

Soln - 1

For gear A

Shaft diameter $d_A = 44.45 \text{ mm}$ or $r_A = 22.225 \text{ mm}$ from the given table we get $W \times H = 14 \text{ mm} \times 9 \text{ mm}$ (+1)

~~Torque acting on gear A = $r_A \times F_A \cos 20^\circ$~~

~~$= 0.022225 \times 1334.466 \times 0.9397$~~

≠

$$\text{Torque acting on gear A} = R_A \times F_A \cos 20^\circ$$

$$T_A = 0.0254 \times 1334.466 \times 0.9397$$

$$= 318.52 \text{ Nm}$$

(+1) T_A or F_{key}

$$\text{Force acting on the key } F_{key} = T_A / r_A$$

$$= 318.52 / 0.022225$$

$$= 14331.61 \text{ N}$$

$$\text{Average direct shear} = F_{key} / A_{\text{shear}} = F_{key} / L_s W$$

$$= 14331.61 / L_s \times 14 = 1023.69 / L_s \text{ N/mm}^2$$

$$\text{for shear failure } \tau_{\max} = \frac{\sigma_{ys}}{FOS} \quad \left(\begin{array}{l} \sigma_{ys} = \sigma_y / 2 \\ \sigma_{ys} = \sigma_y / \sqrt{3} \end{array} \right)$$

Using maximum shear stress theory

$$\sigma_y / 2$$

$$\frac{1023.69}{L_s} = \frac{372}{1.2 \times 2}$$

$$\Rightarrow L_s = 6.6 \text{ mm}$$

(+1) L_s

Using distortion energy theory

$$\sigma_y / \sqrt{3}$$

$$\frac{1023.69}{L_s} = \frac{372}{1.2 \times \sqrt{3}}$$

$$L_s = 5.72 \text{ mm}$$

Average crushing stress $\sigma_c = F_{\text{key}} / A_{\text{crush}} = F_{\text{key}} / L_c H / 2$

$$\Rightarrow \sigma_c = \frac{2 \times 14331.61}{L_c \times 9} = \frac{3184.8}{L_c} \text{ N/mm}^2$$

& for crushing failure $\sigma_{c \text{ max}} = \sigma_y / FOS$

$$\Rightarrow \frac{3184.8}{L_c} = \frac{372}{1.2}$$

(+1)

$$\text{or } L_c = 10.27 \text{ mm}$$

$$\therefore \text{length of key for gear A} = \max(L_s, L_c)$$
$$= \underline{\underline{10.27 \text{ mm}}}$$

~~= 10.27 mm~~ (+1)

for gear B

shaft diameter = 25.4 mm

key's $W \times H = 8 \times 7 \text{ mm}^2$ (+1)

Torque acting would be same & = 318.5 Nm

Forces acting on the key = T / r_{shaft}

$$F_B = 25078.7 \text{ N}$$

(+1), [12]

Average direct shear for B $\tau_B = F_B / L W$
 $= 3134.84 / L \text{ N/mm}^2$

\therefore for shear failure $\tau_B = \sigma_y / \sqrt{3} \times \text{FOS}$

$$\Rightarrow \frac{3134.84}{L_s} = \frac{372}{\sqrt{3} \times 1.2}$$

(+1), [13]

using $\left(\frac{\sigma_d}{2}\right)$) $L_s = 20.22 \text{ mm}$ $L_s = 17.51 \text{ mm}$

Average crushing stress = $\sigma_{\text{Bcrush}} = 2F_B / L H$
 $= 7165.34 / L \text{ N/mm}^2$

\therefore for crushing failure $\sigma_{\text{Bcrush}} = \sigma_y / \text{FOS}$

$$\Rightarrow \frac{7165 \cdot 34}{L_c} = \frac{372}{1.2}$$

$$\text{or } L_c = 23.11 \text{ mm} \quad (+1)$$

$$\therefore \text{length of key for gear B} = \max(L_s, L_c) \\ = 23.11 \text{ mm} \quad (+1)$$

ME 423 - Quiz 2

- 2) Given :- Desired life = $L_{10h} = 5000$ hrs
 Speed = $N = 1500$ rpm
 Load Application factor = $K_a = 1.2$
 $F_A = 1334.466$ N

To find:- C_{10} for bearing at 'O' and 'C'

Solution:- For given shaft system.

