

Chromatic Dispersion

Due to signal never being purely monochromatic and the refractive index (phase index) of silica being a function of λ , pulses will broaden temporally as they propagate along the fibre. If the broadening is great, intersymbol interference occurs leading to increased Bit Errors & eventually the complete failure of the system.

Attenuation

In order to discriminate between '0' and '1' logic levels, a sufficiently large signal (compared to the noise floor) is required. For a given data rate a certain power at the receiver is required for a given bit error rate. The total losses in a system (including margin) cannot therefore exceed the difference in launch & receiver powers in dBm.

Using 7 dB for loss in fibre.

Using $BLDA \leq \frac{1}{4}$

(n.b. assumption \rightarrow allow bit to broaden by $\frac{1}{4}$ but slot time - could be $\frac{1}{2}$ but doesn't change result in end.)

(use $\frac{1}{2}$ instead of $\frac{1}{4}$)

Disp limit

Loss Limit

1.35 μm

50 km (25 km)

17.5 km

calcs over \Rightarrow

1.55 μm

3.33 km (1.6 km)

35 km

so best to use 1.35 μm for loss limited transmission up to 17.5 km link length (10)

To send @ 10 Gbits/sec.

i) DFB @ 1.35 or 1.55. 1.55 better as (2)
35 km link length possible. (2)

ii) WDM system \rightarrow 10 multiplexed 1 GBit transmitters @ \sim 1.35 μm . (2)

Dispersion Limits.

1.3

$$BLD \Delta\lambda \leq \frac{1}{4} \quad \Rightarrow \quad L = \frac{1}{4BD\Delta\lambda}$$

$$B = 1 \times 10^9$$

$$L = ?$$

$$D = 1 @ 1.35, 15 @ 1.55 \quad (\text{ps/nm.km})$$

$$\Delta\lambda = 5 \text{ nm}$$

$$\underline{1.35 \mu\text{m}} \quad L = \frac{1}{4 \times 1 \times 10^9 \times 5 \times 10^{-12}} \quad (\text{km})$$

$$= \frac{1}{20 \times 10^{-3}} \quad (\text{km})$$

$$= \underline{\underline{50 \text{ km}}}$$

(n.b = 25 km if assume $\frac{1}{2}$ Bit slot broadening).

$$\underline{1.55 \mu\text{m}} \quad L = \frac{1}{4 \times 1 \times 10^9 \times 5 \times 15 \times 10^{-12}} \quad (\text{km})$$

