### LibMesh

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- Goals and example applications of the libMesh library.
- Some basic steps in writing a simple libMesh application.
- Design frameworks for more complex applications.
- Adaptive Mesh Refinement.





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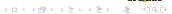
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- A physics implementation.
- A stand-alone application.

- A software library and toolkit.
- Objects and functions for writing parallel adaptive finite element applications.
- An interface to linear algebra, meshing, partitioning, etc. libraries.





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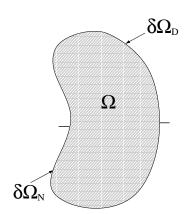


For this talk we will assume there is a mathematical model (Partial Differential Equation) to be solved in an engineering analysis:

$$\frac{\partial u}{\partial t} = \mathcal{R}(u) \in \Omega$$

$$u = u_D \in \partial \Omega_D$$

$$\nabla u \cdot n = u_N \in \partial \Omega_N$$

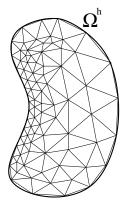






- Associated to the problem domain Ω is a libMesh data structure called a Mesh
- A Mesh is essentially a collection of finite elements

$$\Omega^h:=\bigcup\Omega_e$$

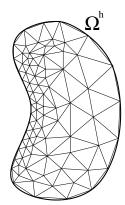






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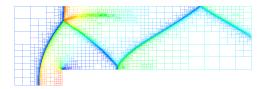


 libMesh provides some simple structured mesh generation routines as well as an interface to Triangle.





# Compressible Gas Flow

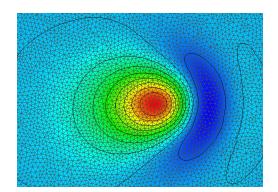


Mach 3 flow over a forward facing step.





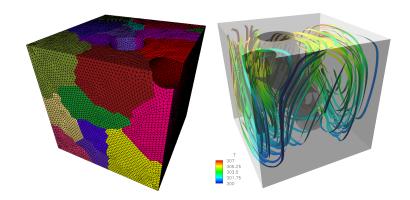
## **Shallow Water Flow**



Wave propagation from depth-averaged equations



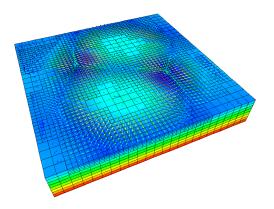
### Natural Convection



• Tetrahedral mesh of "pipe" geometry. Stream ribbons colored by temperature.



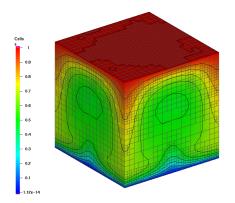
## Surface-Tension-Driven Flow



 Adaptive grid solution shown with temperature contours and velocity vectors.



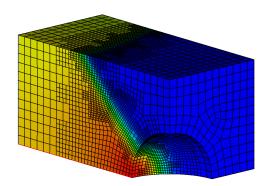
## **Double-Diffusive Convection**



• Solute contours: a plume of warm, low-salinity fluid is convected upward through a porous medium.



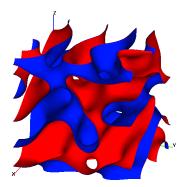
# **Tumor Angiogenesis**



 The tumor secretes a chemical which stimulates blood vessel formation.



## Cahn-Hilliard Phase Decomposition



 Quenching separates fluid or alloy mixtures into multiple material phases.





