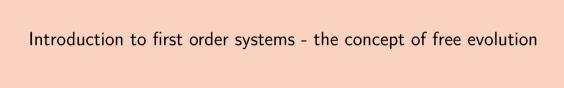
### TTK4225 - Systems Theory, Autumn 2020

Damiano Varagnolo





#### Roadmap

- generalization of our examples of first order systems
- the concept of free evolution
- introduction to stability
- free evolution # forced response

train velocity

$$\dot{v} = -\frac{k}{m}v(t) + \frac{k}{m}F(t) \tag{1}$$

RC-circuit

$$\dot{v}_C = -\frac{1}{RC}v_C + \frac{1}{RC}V(t) \tag{2}$$

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• train velocity

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In general:

$$\dot{y} = ay + bu \tag{3}$$

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$$\dot{y} = ay + bu \tag{4}$$

$$\dot{y} = ay + bu \tag{4}$$

#### Qualitative discussions:

• what happens if u = 0,  $y_0 = 0$ ?

$$\dot{y} = ay + bu \tag{4}$$

- what happens if u = 0,  $y_0 = 0$ ?
- what happens if u = 0,  $y_0 > 0$ , and a > 0?

$$\dot{y} = ay + bu \tag{4}$$

- what happens if u = 0,  $y_0 = 0$ ?
- what happens if u = 0,  $y_0 > 0$ , and a > 0?
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- what happens if u = 0,  $y_0 = 0$ ?
- what happens if u = 0,  $y_0 > 0$ , and a > 0?
- what happens if u = 0,  $y_0 < 0$ , and a > 0?
- what happens if u = 0,  $y_0 \neq 0$ , and a < 0?

$$\dot{y} = ay + bu \tag{4}$$

- what happens if u = 0,  $y_0 = 0$ ?
- what happens if u = 0,  $y_0 > 0$ , and a > 0?
- what happens if u = 0,  $y_0 < 0$ , and a > 0?
- what happens if u = 0,  $y_0 \neq 0$ , and a < 0?
- what happens if u = 0, and a = 0?

#### stability = extremely important topic!

will be analysed in more details later on in this course and much more extensively in others

(feat. Lyapunov, Krasovskii, La-Salle among others)

# An important case: free evolution

$$\dot{y} = ay / \sqrt{y} \qquad \qquad y(0) = y_0 \neq 0$$

(5)

# Towards the solution of the free evolution starting from a simplified case

$$\dot{y} = y$$
  $y(0) = y_0 \neq 0$  (6)

(in other words, which function is equal to its derivative?)

# The solution of the free evolution in general

$$\dot{y} = ay \qquad y(0) = y_0 \neq 0 \tag{7}$$

# The solution of the free evolution in general

$$\dot{y} = ay \qquad \qquad y(0) = y_0 \neq 0$$
 Alternatively:

$$\dot{y} = \frac{dy}{dt} = ay(t)$$

$$\frac{dy}{y(t)} = a dt$$

 $\ln(v(t)) = \ln(y_0) + at$ 

 $y(t) = y_0 e^{at}$ 

 $y(t) = e^{\ln(y_0)at} = e^{\ln(y_0)}e^{at}$ 

$$\int_0^t \frac{dy}{y(\tau)} = \int_0^t a \, d\tau$$
$$\left[\ln y(\tau)\right]_0^t = a\left[\tau\right]_0^t$$

(12)

(13)

(14)

(7)

(8)

(9)

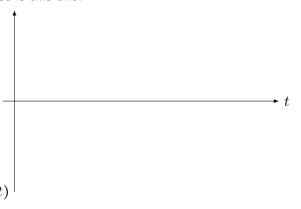
# And what about the vectorial generalization?

$$\dot{\boldsymbol{y}} = A\boldsymbol{y}$$

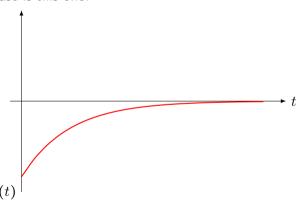
⇒ later in the course, and extensively!

$$\dot{y} = ay \qquad y(0) = y_0 \neq 0 \qquad \Longrightarrow \qquad y(t) = y_0 e^{at} \tag{15}$$

