

The following shows the application of the C matrix to the Active Transformation equations to determine I' , Z' and finally V' . This is shown for the conductive compensated series machine and the uncompensated series machine.....

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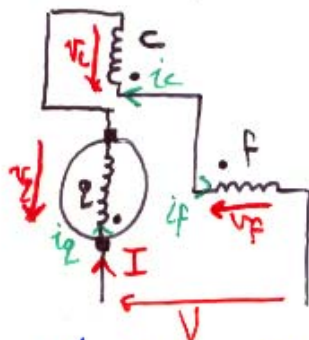
k30b

ACTIVE TRANSFORMATION FOR CONDUCTIVE COMPENSATION

$$\begin{bmatrix} V_q \\ V_c \\ V_f \end{bmatrix} = \begin{bmatrix} (R_2 + jX_2) & jX_{2c} & NX_m \\ jX_{c2} & (R_c + jX_c) & 0 \\ 0 & 0 & (R_f + jX_f) \end{bmatrix} \cdot \begin{bmatrix} I_a \\ I_c \\ I_f \end{bmatrix}$$

$$[V] = [Z] \cdot [I]$$

• From inspection, $I = I_2 = I_f = -I_c$, hence, we have:



$$\begin{matrix} I \\ \text{(PRIMITIVE)} \end{matrix} = \begin{matrix} C \\ \text{CONNECTION} \end{matrix} \begin{matrix} I' \\ \text{ACTUAL} \end{matrix}$$

$$\begin{bmatrix} I_2 \\ I_c \\ I_f \end{bmatrix} = \begin{bmatrix} 1 \\ -1 \\ 1 \end{bmatrix} \cdot [I]$$

• $V' = C_t \cdot V = C_t V$ since C_t is real

• Also, $V' = Z' I'$, where $Z' = C_t \cdot ZC = C_t ZC$

$$\begin{matrix} V' \\ \text{(ACTUAL)} \end{matrix} = \begin{matrix} C_t \\ \text{(TRANSPOSE OF C)} \end{matrix} \begin{matrix} V \\ \text{(PRIMITIVE)} \end{matrix}$$

$$[V] = \begin{bmatrix} 1 & -1 & 1 \end{bmatrix} \begin{bmatrix} V_q \\ V_c \\ V_f \end{bmatrix}$$

$$V = V_q - V_c + V_f$$

$$\cdot ZC = \underbrace{\begin{bmatrix} (R_2 + jX_2) & jX_{2c} & NX_m \\ jX_{c2} & (R_c + jX_c) & 0 \\ 0 & 0 & (R_f + jX_f) \end{bmatrix}}_Z \cdot \underbrace{\begin{bmatrix} 1 \\ -1 \\ 1 \end{bmatrix}}_C$$

$$ZC = \begin{bmatrix} (R_2 + jX_2) - jX_{2c} + NX_m \\ jX_{c2} - (R_c + jX_c) \\ (R_f + jX_f) \end{bmatrix}$$

$$Z' = C_t ZC = \begin{bmatrix} 1 & -1 & 1 \end{bmatrix} \begin{bmatrix} (R_2 + jX_2) - jX_{2c} + NX_m \\ jX_{c2} - (R_c + jX_c) \\ (R_f + jX_f) \end{bmatrix}$$

$$= [(R_2 + jX_2 - jX_{2c} + NX_m) - (jX_{c2} - R_c - jX_c) + (R_f + jX_f)]$$

collecting terms.....

$$= (R_2 + R_c + R_f) + NX_m + j(X_c + X_f - X_{2c} - X_{c2} + jX_2)$$

as before, $X_{2c} = X_{c2}$ & assuming perfect coupling & same

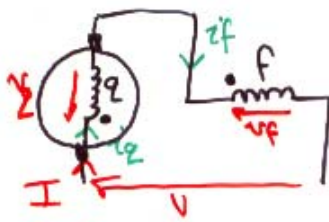
no. turns, $X_{2c} = X_{c2} = X_c = X_2$

$$Z' = (\underbrace{R_2 + R_c + R_f}_R) + NX_m + jX_f$$

$$\cdot \text{Finally, } V' = Z'I' = (R + NX_m + jX_f)I$$

- The voltage equation for the transformed (actual) circuit

Same principle for uncompensated m/c



$$\begin{bmatrix} I_f \\ I_2 \end{bmatrix} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \cdot \begin{bmatrix} I' \end{bmatrix}$$

$$\begin{bmatrix} V' \\ V \end{bmatrix} = \begin{bmatrix} 1 & 1 \end{bmatrix} \begin{bmatrix} V_f \\ V_2 \end{bmatrix}$$

$$V = V_f + V_2$$

$$Z = \begin{bmatrix} (R_f + jX_f) & 0 \\ NX_m & (R_2 + jX_2) \end{bmatrix}$$

$$Z_C = \begin{bmatrix} (R_f + jX_f) & 0 \\ NX_m & (R_2 + jX_2) \end{bmatrix} \cdot \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} (R_f + jX_f) + 0 \\ NX_m + (R_2 + jX_2) \end{bmatrix}$$

$$Z' = C_t Z_C = \begin{bmatrix} 1 & 1 \end{bmatrix} \begin{bmatrix} (R_f + jX_f) + 0 \\ NX_m + (R_2 + jX_2) \end{bmatrix}$$

$$= (R_f + jX_f) + NX_m + (R_2 + jX_2)$$

$$= (R_f + R_2) + NX_m + j(X_f + X_2)$$

again, for $X_f = X_2 = X$

$$Z' = R + NX_m + j2X$$

$$\Rightarrow V' = Z' I' = (R + NX_m + j2X) I$$