4**a. (10 marks)**

$$\frac{v_o}{v_i} = \frac{\frac{\frac{R}{j\omega C_2}}{R + \frac{1}{j\omega C_2}}}{\frac{1}{j\omega C_1} + \frac{\frac{R}{j\omega C_2}}{R + \frac{1}{j\omega C_2}}}$$

(2 marks)

$$= \frac{\frac{R}{1+j\omega C_2 R}}{\frac{1}{j\omega C_1} + \frac{R}{1+j\omega C_2 R}} = \frac{j\omega C_1 R}{1+j\omega C_2 R + j\omega C_1 R}$$

(2 marks)

$$= \frac{j\omega C_1 R}{1+j\omega(C_1+C_2)R} = \frac{C_1}{C_1+C_2} \frac{j\omega(C_1+C_2)R}{1+j\omega(C_1+C_2)R} = k \frac{j\frac{\omega}{\omega_0}}{1+j\frac{\omega}{\omega_0}}$$

(2 marks)

where $\omega_0 = 1/R (C_1 + C_2)$ and $k = C_1/(C_1 + C_2)$.

(2 marks)

This is a high pass circuit.

(2 marks)

b. (10 marks)

$$\begin{aligned} \frac{v_o}{v_i} &= \frac{R_1 + \frac{R_2 \left(R_3 + \frac{1}{sC} \right)}{R_2 + R_3 + \frac{1}{sC}}}{R_1} \\ &= \frac{R_1 R_2 + R_1 R_3 + \frac{R_1}{sC} + R_2 R_3 + \frac{R_2}{sC}}{R_1 R_2 + R_1 R_3 + \frac{R_1}{sC}} \\ &= \frac{R_1 + R_2 + sC (R_1 R_2 + R_1 R_3 + R_2 R_3)}{R_1 (sC (R_2 + R_3) + 1)} \end{aligned}$$

(2 marks)

$$= \frac{R_1 + R_2}{R_1} \frac{1 + sC \left(\frac{R_1 R_2 + R_1 R_3 + R_2 R_3}{R_1 + R_2} \right)}{1 + sC (R_2 + R_3)}$$

(2 marks)

$$\equiv k_L \frac{1 + j \frac{\omega}{\omega_1}}{1 + j \frac{\omega}{\omega_0}}$$

$$\omega_0 = \text{pole frequency} = \frac{1}{C (R_2 + R_3)} = 2 \pi 10$$

$$\omega_1 = \text{zero frequency} = \frac{R_1 + R_2}{C (R_1 R_2 + R_1 R_3 + R_2 R_3)} = 2 \pi 500$$

$$k_H = \text{high frequency gain} = \frac{R_1 R_2 + R_1 R_3 + R_2 R_3}{R_1 (R_2 + R_3)} = 10$$

(3 marks)

Solving the above three equations, we obtain

$$R_2 = 4.99 \text{M}\Omega.$$

$$R_3 = 91.6 \text{k}\Omega$$

$$C = 3.13 \text{nF}$$

(3 marks)

Question 5**a. (8 marks)**

For a unit step input, the output is given by

$$Y(s) = H(s)U(s) = \frac{s/3}{(s+1)(s+2)} \frac{1}{s} = \frac{1/3}{(s+1)(s+2)} = \frac{k_1}{s+1} + \frac{k_2}{s+2} \quad (2 \text{ marks})$$

Using partial fraction expansion, we have

$$k_1 = \frac{1/3}{(s+1)(s+2)} (s+1) \Big|_{s=-1} = \frac{1/3}{s+2} \Big|_{s=-1} = \frac{1}{3}$$

$$k_2 = \frac{1/3}{(s+1)(s+2)} (s+2) \Big|_{s=-2} = \frac{1/3}{s+1} \Big|_{s=-2} = -\frac{1}{3} \quad (2 \text{ marks})$$

