

## EEE225: Analogue and Digital Electronics

### Lecture III

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EEE225: Lecture 3

### This Lecture

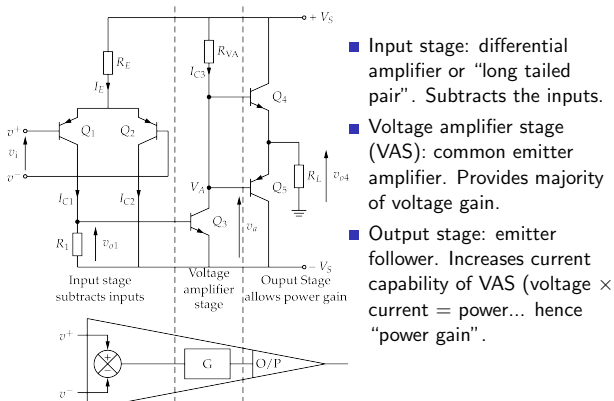
- 1 Into The Opamp
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  - Opamp Circuit DC Conditions
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- 2 The "Voltage Amplifier" stage
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↳ Into The Opamp

↳ Simplified Schematic of an Opamp



- Input stage: differential amplifier or "long tailed pair". Subtracts the inputs.
- Voltage amplifier stage (VAS): common emitter amplifier. Provides majority of voltage gain.
- Output stage: emitter follower. Increases current capability of VAS (voltage × current = power... hence "power gain").

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↳ Into The Opamp

↳ Opamp Circuit DC Conditions

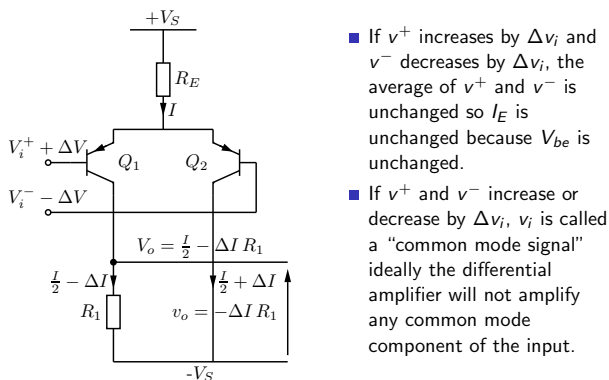
- Opamp will not work properly without feedback. Feedback controls the gain of the circuit but also helps define the DC conditions. Feedback adjusts  $v_i$  in order to achieve the internal voltage drops required for proper operation. If  $v_o = 0$ ,  $v_i$  will be at the value it needs to be in order to make  $v_o = 0$ . Feedback is *not* shown on prior slide.
- If  $v^+ \approx v^- \approx 0$ ,  $V_{E1}$  and  $V_{E2} \approx 0.7$  so  $I_E \approx (+V_S - 0.7)/R_E$ .
- $I_E$  splits between  $Q_1$  and  $Q_2$  to form  $I_{C1}$  and  $I_{C2}$ .
- $I_{C1}$  has two functions 1) create a voltage drop of 0.7 V across  $R_1$  in order to bias  $Q_3$  into conduction. 2) Provide the base current for  $Q_3$ .  $I_{C1}$  will be  $0.7/R_1 + I_{C3}/h_{FE3}$ .
- The value of  $I_{C3}$  varies with  $V_A$  and hence with  $V_{o4}$  but assuming  $V_A = 0$ ,  $I_{C3} \approx +V_S/R_{VA}$ .
- $I_{C2}$  is returned directly to the negative supply.
- In the case where  $v^+ \approx v^- \neq 0$ , there is a common mode input voltage,  $v_{cm}$ , and  $I_E \approx (+V_S - v_{cm})/R_E$ .

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↳ Into The Opamp

↳ Differential Amplifier



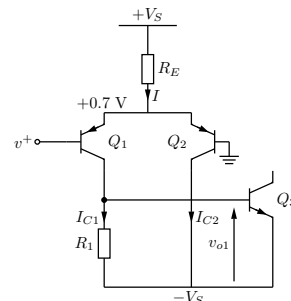
- If  $v^+$  increases by  $\Delta v_i$  and  $v^-$  decreases by  $\Delta v_i$ , the average of  $v^+$  and  $v^-$  is unchanged so  $I_E$  is unchanged because  $V_{be}$  is unchanged.
- If  $v^+$  and  $v^-$  increase or decrease by  $\Delta v_i$ ,  $v_i$  is called a "common mode signal" ideally the differential amplifier will not amplify any common mode component of the input.