 The point of departure in any FE analysis which uses LibMesh is the weighted residual statement

$$(\mathscr{R}(u), v) = 0 \qquad \forall v \in \mathcal{V}$$

• Or, more precisely, the weighted residual statement associated with the finite-dimensional space  $V^h \subset V$ 

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### Poisson Equation

$$-\Delta u = f \in \Omega$$





### **Poisson Equation**

$$-\Delta u = f \in \Omega$$

### Weighted Residual Statement

$$(\mathscr{R}(u), v) := \int_{\Omega} \left[ \nabla u \cdot \nabla v - f v \right] dx$$
$$+ \int_{\partial \Omega_N} \left( \nabla u \cdot \boldsymbol{n} \right) v \, ds$$





### Linear Convection-Diffusion

$$-k\Delta u + \boldsymbol{b} \cdot \nabla u = f \in \Omega$$





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### Weighted Residual Statement

$$(\mathcal{R}(u), v) := \int_{\Omega} [k \nabla u \cdot \nabla v + (\boldsymbol{b} \cdot \nabla u)v - fv] dx + \int_{\partial \Omega} k (\nabla u \cdot \boldsymbol{n}) v ds$$





### Stokes Flow

$$\nabla p - \nu \Delta \mathbf{u} = \mathbf{f} \\
\nabla \cdot \mathbf{u} = 0 \qquad \in \Omega$$





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$$\begin{array}{rcl}
\nabla p - \nu \Delta \boldsymbol{u} &= \boldsymbol{f} \\
\nabla \cdot \boldsymbol{u} &= 0
\end{array}
\in \Omega$$

### Weighted Residual Statement

$$u := [\boldsymbol{u}, p]$$
 ,  $v := [\boldsymbol{v}, q]$ 

$$(\mathcal{R}(\boldsymbol{u}), \boldsymbol{v}) := \int_{\Omega} \left[ -p \left( \nabla \cdot \boldsymbol{v} \right) + \nu \nabla \boldsymbol{u} : \nabla \boldsymbol{v} - \boldsymbol{f} \cdot \boldsymbol{v} \right.$$
$$+ \left. \left( \nabla \cdot \boldsymbol{u} \right) q \right] d\boldsymbol{x} + \int_{\partial \Omega_{N}} \left( \nu \nabla \boldsymbol{u} - p \boldsymbol{I} \right) \cdot \boldsymbol{n} \cdot \boldsymbol{v} ds$$



• To obtain the approximate problem, we simply replace  $u \leftarrow u^h$ ,  $v \leftarrow v^h$ , and  $\Omega \leftarrow \Omega^h$  in the weighted residual statement.





# Poisson Equation

• For simplicity we will focus on the weighted residual statement arising from the Poisson equation, with  $\partial \Omega_N = \emptyset$ .

$$(\mathscr{R}(u^h), v^h) :=$$

$$\int_{\Omega^h} \left[ \nabla u^h \cdot \nabla v^h - f v^h \right] dx = 0 \qquad \forall v^h \in \mathcal{V}^h$$





• The integral over  $\Omega^h$  ...

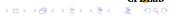
$$0 = \int_{\Omega^h} \left[ \nabla u^h \cdot \nabla v^h - f v^h \right] dx \quad \forall v^h \in \mathcal{V}^h$$



• The integral over  $\Omega^h$  ... is written as a sum of integrals over the  $N_e$  finite elements:

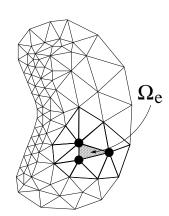
$$0 = \int_{\Omega^h} \left[ \nabla u^h \cdot \nabla v^h - f v^h \right] dx \quad \forall v^h \in \mathcal{V}^h$$
$$= \sum_{h=1}^{N_e} \int_{\Omega_e} \left[ \nabla u^h \cdot \nabla v^h - f v^h \right] dx \quad \forall v^h \in \mathcal{V}^h$$





- An element integral will have contributions only from the global basis functions corresponding to its nodes.
- We call these local basis functions  $\phi_i$ ,  $0 \le i \le N_s$ .

$$\left|v^{h}\right|_{\Omega_{e}}=\sum_{i=1}^{N_{s}}c_{i}\phi_{i}$$



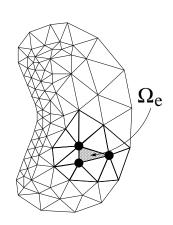




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$$v^h\big|_{\Omega_e} = \sum_{i=1}^{N_s} c_i \phi_i$$

$$\int_{\Omega_e} v^h \, dx = \sum_{i=1}^{N_s} c_i \int_{\Omega_e} \phi_i \, dx$$







