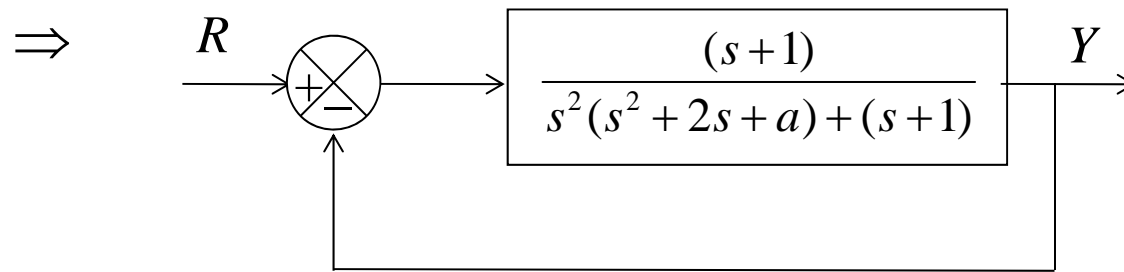
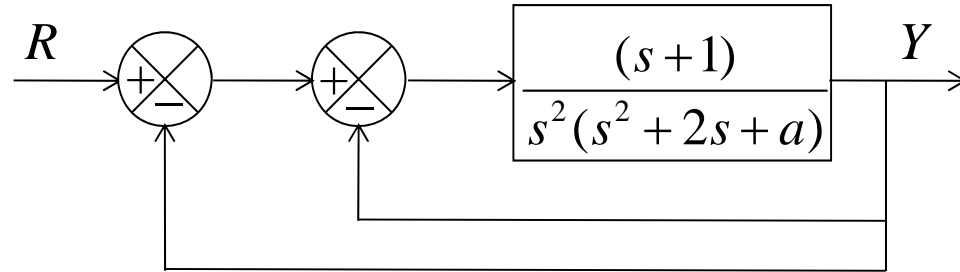


EE3011 MODEL& CONTROL
Tutorial 5 (Solutions) System Performance

1.



$$G(s) = \frac{(s+1)}{s^2(s^2 + 2s + a) + (s+1)}$$

The system is type '0' (with respect to $R(s)$)!

$$\frac{Y}{R} = \frac{G(s)}{1+G(s)} = \frac{s+1}{s^2(s^2 + 2s + a) + 2(s+1)}$$

When $a = 5$, C.E.: $q(s) = s^4 + 2s^3 + 5s^2 + 2s + 2 = 0$

The Routh array is

s^4	1	5	2
s^3	2	2	
s^2	4	2	
s^1	1		
s^0	2		

The system is stable and hence

$$K_{pos} = \lim_{s \rightarrow 0} G(s) = \lim_{s \rightarrow 0} \frac{(s+1)}{s^2(s^2 + 2s + 5) + (s+1)} = 1$$

K_{vel} and K_{acc} are both zero because the system is type '0'.

The steady-state value of $y(t)$ w.r.t unit step input is

$$y_{ss}(\text{unit-step}) = \lim_{s \rightarrow 0} sY(s) = \lim_{s \rightarrow 0} s \frac{(s+1)}{s^2(s^2 + 2s + 5) + 2(s+1)} \times \frac{1}{s} = \frac{1}{2}$$

When $a = 2$, C.E.: $q(s) = s^4 + 2s^3 + 2s^2 + 2s + 2 = 0$

The Routh array is

s^4	1	2	2
s^3	2	2	
s^2	1	2	
s^1	-2		
s^0	2		

The system is unstable and hence the notions of error constants are not useful here. If one simply compute steady-state value of $y(t)$ w.r.t unit step input using final value theorem,

$$y_{ss}(\text{unit-step}) = \lim_{s \rightarrow 0} sY(s) = \lim_{s \rightarrow 0} s \frac{(s+1)}{s^2(s^2 + 2s + 2) + 2(s+1)} \times \frac{1}{s} = \frac{1}{2}$$

one would get a wrong answer. Here, the system is unstable and hence the steady state error w.r.t. unit-step input is infinity!

