

[Q3a]

$$(i) \quad V^- = V_{out} \frac{R_2}{R_1 + R_2} \quad \& \quad V^+ = V_{in}$$

$$V_{out} = A_v (V^+ - V^-)$$

$$V_{out} + A_v V_{out} \frac{R_2}{R_1 + R_2} = A_v V_{in}$$

$$\frac{V_{out}}{V_{in}} = \frac{A_v}{1 + A_v \frac{R_2}{R_1 + R_2}} = \frac{1}{\frac{1}{A_v} + \frac{R_2}{R_1 + R_2}}$$

$$A_v = \frac{A_o}{1 + \frac{j\omega}{\omega_o}}$$

$$\frac{V_{out}}{V_{in}} = \frac{1}{1 + \frac{j\omega}{\omega_o} + \frac{R_2}{A_o}}$$

$$\frac{V_{out}}{V_{in}} = \frac{1}{\frac{1}{A_o} + \left(\frac{j\omega}{\omega_o A_o} \right) + \frac{R_2}{(R_1 + R_2)}}$$

$$\frac{V_{out}}{V_{in}} \approx \frac{\frac{(R_1 + R_2)}{R_2}}{1 + \left(\frac{j\omega}{\omega_o A_o} \right) \left(\frac{(R_1 + R_2)}{R_2} \right)} = \frac{k}{1 + \frac{j\omega}{\omega_1}}$$

(5 marks)

$$(ii) \quad \text{dc gain} = k = \frac{R_1 + R_2}{R_2}$$

$$\text{dc gain} = \frac{1 \times 10^3 + 100 \times 10^3}{1 \times 10^3} = 101 \text{ V/V}$$

$$\text{gain-bandwidth product} = f_0 \times A_0 = f_1 \times k$$

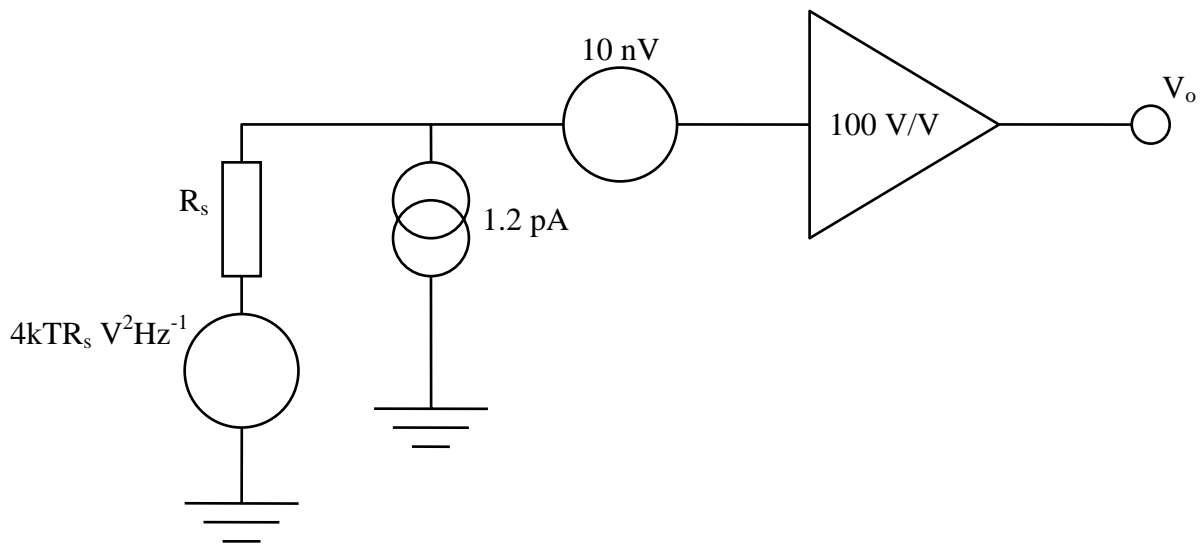
$$50 \times 10^6 = f_1 \times 101$$

$$f_1 = \frac{50 \times 10^6}{101} = 495 \text{ kHz}$$

(5 marks)

[Q3b]

(i)



$$\text{Noise factor} = \frac{\text{Noise power at output of real amplifier}}{\text{Noise power at output of ideal version of amplifier}}$$

$$\text{Noise factor} = \frac{\left[4kTR_s + (1.2\text{pA} \times R_s)^2 + (10\text{nV})^2 \right] \times 100^2}{4kTR_s \times 100^2}$$

$$\text{Noise factor} = \frac{\left[24.8 \times 10^{-18} + 3.24 \times 10^{-18} + 100 \times 10^{-18} \right] \times 100^2}{24.8 \times 10^{-18} \times 100^2}$$

$$\text{Noise factor} = 5.16$$

(5 marks)