• The element integrals ...

$$\int_{\Omega_e} \left[ \nabla u^h \cdot \nabla v^h - f v^h \right] dx$$





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$$\int_{\Omega_e} \left[ \nabla u^h \cdot \nabla v^h - f v^h \right] dx$$

• are written in terms of the local " $\phi_i$ " basis functions

$$\sum_{i=1}^{N_s} u_i \int_{\Omega_e} \nabla \phi_i \cdot \nabla \phi_i \, dx - \int_{\Omega_e} f \phi_i \, dx \quad , \quad i = 1, \dots, N_s$$



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• This can be expressed naturally in matrix notation as

$$K^eU^e - F^e$$





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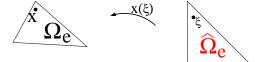
 The element stiffness matrices and right-hand sides can be "assembled" to obtain the global system of equations

$$KU = F$$





• The integrals are performed on a "reference" element  $\hat{O}$ 







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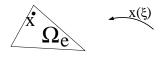
• The Jacobian of the map  $x(\xi)$  is J.

$$m{F}_i^e = \int_{\Omega_e} f \phi_i dx = \int_{\hat{\Omega}_e} f(x(\xi)) \phi_i |J| d\xi$$





• The integrals are performed on a "reference" element  $\hat{\Omega}_{\rho}$ 





• Chain rule:  $\nabla = J^{-1}\nabla_{\xi} := \hat{\nabla}_{\xi}$ .

$$\mathbf{K}_{ij}^{e} = \int_{\Omega_{e}} \nabla \phi_{j} \cdot \nabla \phi_{i} \, dx = \int_{\hat{\Omega}_{e}} \hat{\nabla}_{\xi} \phi_{j} \cdot \hat{\nabla}_{\xi} \phi_{i} \, |J| d\xi$$





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$$F_i^e = \int_{\hat{\Omega}_e} f\phi_i |J| d\xi$$

$$\approx \sum_{q=1}^{N_q} f(x(\xi_q))\phi_i(\xi_q) |J(\xi_q)| w_q$$





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ullet LibMesh provides the following variables at each quadrature point q

Code	Math	Description
JxW[q]	$ J(\xi_q) w_q$	Jacobian times weight
phi[i][q]	$\phi_i(\xi_q)$	value of $i^{th}$ shape fn.
dphi[i][q]	$\hat{\nabla}_{\xi}\phi_{i}(\xi_{q})$	value of $i^{th}$ shape fn. gradient
xyz[d]	$x(\xi_q)$	location of $\xi_q$ in physical space







$$F_i^e = \sum_{q=1}^{N_q} f(x(\xi_q))\phi_i(\xi_q)|J(\xi_q)|w_q|$$



$$\boldsymbol{F}_{i}^{e} = \sum_{q=1}^{N_{q}} f(x(\xi_{q}))\phi_{i}(\xi_{q})|\boldsymbol{J}(\xi_{q})|\boldsymbol{w}_{q}|$$



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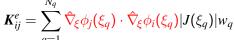
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- Concrete Subclasses implement functionality.
- One physics code can work with many discretizations





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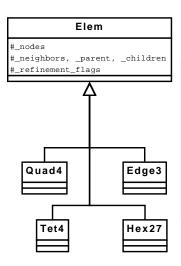


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## Geometric Element Classes

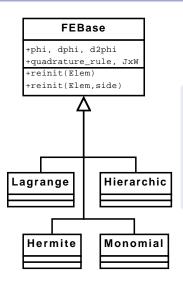


- Abstract interface gives mesh topology
- Concrete instantiations of mesh geometry
- Hides element type from most applications





## Finite Element Classes



- Finite Element object builds data for each Geometric object
- User only deals with shape function, quadrature data





