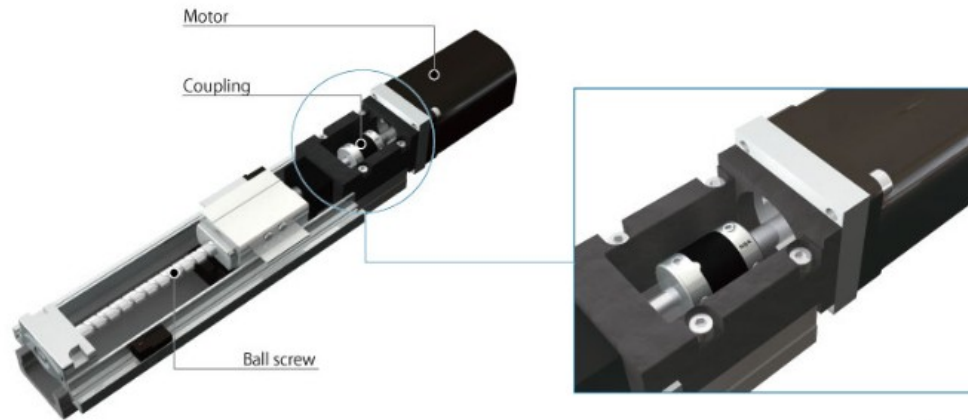


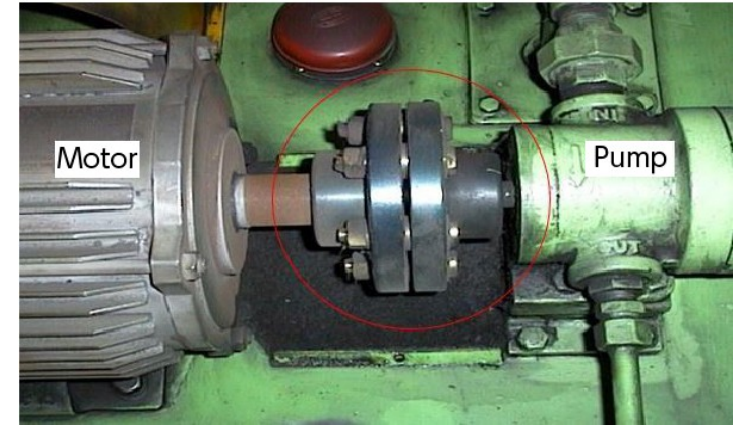
# Shaft Couplings

- To connect the driver shafts to the driven shafts
- To adjust for the misalignments of the shafts
- To reduce transmission of shock loads from one shaft to the other
- To provide protection against overloads



Motion control

<https://www.nbk1560.com/en/resources/coupling/article/powertransmission-about/>



Power transmission  
(strength, high torque)

Accuracy, zero backlash – high torsional stiffness

# Typed of Shaft Couplings

## Rigid Couplings

Connects two shafts that are perfectly aligned

Sleeve/Muff coupling

Clamp or compression coupling

Flange coupling

## Flexible Couplings

Connects two shafts that have lateral and/or

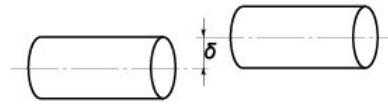
Angular **misalignment**

Bush type pin coupling

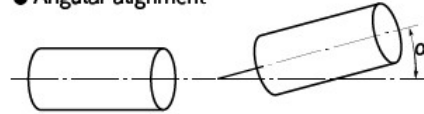
Universal coupling

Oldham coupling

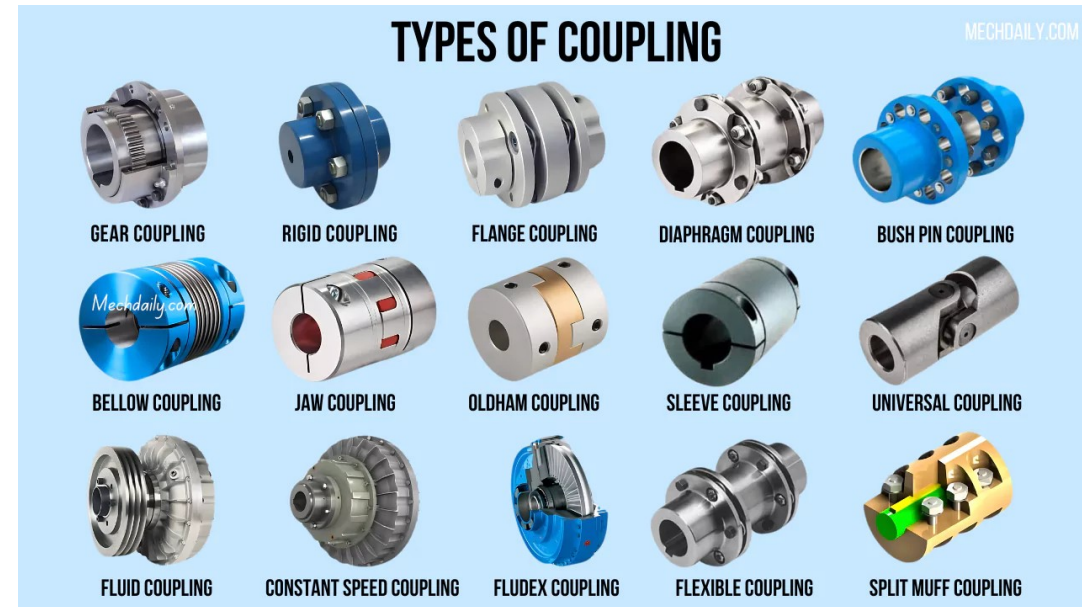
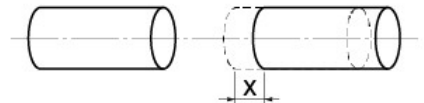
● Eccentricity



