### TTK4225 - Systems Theory, Autumn 2020

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matrix exponentials and ODEs

### Roadmap

- definition of matrix exponentials
- which role they play in solving ODEs
- different ways of computing matrix exponentials
- the Cayley-Hamilton theorem
- Jordan forms: the way of seeing LTIs

## Looking back: general solution of 1-st order differential equations

$$\dot{x} = ax + bu \implies x(t) = e^{at}x_0 + \int_0^t e^{a\tau}bu(t-\tau)d\tau$$

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What about multi-dimensional systems? May it be

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but what is  $e^{At}$ ?

#### WRONG way of doing it:

$$A = \begin{bmatrix} a_{11} & a_{21} \\ a_{21} & a_{22} \end{bmatrix} \implies e^{At} := \begin{bmatrix} e^{a_{11}t} & e^{a_{12}t} \\ e^{a_{21}t} & e^{a_{22}t} \end{bmatrix}$$

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$$A = \begin{bmatrix} a_{11} & a_{21} \\ a_{21} & a_{22} \end{bmatrix} \implies e^{At} \coloneqq \begin{bmatrix} e^{a_{11}t} & e^{a_{12}t} \\ e^{a_{21}t} & e^{a_{22}t} \end{bmatrix}$$

This is wrong because exponentials must be s.t.  $e^{as}e^{at}=e^{a(s+t)}$ , and the definition above does not hold:

$$e^{As}e^{At} = \begin{bmatrix} e^{a_{11}s} & e^{a_{12}s} \\ e^{a_{21}s} & e^{a_{22}s} \end{bmatrix} \begin{bmatrix} e^{a_{11}t} & e^{a_{12}t} \\ e^{a_{21}t} & e^{a_{22}t} \end{bmatrix}$$
$$= \begin{bmatrix} e^{a_{11}s+a_{11}t} + e^{a_{12}s+a_{21}t} & e^{a_{11}s+a_{12}t} + e^{a_{12}s+a_{22}t} \\ e^{a_{21}s+a_{11}t} + e^{a_{22}s+a_{21}t} & e^{a_{21}s+a_{12}t} + e^{a_{22}s+a_{22}t} \end{bmatrix} \neq e^{A(s+t)}$$

Good definition = through Taylor expansions:

$$e^{at} = \sum_{n=0}^{+\infty} \frac{(at)^n}{n!} = 1 + at + \frac{a^2t^2}{2!} + \frac{a^3t^3}{3!} + \dots$$

implies

$$e^{At} = \sum_{n=0}^{+\infty} \frac{(At)^n}{n!} = I + At + \frac{1}{2!}A^2t^2 + \frac{1}{3!}A^3t^3 + \dots$$

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**Implications** 

- $\frac{d}{dt}e^{At} = Ae^{At}$  (i.e., as expected and desired)
- $\bullet$   $e^{As}e^{At}=e^{A(s+t)}$  (i.e., as expected and desired)

### Additional results

derivation product of same exponentials	$\frac{d}{dt}e^{At} = Ae^{At}$
product of same exponentials	$e^{As}e^{At} = e^{A(s+t)}$
preservation of commutativity	$AB = BA \iff e^A e^B = e^B e^A$
exponential of zero	$e^{0} = I$
non-null determinant	$\det(e^A) \neq 0$
inversion	$(e^{At})^{-1} = e^{-At}$
decomposition	$e^{\boldsymbol{P}B\boldsymbol{P}^{-1}} = \boldsymbol{P}e^{B}\boldsymbol{P}^{-1}$

$$\dot{x} = Ax + Bu$$
  $\Longrightarrow$   $x(t) = e^{A(t-t_0)}x_0 + \int_{t_0}^t e^{A\tau}Bu(t-\tau)d\tau$ 

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Proof:

**①** assume x(t) to be of the form  $x(t) = e^{At}y(t)$  for an opportune y(t)

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- 2 this means assuming  $\dot{x}(t) = Ae^{At}y(t) + e^{At}\dot{y}(t) = Ax(t) + e^{At}\dot{y}(t)$
- inserting this in the original ODE implies

$$e^{At}\dot{\boldsymbol{y}}(t) = B\boldsymbol{u} \iff \dot{\boldsymbol{y}}(t) = e^{-At}B\boldsymbol{u} \iff \boldsymbol{y}(t) = \int_{t_0}^t e^{-A\tau}B\boldsymbol{u}(\tau)d\tau + \boldsymbol{k}$$

with  $oldsymbol{k}$  an opportune constant

$$\dot{x} = Ax + Bu$$
  $\Longrightarrow$   $x(t) = e^{A(t-t_0)}x_0 + \int_{t_0}^t e^{A\tau}Bu(t-\tau)d\tau$ 

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$$e^{At}\dot{y}(t) = Bu \iff \dot{y}(t) = e^{-At}Bu \iff y(t) = \int_{t_0}^t e^{-A\tau}Bu(\tau)d\tau + k$$

with  $oldsymbol{k}$  an opportune constant

plugging in this result back gives then

$$\boldsymbol{x}(t) = e^{At} \left( \int_{t_0}^t e^{-A\tau} B \boldsymbol{u}(\tau) d\tau + \boldsymbol{k} \right) = \int_{t_0}^t e^{A(t-\tau)} B \boldsymbol{u}(\tau) d\tau + e^{At} \boldsymbol{k} \implies \boldsymbol{k} = \boldsymbol{x}_0 e^{-At_0}$$

 $e^{At} := transition matrix$ 

#### Notation

 $e^{At} \coloneqq \mathsf{transition} \ \mathsf{matrix} = \Phi(t)$ 

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computers will do the computations. You though need to know what are the concepts

# Finding the transition matrix $\Phi(t) = e^{At}$ using Taylor expansions

$$e^{\mathbf{A}t} \approx I + At + \frac{A^2t^2}{2!} + \dots + \frac{A^kt^k}{k!}$$

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$$e^{\mathbf{A}t} \approx I + At + \frac{A^2t^2}{2!} + \dots + \frac{A^kt^k}{k!}$$

Note that this approximation may actually be exact if there exists m s.t.  $A^m = \mathbf{0}$ , since in this case

$$e^{At} = I + At + \frac{A^2t^2}{2!} + \dots + \frac{A^{(m-1)}t^{(m-1)}}{(m-1)!}$$

#### Example

$$A = \begin{bmatrix} 0 & 1 & 1 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix} \implies A^2 = \begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \implies A^3 = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\implies e^{At} = I + At + \frac{A^2t^2}{2!} = \begin{bmatrix} 1 & t & t + \frac{t^2}{2} \\ 0 & 1 & t \\ 0 & 0 & 1 \end{bmatrix}$$

# Practical example: spring-mass system (with m = 1)

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k & -f \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

Practical example: very particular spring-mass system (with  $m=1,\ f=0,$  and k=0)

$$A = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \implies A^2 = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \implies e^{At} = I + At = \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix}$$

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this means that no friction and no spring implies that if

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leads to

$$\boldsymbol{x}(t) = e^{At} \boldsymbol{x}(0) = \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix} \begin{bmatrix} p_0 \\ v_0 \end{bmatrix} = \begin{bmatrix} p_0 + v_0 t \\ v_0 \end{bmatrix}$$

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Meaning: the velocity keeps constant, the position grows linearly

# And what about a generic spring-mass system (with m = 1)?

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k & -f \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

need is to compute  $e^{At}$  explicitly!