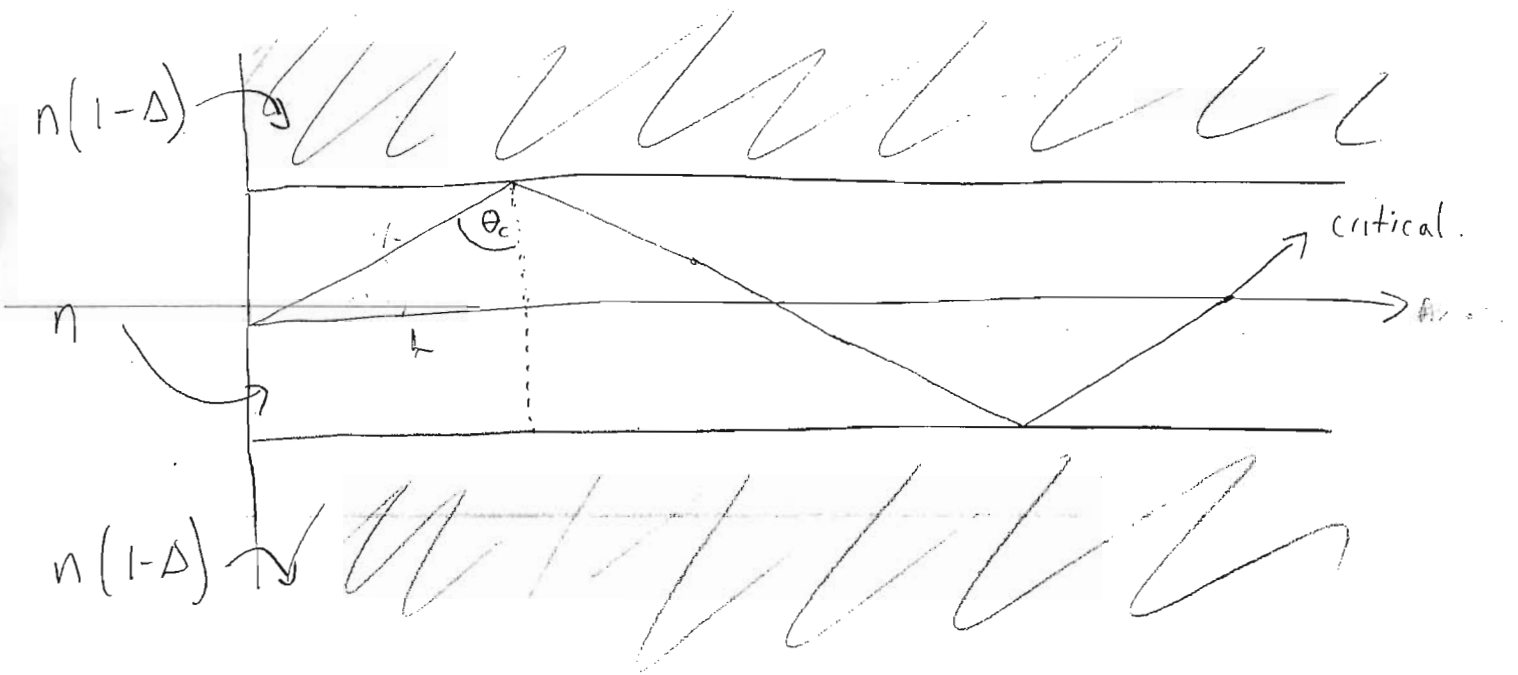
$$= \underline{\underline{3.33 \text{ km}}}$$

Loss Limit

7 dB loss.

$$@ 1.35 \quad 0.4 \text{ dB/km} \Rightarrow \underline{\underline{17.5 \text{ km}}}$$

$$@ 1.55 \quad 0.2 \text{ dB/km} \Rightarrow \underline{\underline{35 \text{ km}}}$$



for meridional ray :

$$t_{\text{meridional}} = \frac{L}{v_1} = \frac{Ln}{c}$$

for critical ray, fibre length $L \rightarrow$ signal travels $\frac{L}{\sin \theta_c}$

$$t_{\text{critical}} = \frac{Ln}{c \sin \theta_c}$$

$$\text{Differential} = t_{\text{critical}} - t_{\text{meridional}}$$

$$\delta t = \frac{Ln}{c \sin \theta_c} - \frac{Ln}{c}$$

Snells law defines $\sin \theta_c = \frac{n(1-\Delta)}{n}$

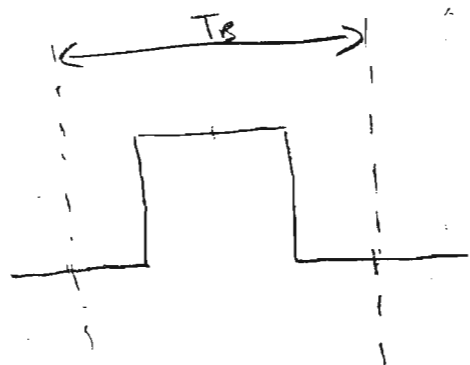
$$\delta t = \frac{L n}{c(1-\Delta)} - \frac{L n}{c}$$

$$= \frac{L n - L n (1-\Delta)}{c(1-\Delta)}$$

$$\delta t = \frac{L n \Delta}{c(1-\Delta)}$$

[5]