 For linear problems, we have already seen how the weighted residual statement leads directly to a sparse linear system of equations

$$KU = F$$





For time-dependent problems,

$$\frac{\partial u}{\partial t} = \mathscr{R}(u)$$

• we also need a way to advance the solution in time, e.g. a  $\theta$ -method

$$\left(\frac{u^{n+1}-u^n}{\Delta t},v^h\right) = \left(\mathscr{R}(u_\theta),v^h\right) \ \forall v^h \in \mathcal{V}^h$$
$$u_\theta := \theta u^{n+1} + (1-\theta)u^n$$

• Leads to KU = F at each timestep.





 For nonlinear problems, typically a sequence of linear problems must be solved, e.g. for Newton's method

$$(\mathscr{R}'(u^h)\delta u^h, v^h) = -(\mathscr{R}(u^h), v^h)$$

where  $\mathcal{R}'(u^h)$  is the linearized (Jacobian) operator associated with the PDE.

 Must solve KU = F (Inexact Newton method) at each iteration step.





Introduction Applications Weighted Residuals Finite Elements Essential BCs Complex Problems Adaptivity

## Boundary Value Problem Framework Goals

#### Goals:

- Improving test coverage and reliability
- Hiding of implementation details from user code
- Rapid prototyping of differential equation approximations
- Improved error estimation

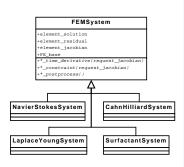
#### Methods:

- Object-oriented System and Solver classes
- Numerical Jacobian verification





# FEM System Classes

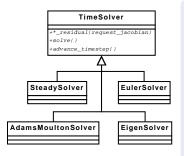


- Generalized IBVP representation
- FEMSystem does all initialization, global assembly
- User code only needs weighted time derivative and/or constraint functions





### **ODE Solver Classes**

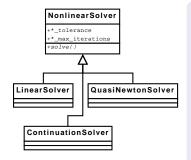


- Calls user code on each element
- Assembles
   element-by-element
   time derivatives,
   constraints, and
   weighted old
   solutions





### Nonlinear Solver Classes



- Acquires residuals, jacobians from ODE solver
- Handles inner loops, inner solvers and tolerances, convergence tests, etc





# 1D refinement example

Consider the 1D model convection-diffusion equation equation

$$\begin{cases}
-u'' + bu' = 0 & \in 0 \le x \le 1 \\
u(0) = 0 \\
u(1) = 1
\end{cases}$$

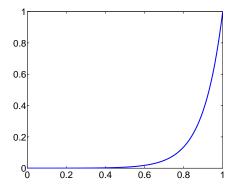
- The convection-diffusion equation can be thought of as a particularly simple form of the drift-diffusion equation.
- The exact solution is

$$u = \frac{1 - \exp(bx)}{1 - \exp(b)}$$





- For large values of b, the solution changes rapidly near x = 1.
- The solution for b = 10.







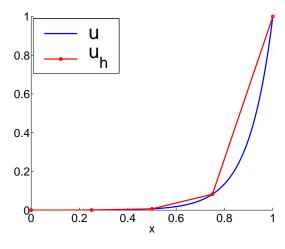
- We assume here that we have an approximate solution u<sub>h</sub> which is the *linear interpolant* of u.
- We will measure the error between the exact solution u and the approximate solution  $u_h$  in the following  $(L_2)$  norm:

$$||e||_{L_2}^2 := ||u - u_h||_{L_2}^2$$
  
=  $\int_0^1 (u - u_h)^2 dx$ 

• Consider a sequence of uniformly-refined meshes . . .