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↳ Into The Opamp

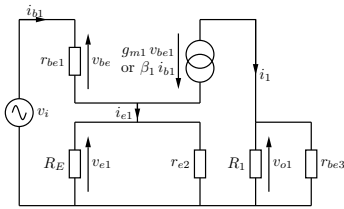
↳ Differential Amplifier



We must consider the effects of three transistors.  $Q_1$  and  $Q_2$  are the input differential pair.

$Q_3$  must also be considered now because its input resistance forms part of  $Q_1$ 's collector load resistance. If the input signal is regarded as  $v^+$  with respect to ground,  $Q_2$  looks like a common base connection and can be represented by its common base input resistance  $1/g_{m2}$ . The collector current of  $Q_1$  sees two resistors in parallel,  $R_1$  and the input resistance of  $Q_3$ .  $Q_3$  is a common emitter amplifier *without* degeneration. Its input resistance is  $r_{be3}$ .

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A small signal equivalent circuit describes the three transistor circuit block according to our simplifications.

This small signal model is very similar to the common emitter *with* degeneration from Lecture 1. In this case  $R_S = 0$  and  $R_E$  and  $R_L$  are parallel combinations  $R_E // r_{e2}$  and  $R_1 // r_{be3}$ . Since  $R_E \gg r_{e2}$ ,  $r_{e2}$  dominates. The gain expression for the circuit is (based on the degenerated CE analysis)

$$\frac{v_{o1}}{v_i} \approx -\frac{g_{m1} \cdot R_1 // r_{be3}}{2} \quad (1)$$

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- To maximise gain make both  $R_1$  and  $r_{be3}$  as big as possible.
- Could try to increase  $g_{m1}$  however, since  $g_{m1} = \frac{e I_{C1}}{k T}$  increasing  $g_{m1}$  would require an increase of  $I_{C1}$ .  $I_{C1}$  can't change without decreasing  $R_1$  in order to maintain the DC conditions of  $I_{C1} R_1 = 0.7 \text{ V}$ . There is no advantage in trying to increase  $g_{m1}$  to yield a larger gain. Other factors such as base currents and frequency dependent behaviour would also be affected.

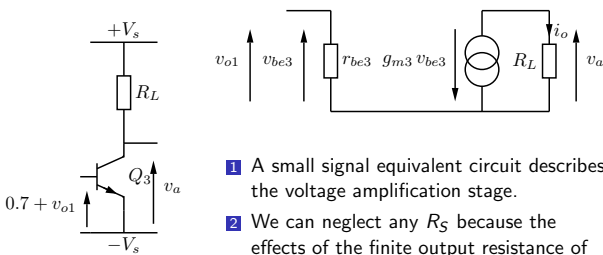
The input resistance of the circuit is given by

$$r_i = r_{be1} + (\beta_1 + 1) r_{e2} \quad (2)$$

which is similar to the common emitter amplifier *with* degeneration. If  $I_{C1} \approx I_{C2}$  and  $\beta_1 \approx \beta_2$  i.e.  $Q_1$  and  $Q_2$  are balanced and identical,  $r_i = 2 r_{be1}$ .

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## Voltage Amplifier Stage



The VAS is a non-degenerated common emitter circuit.

- 1 A small signal equivalent circuit describes the voltage amplification stage.
- 2 We can neglect any  $R_S$  because the effects of the finite output resistance of the differential stage have already been taken into account - we included  $r_{be3}$  in our earlier calculations.
- 3  $v_{o1}$  and  $v_{be3}$  are equal.

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## Voltage Amplifier Stage Gain

The resistance a small signal sees looking out from  $Q_3$ 's collector is the parallel combination of:

- 1 The input resistance of  $Q_4$ ,  $r_{i4}$ .
- 2 The input resistance of  $Q_5$ ,  $r_{i5}$ .
- 3 The Early resistance of  $Q_3$ ,  $r_{ce3}$ .
- 4 The resistor  $R_{VA}$ .

$R_{VA}$  is much smaller than any of the others and so dominates the value of  $R_L$ .  $R_L \approx R_{VA}$ .