Bit slot & Allowed Broadening.



$$T_B = \frac{1}{B} \quad B = \text{Data rate.}$$

Assume broadening to be $\frac{T_B}{4}$
(may be $T_B/2 \dots$)

$$\delta t \leq \frac{T_B}{4} \leq \frac{1}{4B}$$

$$\frac{1}{4B} \leq \frac{L n \Delta}{c(1-\Delta)}$$

$$L \leq \frac{c(1-\Delta)}{4 n \Delta B}$$

[5]

$$L \leq \frac{3 \times 10^8 \times 0.99}{4 \times 1.5 \times 0.01 \times 50 \times 10^6}$$

$$L \leq \frac{3 \times 10^8 \times 0.99}{3 \times 10^6}$$

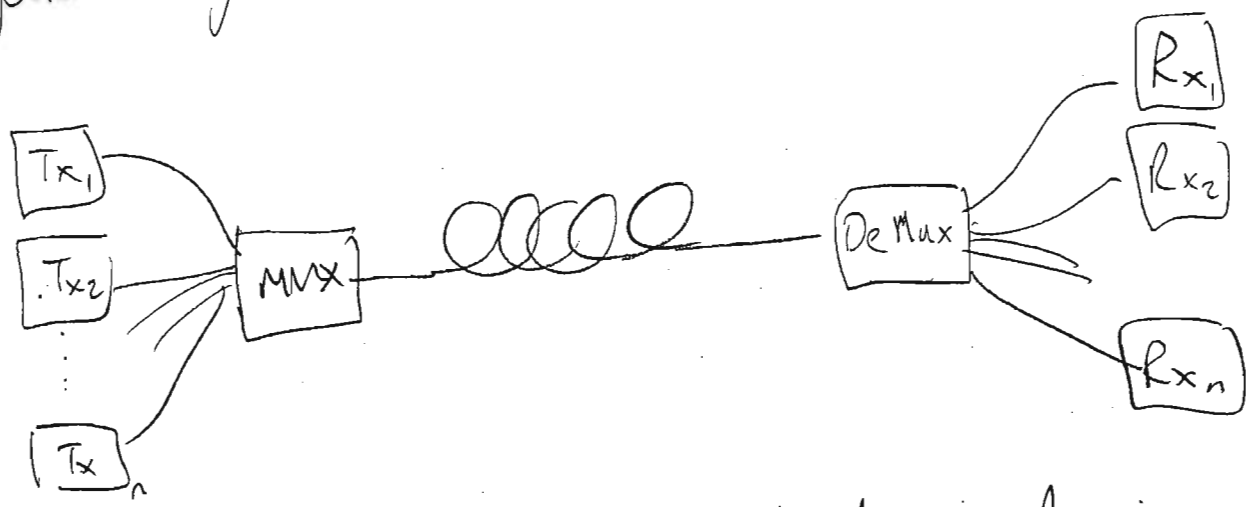
$$L \leq 99 \text{ m}$$

[2]

So maximum link length $\sim 100 \text{ m}$.

WDM

Relies on capability of fibre to carry light of different wavelengths, without the interactions of the optical signal.



Requires components to combine optical signals in a fibre (mux) and to filter multiple optical channels in one physical channel into one optical channel in each physical channel.