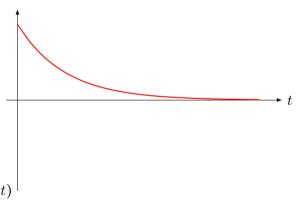
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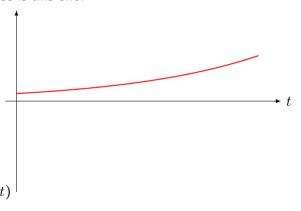
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•

#### Introduction to stability

```
stable system: y(t) \to 0 for t \to +\infty
```

unstable system:  $|y(t)| \to +\infty$  for  $t \to +\infty$ 

marginally stable system:  $y(t) = y_0$  for every t

#### Introduction to stability

```
stable system: y(t) \to 0 for t \to +\infty
```

unstable system: 
$$|y(t)| \to +\infty$$
 for  $t \to +\infty$ 

marginally stable system:  $y(t) = y_0$  for every t

much more on stability both later on & in later courses!

Are we done with studying the response of first order dynamical models?

$$\dot{y} = ay + bu \tag{16}$$

### Forced response

$$\dot{y} = ay + bu$$
  $y(0) = y_0 = 0$  (17)

(remember: free evolution = "
$$u = 0, y_0 \neq 0$$
")

#### Forced response

$$\dot{y} = ay + bu$$
  $y(0) = y_0 = 0$  (17)

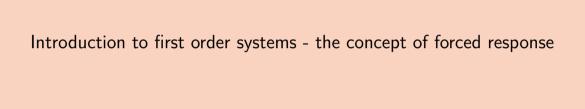
(remember: free evolution = "
$$u = 0, y_0 \neq 0$$
")

*Discussion:* does  $y(0) = y_0 = 0$  imply that we should study  $\dot{y} = bu$ ?

#### Try it yourself at home!

GitHub/TTK4225/trunk/Jupyter/
first-order-system-introduction-with-P-controller.ipynb

-



#### Roadmap

- the concept of "forced response"
- the convolution operator
- some properties of convolution

$$\dot{y} = ay + bu \tag{18}$$

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first-order-system-introduction-with-P-controller.ipynb

# Overarching question towards model-based control: how does y evolve?

$$\dot{y} = ay + bu \tag{19}$$

# Free evolution vs. forced response

$$\dot{y} = ay + bu \tag{20}$$

free evolution: u = 0,  $y_0 \neq 0$ 

forced response:  $u \neq 0$ ,  $y_0 = 0$ 

## Solution to the forced response

(actual solution through equations (2.11)–(2.17) in Balchen's book)

$$\dot{y} = ay + bu, \quad y(0) = y_0 = 0 \qquad \Longrightarrow \qquad y(t) = \int_{-\infty}^{+\infty} h(\tau)bu(t - \tau)d\tau \qquad \text{(21)}$$
 with 
$$h(\tau) = \begin{cases} 0 & \text{if } t < 0 \\ e^{a(\tau)} & \text{otherwise} \end{cases}$$

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extremely important definition: convolution := 
$$h * u(t) := \int_{-\infty}^{+\infty} h(\tau)u(t-\tau)d\tau$$

Visualizing 
$$h * u(t) \coloneqq \int_{-\infty}^{+\infty} h(\tau) u(t-\tau) d\tau$$

#### **Discussions**

$$h * u(t) \coloneqq \int_{-\infty}^{+\infty} h(\tau) u(t - \tau) d\tau$$

**1** is 
$$h * u(t) = u * h(t)$$
?

#### **Discussions**

$$h * u(t) \coloneqq \int_{-\infty}^{+\infty} h(\tau) u(t - \tau) d\tau$$

- is h \* u(t) = u \* h(t)?
- **2** is  $(\alpha h_1 + \beta h_2) * u(t) = \alpha (h_1 * u(t)) + \beta (h_2 * u(t))$ ?

#### **Discussions**

$$h * u(t) \coloneqq \int_{-\infty}^{+\infty} h(\tau) u(t - \tau) d\tau$$

- is h \* u(t) = u \* h(t)?
- **2** is  $(\alpha h_1 + \beta h_2) * u(t) = \alpha (h_1 * u(t)) + \beta (h_2 * u(t))$ ?
- assuming

$$h(\tau) = \begin{cases} 0 & \text{if } t < 0 \\ e^{a(\tau)} & \text{otherwise} \end{cases} \quad \text{and} \quad u(t) = 0 \text{ if } t < 0,$$

can we simplify

$$y(t) = \int_{-\infty}^{+\infty} h(\tau)bu(t-\tau)d\tau$$

somehow?