Conceptual tool:  $e^{At}$  when A is diagonalizable

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Obvious result: product of diagonal matrices = diagonal matrix:

$$\begin{bmatrix} a & 0 & 0 \\ 0 & b & 0 \\ 0 & 0 & c \end{bmatrix} \begin{bmatrix} d & 0 & 0 \\ 0 & e & 0 \\ 0 & 0 & f \end{bmatrix} = \begin{bmatrix} ad & 0 & 0 \\ 0 & eb & 0 \\ 0 & 0 & cf \end{bmatrix}$$

# Conceptual tool: $e^{\Lambda t}$ when $\Lambda$ is diagonal

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$$= \begin{bmatrix} \sum_{k=0}^{+\infty} \frac{1}{k!} \lambda_1^k t & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & \sum_{k=0}^{+\infty} \frac{1}{k!} \lambda_n^k t \end{bmatrix}$$

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$$= \begin{bmatrix} e^{\lambda_1 t} & \cdots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \cdots & e^{\lambda_n t} \end{bmatrix}$$

 $\implies$  the transition matrix of a diagonal system can be computed immediately

### Summarizing: dynamics of the system when $\Lambda$ is diagonal

$$\dot{\boldsymbol{x}} = \Lambda \boldsymbol{x}(t) + B\boldsymbol{u}(t)$$

implies

$$\boldsymbol{x}(t) = e^{\Lambda(t-t_0)} \boldsymbol{x}(t_0) + \int_{t_0}^t e^{\Lambda \tau} B \boldsymbol{u}(t-\tau) d\tau$$

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### Summarizing: dynamics of the system when $\boldsymbol{A}$ is diagonalizable

$$\dot{\boldsymbol{x}} = A\boldsymbol{x}(t) + B\boldsymbol{u}(t)$$
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Then choosing

$$\widetilde{\boldsymbol{x}} = T^{-1} \boldsymbol{x}$$
  $\widetilde{B} = T^{-1} B$ 

leads to

$$\dot{\widetilde{\boldsymbol{x}}} = \Lambda \widetilde{\boldsymbol{x}}(t) + \widetilde{B} \boldsymbol{u}(t)$$

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and thus to

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and thus to

$$\boldsymbol{x}(t)$$
 =  $T\widetilde{\boldsymbol{x}}(t)$ 

Building on top of the practical example before: spring-mass system with  $m=1,\ f=0,\ {\rm and}\ k=1$ 

$$\dot{\boldsymbol{x}} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \boldsymbol{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

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spring-mass system with 
$$m = 1$$
,  $f = 0$ , and  $k = 1$ 

$$\begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} = T\Lambda T^{-1} = \begin{bmatrix} j & -j \\ 1 & 1 \end{bmatrix} \begin{bmatrix} -j & 0 \\ 0 & j \end{bmatrix} \left( \frac{1}{2j} \begin{bmatrix} 1 & j \\ -1 & j \end{bmatrix} \right)$$

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$$\begin{aligned} \Phi(t) &= e^{At} \\ &= \frac{1}{2j} \begin{bmatrix} j & -j \\ 1 & 1 \end{bmatrix} \begin{bmatrix} e^{-j} & 0 \\ 0 & e^{j} \end{bmatrix} \begin{bmatrix} 1 & j \\ -1 & j \end{bmatrix} \\ &= \begin{bmatrix} \frac{1}{2} \left( e^{-j} + e^{j} \right) & \frac{1}{2j} \left( e^{j} - e^{-j} \right) \\ -\frac{1}{2j} \left( e^{j} - e^{-j} \right) & \frac{1}{2} \left( e^{-j} + e^{j} \right) \end{bmatrix} \end{aligned}$$

spring-mass system with m = 1, f = 0, and k = 1

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$$\Phi(t) = e^{At} 
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= \begin{bmatrix} \frac{1}{2} (e^{-j} + e^{j}) & \frac{1}{2j} (e^{j} - e^{-j}) \\ -\frac{1}{2j} (e^{j} - e^{-j}) & \frac{1}{2} (e^{-j} + e^{j}) \end{bmatrix} 
= \begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix}$$

spring-mass system with m = 1, f = 0, and k = 1

$$\dot{\boldsymbol{x}} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \boldsymbol{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

