



The  
University  
Of  
Sheffield.

## DEPARTMENT OF ELECTRONIC AND ELECTRICAL ENGINEERING

Spring Semester 2014-15 (2.0 hours)

### EEE305 Machine Design

Answer **THREE** questions. **No marks will be awarded for solutions to a fourth question.** Solutions will be considered in the order that they are presented in the answer book. Trial answers will be ignored if they are clearly crossed out. **The numbers given after each section of a question indicate the relative weighting of that section.**

1. a. From the expression of Lorentz force, show that the torque density of a cylindrical electrical machine can be expressed in terms of the magnetic and electrical loadings,  $B$  and  $Q$ , respectively. List the major assumptions which you make in the derivation. (5)
- b. Derive an expression for estimating the airgap flux density in an interior permanent magnet machine with circumferentially magnetized magnets, such as shown in Figure 1. Explain why the air-gap flux density may be higher than the magnet remanence.

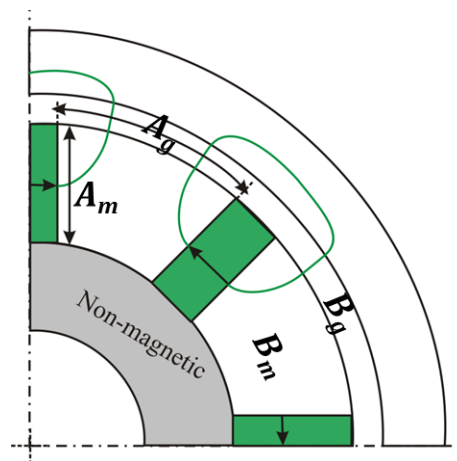


Figure 1

- c. Neglecting all the leakage flux, show that when a magnet is required to produce a specific flux density  $B_g$  in an air-gap of length  $L_g$  and an area  $A_g$ , it is possible to minimize the magnet volume required by operating it at its maximum energy product working point  $(BH)_{\max}$ . Explain why this design approach for the magnet is rarely adopted in practical electrical machines. (5)
- d. List the main factors that affect the iron losses of electrical machines, and explain how the influence of iron losses on high speed machines can be minimised. (4)

2. a. Derive general expressions for the winding pitch factor,  $K_p$ , and the distribution factor,  $K_d$ , for both the fundamental and the  $n^{\text{th}}$  harmonic EMF components. Based on the coil EMF vectors, in order to obtain a maximum winding factor, determine the coil connections for a 3-phase, 12-slot, 8-pole surface mounted permanent magnet machine with single layer windings. (8)
- b. Show that the winding skew factor can be derived using similar method as for the winding distribution factor. Explain the main advantages and disadvantages of using winding skew. (4)
- c. A concentric winding which is distributed in the slots over one pole pitch in a machine having evenly spaced slots, as shown in Figure 2. Calculate the winding factor for the fundamental EMF.

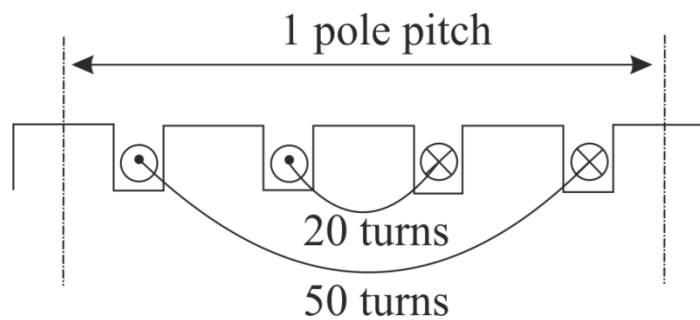


Figure 2

- d. Describe the main advantages and disadvantages of the short-pitched concentrated winding, and the fully-pitched distributed winding. (5)
- (3)

3. A 2-pole permanent magnet DC motor, having its magnet arcs mounted adjacent to the airgap, has the following main dimensions:

Rotor active length  $L = 40$  mm

Rotor outer diameter  $D = 60$  mm,

Effective air-gap length  $l_g = 0.8$  mm

Magnet radial thickness  $l_m = 5$  mm

Magnet pole arc =  $110^\circ$

The magnet material has recoil permeability ( $\mu_r$ ) of 1.1 and its B-H characteristic is shown in Figure 3.

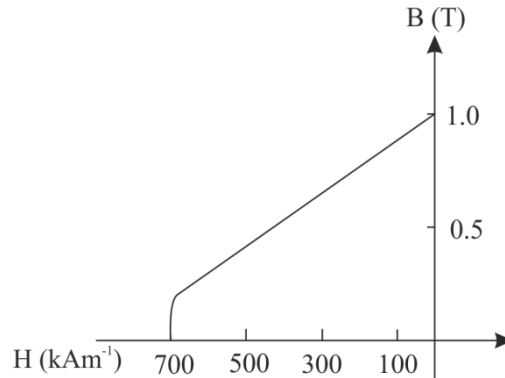


Figure 3  $H_{lim} = 650$  kA/m

- a. Use analytical techniques to calculate the flux per pole for the motor. (5)
- b. If the rotor has a total of 1532 conductors, connected in two parallel paths by the brushes, calculate the speed EMF constant for the motor and the corresponding no-load speed when operating on a 100V dc supply. (5)
- c. The rotor winding has an effective resistance of  $3 \Omega$ , calculate the stall-torque using a dc supply of 100V supply and show whether or not the motor can tolerate the stall under these conditions without demagnetizing the magnets. (5)
- d. Show graphically the difference between reversible and irreversible demagnetizations. Explain the influence of temperature on the irreversible demagnetization for both Ferrite and NdFeB permanent magnets. (5)

4. For a slot shown in Figure 4, specify any assumptions that need to be made in order to derive analytically the expressions of:
- The coil slot leakage inductance per-unit length for coil 'a' (5)
  - The coil slot leakage inductance per-unit length for coil 'b' (3)
  - The mutual inductance per-unit length between coils 'a' and 'b' (7)

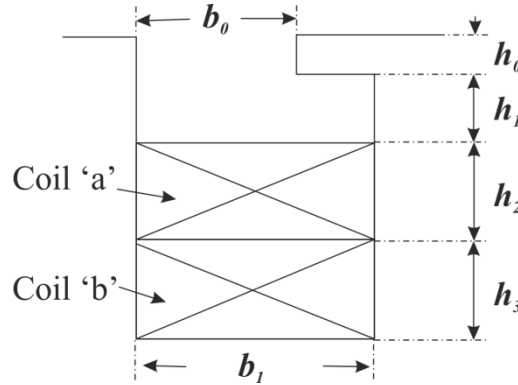


Figure 4 Numbers of turns in the slot for coil 'a' and 'b' are  $N_a$  and  $N_b$ , respectively.

- Show graphically the difference between a single layer, concentrated winding and a double layer, concentrated winding. Describe the main advantages of the single layer, concentrated winding over the double layer, concentrated winding. (5)

(Full marks will not be given if the appropriate assumptions are not specified)

GJL/JBW