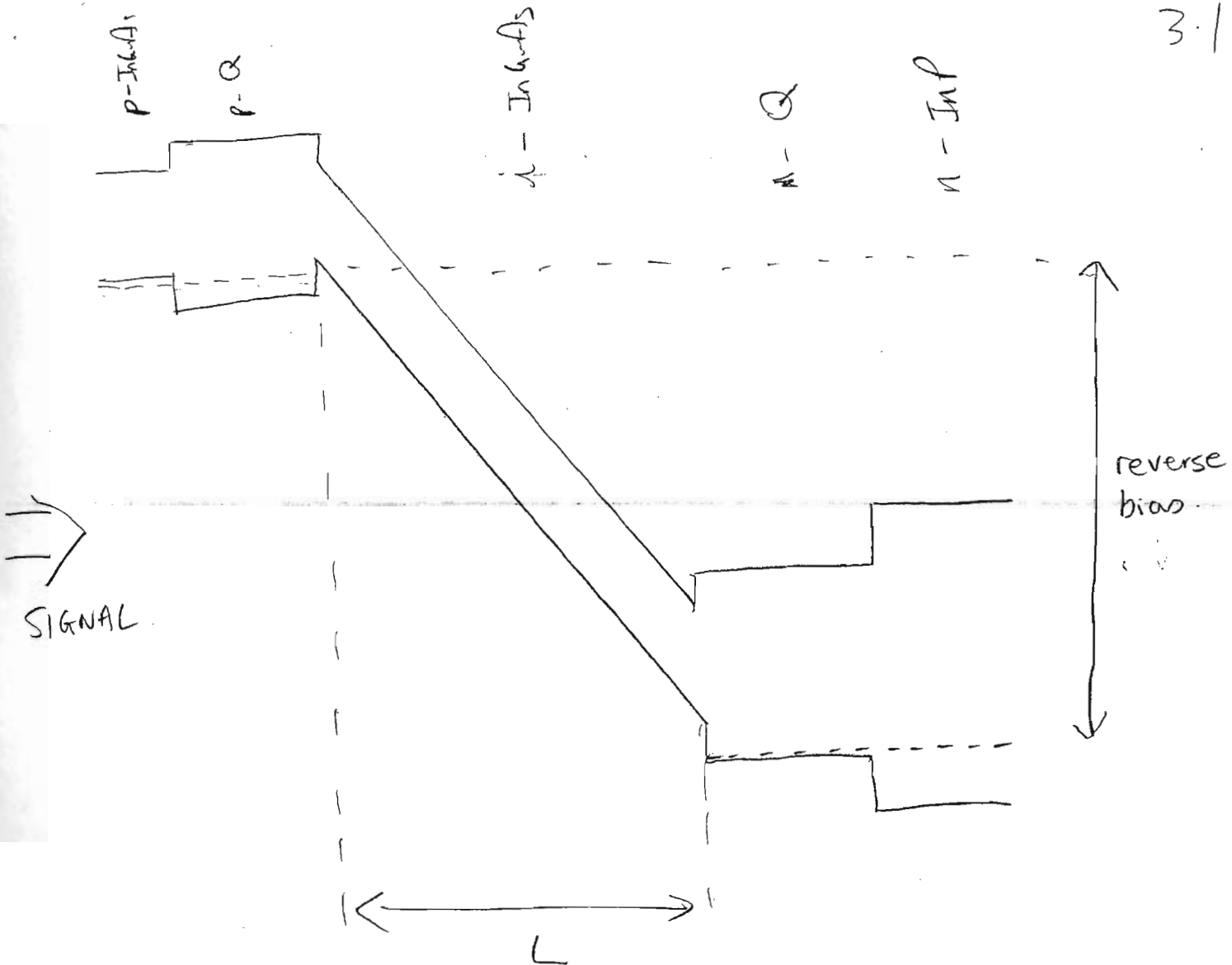
[5]