● Angular alignment

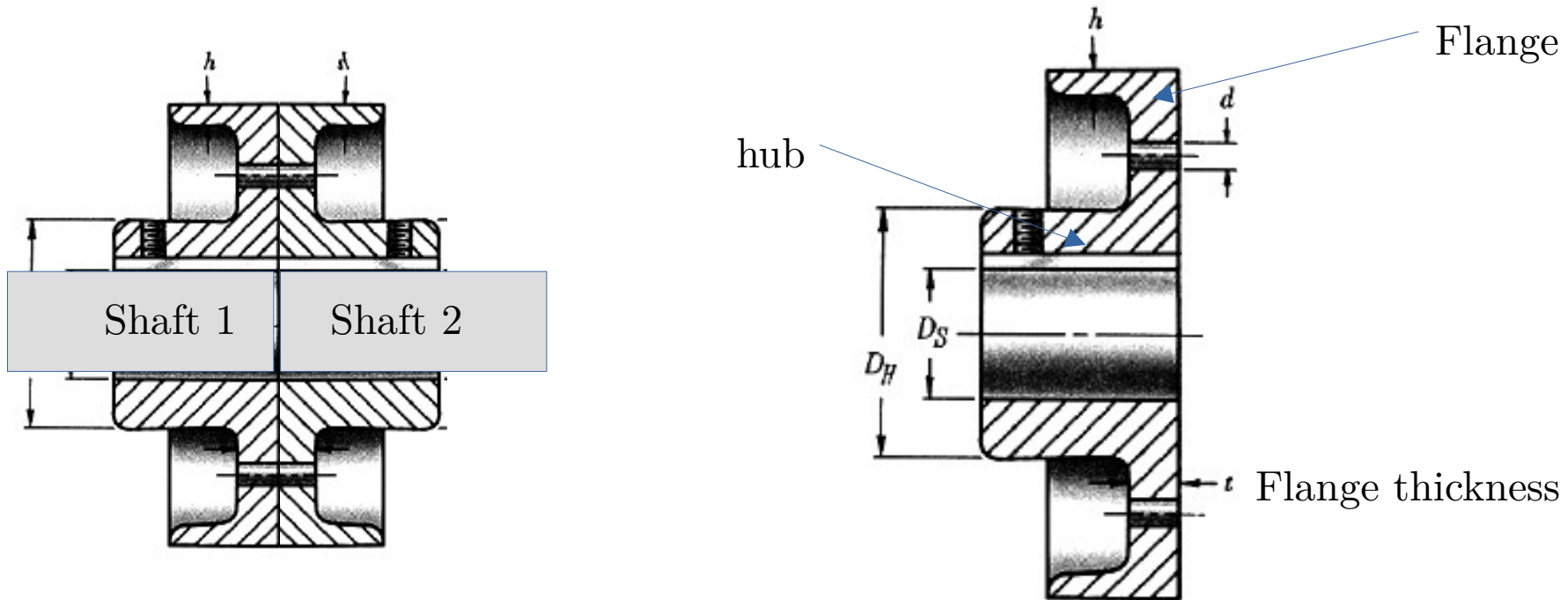


● End-play



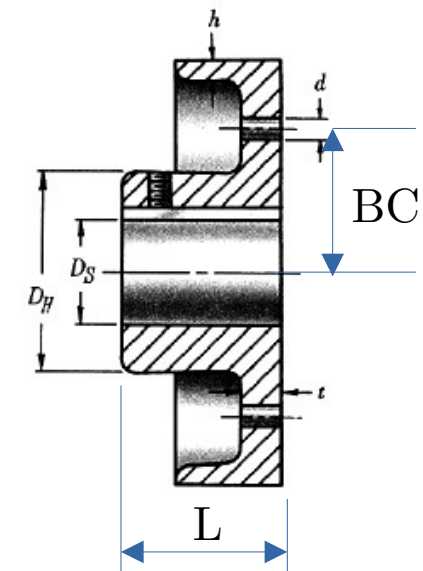
<https://www.mechdaily.com/what-is-coupling-and-types-of-coupling/>

# Design of Rigid Coupling - Nomenclature



# Design of Rigid Coupling

Consider the solid coupling shown in the figure. Assume that there are 6 bolts connecting the two flanges and that the load transfer takes place through the bolts. The shaft carries a steady load of 40 kW at 150 rpm. For all the parts, the yield stress in tension is 400 MPa and the yield stress in shear is 200 MPa. Identify the critical locations and find the factor of safety at each of the locations based on the yield stress. Assume  $D_S = 56$  mm,  $D_H = 108$  mm,  $t = 7$  mm,  $d = 8$  mm. The key dimensions are as follows:  $W = 16$  mm,  $T = 10$  mm,  $L = 90$  mm,  $BC = \underline{152}$  mm



## Critical Locations

Key – failure: shear stress, crushing stress

Bolts – failure: shear stress, crushing stress

Flange – failure: shear

Hub – failure: shear

# Design of Rigid Coupling

$$\begin{aligned}
 &P := 40 \text{ kW} \quad N := 6 \quad BC := 76 \text{ mm} \quad Wi := 16 \text{ mm} \quad Ds := 56 \text{ mm} \quad d := 8 \text{ mm} \\
 &w := 150 \text{ rpm} = 15.708 \frac{\text{rad}}{\text{s}} \quad Th := 10 \text{ mm} \quad Le := 90 \text{ mm} \quad t := 7 \text{ mm} \quad Dh := 108 \text{ mm} \\
 &y_{st} := 400 \text{ MPa} \quad y_{ss} := 200 \text{ MPa} \\
 &T := \frac{P}{w} = 2546.4791 \text{ N m}
 \end{aligned}$$

## Key calculations

$$\begin{aligned}
 F &:= \frac{T}{\left(\frac{Ds}{2}\right)} = 90945.6818 \text{ N} \\
 K_{ss} &:= \frac{F}{Wi \cdot Le} = 63.1567 \text{ MPa} \quad FOS1 := \frac{y_{ss}}{K_{ss}} = 3.1667 \\
 K_{bs} &:= \frac{F}{(Th \cdot 0.5 \cdot Le)} = 202.1015 \text{ MPa} \quad FOS2 := \frac{y_{st}}{K_{bs}} = 1.9792
 \end{aligned}$$

## Bolt Calculations

### Force carried by each bolt

$$Fb := \frac{T}{(6 \cdot BC)} = 5584.384 \text{ N}$$

### Shear stress in a bolt

$$B_{ss} := \frac{Fb}{\frac{\pi}{4} \cdot d^2} = 111.0978 \text{ MPa} \quad FOS3 := \frac{y_{ss}}{B_{ss}} = 1.8002$$

### Bearing stress in the bolt

$$B_{bs} := \frac{Fb}{t \cdot d} = 99.7211 \text{ MPa} \quad FOS4 := \frac{y_{st}}{B_{bs}} = 4.0112$$