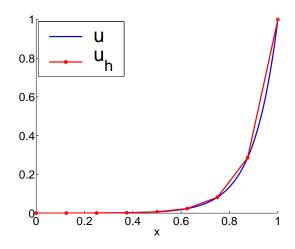




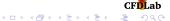
4 elements,  $||e||_{L_2} = 0.09$ 

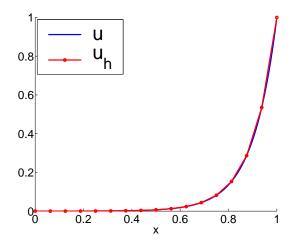






8 elements,  $||e||_{L_2} = 0.027$ 





16 elements,  $||e||_{L_2} = 0.0071$ 





### Adaptive Refinement

- Q: Can we do "better" than uniform refinement?
- A: Yes, if we refine cells which have higher error relative to others.





# A Simple Error Indicator

- In general we don't know the exact solution, and so we need a way of estimating the error.
- Consider the following formula for estimating the error,  $\eta$ , in an element defined on the interval  $(x_i, x_{i+1})$

$$\eta^2 := \frac{h}{2} \sum_{k=i}^{i+1} [\![u'(x_k)]\!]^2$$

where  $h := x_{i+1} - x_i$  is the element length, and

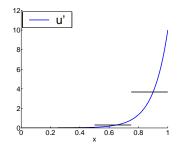
• The "jump" in u' is

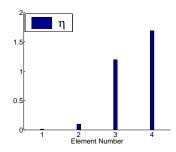
$$[\![u'(x_k)]\!] := |u'(x_k^+) - u'(x_k^-)|$$





### Error Indicator, Uniformly-Refined Grids



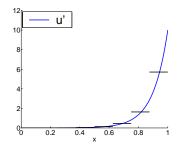


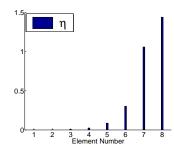
4 elements





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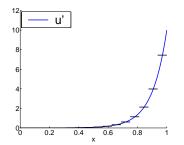


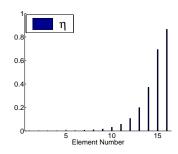
8 elements





## Error Indicator, Uniformly-Refined Grids





16 elements





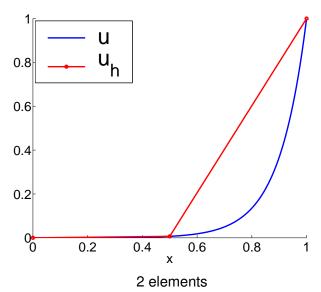
## **Adaptation Strategy**

 A simple adaptive refinement strategy with r\_max refinement steps for this 1D example problem is:

```
r=0;
while (r < r_max)
  Compute the FE solution (linear interpolant)
  Estimate the error (using flux-jump indicator)
  Refine the element with highest error
  Increment r
end</pre>
```