Crosstalk

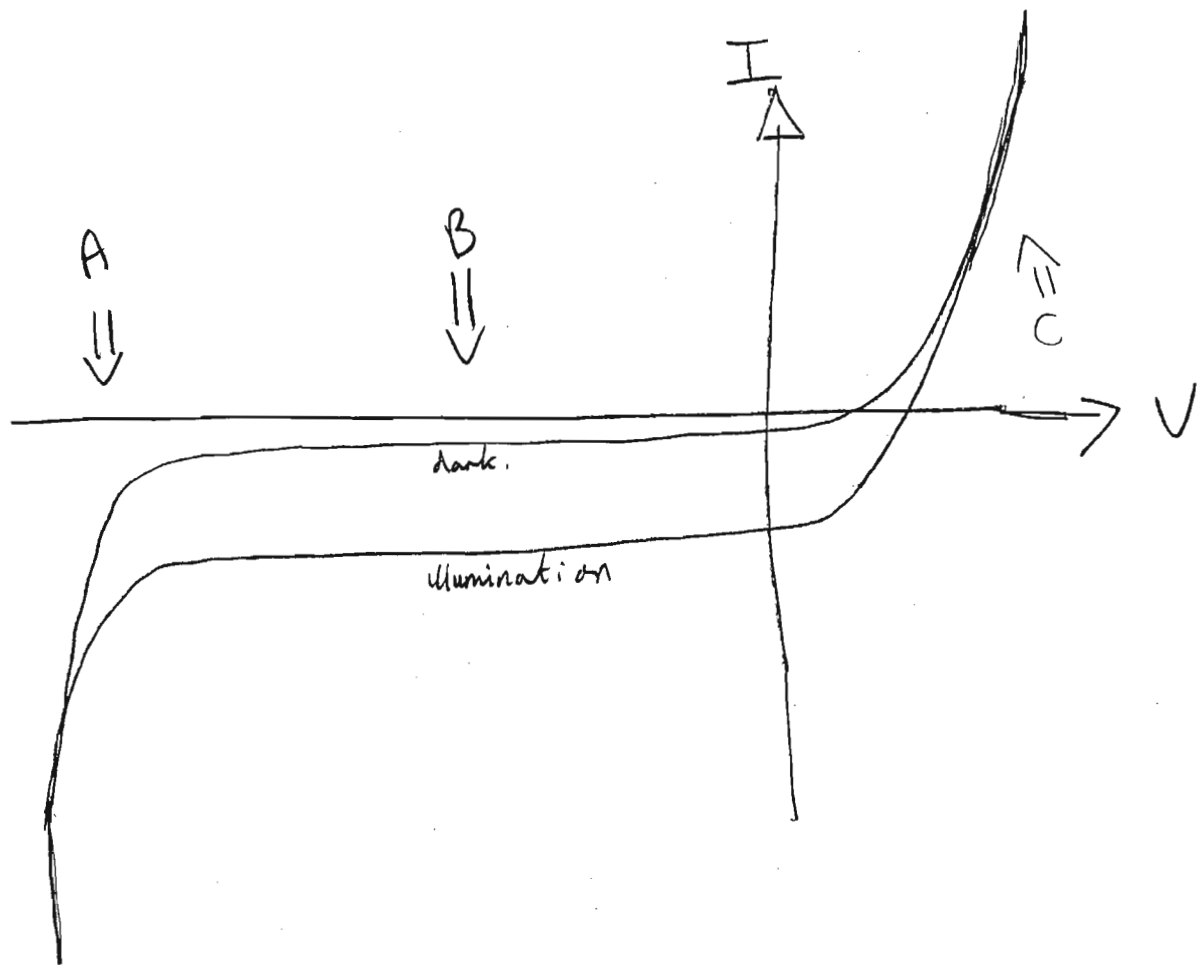
2.4

1. \Rightarrow De-Mux not 100% efficient at removing other channels. (out-of-band - X-talk).
2. \Rightarrow If EDFA used in system can get X-gain modulation or cross-talk.

[3]



IV



3.2
A \rightarrow Reverse Breakdown due to either
Avalanche (high purity crystal) or
Zener (defective material) breakdown.

B \Rightarrow Dark & Photo-current in operating
regime: Dark current due to defects /
unpassivated surfaces.

C \Rightarrow Forward bias \rightarrow light emission.

[8]

For High internal Quantum Efficiency, need
 $\alpha L \gg 1$ ($\eta_{int} = 1 - e^{-\alpha L}$) so need to
maximize L .