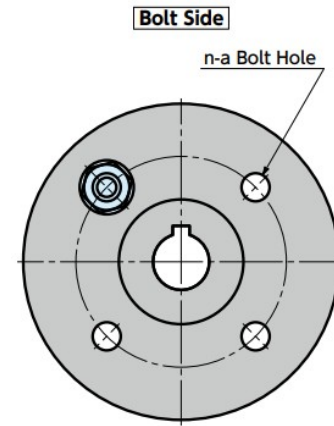
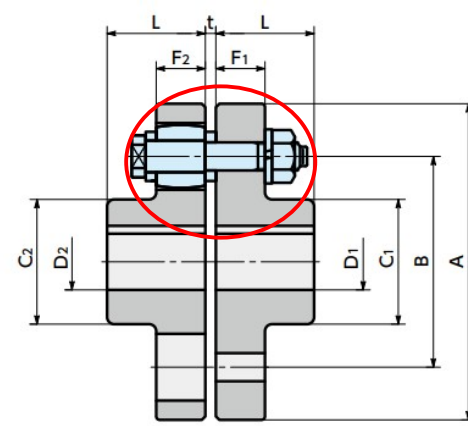
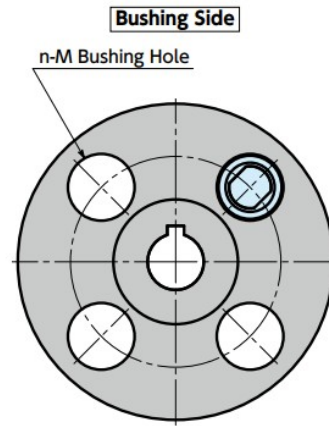
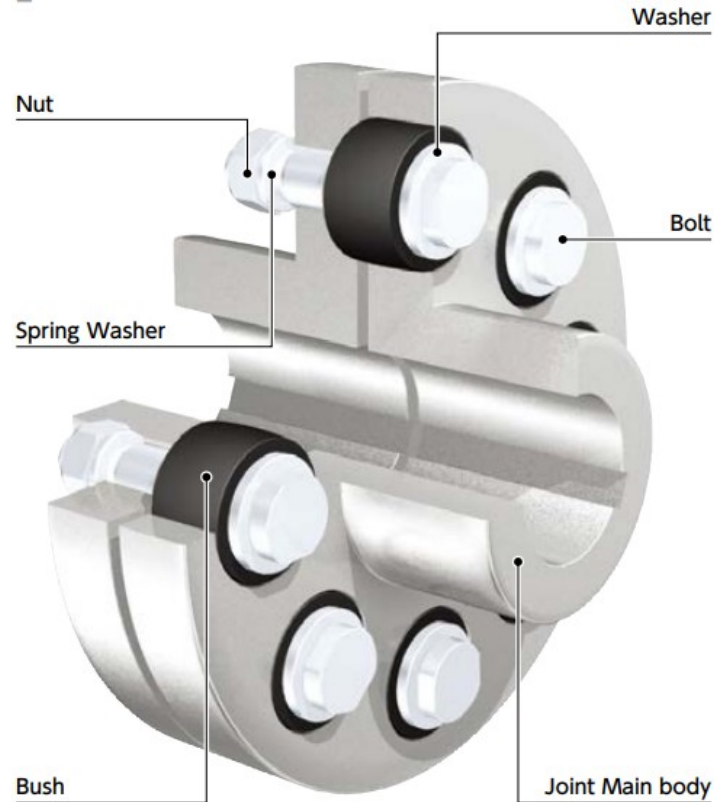
## Flange thickness Calculations

$$H_{ss} := \frac{T}{\pi \cdot 0.5 \cdot Dh^2 \cdot t} = 19.8552 \text{ MPa} \quad FOS5 := \frac{y_{ss}}{H_{ss}} = 10.0729$$

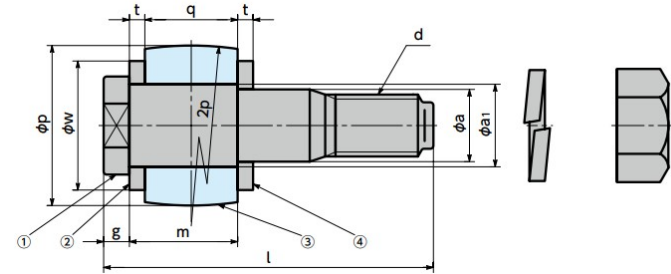
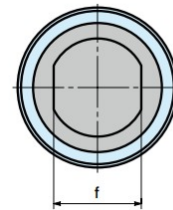
## Additional calculations:

$$(\tau_{max})_{hub} = \frac{TJ(D_H/2)}{G}, \quad J = \frac{\pi}{16}(D_H^4 - D_S^4)$$

# Design of Flexible Coupling (Bush-Pin Flexible Coupling)



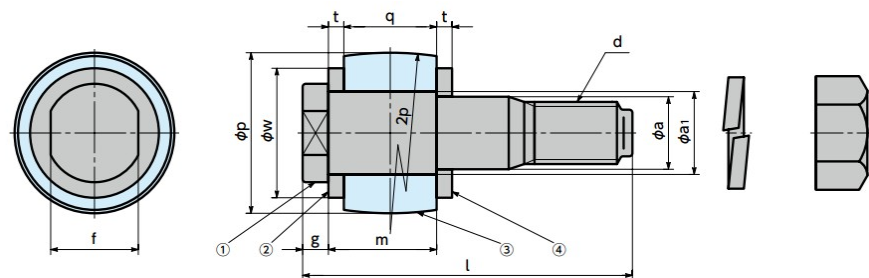
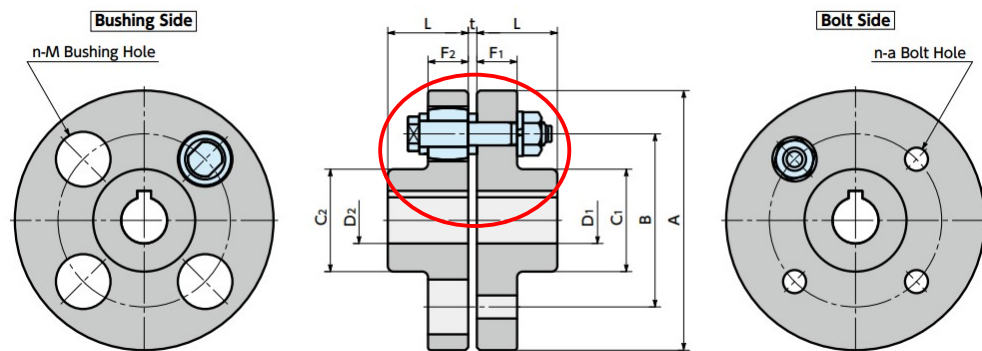
• The bolt hole positions are roughly arranged for the keyway.