implies

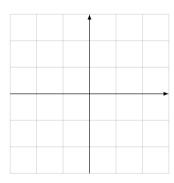
$$\boldsymbol{x}(t) = e^{At}\boldsymbol{x}_0 + \int_0^t e^{A\tau}B\boldsymbol{u}(t-\tau)d\tau$$

with

$$e^{At} = \begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix}$$

#### Once again

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} x \implies x(t) = \begin{bmatrix} \cos(t) & \sin(t) \\ -\sin(t) & \cos(t) \end{bmatrix} x_0$$



and what about non-diagonalizable A 's?

# A first tool to compute $\Phi(t)$ for non-diagonalizable A's: the Cayley-Hamilton's teorem

Starting ingredient: characteristic polynomial:

$$\det(sI - A) = \prod_{i=1}^{d} (s - \lambda_i)^{\mu(\lambda_i)}$$

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$$\det(sI - A) = \prod_{i=1}^{d} (s - \lambda_i)^{\mu(\lambda_i)} = s^n + \alpha_{n-1}s^{n-1} + \dots + \alpha_1s + \alpha_0$$

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#### Cayley-Hamilton's teorem:

$$A^{n} + \alpha_{n-1}A^{n-1} + \ldots + \alpha_{1}A + \alpha_{0}I = \mathbf{0}$$

$$A \in \mathbb{R}^{n \times n} \implies A^n + \alpha_{n-1}A^{n-1} + \ldots + \alpha_1A + \alpha_0I = \mathbf{0}$$

(with the coefficients  $\alpha$  the coefficients of the characteristic polynomial of A).

$$A \in \mathbb{R}^{n \times n} \implies A^n + \alpha_{n-1}A^{n-1} + \ldots + \alpha_1A + \alpha_0I = \mathbf{0}$$

(with the coefficients  $\alpha$  the coefficients of the characteristic polynomial of A). First implication:  $A^n$  is a linear combination of  $A^{n-1}, \ldots, A, I$ :

$$A^n = -\alpha_{n-1}A^{n-1} - \dots - \alpha_1A - \alpha_0I$$

$$A \in \mathbb{R}^{n \times n} \implies A^n + \alpha_{n-1}A^{n-1} + \ldots + \alpha_1A + \alpha_0I = \mathbf{0}$$

(with the coefficients  $\alpha$  the coefficients of the characteristic polynomial of A). Second implication: also  $A^{n+1}$  is a linear combination of  $A^{n-1}, \ldots, A, I$ :

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but since  $A^{n-1}A = A^n$  is a linear combination of  $A^{n-1}, \ldots, A, I$  then the claim follows

$$A \in \mathbb{R}^{n \times n} \implies A^n + \alpha_{n-1}A^{n-1} + \ldots + \alpha_1A + \alpha_0I = \mathbf{0}$$

*Discussion:* do you think that the following claim is true? all the  $A^{n+k}$  is a linear combination of  $A^{n-1}, \ldots, A, I$ , for every  $k \in \mathbb{N}_+$ 

### The actual meaning of Cayley-Hamilton

Remember:

$$e^{At} = \sum_{n=0}^{+\infty} \frac{(At)^n}{n!} = I + (At) + \frac{(At)^2}{2!} + \frac{(At)^3}{3!} + \dots$$

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**3** if I do the same trick above for several  $\lambda$ 's, then I may get a system in  $c_0, \ldots, c_{n-1}t^{n-1}$ 

# Example of evaluating $e^{At}$ via Cayley-Hamilton: spring-mass system with $m=1,\ k=0,\ f=1$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

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$$A^2 + A = 0 \implies A^2 = -A$$

and

$$e^{At}$$
 =  $c_0(t)I$  +  $c_1(t)At$  for opportune  $c_0,c_1$ 

and

 $e^{\lambda t} = c_0(t)I + c_1(t)\lambda t$  if  $\lambda$  is an eigenvalue

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$$m = 1$$
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 = 0,  $\lambda_2$  = -1 and  $e^{\lambda t}$  =  $c_0 I + c_1 \lambda t$  imply then

$$\begin{cases} e^{0t} = c_0(t) + c_1(t)(0t) \\ e^{-1t} = c_0(t) + c_1(t)(-1t) \end{cases}$$