For Speed 2 factors.

1.) RC time constant $\Rightarrow C = \frac{\epsilon \epsilon_0 A}{L}$ want L Big.

2.) Carrier transit time $\Rightarrow t_{transit} = \frac{L}{V_{sat}}$ (\leftarrow saturation vel)
want L small.

[6]

Responsivity

(or edge entry/waveguide config)

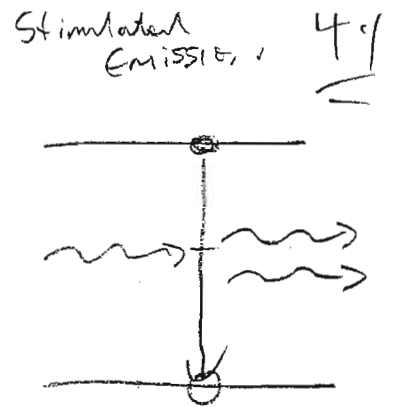
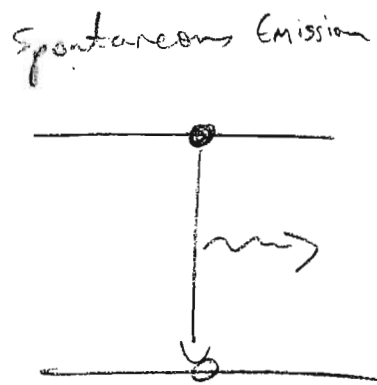
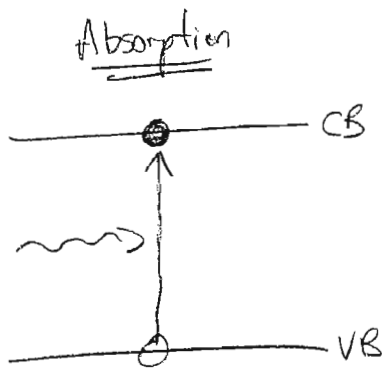
1.) Use substrate entry. ~~✓~~ p-InGaAs caps will absorb light but not contribute to signal photocurrent.

2.) Use Anti-Reflection coatings \rightarrow loss $\sim 30\%$

$$[R = \left(\frac{n_1 - n_2}{n_1 + n_2} \right)^2 \dots n_1 = 1 \quad n_2 \sim 3.5]$$

3.) Redesign to utilize avalanche multiplication \rightarrow
APD

[6]



4.1

Absorption → A photon with sufficient energy can excite an electron from the valence band to the conduction band. The absence of an electron in the v-b is termed a 'hole'.

Spontaneous Emission → An electron and hole, being of opposite charge are attracted to each other. The electron loses its energy to a photon and relaxes to the valence band. Emitted photon has random phase & direction.

Stimulated Emission → This is the emission of a photon by the relaxation of an electron from the conduction band to the valence band—but the process is stimulated by an incident photon. The emitted photon is of the same energy, phase & direction to the stimulating photon.

for LD

Applying small current get spontaneous emission due to injected holes & electrons. As carrier density is increased Absorption is bleached (reduced electrons in VB, ...) and stimulated emission becomes more

probable. When stimulated emission is more likely than $\frac{4.2}{6}$ absorption an incident signal experiences gain.