<https://www.nbk1560.com/en/resources/coupling/article/powertransmission-about/>



# Design of Flexible Coupling (Bush-Pin Flexible Coupling)

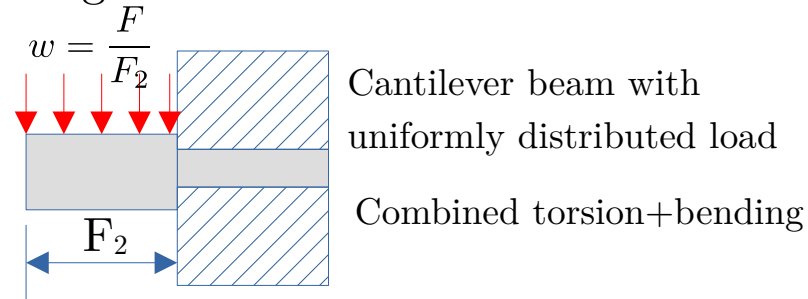


Additional calculations as compared to the rigid coupling:

- Flange thicknesses are not identical  $F_1 \neq F_2$  (independent calculations required)
- Bush failure – bearing pressure greater than permissible

$$p_{bush} = \frac{F}{F_2 d_{bush}}$$

- Bolt or Pin failure – check for combined bending and torsion

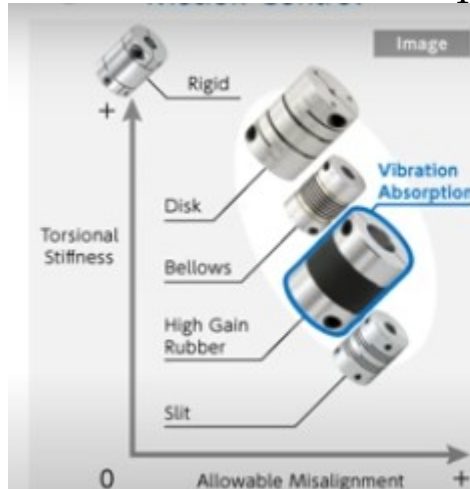


<https://www.nbk1560.com/en/resources/coupling/article/powertransmission-about/>

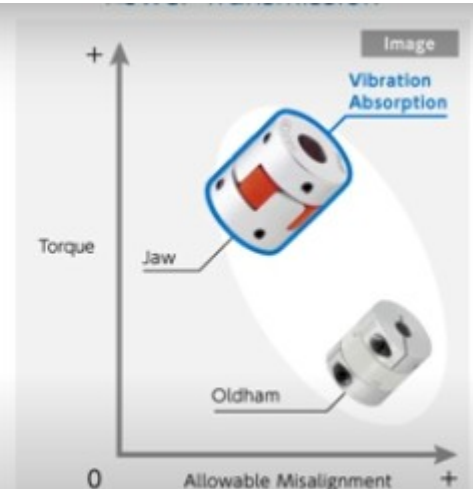
# Selection of Coupling

- **Type of coupling** – depends on features such as vibration absorption capacity, torque transmission, torsional stiffness, misalignment, ect
- **Material of the coupling** – depends on the environmental conditions
- **Size of the coupling** – torque transmission requirements, diameter of the shafts to be connected
- **Fastening method** – how to connect the coupling to the shaft

Motion control



Power transmission

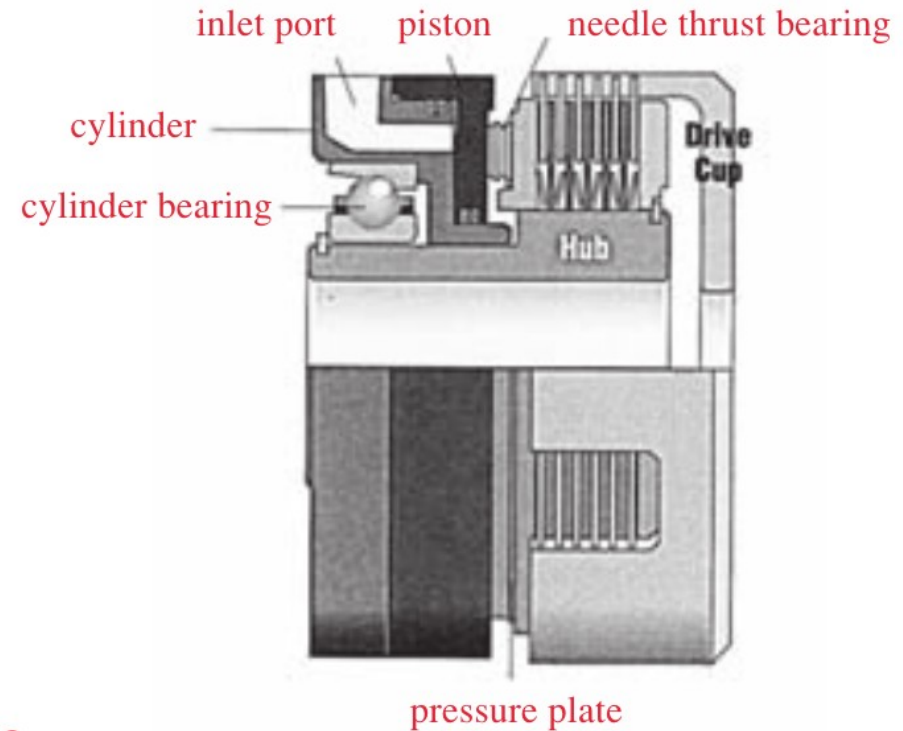
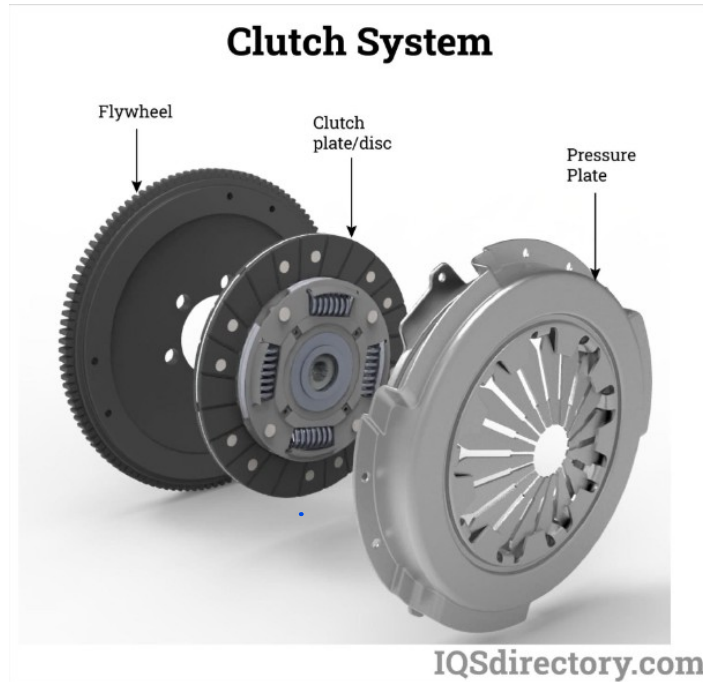