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#### Our LTI case

$$\dot{y} = ay + bu$$
,  $y(0) = y_0 = 0$ 

implies

$$y(t) = \int_0^t h(\tau)u(t-\tau)d\tau$$

(or, alternatively and equivalently,  $y(t) = \int_0^t h(t-\tau)u(\tau)d\tau$ )

## Example

$$y(t) = \int_0^t h(\tau)u(t-\tau)d\tau,$$

$$u(t) = \begin{cases} 1 & \text{for } t \in [1,2] \\ 0 & \text{otherwise} \end{cases} \qquad h(t) = \begin{cases} 2 & \text{for } t \in [0,1) \\ 1 & \text{for } t \in [1,2] \\ 0 & \text{otherwise} \end{cases}$$

#### Discussion:

What is y(t) = h \* u(t) for the case

$$u(t) = \begin{cases} 1 & \text{for } t \in [1,2] \text{ and } t \in [2,3] \\ 0 & \text{otherwise} \end{cases} \qquad h(t) = \begin{cases} 2 & \text{for } t \in [0,2) \\ 0 & \text{otherwise} \end{cases} ?$$

GitHub/TTK4225/trunk/Jupyter/convolution-example.ipynb

## Summary

$$\dot{y} = ay + bu \tag{22}$$

```
free evolution: u = 0, y_0 \neq 0; implies y(t) = y_{\text{free}}(t) = y_0 e^{at} forced response: u \neq 0, y_0 = 0; implies y(t) = y_{\text{forced}}(t) = h * u(t) with h(t) = e^{at}
```

# Summary

$$\dot{y} = ay + bu \tag{22}$$

free evolution: 
$$u = 0$$
,  $y_0 \neq 0$ ; implies  $y(t) = y_{\text{free}}(t) = y_0 e^{at}$  forced response:  $u \neq 0$ ,  $y_0 = 0$ ; implies  $y(t) = y_{\text{forced}}(t) = h * u(t)$  with  $h(t) = e^{at}$ 

$$e^{at}$$
 = "impulse response"

yet another pillar concept for automatic control
→ will be discussed better in a dedicated module
and re-discussed in **every** control-oriented course

# General response

$$\dot{y} = ay + bu \tag{23}$$

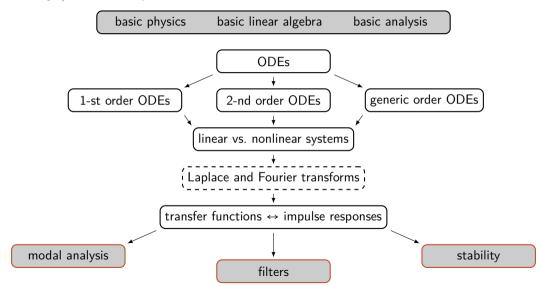
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free evolution: u = 0, y_0 \neq 0; implies y(t) = y_{\text{free}}(t) = y_0 e^{at}
forced response: u \neq 0, y_0 = 0; implies y(t) = y_{\text{forced}}(t) = h * u(t) with h(t) = e^{at}
```

# General response

$$\dot{y} = ay + bu \tag{23}$$