Alternatively,

$$H(s) = \frac{1/3}{(s+1)(s+2)} = \frac{k_1(s+2) + k_2(s+1)}{(s+1)(s+2)}$$

$$\frac{1}{3} = (k_1 + k_2)s + 2k_1 + k_2$$

$$k_1 + k_2 = 0$$

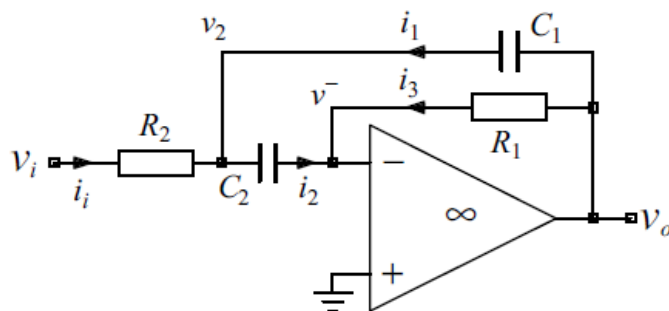
$$2k_1 + k_2 = 1/3$$

$$k_1 = 1/3, \text{ and } k_2 = -1/3$$

$$Y(s) = \frac{1/3}{s+1} - \frac{1/3}{s+2} \quad (2 \text{ marks})$$

Therefore, the unit step response in time domain is given by

$$y(t) = \frac{1}{3}e^{-t}u(t) - \frac{1}{3}e^{-2t}u(t). \quad (2 \text{ marks})$$

b. (12 marks)

i)

Begin by summing currents at the v_2 node:

$$i_i + i_1 = i_2 \text{ or,}$$

$$\frac{v_i - v_2}{R_2} + (v_o - v_2)sC_1 = v_2sC_2 \quad (2 \text{ marks})$$

$$v^- = 0 \quad (1 \text{ mark})$$

$$i_2 + i_3 = 0 = v_2 s C_2 + \frac{v_o}{R_1} \quad (1 \text{ marks})$$

v_2 can be eliminated from these two equations to give,

$$v_2 = \frac{v_i + v_o s C_1 R_2}{1 + s (C_1 + C_2) R_2} = - \frac{v_o}{s C_2 R_1} \text{ which can be developed as follows:}$$

$$v_i s C_2 R_1 + v_o s^2 C_1 R_2 C_2 R_1 = - v_o (1 + s (C_1 + C_2) R_2)$$

$$v_i s C_2 R_1 = - v_o (1 + s (C_1 + C_2) R_2 + s^2 C_1 R_2 C_2 R_1)$$

(1 mark)

$$\frac{v_o}{v_i} = \frac{-s C_2 R_1}{1 + s (C_1 + C_2) R_2 + s^2 C_1 R_2 C_2 R_1} = \frac{C_2 R_1}{(C_1 + C_2) R_2} \frac{-s (C_1 + C_2) R_2}{1 + s (C_1 + C_2) R_2 + s^2 C_1 R_2 C_2 R_1}$$

(1 marks)

The response is a band-pass response with a standard form

$$\frac{v_o}{v_i} = k \frac{\frac{s}{\omega_0 q}}{1 + \frac{s}{\omega_0 q} + \frac{s^2}{\omega_0^2}}$$

(2 marks)

ii)

If $C_1 = C_2 = C$,

$$\omega_0^2 = \frac{1}{C^2 R_1 R_2}, \quad \frac{1}{\omega_0 q} = 2CR_2 \text{ and therefore } q = \frac{1}{2} \sqrt{\frac{R_1}{R_2}}$$

For a q of 3, $R_1/R_2 = 36$

(4 marks)

Question 6**a. (3 marks)**

Since the cable is very long, we can assume that there is not reflection.

(1 marks)

For a unidirectional wave with no reflection, $Z_0 = V/I$ at all points along the transmission line, hence the probe adds a load of 46Ω to the circuit.

(2 marks)

b. (9 marks)

The reflection coefficients at the load and the source are both $1/3$.

(2 marks)

The voltage of the first forward wave is $144 \times 50 / 150 = 48\text{V}$.

(1 marks)

Each reflection will produce a wave with amplitude reduced by $1/3$.

$$t=1\mu\text{s} \quad V_{f1}=48\text{V}$$

$$V_{\text{total}}=48+48/3=64\text{V}$$

$$V_{b1}=48/3$$

(2 marks)