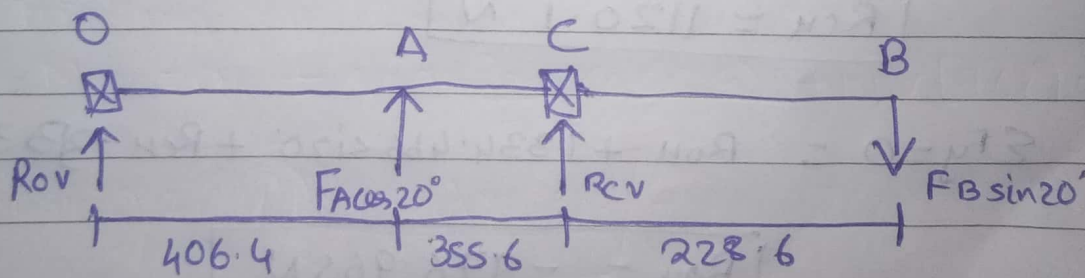
$$\text{Torque A} + \text{Torque B} = 0$$

$$F_A \cos 20^\circ \times \frac{508}{2} - F_B \sin 20^\circ \times \frac{203.2}{2} = 0$$

$$F_B = \frac{F_A \times 508}{203.2} = \frac{1334.466 \times 508}{203.2}$$

$$\boxed{F_B = 3336.165 \text{ N}}$$

Now vertical loading diagram.



$$\sum M_O = F_A \cos 20^\circ \times 406.4 + R_{cv} (762) - F_B \sin 20^\circ (990.6) = 0$$

$$R_{cv} = \frac{3336.165 \times \sin 20^\circ \times 990.6 - 1334.466 \times \cos 20^\circ \times 406.4}{762}$$

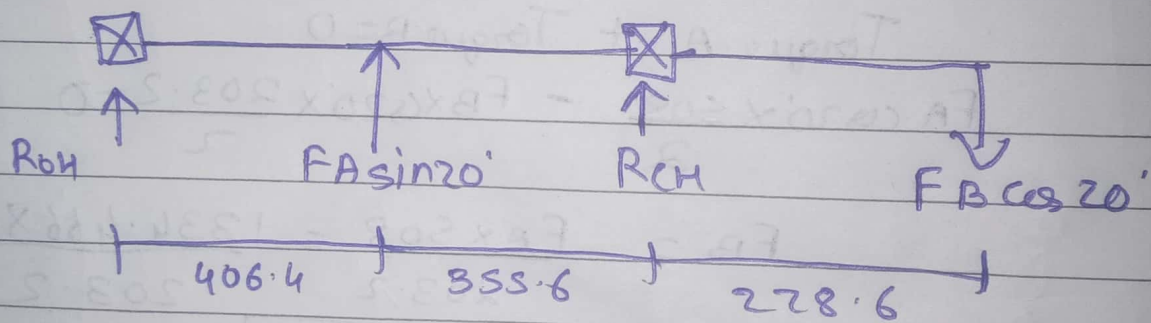
$$\boxed{R_{cv} = 3669.018 \text{ N}}$$

$$\sum F_y = 0 \quad R_{ov} + F_A \cos 20^\circ + R_{cv} - F_B \sin 20^\circ = 0$$

$$R_{ov} = 3336.16 \sin 20^\circ - 1334.46 \cos 20^\circ - 3669.08$$

$$R_{ov} = -1167.85 \text{ N}$$

Horizontal loading diagram:-



$$\sum M_o = 0 = 1334.466 \times \sin 20^\circ \times 406.4 + R_{ch} \times 762 - 3336.16 \times \cos 20^\circ \times 990.6 = 0$$

$$R_{ch} = 1120.1 \text{ N}$$

$$\sum F_y = 0 = R_{oh} + 1334.466 \sin 20^\circ + R_{ch} - 3336.16 \cos 20^\circ$$