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and thus

$$e^{At} = c_0(t)I + c_1(t)At = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + (1 - e^{-t})\begin{bmatrix} 0 & 1 \\ 0 & -1 \end{bmatrix} = \begin{bmatrix} 1 & 1 - e^{-t} \\ 0 & e^{-t} \end{bmatrix}$$

Damiano's personal view on this way of computing transition matrices: useless from a practical point of view, but useful from an understanding point of view

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#### In other words:

- $\bullet$  to compute  $e^{At}$  use Matlab, Mathematica, whatever. Don't do things by hand
- remember though the concepts, and what the previous ingredients gave us in terms of understanding

## Summary of the messages from Cayley-Hamilton

- square matrices are annihilate their characteristic polynomial
- A is a linear combination of  $I, A, ..., A^{n-1}$
- $e^{At}$  is a time-varying linear combination of  $I, A, \dots, A^{n-1}$
- $\bullet$   $e^{\lambda t}$  with  $\lambda$  eigenvalue of A is a time-varying linear combination of  $1, \lambda, \dots, \lambda^{n-1}$

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Cayley-Hamilton is essential to understand controllability and observability Jordan forms: for sure the best way of understanding the structure of the the modes of LTI systems

If 
$$A = \begin{bmatrix} \lambda & 1 & & 0 \\ & \ddots & \ddots & \\ & & \ddots & 1 \\ 0 & & \lambda \end{bmatrix}$$
 then

$$e^{At} = I + At + A^2 \frac{t^2}{2!} + A^3 \frac{t^3}{3!} + \dots$$

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$$= \begin{bmatrix} e^{\lambda t} & te^{\lambda t} & t^{2}/2!e^{\lambda t} & t^{3}/3!e^{\lambda t} & \dots \\ e^{\lambda t} & te^{\lambda t} & t^{2}/2!e^{\lambda t} & \dots \\ & & \ddots & \\ 0 & & & e^{\lambda t} \end{bmatrix}$$

$$A = \lambda I + N$$
  $\Longrightarrow$   $e^{At} = e^{\lambda It + Nt} = e^{\lambda It}e^{Nt}$ 

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$$e^{\lambda It} = e^{\lambda t}I$$

$$e^{Nt} = I + Nt + N^2 \frac{t^2}{2!} + N^3 \frac{t^3}{3!} + \dots$$

$$= \begin{bmatrix} 1 & t & t^2/2! & t^3/3! & \dots \\ 1 & t & t^2/2! & \dots \\ & & \ddots & \\ 0 & & & 1 \end{bmatrix}$$

### Extremely important message

$$e^{Jt} = \begin{bmatrix} e^{\lambda t} & te^{\lambda t} & t^2/2!e^{\lambda t} & t^3/3!e^{\lambda t} & \cdots \\ & e^{\lambda t} & te^{\lambda t} & t^2/2!e^{\lambda t} & \cdots \\ & & & \ddots & \\ & & & & e^{\lambda t} \end{bmatrix}$$

## Example

$$\dot{x} = Ax(t) + Bu(t)$$
 with  $A = TJT^{-1}$ 

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Then choosing

$$\widetilde{\boldsymbol{x}} = T^{-1} \boldsymbol{x}$$
  $\widetilde{B} = T^{-1} B$ 

leads to

$$\dot{\widetilde{\boldsymbol{x}}} = J\widetilde{\boldsymbol{x}}(t) + \widetilde{B}\boldsymbol{u}(t)$$

$$\dot{\boldsymbol{x}} = A\boldsymbol{x}(t) + B\boldsymbol{u}(t)$$
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and thus to

$$\widetilde{\boldsymbol{x}}(t) = e^{J(t-t_0)}\widetilde{\boldsymbol{x}}(t_0) + \int_{t_0}^t e^{J\tau}\widetilde{B}\boldsymbol{u}(t-\tau)d\tau$$