$$t=3\mu\text{s} \quad V_{f1}=48\text{V}$$

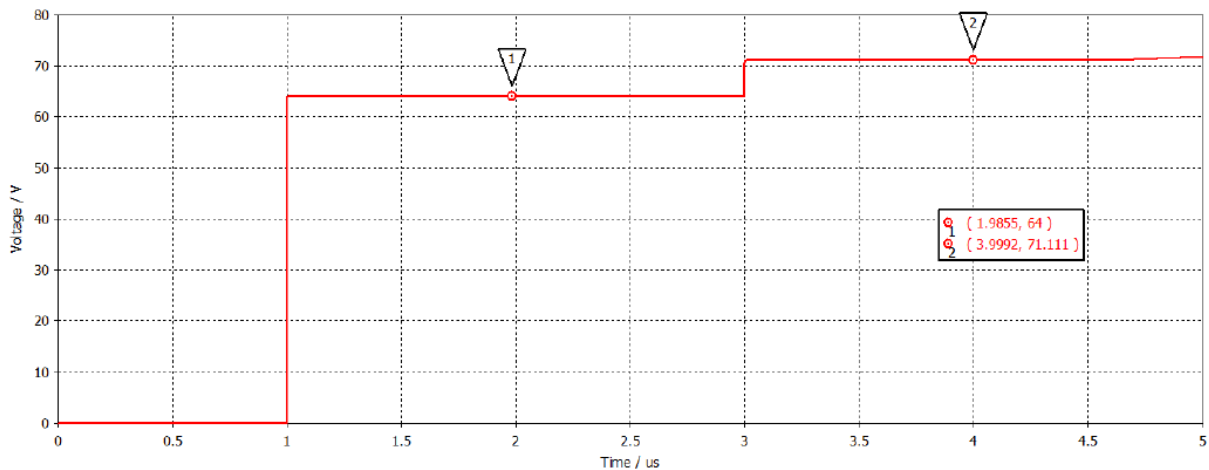
$$V_{\text{total}} = 48+48/3+48/9+48/27=71.1\text{V}$$

$$V_{b1}=48/3$$

$$V_{f2}=V_{b1}/3=48/9$$

$$V_{b2}=V_{f2}/3=48/27$$

(2 marks)



(2 mark)

c. (8 marks)

The source and load reflection coefficients are both -1 .

(2 marks)

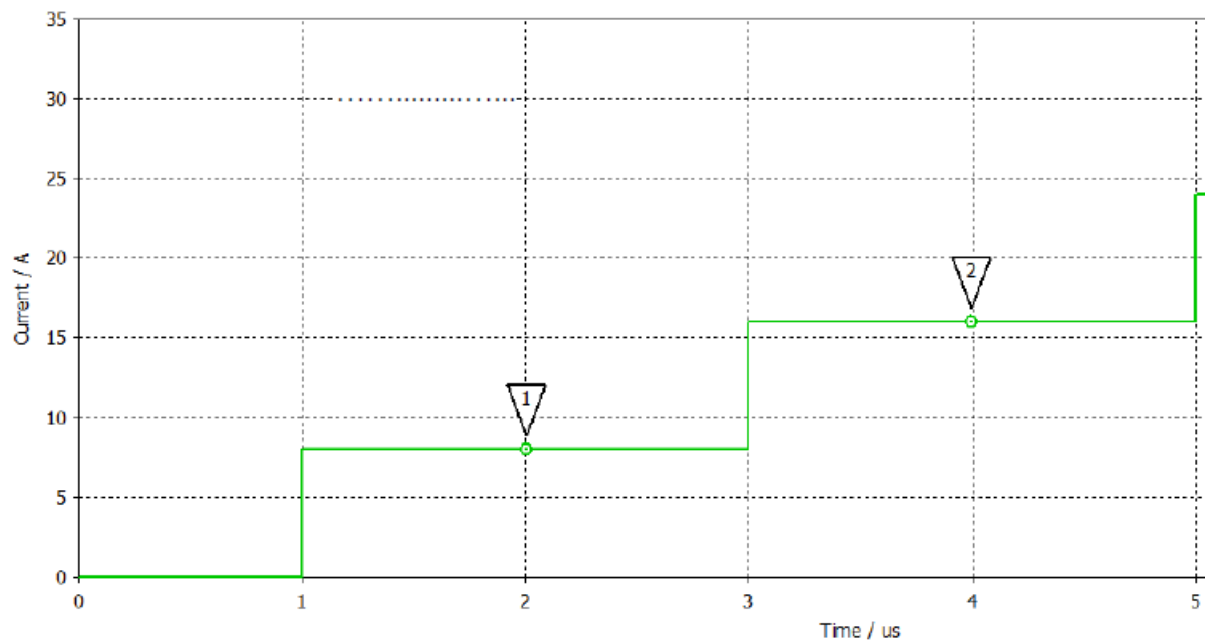
Just after the switch is closed, the current is $I = V/Z = 100/25 = 4\text{A}$.

(1 marks)

After $1\mu\text{s}$, the forward wave reflects and the current in the short circuit is

$$I = I_f - I_r = 4 - -4 = 8\text{A.} \quad (2 \text{ marks})$$

Every $2\mu\text{s}$ after this an additional 8A is added to the current in the short circuit. (1 marks)



(2 marks)