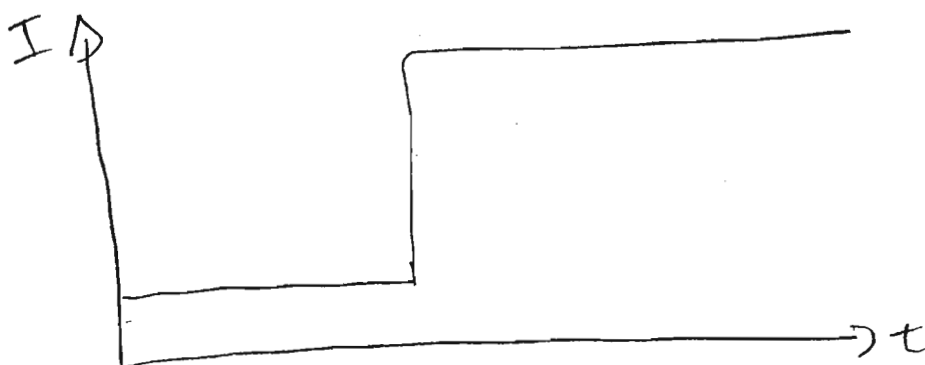
2) Longitudinal \Rightarrow Reduce spectral width & reduce chromatic dispersions. Achieved by reducing length of FP laser or better to introduce a wavelength selective filter within the laser structure.

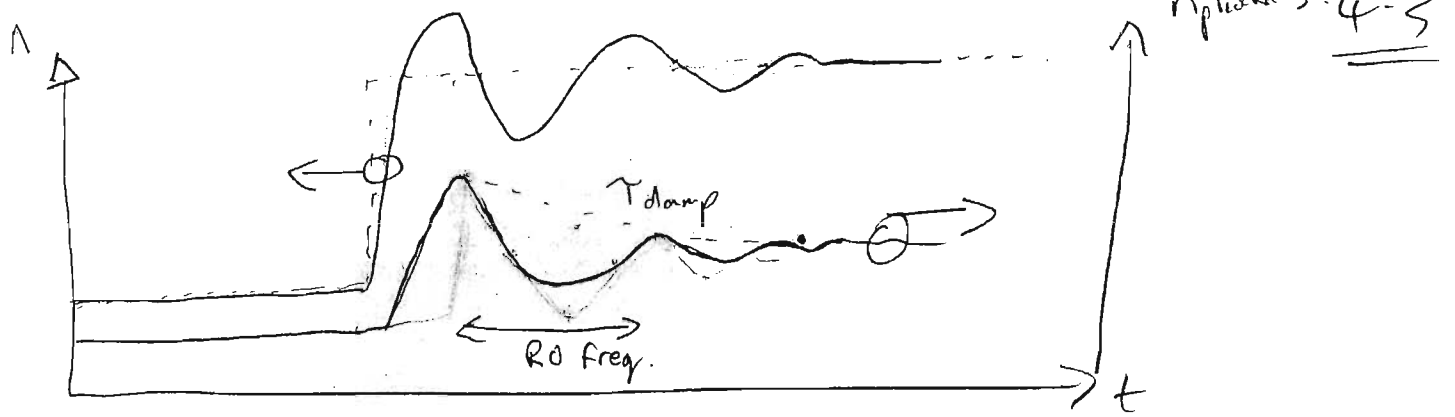
Transverse \Rightarrow Need to fibre-couple laser. Additional lateral modes do not couple efficiently to fibre. Remove by making laser width sufficiently small that higher order optical modes experience a high loss and have a high threshold compared to the fundamental. [4]

③ Carriers & photons coupled.

$$\frac{dn_{el}}{dt} = \frac{I}{qV} - \frac{n}{\tau_{sp}} - g n_{photon}$$

$$\frac{dn_{photon}}{dt} = g n_{photon} - \frac{n_{photon}}{\tau_{photon}} + \frac{\beta n}{\tau_{sp}}$$





[4]

STRATEGIES FOR INC. W_0

$\frac{dg}{dn} \rightarrow$ increase \rightarrow δ - p -doping to remove carrier transport effects.

\rightarrow Use QWs, strained QWs, QDs to reduce DOS.

$N_{photon} \rightarrow$ increase \rightarrow High current \rightarrow High Power
 \rightarrow problems with heat, facet damage.

$\tau_{photon} \rightarrow$ decrease \rightarrow short cavity \rightarrow J_{th} increases
 \rightarrow thermal problems

[6]