2a. Let's focus on the output due to disturbance input $W(s) = \frac{a}{s}$

$$\begin{aligned}\frac{Y_W}{W} &= \frac{\frac{1}{s(s+10)}}{1 + \frac{sK_P + K_I}{s^2(s+10)}} \\ &= \frac{s}{s^3 + 10s^2 + sK_P + K_I} \quad (\text{notice the } s \text{ term in the numerator})\end{aligned}$$

$$Y_W = \frac{s}{s^3 + 10s^2 + sK_P + K_I} \times \frac{a}{s}$$

$$y_{ssw} = \lim_{s \rightarrow 0} sY_W(s) = \begin{cases} 0 & \text{if } K_I \neq 0 \text{ and } 10K_P > K_I > 0 \\ \frac{a}{K_P} & \text{if } K_I = 0 \text{ and } K_P > 0 \end{cases}$$

2b. With disturbance input enters at the output:

$$\begin{aligned}\frac{Y_W}{W} &= \frac{1}{1 + \frac{sK_P + K_I}{s^2(s+10)}} \\ &= \frac{s^2(s+10)}{s^3 + 10s^2 + sK_P + K_I} \quad (\text{notice the } s^2 \text{ term in the numerator})\end{aligned}$$

$$Y_W = \frac{s^2(s+10)}{s^3 + 10s^2 + sK_P + K_I} \times \frac{a}{s}$$

$$y_{ssw} = \lim_{s \rightarrow 0} sY_W(s) = \begin{cases} 0 & \text{if } K_I \neq 0 \text{ and } 10K_P > K_I > 0 \\ 0 & \text{if } K_I = 0 \text{ and } K_P > 0 \end{cases}$$

$$3. \quad G(s) = \frac{K}{s(s+a)(s+b)} = \frac{K}{s^3 + (a+b)s^2 + abs}$$

$$T(s) = \frac{Y(s)}{R(s)} = \frac{G(s)}{1+G(s)} = \frac{K}{s(s+a)(s+b) + K}$$

$$\begin{aligned} S_K^T &= \frac{dT(s)}{dK} \cdot \frac{K}{T(s)} = \frac{(s(s+a)(s+b) + K) - K}{(s(s+a)(s+b) + K)^2} \cdot \frac{s(s+a)(s+b) + K}{1} \\ &= \frac{s(s+a)(s+b)}{s(s+a)(s+b) + K} = \frac{1}{1 + \frac{K}{s(s+a)(s+b)}} \end{aligned}$$

Or

$$\begin{aligned} S_K^T &= \frac{dT(s)}{dG(s)} \cdot \frac{dG(s)}{dK} \cdot \frac{K}{T(s)} = \frac{1}{(1+G)^2} \cdot \frac{1}{s(s+a)(s+b)} \cdot \frac{s(s+a)(s+b) + K}{1} \\ &= \frac{1}{1 + \frac{K}{s(s+a)(s+b)}} \end{aligned}$$

$$\begin{aligned}
S_a^T &= \frac{dT(s)}{dG(s)} \cdot \frac{dG(s)}{da} \cdot \frac{a}{T(s)} \\
&= \frac{1}{(1+G)^2} \cdot \frac{-K(s^2 + bs)}{(s(s+a)(s+b))^2} \cdot \frac{a(s(s+a)(s+b) + K)}{K} \\
&= \frac{-a(s^2 + bs)}{s(s+a)(s+b) + K} = \frac{-1}{1 + \frac{s^3 + bs^2 + K}{a(s^2 + bs)}}
\end{aligned}$$

$$\begin{aligned}
S_b^T &= \frac{dT(s)}{dG(s)} \cdot \frac{dG(s)}{db} \cdot \frac{b}{T(s)} \\
&= \frac{1}{(1+G)^2} \cdot \frac{-K(s^2 + as)}{(s(s+a)(s+b))^2} \cdot \frac{b(s(s+a)(s+b) + K)}{K} \\
&= \frac{-b(s^2 + as)}{s(s+a)(s+b) + K} = \frac{-1}{1 + \frac{s^3 + as^2 + K}{b(s^2 + as)}}
\end{aligned}$$

4. For the open-loop system:

$$T_1(s) = \frac{Y(s)}{R(s)} = \frac{K}{s + \alpha} = \frac{K}{s + 10} \quad \text{when } \alpha = 10$$