```
free evolution: u=0, y_0\neq 0; implies y(t)=y_{\rm free}(t)=y_0e^{at} forced response: u\neq 0, y_0=0; implies y(t)=y_{\rm forced}(t)=h*u(t) with h(t)=e^{at} general response: u\neq 0, y_0\neq 0; implies y(t)=y_{\rm free}(t)+y_{\rm forced}(t) thanks to the fact that the model is linear (will be seen in more details later on)
```

## Summary / Roadmap of TTK4225



Introduction to first order systems - visualizing the system through a block scheme

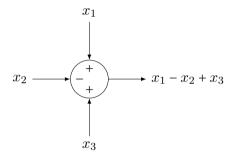
## Roadmap

- the most common block schemes
- first order systems as block schemes

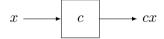
## Block diagrams - why?

- used very often in companies
- aid visualization (until a certain complexity is reached...)
- enable "drag & drop" way of programming
- in this course, primarily used for interpretations

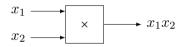
# Most common block diagrams - sum of n signals



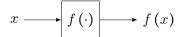
## Most common block diagrams - multiplication for a constant



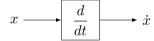
## Most common block diagrams - multiplication of two signals



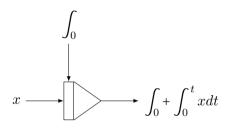
# Most common block diagrams - generic functions



## Most common block diagrams - derivatives



## Most common block diagrams - integrals

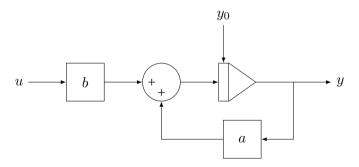


Discussion: how do we represent a first order DE with a block scheme?

$$\dot{y} = ay + bu$$

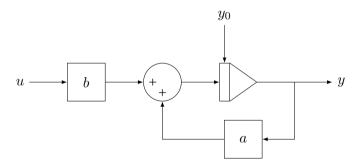
## The solution

$$\dot{y} = ay + bu$$



#### The solution

$$\dot{y} = ay + bu$$



Discussion: do you note the presence of a feedback loop?

## Introduction to Simulink

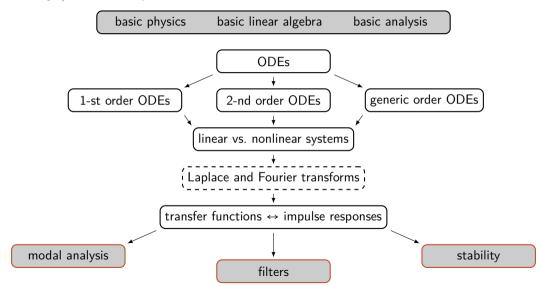
?

Introduction to generic order systems

## Roadmap

- from first order to second order
- generic orders
- classification of the different types of ODEs

## Summary / Roadmap of TTK4225



#### From first order to second order

Discussion: if we can write

$$\dot{y} = ay + bu \; ,$$

can we also write

$$\ddot{y} = a_1 \dot{y} + a_0 y + bu ?$$

## From first order to second order, third order

Discussion: if we can write

$$\dot{y} = ay + bu \; ,$$

can we also write

$$\ddot{y} = a_1\dot{y} + a_0y + bu ?$$

And at this point also

$$\ddot{y} = a_2 \ddot{y} + a_1 \dot{y} + a_0 y + bu ?$$

# From first order to second order, third order

Discussion: if we can write

$$\dot{y} = ay + bu \; ,$$

can we also write

$$\ddot{y} = a_1 \dot{y} + a_0 y + bu ?$$

And at this point also

$$\ddot{y} = a_2 \ddot{y} + a_1 \dot{y} + a_0 y + bu ?$$

And why not

$$\ddot{y}=a_2\ddot{y}+a_1\dot{y}+a_0y+b_1\dot{u}+b_0u \ ?$$

#### ARMA models

$$y^{(n)} = a_{n-1}y^{(n-1)} + \ldots + a_0y + b_mu^{(m)} + \ldots b_0u$$
?

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$$y^{(n)} = a_{n-1}y^{(n-1)} + \ldots + a_0y + b_mu^{(m)} + \ldots b_0u$$
?

*Discussion*: and why don't we have  $a_n y^{(n)}$ , instead of only  $y^{(n)}$  on the LHS?

$$y^{(n)} = a_{n-1}y^{(n-1)} + \ldots + a_0y + b_mu^{(m)} + \ldots b_0u$$
?

$$y^{(n)} = a_{n-1}y^{(n-1)} + \ldots + a_0y + b_mu^{(m)} + \ldots b_0u$$
?

time-varying:  $\dot{y} = a(t)y + b(t)u$ 

$$y^{(n)} = a_{n-1}y^{(n-1)} + \ldots + a_0y + b_mu^{(m)} + \ldots b_0u$$
?

time-varying:  $\dot{y} = a(t)y + b(t)u$ 

non-homogeneous:  $\dot{y} = a(t)y + b(t)u + c$ 

$$y^{(n)} = a_{n-1}y^{(n-1)} + \ldots + a_0y + b_mu^{(m)} + \ldots b_0u$$
?

time-varying:  $\dot{y} = a(t)y + b(t)u$ 

non-homogeneous:  $\dot{y} = a(t)y + b(t)u + c$ 

