



## DEPARTMENT OF ELECTRONIC AND ELECTRICAL ENGINEERING

**Autumn Semester 2009-2010 (2 hours)** 

**Introduction to Avionics 6** 

Answer THREE questions. No marks will be awarded for solutions to a fourth question. Solutions will be considered in the order that they are presented in the answer book. Trial answers will be ignored if they are clearly crossed out. The numbers given after each section of a question indicate the relative weighting of that section.

1.

- **a.** Give a brief description of task automation avionic systems. (6)
- **b.** Give a brief description of an air data system. (6)
- c. The true airspeed of a certain aircraft flying in the troposphere region is  $V_T = 560$  km/h, the static air temperature is  $T_S = -34.5$  °C and the static pressure is  $P_S = 37.65$  kPa:
  - i. Calculate the Mach number M.
  - ii. Calculate the altitude of the aircraft.
  - iii. Calculate the air density  $\rho$ .
  - iv. Calculate the calibrated airspeed  $V_c$ . (8)

## The following may be assumed:

Gas constant for unit mass of dry air :  $R_a = 287.0529 \text{ J/}^{\circ} \text{K}$ .kg

Impact pressure = 
$$P_0 \left( \left( 1 + \frac{(\gamma - 1)(V_c/A_0)^2}{2} \right)^{\gamma/(\gamma - 1)} - 1 \right)$$
 and

$$\frac{P_T}{P_s} = \left(1 + \frac{(\gamma - 1)}{2}M^2\right)^{\frac{\gamma}{(\gamma - 1)}}$$

 $\gamma = \frac{\text{specific heat of air at constant pressure}}{\text{specific heat of air at constant volume}}$  and  $P_T$  is the total pressure.

At sea level: the static pressure  $P_0 = 101.325$  kPa, the absolute static air temperature is  $T_0 = 288.15$  °K, the air density  $\rho_0 = 1.225$  kg/m<sup>3</sup> and the speed of sound  $A_0 = 340.3$  m/s.

2.

b.

- **a.** Sketch a figure illustrating the main components of a MIL STD 1553B data bus system (5) and summarise its main features.
  - Summarise the main advantages of a Fly-By-Wire flight control system, and sketch a (6)

(9)

- figure illustrating its essential features. **c.** The typical failure rate of a Fly-By-Wire channel is  $\lambda = 3.35 \times 10^{-4}$  /hour. Therefore, in order to meet stricter reliability requirements, an *n* Fly-By-Wire channel redundancy configuration is usually employed. Calculate the probability of failure of the redundancy
  - i. When n = 3 and a majority voting scheme is adopted.
  - ii. When n = 4 and a non-adaptive majority voting scheme is adopted.
  - iii. When n = 4 and an adaptive majority voting scheme is adopted.

*The following may be assumed:* 

configuration during a 10-hour flight:

Reliability function for <u>m-out-of-n system (active):</u>

$$R(t) = \sum_{k=m}^{n} \frac{n!}{k!(n-k)!} \left[ e^{-\lambda kt} \right] \left[ 1 - e^{-\lambda t} \right]^{n-k}$$

Reliability function for <u>m-out-of-n system (passive)</u>:  $R(t) = e^{-\lambda mt} \sum_{k=m}^{n} \frac{(m \lambda t)^{k-m}}{(k-m)!}$ 

**3.** 

- **a.** Describe what is meant by the term 'System Type' and the effect it has on the steady-state error of the resulting closed-loop system for step, ramp and parabolic inputs.
- (6)

**(6)** 

**(4)** 

**b.** Figure 3.1 shows a dynamic model of a remote camera positioning system. The system is controlled using only a proportional compensator,  $K_p$ .

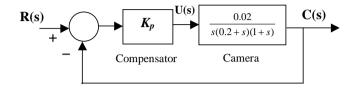


Figure 3.1: Remote camera positioning system

For the system shown in Figure 3.1, determine the value of  $K_p$  to provide an open-loop Phase Margin of 45°, by following the steps below:

- (i) Using asymptotes as an aid, construct the Bode plot of the open-loop plant transfer function  $\frac{0.02}{s(0.2+s)(1+s)}$ .
- (ii) From the Bode plot estimate the value of  $K_p$  which is required to provide a Phase Margin of 45°. Estimate the resulting closed-loop bandwidth of the system with this value of  $K_p$ .
- (iii) If a gain of  $K_p = 100$  were selected, what Gain Margin and Phase Margin would the system possess? Will the system be stable or unstable? (4)

**ENSURE YOUR BODE DIAGRAM IS ATTACHED TO YOUR ANSWER BOOKLET** 

**(7)** 

4.

A spacecraft has the short-period dynamic behaviour characterised by the state-variable description in the equation below, where  $\delta_f(t)$  is the perturbed control fin deflection,  $\tau(t)$  is the tilt angle, and r(t) is the roll rate.

$$\begin{bmatrix} \dot{\tau} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} -0.32 & 1 \\ -3.70 & -0.48 \end{bmatrix} \begin{bmatrix} \tau \\ r \end{bmatrix} + \begin{bmatrix} -0.03 \\ -2.80 \end{bmatrix} \delta_f$$

Or:  $\dot{x} = Ax + B u$ 

where: 
$$x = \begin{bmatrix} \dot{\tau} \\ \dot{r} \end{bmatrix}$$
,  $A = \begin{bmatrix} -0.32 & 1 \\ -3.70 & -0.48 \end{bmatrix}$ ,  $B = \begin{bmatrix} -0.03 \\ -2.80 \end{bmatrix}$ , and  $u = \delta_f$ 

- a. Calculate the Eigenvalues of the open-loop system in above equation, and thereby suggest why the spacecraft may need the addition of a control system to provide adequate flying qualities. (5)
- **b.** Calculate the Controllability Matrix, *C*, and thereby show that the spacecraft is fully controllable. (3)
- **c.** Using Ackermann's method, design a state-feedback controller u = -k x, such that the resulting closed loop system has Eigenvalues at:

$$\lambda_1 - 1.95 + j2.49$$
  
 $\lambda_2 - 1.95 - j2.49$ 

That is, calculate an appropriate state-feedback gain matrix, k

**d.** Sketch the block diagram structure of the resulting closed loop system — include appropriate integrators, states and the controller gain terms. (5)

KA / KM