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and thus to

$$\boldsymbol{x}(t)$$
 =  $T\widetilde{\boldsymbol{x}}(t)$ 

## Jordan form = making the modes explicit

$$y$$
 =  $\widetilde{C}\widetilde{x}$ 

with

$$\widetilde{\boldsymbol{x}}(t) = e^{J(t-t_0)}\widetilde{\boldsymbol{x}}(t_0) + \int_{t_0}^t e^{J\tau}\widetilde{B}\boldsymbol{u}(t-\tau)d\tau$$

and  $e^{J(t-t_0)}$  showing all the modes explicitly

?

# Final summary: all the methods to compute $e^{At}$

#### Direct computation

- use the definition  $e^{At} = I + At + \frac{1}{2!}A^2t^2 + \dots$
- if there exists a k for which  $A^k = \mathbf{0}$  then you can find the exact solution, otherwise it will be approximate

#### By diagonalizing / reducing to a Jordan form

- ullet change the basis of the system so to go from A to  $\Lambda$  or J
- find  $e^{\Lambda t}$  or  $e^{Jt}$  immediately

#### Cayley-Hamilton

- find the coefficients  $c_0(t),\ldots,c_{n-1}(t)$  that give  $e^{At}=c_0(t)I+\ldots+c_{n-1}(t)A^{n-1}$  using the eigenvalues of A
- ullet compute  $e^{At}$  in that way

(we did not see this, and we won't)Inverse Laplace-transforming

A matrix: a strange collection of numbers, or a precise way of defining the dynamics of a system?

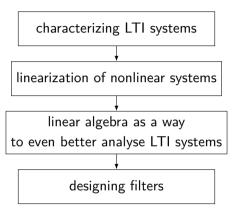
$$\begin{bmatrix} -2 & 2 & -3 \\ 2 & 1 & -6 \\ -1 & -2 & 0 \end{bmatrix}$$

doing systems theory for LTI systems means studying the inner structure of  $\dot{x}=Ax$ . Indeed the Jordan form of A says precisely how the state evolves, while Y(s)=H(s)U(s) tells only what happens between the input and the output

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state-space representations are "richer" than inputoutput ones  $\implies$  one can design control systems better when working with state-space representations

#### Where are we now?



-

A complete example, from the beginning to the end

### Roadmap

• Lotka-Volterra, but this time from the beginning to the end

#### Lotka-Volterra

- $y_{\text{prey}} := \text{prey}$
- $y_{\text{pred}} := \text{predator}$

$$\begin{cases} \dot{y}_{\text{prey}} = \alpha y_{\text{prey}} - \beta y_{\text{prey}} y_{\text{pred}} \\ \dot{y}_{\text{pred}} = -\gamma y_{\text{pred}} + \delta y_{\text{prey}} y_{\text{pred}} \end{cases}$$

GitHub/TTK4225/trunk/Jupyter/Lotka-Volterra-introduction.ipynb

$$\begin{cases} \dot{y}_{\text{prey}} &= 10y_{\text{prey}} - 1y_{\text{prey}}y_{\text{pred}} - u_{\text{prey}} \\ \dot{y}_{\text{pred}} &= -0.1y_{\text{pred}} + y_{\text{prey}}y_{\text{pred}} - u_{\text{pred}} \end{cases}$$

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#### Steps:

find the equilibria

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- Iinearize the system around the equilibria

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- find the equilibria
- linearize the system around the equilibria
- find the stability properties of these equilibria
- characterize the trajectories of the system in the neighborhood of these equilibria
- understand the controllability and observability properties of the system (not in this course)
- design minimal human interventions that make the system behave as desired (not in this course)

!