$$R_{oh} = -976.96 \text{ N}$$

$$\therefore \text{Radial load at 'O'} = \sqrt{R_{Ou}^2 + R_{Ov}^2}$$

$$= \sqrt{(-976.965)^2 + (-1167.85)^2}$$

$$\boxed{R_O = 1522.61 \text{ N}}$$

$$\text{Radial load at 'C'} = \sqrt{R_{Cu}^2 + R_{Cv}^2}$$

$$= \sqrt{(1120.1)^2 + (3669.018)^2}$$

$$\boxed{R_C = 3836.185 \text{ N}}$$

\therefore Equivalent ~~static~~ dynamic load on Bearing 'O', 'C'

$$P_{EO} = K_a R_O = 1.2 \times 1522.61$$

$$= 1827.132 \text{ N}$$

$$P_{EC} = K_a R_C = 1.2 \times 3836.185$$

$$= 4603.422 \text{ N}$$

Now for bearing $L_{10} = \frac{L_{10h} \times N \times 60}{10^6}$ million rev

$$= \frac{5000 \times 1500 \times 60}{10^6}$$

$$= 450$$

$$L_{10} = \left(\frac{C}{P_e} \right)^3 \text{ for ball bearing.}$$

for Bearing 'O' $450 = \left[\frac{C}{1827.132} \right]^3$ $C = 14.001 \text{ kN}$

for Bearing 'C' $450 = \left[\frac{C}{4603.422} \right]^3$ $C = 35.276 \text{ kN}$

$a=3$ (roller Bearing)

Q₃

Bearing A →

$$F_A = 2 \text{ kN}$$

$$L_A = 3000 \times 500 \times 60 \text{ cycles} \\ = 9 \times 10^7 \text{ cycles}$$

Bearing B

$$C_B = 7 \text{ kN}$$

$$L_B = 10^6 \text{ cycles}$$

To compare the both, they need to be rated in terms of the same Catalog rating system. (10^6 cycles)

$$C_A = F_A \times \left(\frac{L_A}{L_B} \right)^{1/a} = 2 \times \left(\frac{9 \times 10^7}{10^6} \right)^{1/3} = 8.96 \text{ kN}$$

Catalogue rating of Bearing A for 10^6 cycles is 8.96 kN
Catalogue rating of Bearing B for 10^6 cycles is 7.0 kN
 $C_A > C_B$

∴ Bearing A can carry the larger load.

→ Calculation of number of cycles → 1 mark

→ Using $L_{10} C_{10}^3 = \text{constant}$ → 1 mark

→ Finding $(C_{10})_A$ Or $L_{10} C_{10}^3 = \text{constant}$ → 1 mark
(calculation of constant)

→ Final Comparison of Bearing A & B → 1 mark

[0.4]