Some standard analysis...

$$v_a = i_o R_L \quad (3)$$

$$i_o = -g_{m3} v_{be3} \quad (4)$$

$$\text{so } v_a = -g_{m3} v_{be3} R_L \quad (5)$$

$$\text{but } v_{be3} = v_{o1} \quad (6)$$

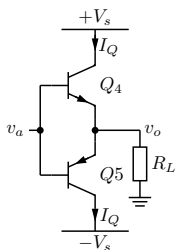
$$\text{so } v_a = -g_{m3} v_{o1} R_L \quad (7)$$

$$\frac{v_a}{v_{o1}} = -g_{m3} R_L \quad (8)$$

For typical values the gain of the voltage amplifier stage when  $R_{VA}$  is a resistor is a few hundred.

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## The Output Stage

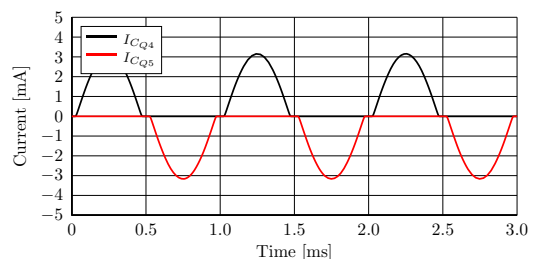


An NPN and PNP emitter follower.

- The output stage operates on "large" signals.
- $Q_4$  deals with positive currents - from  $+V_s$  into the ground via  $R_L$
- $Q_5$  deals with negative currents - from the ground via  $R_L$  into  $-V_s$
- The signals are "large" because the quiescent current  $I_Q$  is *not* many times bigger than the signal currents.
- The signal currents upset the quiescent conditions. It is not fruitful to draw a small signal diagram.

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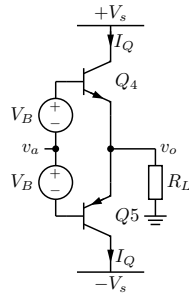
- The voltage gain of the output stage is approximately unity.
- The objective of the output stage is to increase the VAS's ability to drive current into the load resistance.
- The combination of the VAS and OPS provide power gain.
- The transistors must be turned on by the signal, consequently a kind of distortion - "Crossover Distortion" exists around the transition between  $Q_4$  conduction and  $Q_5$  conduction.



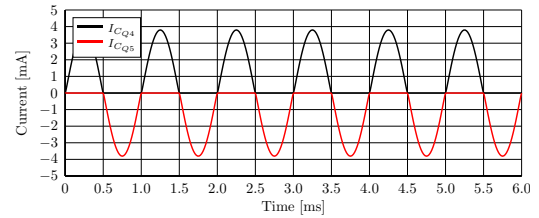
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## Biasing the Output Stage

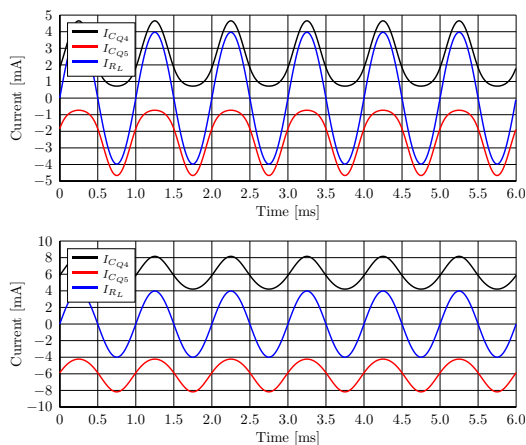
- Biasing the transistors into conduction can lessen the effect of crossover distortion a great deal.
- It also allows us to think about the relationship between the quiescent current and the signal current in the push pull stage.
- These thoughts can be widely generalised.
- Consider five sets of  $V_B$  which yield differing "angles of conduction".
- Without any bias each transistor conducts for slightly less than  $1/2$  a cycle  $< 180^\circ$



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## Review

- Reviewed structure of the Opamp.
- Considered DC conditions of the input and voltage amplifier stages.
- Described the gain and input resistance of the input stage to a differential signal.
- Analysed the voltage amplification stage from a small signal perspective.
- Qualitatively described the push-pull emitter follower output stage.
- Introduced the idea of "classes" of amplifier and "conduction angle".
- Noted that the relative size of the quiescent current and the signal current will determine the conduction angle and so the class of amplifier.

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