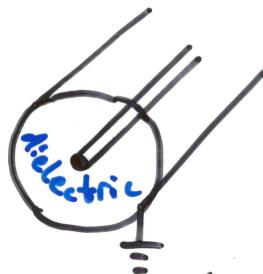


transmission lines (1D)

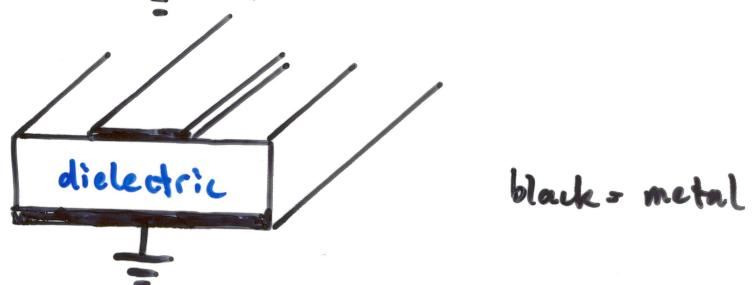
forms: twin wires



coaxial cable



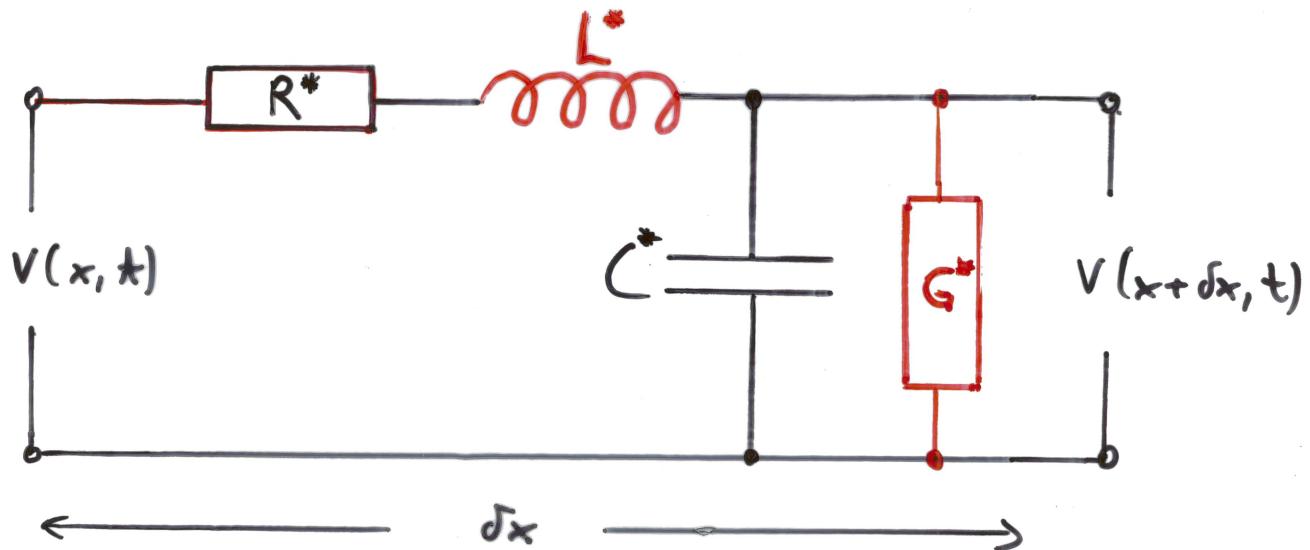
microstrip



black = metal

consider infinitesimal length δx of transmission line
to get a

model of transmission line element ideal /with losses



R^* , G^* , C^* , L^* are specific resistance per length (Ω/m)
conductance (S/m)
capacitance (F/m)
inductance (H/m)

now consider for lossy transmission line

a) voltage drop along the lines:

$$-\Delta V = R^* \delta x \cdot I + L^* \delta x \frac{\partial I}{\partial t}$$

$$-\frac{\partial V}{\partial x} = R^* I + L^* \frac{\partial I}{\partial t}$$

b) leakage current between the lines:

$$-\Delta I = G^* \delta x \cdot V + C^* \delta x \frac{\partial V}{\partial t}$$

$$-\frac{\partial I}{\partial x} = G^* V + C^* \frac{\partial V}{\partial t}$$

1. case: ideal case $R^* = G^* = 0$

$$a) -\frac{\partial V}{\partial x} = L^* \frac{\partial I}{\partial t} \Rightarrow -\frac{\partial^2 V}{\partial x^2} = L^* \frac{\partial^2 I}{\partial t^2} \quad (i)$$

$$b) -\frac{\partial I}{\partial x} = C^* \frac{\partial V}{\partial t} \Rightarrow -\frac{\partial^2 I}{\partial x^2} = C^* \frac{\partial^2 V}{\partial t^2} \quad (ii)$$

insert (ii) into (i)

$$\Rightarrow -\frac{\partial^2 V}{\partial x^2} = L^* (-C^*) \frac{\partial^2 V}{\partial t^2}$$

$$\Rightarrow \frac{\partial^2 V}{\partial t^2} = \frac{1}{LC} \frac{\partial^2 V}{\partial x^2} \quad \text{is propagating } V(x,t)$$

$$a) \text{ analogue: } \frac{\partial t}{\partial x} -\frac{\partial^2 V}{\partial t \partial x} = L^* \frac{\partial^2 I}{\partial t^2} \quad (iii)$$

$$b) \frac{\partial x}{\partial t} -\frac{\partial^2 I}{\partial x \partial t} = C^* \frac{\partial^2 V}{\partial t \partial x} \quad (iv)$$

insert (iii) into (iv)

$$\Rightarrow -\frac{\partial^2 I}{\partial x^2} = C^* (-L^* \frac{\partial^2 I}{\partial t^2})$$

$$\Rightarrow \frac{\partial^2 I}{\partial t^2} = \frac{1}{LC} \frac{\partial^2 I}{\partial x^2} \quad \text{is propagating } I(x,t)$$

if $R^* = G^* = 0$ (ideal transmission line), then both V and I obey wave equations with wave velocity $v = \sqrt{\frac{1}{LC}}$

As $v = \lambda \cdot f = \frac{\omega}{k}$ we could also write

$$k = \omega \sqrt{LC}$$

2. case : zero resistance but small, finite conductance
 $(R^* = 0)$ $(G^* \text{ small})$

$$a) -\frac{\partial V}{\partial x} = L^* \frac{\partial I}{\partial t}$$

$$b) -\frac{\partial I}{\partial x} = G^* V + C^* \frac{\partial V}{\partial t}$$

$$\text{from a)} \xrightarrow{\frac{\partial t}{\partial x}} \frac{\partial^2 V}{\partial t \partial x} = -L^* \frac{\partial^2 I}{\partial t^2} \quad (i)$$

$$\text{from b)} \xrightarrow{\frac{\partial x}{\partial t}} \frac{\partial^2 I}{\partial x \partial t} = -G^* \frac{\partial V}{\partial x} - C^* \frac{\partial^2 V}{\partial x \partial t} \quad (ii)$$

eliminate V by inserting a) and (i) into (ii) :

$$\begin{aligned} \frac{\partial^2 I}{\partial x^2} &= G^* L^* \frac{\partial I}{\partial t} + C^* L^* \frac{\partial^2 I}{\partial t^2} \\ &= L^* C^* \underbrace{\frac{\partial^2 I}{\partial t^2}}_{\substack{\text{as before} \\ (2^{\text{nd}} \text{ derivative})}} + L^* G^* \underbrace{\frac{\partial I}{\partial t}}_{\substack{\text{new} \\ (1^{\text{st}} \text{ derivative})}} \end{aligned}$$

$$\text{assume } V = V_0 e^{j(\omega t - \tilde{k}x)}$$

$$\text{and } I = I_0 e^{j(\omega t - \tilde{k}x)} \text{ for a modified } \tilde{k} \quad (iii)$$