Qiz 2

given

$$a = 90$$

$$b = 80$$

$$e = 30$$

$$r = 40$$

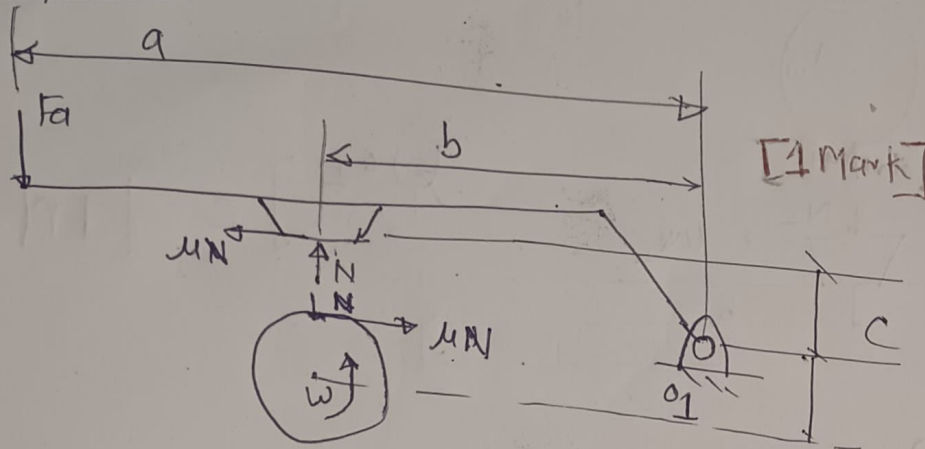
$$w = 60$$

$$\theta = 25^\circ$$

$$P_{\max} = 1.5 \text{ MPa}$$

$$\mu = 0.25$$

Top shoe



① Normal reaction $N = PA = (r\omega) = 1570.796 \text{ (N)} \rightarrow [1 \text{ Mark}]$

② $T_1 = \mu N r = 15.708 \text{ (Nm)} [1 \text{ Mark}]$

③ $c = r - e = 40 - 30 = 10$

$+\uparrow \sum M_{O1} = 0$

$+(F_a \cdot a) - (N \cdot b) + \mu N c = 0 ; F_a = \frac{N(b - \mu c)}{a} = 1352.63 \text{ (N)} [1 \text{ Mark}]$

④ Self lock
if $\mu c \geq b$

here

$$\mu c = 0.25 \times 10 = 2.5$$

$$b = 80 \Rightarrow \therefore \mu c \neq b \Rightarrow \text{no self lock.}$$

⑤ Value of c for self lock $= \frac{b}{\mu} = 80 / 0.25 = 320 \text{ (mm)}$

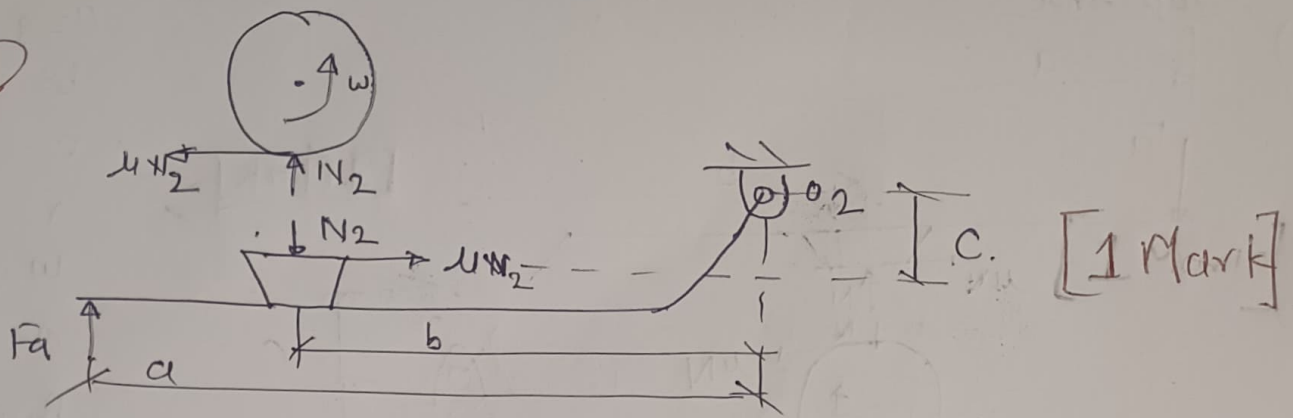
[1 Mark]

⑥

bottom shoe :-

Partial FBD

FBD



$$+\uparrow \Sigma M_{O_2} = 0$$

$$-[F_a \cdot a] + [N_2 \cdot b] + [\mu N_2 c] = 0$$

$$F_a = \frac{N_2(b + \mu c)}{a} \Rightarrow N_2 = F_a \cdot \left[\frac{a}{b + \mu c} \right]$$

$$N_2 = 1475.596 \text{ (N)} \quad [1 \text{ Mark}]$$

⑦

$$T_2 = (\mu N_2 r) = 14.7559 \text{ (Nm)} \approx 14.756 \text{ (Nm)} \quad [1 \text{ Mark}]$$

⑧

$$\text{total torque Capacity} = T_1 + T_2 = 30.464 \text{ (Nm)} \quad [2 \text{ Marks}]$$