non-linear:  $\dot{y} = a\sqrt{y} + bu^{2/3}$ 

Discussion: can we make this linear again?

$$\dot{y} = ay + bu^{2/3}$$

Discussion: can we make this linear again?

$$\dot{y} = ay + bu^{2/3}$$

Another discussion: can we apply the same "linearization trick" to  $\dot{y} = a\sqrt{y} + bu$ ?

main focus in this course:

linear, time invariant, homogeneous (LTI)

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why?

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why?

Remember: predictive control of the type

$$oldsymbol{u}^{\star} = rg\min_{oldsymbol{u} \in \mathcal{U}, oldsymbol{f}(oldsymbol{u}) \in \mathcal{F}} \operatorname{Cost}\left(oldsymbol{f}\left(oldsymbol{u}
ight), oldsymbol{u}
ight)$$

requires to be able to:

- define "Cost"
- ullet compute  $f\left(u
  ight)$  rapidly
- be sure that the model does not have "nasty" properties

# main focus in this course: linear, time invariant, homogeneous (LTI)

why?

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requires to be able to:

- define "Cost"
- ullet compute  $f\left(u
  ight)$  rapidly
- be sure that the model does not have "nasty" properties

from the previous lessons:

1-st order LTI models → impulse responses;

as will be clear later generic order LTI models → also impulse responses

# The question we are trying to answer in this first part of the course

"What will be the solution y(t) to a generic-order LTI ODE starting from a generic initial condition  $y(0) = y_0$  and generic input signal u(t)?"

(our hope: the solution will be structurally easy, and fast to compute)

?

### What is what?

(i.e., a small quiz to see if we are aligned)

	autonomous	linear	homogeneous	time constant
$\frac{\dot{x}}{-}=1$				
x				
$\pi = \dot{x}x$				
$2\dot{x} + \sin t = 0$				
$\sin(t\dot{x}) - x = 0$				
$t\dot{x} = x\sin t$				
$x - e^{-t} = \ddot{x} + \dot{x}$				

Introduction to generic order systems

# Roadmap

- state space representations
- ullet from n-th order to vectorial first order

mathematical model (typically but not limited to of a physical system) as a finite set of inputs, outputs and state variables related by first-order differential equations satisfying the separation principle

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#### Ingredients

• finite number of inputs, outputs and state variables

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- finite number of inputs, outputs and state variables
- first-order differential equations

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#### Ingredients

- finite number of inputs, outputs and state variables
- first-order differential equations
- satisfies the separation principle: the current value of states contains all the information necessary to forecast the future evolution of the outputs and of the states given the inputs

## State space representations - Facts

• the future output depends only on the current state and the future input

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- the future output depends on the past input only through the current state

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- the future output depends on the past input only through the current state
- the state summarizes the effect of past inputs on future output (sort of a "memory" of the system)

### Example

#### Rechargeable flashlight:

- ullet state = level of charge of the battery & on / off button
- ullet output = how much light the device is producing