(ii)

$$\text{Noise at amplifier output} = \left[4kTR_s + (1.2\text{pA} \times R_s)^2 + (10\text{nV})^2 \right] \times 100^2 \times 20 \text{ kHz}$$

$$\text{Noise at amplifier output} = [24.8 + 3.24 + 100] \times 10^{-18} \times 100^2 \times (20 \times 10^3)$$

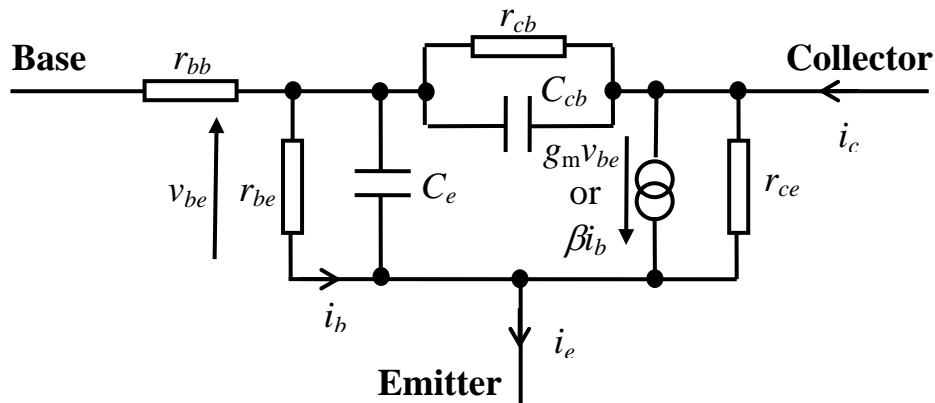
$$\text{Noise at amplifier output} = 2.56 \times 10^{-8} \text{ V}^2$$

$$\text{rms reading} = \sqrt{2.56 \times 10^{-8}} = 160 \text{ } \mu\text{V}$$

(5 marks)

[Q4a]

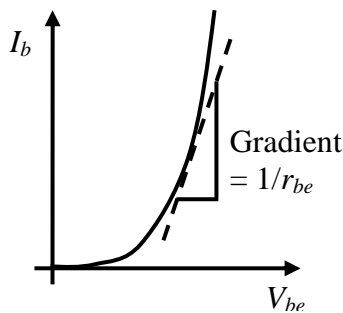
Small signal circuit for a BJT – The hybrid π model



The origins of these circuit elements are as follows:-

r_{bb} – The ‘base spreading resistance’, this is the series resistance between the package wire and the active part of the semiconductor material. Typically $0.5\Omega < r_{bb} < 50\Omega$, and can be ignored in most cases.

r_{be} – Base incremental resistance of the base emitter junction ($\propto 1/I_c$).



r_{bc} – Feedback resistance modelling the Early effect* ($\propto 1/I_c$). Can usually be ignored for analytical purposes, but **must** be considered if the transistor has a high impedance load.

r_{ce} – Models the small slope of the output characteristic, mostly due to the Early effect* ($\propto 1/I_c$). Again, can normally be ignored unless the transistor has a high impedance load.

C_{cb} – The base collector depletion capacitance ($\propto V_{cb}$).

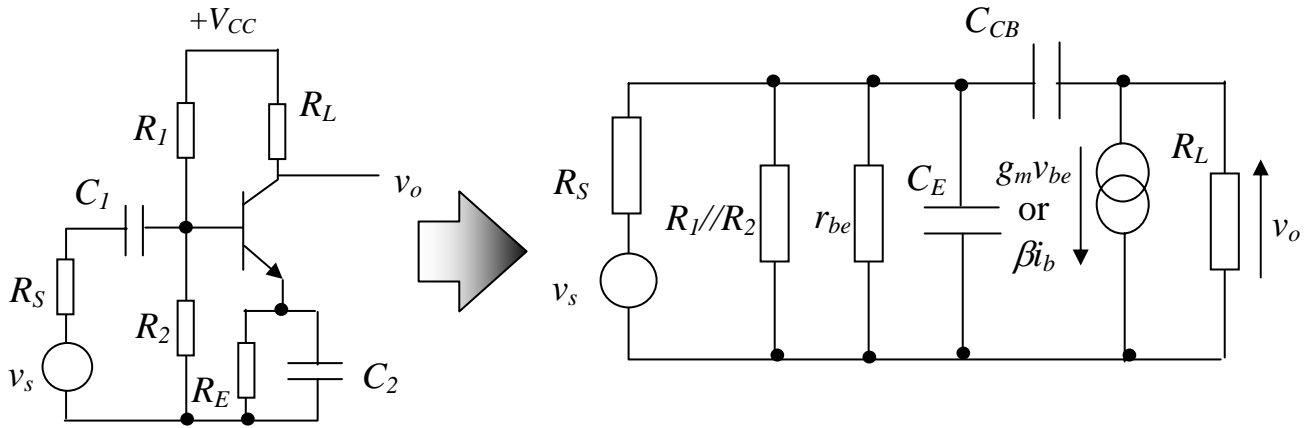
C_e – Emitter diffusion capacitance, models the transient behaviour of charge crossing a p-n junction.