insert (iii) into above and get

$$\text{with } \frac{\partial I}{\partial x} = -j\tilde{k}I, \quad \frac{\partial^2 I}{\partial x^2} = -\tilde{k}^2 I$$

$$\frac{\partial I}{\partial t} = j\omega I, \quad \frac{\partial^2 I}{\partial t^2} = -\omega^2 I$$

$$\Rightarrow -\tilde{k}^2 \cancel{I} = L^* C^* (-\omega^2) \cancel{I} + L^* G^* j\omega \cancel{I}$$

$$\Rightarrow \tilde{k}^2 = \omega^2 L^* C^* - j\omega L^* G^*$$

$$\Rightarrow \tilde{k} = \sqrt{\omega^2 L^* C^* - j\omega L^* G^*}$$

$$= \omega \sqrt{L^* C^*} \sqrt{1 - \frac{jG^*}{\omega C^*}}$$

$$\approx 1 - \frac{jG^*}{2\omega C^*} \quad \text{for small } G^*$$

$$\tilde{k} \approx \underbrace{\omega \sqrt{L^* C^*}}_{\substack{\text{as before}}} \quad \underbrace{\left(1 - \frac{jG^*}{2\omega C^*}\right)}_{\substack{\text{new}}}$$

meaning of the new term can be appreciated by inserting result into (iii):

$$\begin{aligned}
 I &= I_0 e^{j(\omega t - \tilde{k}x)} \quad \text{with } \tilde{k} \approx \omega \sqrt{L^* C^*} \left(1 - \frac{jG^*}{2\omega C^*}\right) \\
 &= I_0 e^{j[\omega t - \omega \sqrt{L^* C^*} x + j \sqrt{L^* C^*} \frac{G^*}{2C^*} x]} \\
 &= I_0 e^{j(\omega t - \omega \sqrt{L^* C^*} x)} \quad e^{-\sqrt{L^* C^*} \frac{G^*}{2C^*} x}
 \end{aligned}$$

propagating wave as before, with $\tilde{k} = \omega \sqrt{L^* C^*}$, as before

attenuation with exponential where $\beta = \sqrt{L^* C^*} \frac{G^*}{2C^*}$ is inverse of $1/e$ decay length

3. case: general solution

$$\text{of } -\frac{\partial V}{\partial x} = R^* I + L^* \frac{\partial I}{\partial t} \quad \text{from page 14} \quad (i)$$

$$-\frac{\partial I}{\partial x} = G^* V + C^* \frac{\partial V}{\partial t} \quad (ii)$$

$$\Rightarrow -\frac{\partial^2 I}{\partial x^2} = G^* \frac{\partial V}{\partial x} + C^* \frac{\partial^2 V}{\partial x \partial t}$$

↓ from (i) ↓ from $\frac{\partial^2 V}{\partial t^2}$ of (i)

$$-R^* I - L^* \frac{\partial I}{\partial t} \quad -R^* \frac{\partial I}{\partial t} - L^* \frac{\partial^2 I}{\partial t^2}$$

$$\Rightarrow \frac{\partial^2 I}{\partial x^2} = L^* C^* \frac{\partial^2 I}{\partial t^2} + R^* G^* I + (R^* C^* + L^* G^*) \frac{\partial I}{\partial t}$$

Assume again $I = I_0 e^{j(\omega t - \tilde{k}x)}$

$$\Rightarrow -\tilde{k}^2 \cancel{I} = -L^* C^* \omega^2 \cancel{I} + R^* G^* \cancel{I} + (R^* C^* + L^* G^*) j \omega \cancel{I}$$

$$\Rightarrow \tilde{k}^2 = \omega^2 L^* C^* - R^* G^* - j \omega (R^* C^* + L^* G^*)$$

\tilde{k}_0^2
for wave
without any
attenuation,
depends on
 ω → dispersion

reduction
in \tilde{k} , i.e.
redshift of
wavelength

describes
exponential
attenuation