# Friction Disk Clutches

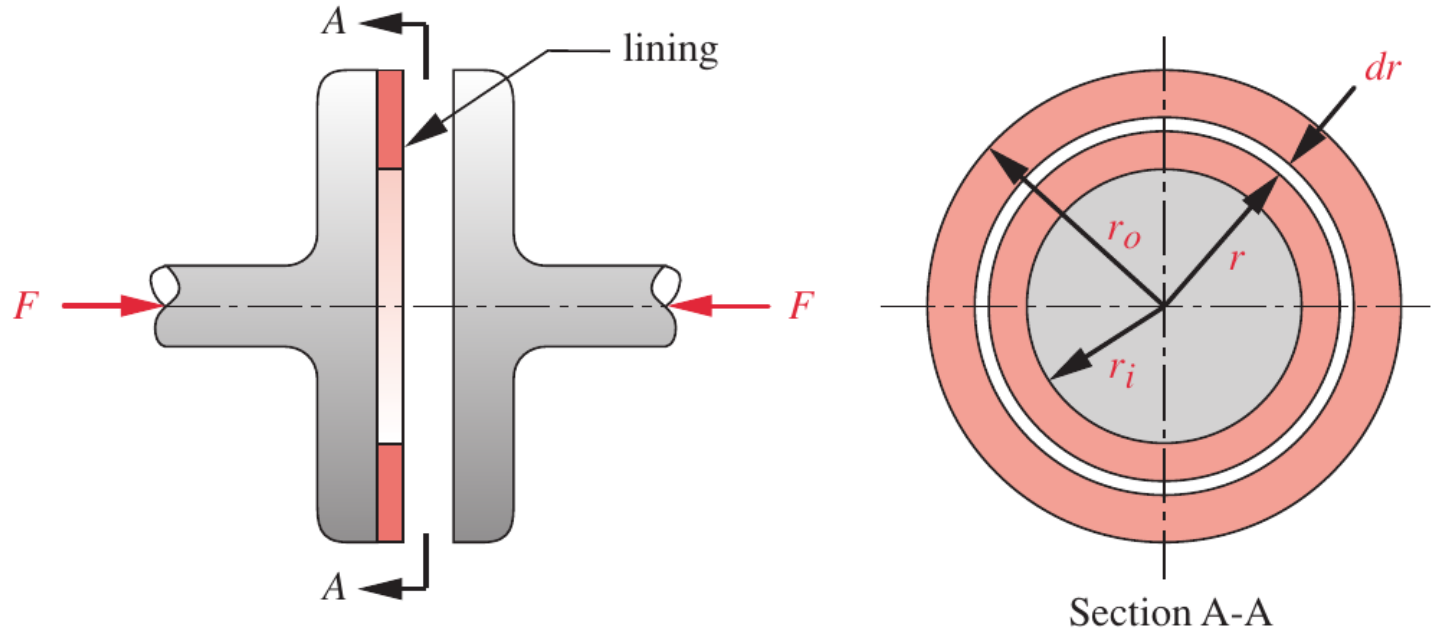
Couplings provide a permanent connection while clutches provide a temporary connection between the shafts

<https://www.youtube.com/watch?v=devo3kdSPQY>



<https://frictionmaterials.com/clutch-disc/>

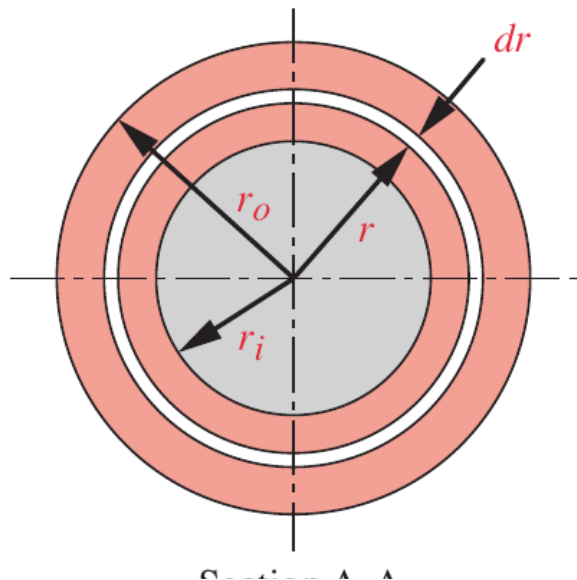
# Friction Disk Clutches



Disk clutch consists of two disks, one lined with a high-friction material, pressed together axially with a normal force to generate the friction force needed to transmit torque.

# Design of Friction Disk Clutches

**Uniform Pressure  $p_o$ .** It is assumed that a constant pressure  $p_o$  acts between the disk



The normal force acting on a ring of thickness  $dr$  at a distance  $r$  is

$$dN = 2\pi p_o r dr$$

Friction force acting on a ring of thickness  $dr$  at a distance  $r$  is

$$dF_r = \mu_f dN = 2\pi p_o \mu_f r dr \quad \mu_f \text{ is the coefficient of friction}$$

Torque transmitted through a ring of thickness  $dr$  at a distance  $r$  is

$$dT = r dF_r = 2\pi p_o \mu_f r^2 dr$$

Total torque transmitted through a disk with inner radius  $r_i$  and outer radius  $r_o$

$$T = \int_{r_i}^{r_o} dT = \frac{2}{3} \pi p_o \mu_f (r_o^3 - r_i^3)$$

Axial force acting on the disk

$$N = \int_{R_i}^{R_o} dN = \pi p_o (r_o^2 - r_i^2)$$

The torque expressed in terms of the axial force is given by

$$T = \frac{2}{3} \mu_f \frac{(r_o^2 + r_o r_i + r_i^2)}{r_i + r_o} N$$

# Design of Friction Disk Clutches

**Constant wear rate  $W$ .** It is assumed that the wear rate is constant over the contacting surfaces.

The wear rate  $W$  at a point is direction proportional to the pressure and the velocity at that point

$W = kpV = kpr\omega$  If the disk is rotating at a constant angular velocity, then  $pr_i = C$ , a constant

The pressure can be expressed in terms of the maximum pressure as:  $p = p_{max} \frac{r_i}{r}$