(8 marks)

[Q4b]

(i)

Since it is likely that $R_L \gg r_{ce}$ and r_{bc} and $R_S \gg r_{bb}$, we shall ignore r_{bb} , r_{bc} and r_{ce} .



(2 marks)

in the mid frequency range:-

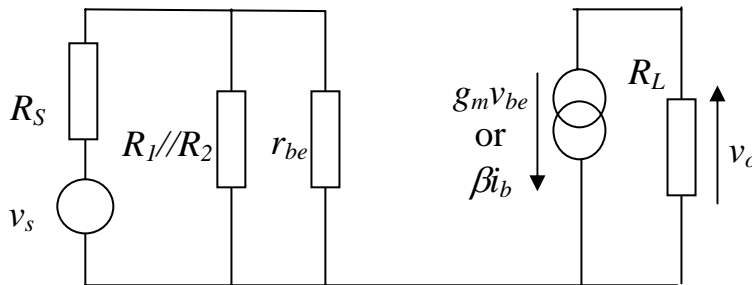
bypass capacitors C_1 and C_2 will be short circuits

(1 mark)

parasitic capacitances C_{cb} and C_e will be open circuits

(1 mark)

Hence the mid-frequency ss circuit is,



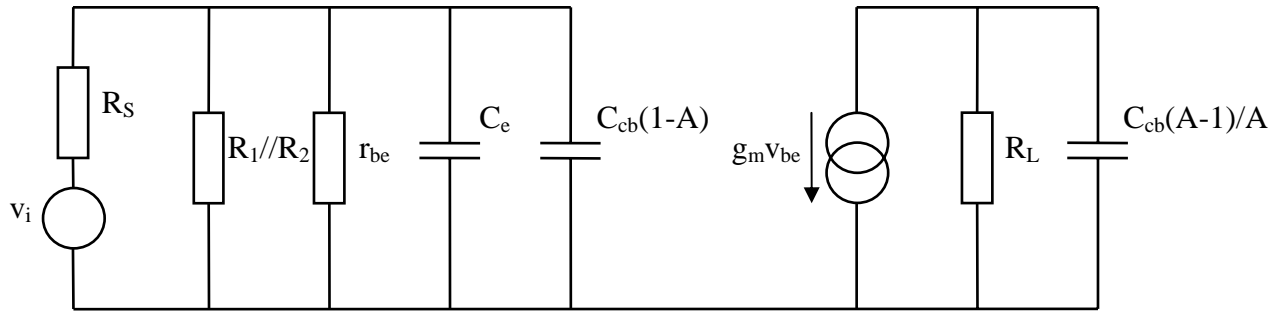
(1 mark)

The mid-frequency gain is thus,

$$A = \frac{v_o}{v_s} = \frac{v_s}{v_{be}} \frac{v_{be}}{v_o} = \frac{R_1 // R_2 // r_{be}}{R_1 // R_2 // r_{be} + R_S} (-g_m R_L)$$

(1 mark)

(ii)



(2 marks)

(iii)

$$A = -g_m R_L$$

$$A = -0.04 \times 5000 = -200$$

$$C_{cb}(1-A) = (5 \times 10^{-12}) \times 201 = 1 \text{ nF}$$

$$f_{upper,input} = \frac{1}{2\pi (R_S // R_1 // R_2 // r_{be})(C_e + C_{cb}(1-A))}$$

$$f_{upper,input} = \frac{1}{2\pi (10 \times 10^3 // 200 \times 10^3 // 100 \times 10^3 // 12 \times 10^3)(20 \times 10^{-12} + 1 \times 10^{-9})}$$

$$f_{upper,input} = 30.9 \text{ kHz}$$

$$f_{upper,output} = \frac{1}{2\pi R_L C_{cb} \frac{(A-1)}{A}}$$

$$f_{upper,output} = \frac{1}{2\pi (5 \times 10^3) \times 5 \times 10^{-12} \times \frac{201}{200}}$$

$$f_{upper,output} = \frac{1}{2\pi (5 \times 10^3) \times 5 \times 10^{-12} \times \frac{201}{200}}$$

$$f_{upper,output} = 6.33 \text{ MHz}$$

Therefore:-

$$f_{upper} = 30.9 \text{ kHz}$$

(4 marks)