```
u_1,\dots,u_m = 	ext{inputs} x_1,\dots,x_n = 	ext{states} y_1,\dots,y_p = 	ext{outputs}
```

```
\dot{x}_{1} = f_{1}(x_{1}, \dots, x_{n}, u_{1}, \dots, u_{m}) 

\vdots 

\dot{x}_{n} = f_{n}(x_{1}, \dots, x_{n}, u_{1}, \dots, u_{m}) 

y_{1} = g_{1}(x_{1}, \dots, x_{n}, u_{1}, \dots, u_{m}) 

\vdots 

y_{p} = g_{n}(x_{1}, \dots, x_{n}, u_{1}, \dots, u_{m})
```

$$\dot{x}_1 = f_1(x_1, \dots, x_n, u_1, \dots, u_m) 
\vdots 
\dot{x}_n = f_n(x_1, \dots, x_n, u_1, \dots, u_m) 
y_1 = g_1(x_1, \dots, x_n, u_1, \dots, u_m) 
\vdots 
y_p = g_n(x_1, \dots, x_n, u_1, \dots, u_m) 
\dot{x} = f(x, u) 
y = g(x, u)$$

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\vdots 
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y_1 = g_1(x_1, \dots, x_n, u_1, \dots, u_m) 
\vdots 
y_p = g_n(x_1, \dots, x_n, u_1, \dots, u_m) 
\dot{x} = f(x, u) 
y = g(x, u)$$

- ullet f= state transition map
- $ullet g = \mathsf{output} \mathsf{ map}$

# Discussion: is any f and g ok?

$$\dot{x} = f(x, u)$$
 $y = g(x, u)$ 

# Discussion: is any f and g ok?

$$\dot{x} = f(x, u)$$
 $y = g(x, u)$ 

*No:* for every given  $x_0$  and u the solution must be:

- unique
- guaranteed to exist for  $t \in [0, \bar{t})$  for some  $\bar{t} > 0$

(check "existence and uniqueness of solutions of ODEs")

# State space representations - Example

$$\begin{cases} \dot{x} = -x^2 \\ y = x \end{cases} \quad \cup \quad x_0 = -1 \qquad \Longrightarrow x(t) = \frac{1}{t-1}$$

# State space representations - Example

$$\begin{cases} \dot{x} = -x^2 \\ y = x \end{cases} \quad \cup \quad x_0 = -1 \qquad \Longrightarrow x(t) = \frac{1}{t-1}$$

Discussion: (a bit outside of the current flow of concepts on ODEs, but still relevant and very important) what happens as  $t \to 1$ ?

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there is a finite escape time!

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# Discussion: can every physical system be described with a state space representation?

#### Noticeable exceptions:

- non-lumped parameters model (i.e., PDEs)
- continuous-time systems with delays (will be discussed better later on)

# Example: dynamics of sugar and insulin concentrations in blood

- $x_1 := sugar concentration$
- $x_2 := insulin concentration$
- $u_1 := food intake$
- $u_2 := \text{insulin intake}$
- c := sugar concentration in fasting

$$\begin{cases} \dot{x}_2 = a_{21} (x_1 - c) - a_{22} x_2 + b_2 u_2 & x_1 \ge c \\ \dot{x}_2 = -a_{22} x_2 + b_2 u_2 & x_1 < c \end{cases}$$

$$\begin{cases} \dot{x}_1 = -a_{11} x_1 x_2 + a_{12} (c - x_1) + b_1 u_1 & x_1 \ge c \\ \dot{x}_1 = -a_{11} x_1 x_2 + b_1 u_1 & x_1 < c \end{cases}$$

?

How can I transform a generic-order ODE into a state space representation (that requires first order DEs)?

$$\ddot{y} = \phi \left( \ddot{y}, \dot{y}, y, \ddot{u}, \dot{u}, u \right);$$

# How can I transform a generic-order ODE into a state space representation (that requires first order DEs)?

$$\ddot{y} = \phi (\ddot{y}, \dot{y}, y, \ddot{u}, \dot{u}, u);$$

change of variables:

$$x = \begin{bmatrix} \ddot{y} \\ \dot{y} \\ y \end{bmatrix}, \ u = \begin{bmatrix} \ddot{u} \\ \dot{u} \\ u \end{bmatrix} \Rightarrow \dot{x} = \begin{bmatrix} \ddot{y} \\ \ddot{y} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} \phi(x, u) \\ [1\ 0\ 0] \ x \\ [0\ 1\ 0] \ x \end{bmatrix} = f(x, u)$$

