

## Worked Solutions to Problems in Tutorial Sheet 3

1. (i)  $\mu_r = 1$ ,  $\rho = 1.72 \times 10^{-8} \Omega m$

$$\therefore \sigma = \frac{1}{1.72 \times 10^{-8}} = 58.1 \times 10^6 \text{ Sm}$$

$$\therefore \delta = \sqrt{\frac{2}{\omega \mu \sigma}} = \sqrt{\frac{2}{314.2 \times 4\pi \times 10^{-7} \times 58.1 \times 10^6}} = 9.34 \text{ mm}$$

(ii)  $\mu_r = 2000$ ,  $\rho = 2.8 \times 10^{-7} \Omega m$

$$\therefore \sigma = 3.57 \times 10^6 \text{ Sm}$$

$$\therefore \delta = \sqrt{\frac{2}{314.2 \times 2000 \times 4\pi \times 10^{-7} \times 3.57 \times 10^6}} = 0.84 \text{ mm}$$

**NOTE:** Even though mild steel is ~16 times less conducting than copper, the skin effect is significantly more pronounced due to its high relative permeability.

2.  $J_x = J_s e^{\alpha y} = \alpha H_s e^{\alpha y}$

Eddy current loss  $P_e = \frac{H_s^2}{2\sigma\delta} w / m^2$

Since skin depth  $\delta \ll$  radius of conductor, thick plate model is a reasonable representation of the circular conductor of radius  $a$

$\therefore$  From Amperes Law,  $H_s = \frac{I}{2\pi a} \text{ A/m}$

$\therefore$  Loss/unit area  $= \left( \frac{I}{2\pi a} \right)^2 \frac{1}{2\sigma\delta} w / m^2$

Loss/m length of conductor  $= \left( \frac{I}{2\pi a} \right)^2 \frac{1}{2\sigma\delta} 2\pi a w / m$

where  $I$  is the peak ac current

$\therefore$  Loss/m length of conductor  $= \frac{1}{2} I^2 R_{ac} w / m$

$$\therefore R_{ac} = \frac{1}{2\pi a \sigma \delta} \Omega / m$$

For  $f = 20 \times 10^3$  Hz

$$a = 2 \times 10^{-3} \text{ m}$$

$$\sigma = \frac{1}{1.72 \times 10^8}$$

$$R_{ac} = 2.9 \times 10^{-3} \Omega/\text{m}$$

$$R_{dc} = \frac{1}{\sigma \pi a^2} = 1.37 \times 10^{-3} \Omega/\text{m}$$

$$\therefore \frac{R_{ac}}{R_{dc}} = 2.11$$