The normal force acting of a ring of thickness  $dr$  at a distance at  $r$  is

$$dN = 2\pi pr dr = 2\pi C dr = 2\pi p_{max} r_i dr$$

Friction force acting of a ring of thickness  $dr$  at a distance at  $r$  is

$$dF_r = \mu_f dN = 2\pi \mu_f p_{max} r_i dr$$

Torque transmitted through a ring of thickness  $dr$  at a distance at  $r$  is

$$dT = r dF_r = 2\pi \mu_f p_{max} r_i r dr$$

Total torque transmitted though a disk with inner radius  $r_i$  and outer radius  $r_o$

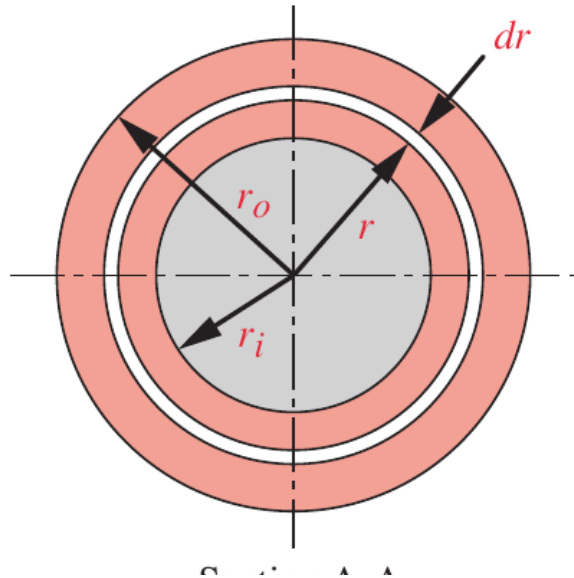
$$T = \int_{r_i}^{r_o} dT = \pi p_{max} \mu_f r_i (r_o^2 - r_i^2)$$

Axial force acting on the disk

$$N = \int_{R_i}^{R_o} dN = 2\pi p_{max} r_i (r_o - r_i)$$

The torque expressed in terms of of the axial force is given by

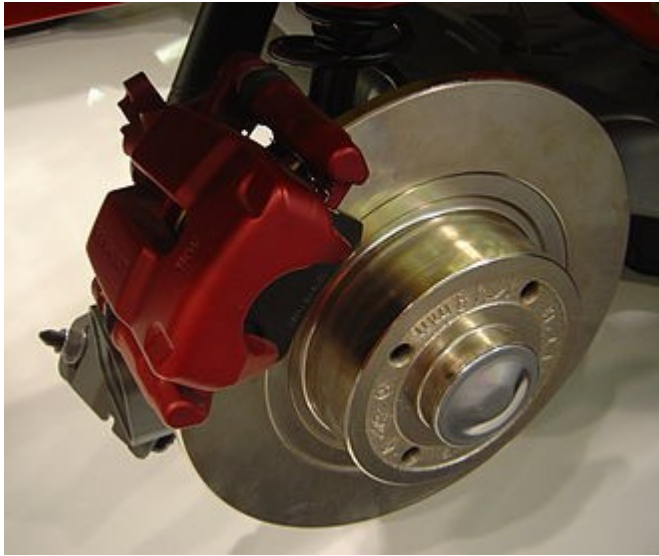
$$T = \frac{1}{2} \mu_f (r_o + r_i) N$$



# Design of Friction Disk Clutches

- The uniform-wear assumption gives a lower torque capacity for the clutch than does the uniform-pressure assumption.
- Clutches are usually designed based on uniform wear.
- A clutch may be close to a uniform-pressure condition when new, but will tend toward a uniform-wear condition with use. As a result, they will have a greater capacity when new but will end up close to the predicted design capacity after they are worn in.

# Disk Brakes



[https://en.wikipedia.org/wiki/Disc\\_brake](https://en.wikipedia.org/wiki/Disc_brake)

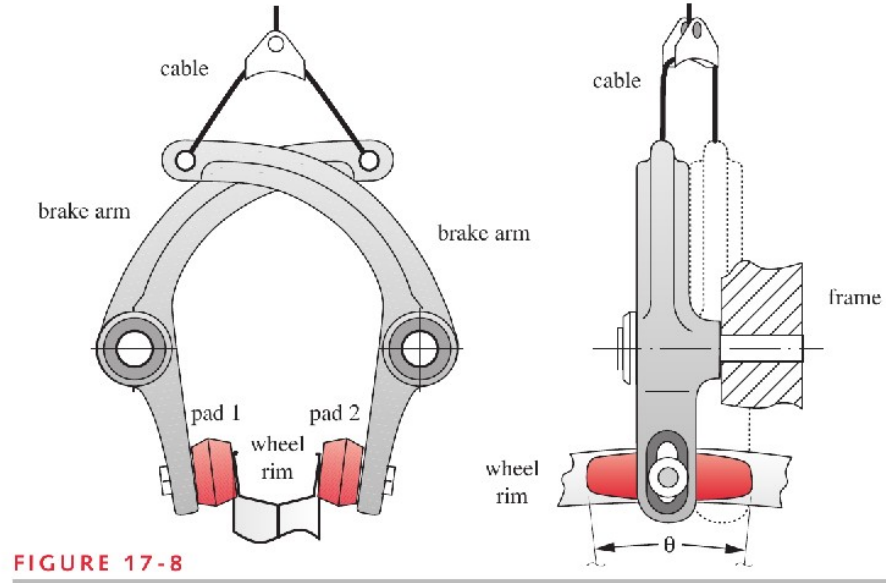
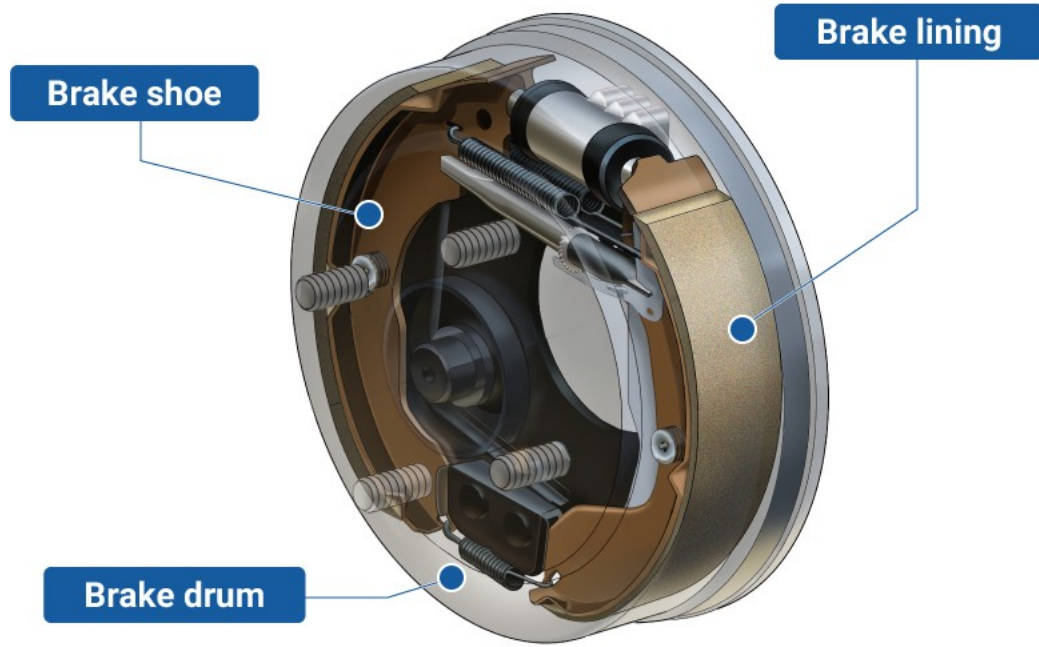