Thus, how do I transform a generic order LTI system into a first order LTI system?

$$\ddot{y} = 2\dot{y} + 3y + 4\ddot{u} + 5\dot{u} + 6u$$

#### Transforming ARMA models

$$y^{(n)} = a_{n-1}y^{(n-1)} + \ldots + a_0y + b_mu^{(m)} + \ldots b_0u$$
?

Discussion: but then any LTI system is a first order vectorial system?

$$\dot{\boldsymbol{y}} = A\boldsymbol{y} + B\boldsymbol{u}$$

Discussion: but then any LTI system is a first order vectorial system?

$$\dot{\boldsymbol{y}} = A\boldsymbol{y} + B\boldsymbol{u}$$

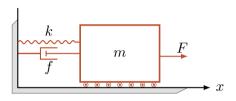
YES, AND THIS IS WHY LINEAR ALGEBRA IS ESSENTIAL FOR CONTROL! ?

Second order systems

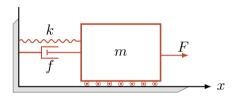
## Roadmap

- interesting examples
- interesting responses
- differences between 1st order and 2nd order

Position of a cart fastened with a spring to a wall and subject to friction:



Position of a cart fastened with a spring to a wall and subject to friction:



#### EOM:

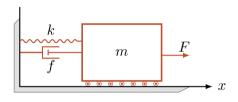
• force from the spring:  $F_x(t) = -kx(t)$ 

• friction:  $F_f(t) = -f\dot{x}(t)$ 

• applied force: F(t)

• Newton's second law:  $\sum F = m\ddot{x}(t)$ 

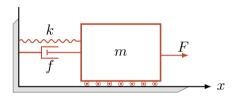
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- force from the spring:  $F_x(t) = -kx(t)$
- friction:  $F_f(t) = -f\dot{x}(t)$
- applied force: F(t)
- Newton's second law:  $\sum F = m\ddot{x}(t)$  $m\ddot{x}(t) = F_x(t) + F_f(t) + F(t)$

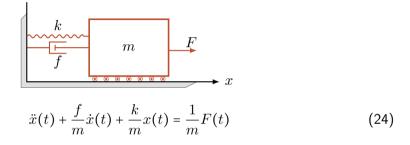
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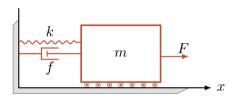
#### EOM:

- force from the spring:  $F_x(t) = -kx(t)$
- friction:  $F_f(t) = -f\dot{x}(t)$
- applied force: F(t)
- Newton's second law:  $\sum F = m\ddot{x}(t)$  $m\ddot{x}(t) = F_x(t) + F_f(t) + F(t) \mapsto m\ddot{x}(t) = -kx(t) - f\dot{x}(t) + F(t)$

Position of a cart fastened with a spring to a wall and subject to friction:



Position of a cart fastened with a spring to a wall and subject to friction:

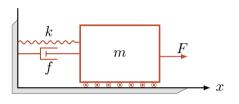


$$\ddot{x}(t) + \frac{f}{m}\dot{x}(t) + \frac{k}{m}x(t) = \frac{1}{m}F(t)$$
(24)

Generalizing:

$$\ddot{x} = a_1 \dot{x} + a_0 x + b_0 u \tag{25}$$

Position of a cart fastened with a spring to a wall and subject to friction:



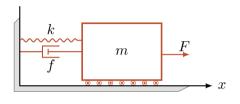
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Discussion: may we write this dynamics using a vectorial first order DE?

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Generalizing:

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Discussion: may we write this dynamics using a vectorial first order DE?

Discussion: may we write this dynamics using a scalar first order DE?

https://youtu.be/lZPtFDXYQRU?t=31

(here there is very little friction, though)

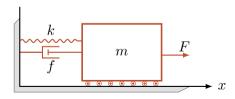
# Example 1: spring-mass systems - stability analysis from intuitive perspectives

*Discussion:*  $\dot{x} = a_0 x + b_0 u$  unstable if . . . ?

# Example 1: spring-mass systems - stability analysis from intuitive perspectives

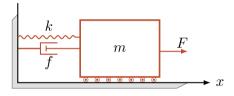