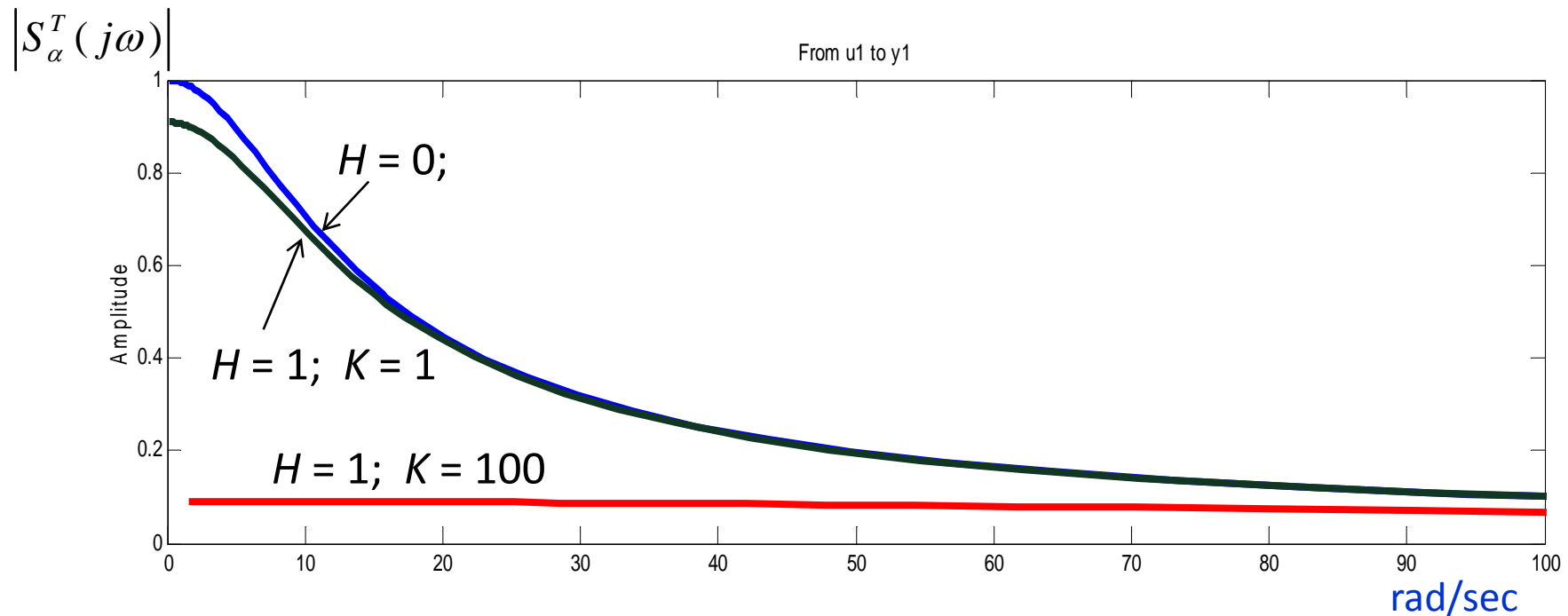
$$S_{\alpha}^{T_1} = \frac{dT_1(s)}{d\alpha} \cdot \frac{\alpha}{T_1(s)} = \frac{-K}{(s + \alpha)^2} \cdot \frac{\alpha(s + \alpha)}{K} = \frac{-\alpha}{s + \alpha} = \frac{-10}{s + 10} \quad \text{when } \alpha = 10$$

The sensitivity function is independent of K !

For the closed-loop system:

$$T_2(s) = \frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)} = \frac{K}{s + \alpha + K} = \frac{K}{s + 10 + K} \quad \text{when } \alpha = 10$$

$$\begin{aligned} S_{\alpha}^{T_2} &= \frac{dT_2(s)}{d\alpha} \cdot \frac{\alpha}{T_2(s)} = \frac{-K}{(s + \alpha + K)^2} \cdot \frac{\alpha(s + \alpha + K)}{K} = \frac{-\alpha}{s + \alpha + K} \\ &= \frac{-10}{s + 10 + K} \quad \text{when } \alpha = 10 \end{aligned}$$



The sensitivity of both the open-loop and closed-loop systems decreases with increasing frequency, with the closed-loop system having lower sensitivity (provided $K > 0$)

The sensitivity for the closed-loop system decreases with increasing K .

5. For the open-loop system:

$$T_1(s) = \frac{Y(s)}{R(s)} = \frac{K}{s^2 + 4s + 5} = \frac{2}{s^2 + 4s + 5} \quad \text{when } K = 2$$

For the closed-loop system:

$$T_2(s) = \frac{Y(s)}{R(s)} = \frac{K}{(s+1)(s+3) + K} = \frac{2}{s^2 + 4s + 5} \quad \text{when } K = 2$$

The sensitivity of the open-loop system:

$$S_K^{T_1} = \frac{dT_1(s)}{dK} \cdot \frac{K}{T_1(s)} = \frac{1}{s^2 + 4s + 5} \cdot \frac{s^2 + 4s + 5}{1} = 1$$

The sensitivity function is 1 for all K , and all frequencies.