FIGURE 17-8

- The disk clutch equations also apply to disk brakes.
- Disk brakes are rarely made with linings covering the entire circumference of the face, because they would then overheat. Need to use the appropriate value of  $\theta$  for the included angle of the brake pads in equation.
- In addition, there will be at least **two** braking surfaces



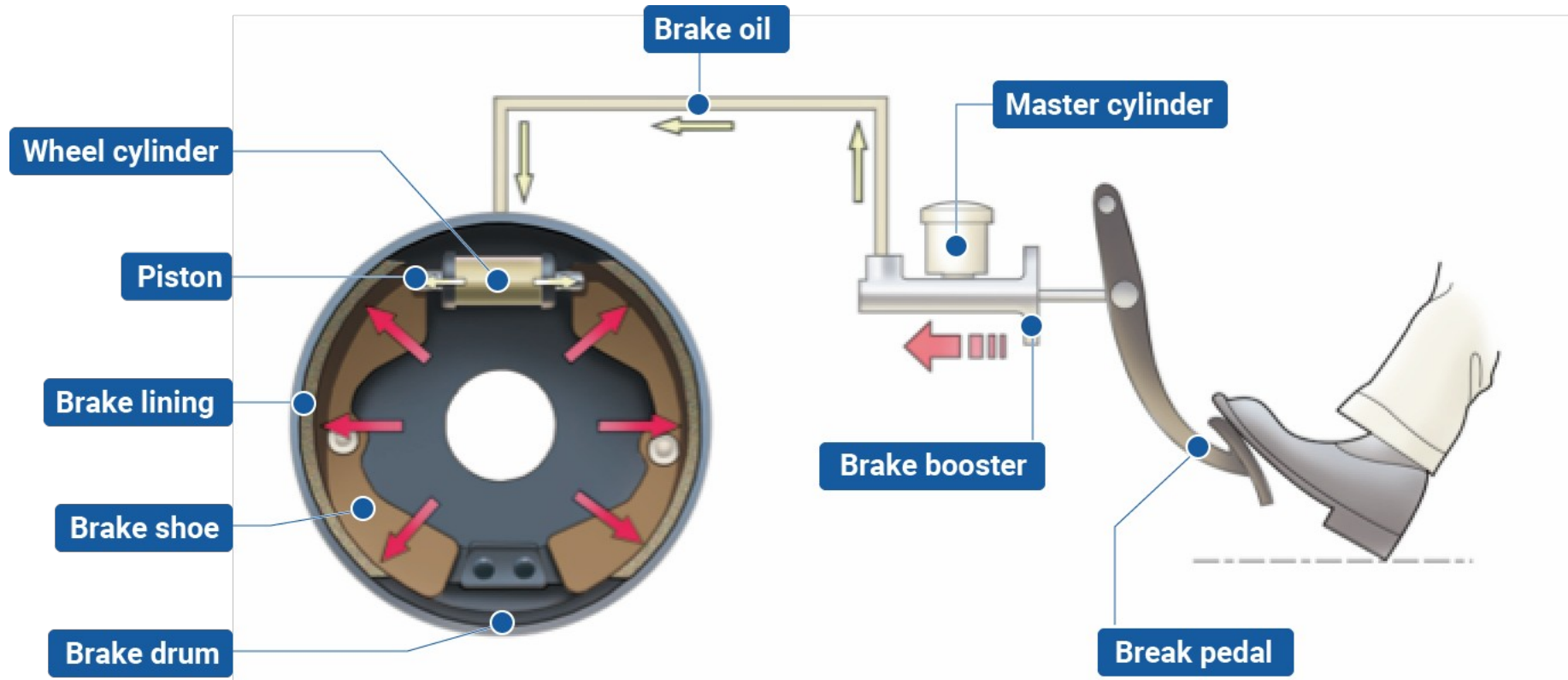
# Design of Drum Brakes



- Drum brakes apply the friction force to the circumference of a cylinder, either externally, internally, or both.
  - The part to which the friction material is riveted or bonded with adhesive is called the brake shoe
  - The part against which the brake shoe rubs is called the brake drum.
- The shoe is forced against the drum to create the friction torque.

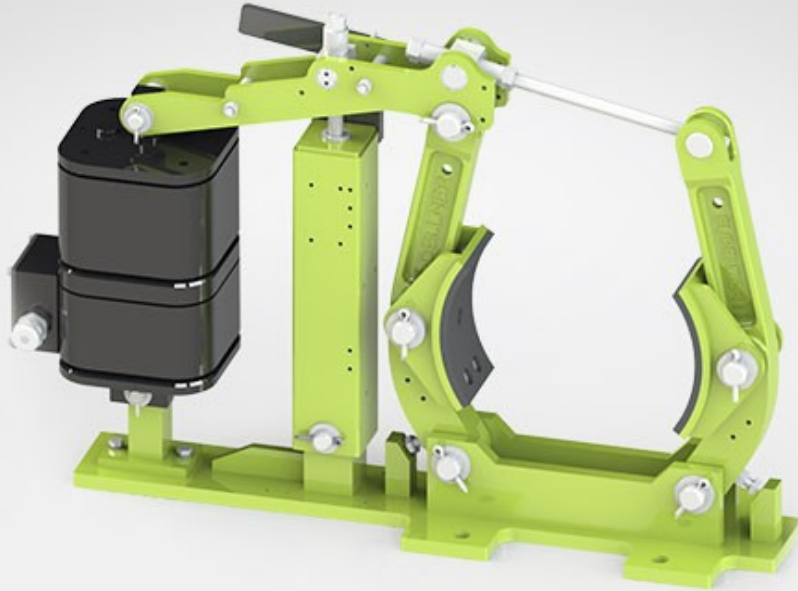
[https://www.akebono-brake.com/english/product\\_technology/product/automotive/drum/](https://www.akebono-brake.com/english/product_technology/product/automotive/drum/)