*Discussion:*  $\dot{x} = a_0 x + b_0 u$  unstable if ...? And What about, from intuitive perspectives, when considering

$$\ddot{x} = a_1 \dot{x} + a_0 x + b_0 u ? {26}$$

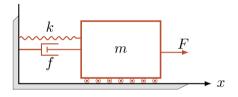


GitHub/TTK4225/trunk/Jupyter/spring-mass-systems-introduction.ipynb

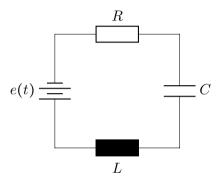
# Intuition: asymptotic stability ↔ dissipation of energy

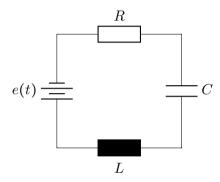


## Intuition: asymptotic stability ↔ dissipation of energy

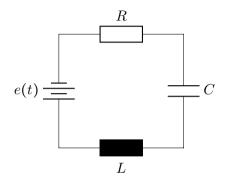


will see this MUCH better in later on courses when discussing about Lyapunov stability



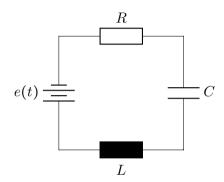


EOM: Kirkhoff laws



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$$v_L(t) = L \frac{di(t)}{dt}$$
  $v_i(t) = Ri(t)$   $v_C(t) = \frac{1}{C} \int_0^t i(\tau) d\tau$ 

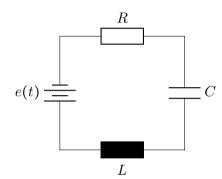


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$$e(t) = v_L(t) + v_R(t) + v_C(t)$$

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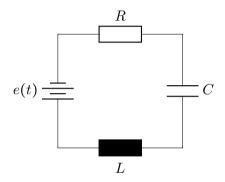


FOM: Kirkhoff laws

$$v_L(t) = L \frac{di(t)}{dt}$$
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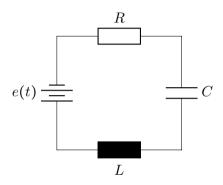
 $e(t) = v_L(t) + v_R(t) + v_C(t) \quad \mapsto \quad e(t) = L \frac{di(t)}{dt} + Ri(t) + \frac{1}{C} \int_0^t i(\tau) d\tau$ 

$$\frac{(t)}{dt}$$
  $v_i(t) = Ri(t)$   $v_C(t) = \frac{1}{C} \int_0^t i(\tau) d\tau$ 



$$e(t) = L\frac{di(t)}{dt} + Ri(t) + \frac{1}{C} \int_0^t i(\tau)d\tau$$

*Discussion:* how do we write it in terms of x,  $\dot{x}$ , ...?

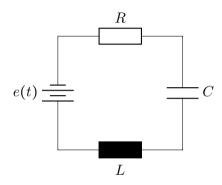


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*Discussion:* how do we write it in terms of  $x, \dot{x}, \dots$ ?

$$x(t) = i(t), \quad u(t) = \dot{e}(t) \qquad \Longrightarrow \qquad \ddot{x} = -\frac{R}{L}\dot{x} - \frac{1}{LC}x + \frac{1}{L}u \qquad (28)$$

168



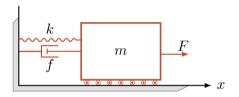
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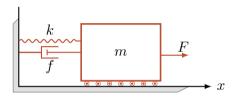
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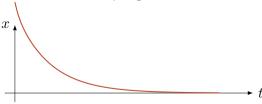
Generalizing:

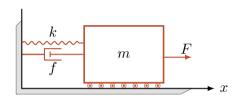
(28)





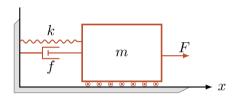
very big friction w.r.t. the spring stiffness  $\implies$  overdamping:





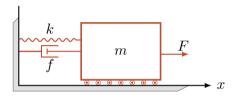
very small friction w.r.t. the spring stiffness  $\implies$  underdamping:





just the right amount of friction w.r.t. the spring stiffness  $\implies$  critical damping, i.e., the combination that leads to the fastest decay to zero without oscillations:



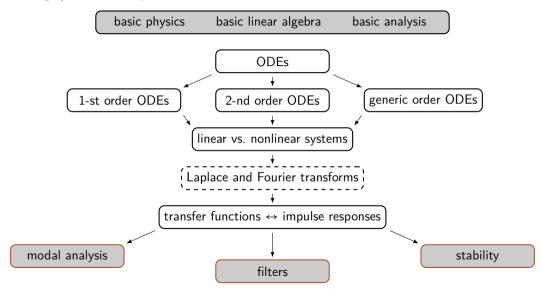


Discussion: can we get these behaviors with a first order system?

How do the free evolutions and forced responses look like numerically?

we will solve this problem with the aid of Laplace transforms

## Summary / Roadmap of TTK4225



#### The essence of TTK4225

A number like 3 is not a particular triplet of things, is about all possible triplets of things. In the same way, a model is not really about a particular system, but is rather about all the possible real-life and physical systems that behave as that model

?