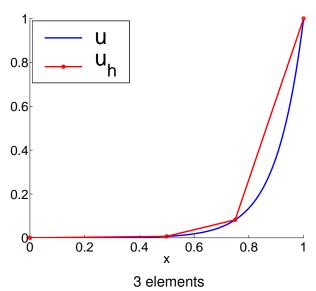






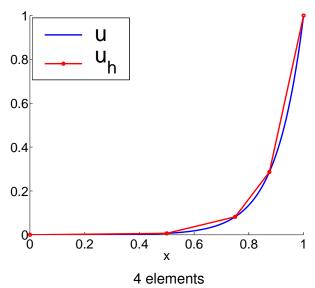






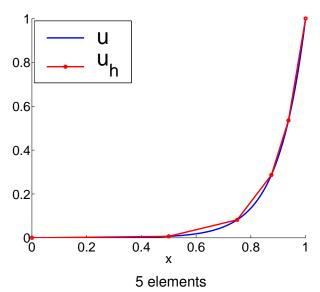






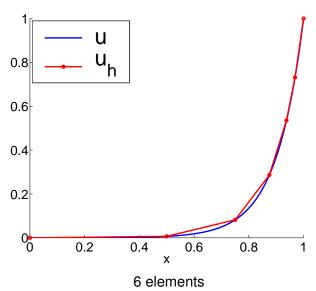






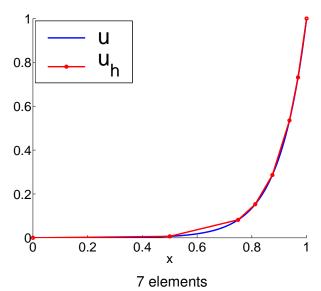






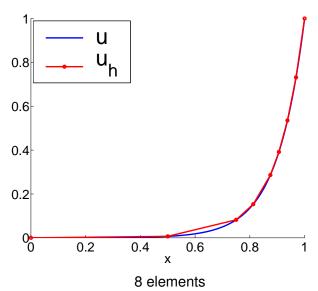






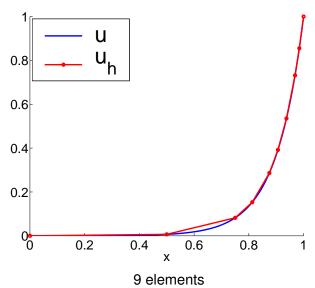






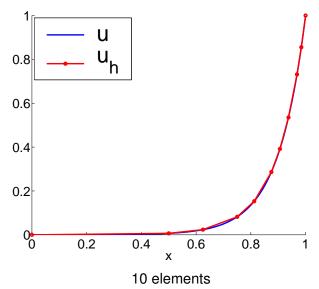






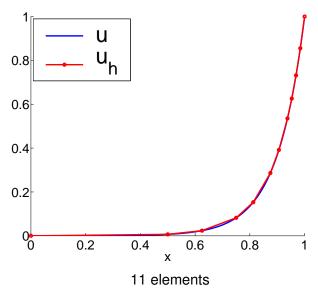






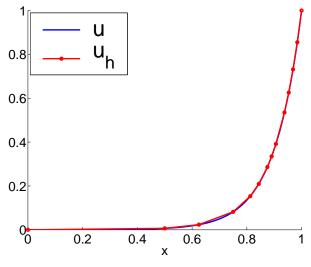








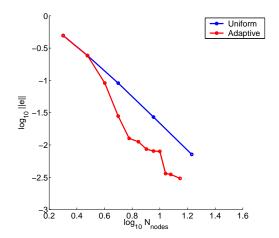




Final: 13 elements



### Error Plot vs. Number of Nodes

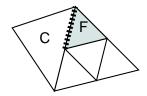






## h Adaptivity Constraints

Non-conforming meshes lead to "hanging nodes", and to provide continuous finite element function the fine element degrees of freedom must be constrained in terms of coarse element degrees of freedom.



$$\sum_{i} u_{i}^{F} \phi_{i}^{F} = u^{C}$$

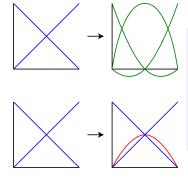
$$\sum_{i} u_{i}^{F} \phi_{i}^{F} = \sum_{j} u_{j}^{C} \phi_{j}^{C}$$

$$u_{i}^{F} = C_{ij} u_{j}^{C}$$





### Adaptive *p* Constraints

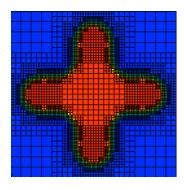


- p refinement is done with hierarchic adaptivity
- Hanging degree of freedom coefficients are simply set to 0





### Diffuse Interface Modeling with AMR/C



- Mesh coarsening in smooth regions is traded for mesh refinement in sharp layers
- Equivalent accuracy is achieved here with 75% fewer degrees of freedom than a uniform mesh





## Installing libMesh

PETSc Download, Installation instructions, Documentation:

http://www-unix.mcs.anl.gov/petsc/petsc-2/

libMesh Downloads, Installation instructions, Documentation:

http://libmesh.sourceforge.net/





#### Reference

 B. Kirk, J. Peterson, R. Stogner and G. Carey, "libMesh: a C++ library for parallel adaptive mesh refinement/coarsening simulations", *Engineering with* Computers, in press.