# Braking System in a Car with Drum Brake



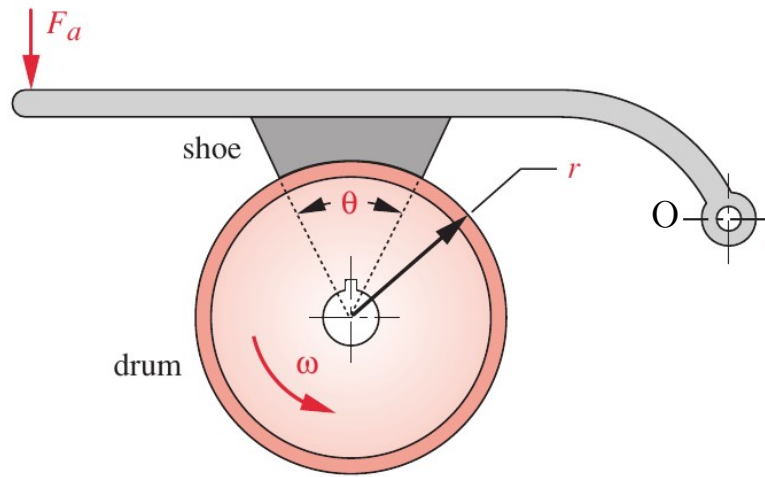
[https://www.akebono-brake.com/english/product\\_technology/product/automotive/drum/](https://www.akebono-brake.com/english/product_technology/product/automotive/drum/)

# External Drum Brake and Band Brake

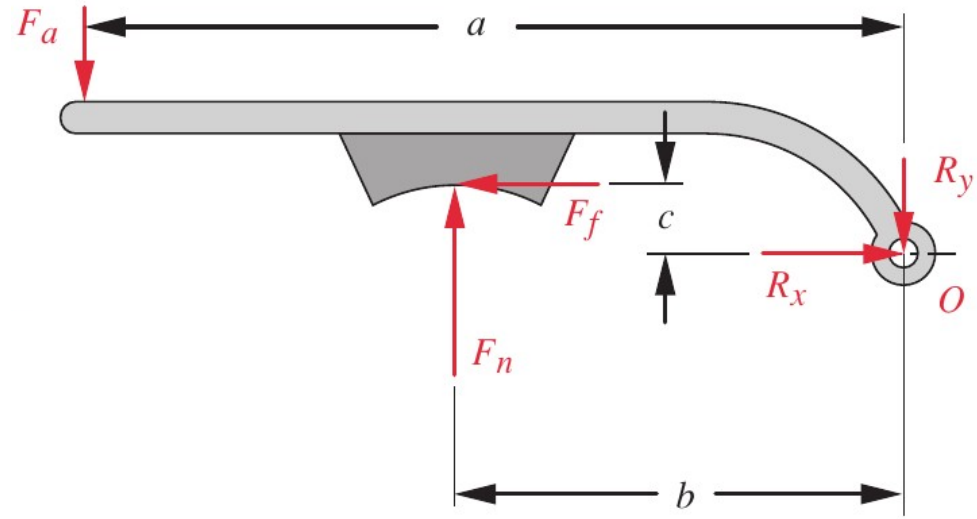


<https://www.dellnerbubenzner.com/product-types/drum-band-brakes>

# Short Shoe External Drum Brake



(a) Brake assembly



Free body diagram

Because the angle is small, we assume that the contact area is symmetric as shown and that the pressure is uniform over the contact area

Then  $F_n = p_o r \theta w$   $F_f = \mu_f F_n$

Taking moment about point

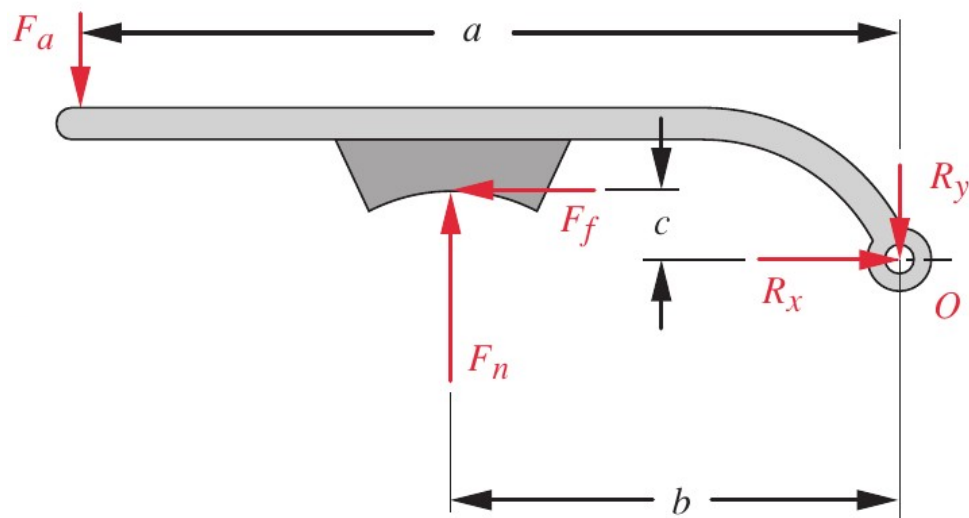
$$\sum M_o = 0$$

$$aF_a + cF_f - bF_n = 0$$

$$aF_a + c\mu_f F_n - bF_n = 0$$

$$F_a = F_n \frac{b - c\mu_f}{a}$$

# Short Shoe External Drum Brake



Free body diagram

Because the angle is small, we assume that the contact area is symmetric as shown and that the pressure is uniform over the contact area

Then  $F_n = p_o r \theta w$   $F_f = \mu_f F_n$

Taking moment about point

$$\sum M_o = 0$$

$$aF_a + cF_f - bF_n = 0$$

$$aF_a + c\mu_f F_n - bF_n = 0$$

$$F_a = F_n \frac{b - c\mu_f}{a}$$

## Self energizing brake

- Moment due to the frictional force acts in the same direction as that due to the applied force
- Less applied force is required to stop the rotating part

## De-energizing brake

- Moment due to the frictional force acts in the opposite direction as that due to the applied force

## Self locking brake

- For a self energizing brake if  $b \leq c\mu_f$  then  $F_a$  needed to actuate the brake becomes zero or negative
- If the shoe touches the drum, it will grab it and lock.

This is most undesirable.

END