The sensitivity of the closed-loop system:

$$\begin{aligned} S_K^{T_2} &= \frac{dT_2(s)}{dK} \cdot \frac{K}{T_2(s)} = \frac{(s+1)(s+3) + K - K}{((s+1)(s+3) + K)^2} \cdot \frac{(s+1)(s+3) + K}{1} \\ &= \frac{1}{1 + \frac{K}{(s+1)(s+3)}} = \frac{1}{1 + \frac{2}{(s+1)(s+3)}} \quad \text{when } K=2 \end{aligned}$$

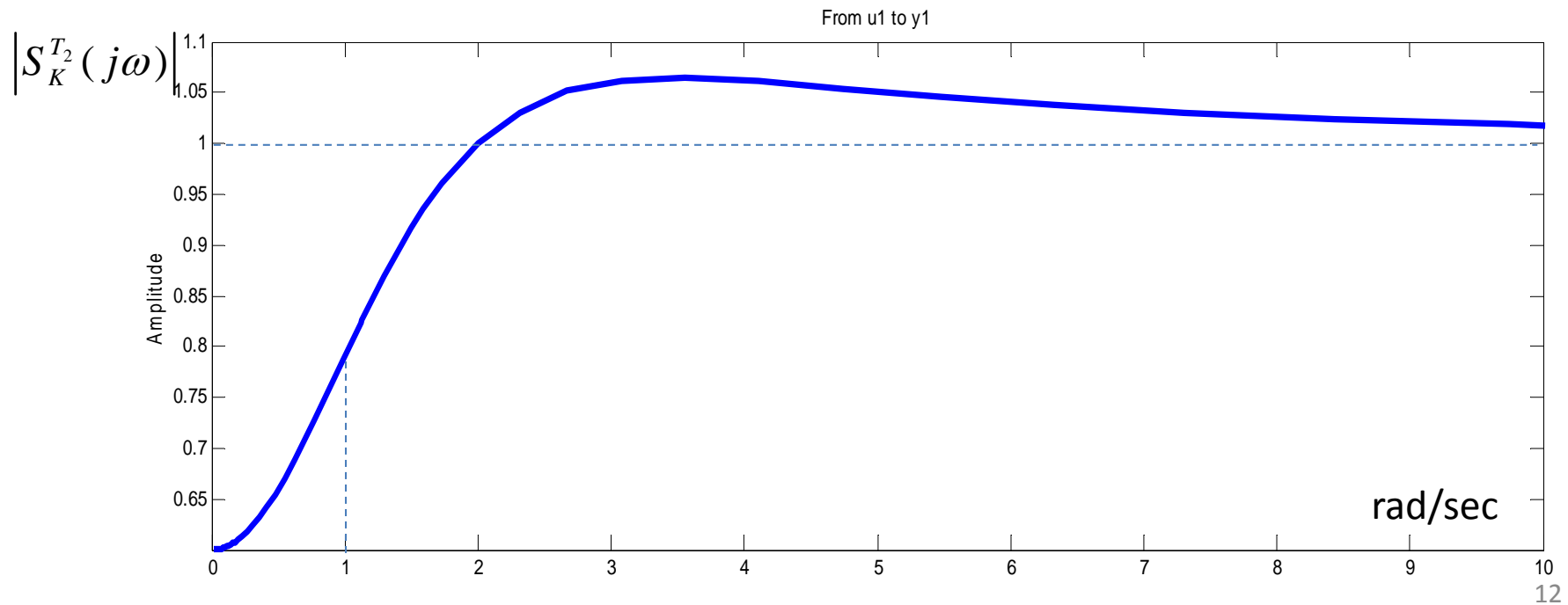
The sensitivity function is dependent on K , and the complex variable s , i.e. it also depends on the frequencies.

Thus, the sensitivity function can be adjusted by varying K or restricting the frequencies of the input function to within an appropriate range.

With $s = j\omega$: $S_K^{T_2}(j\omega) = \frac{1}{1 + \frac{2}{(3 - \omega^2 + j4\omega)}} \quad \text{when } K=2$

When $\omega = 0$, $S_K^{T_2}(j0) = \frac{1}{1 + \frac{2}{3}} = 0.6$

When $\omega = 1 \text{ rad/sec}$, $|S_K^{T_2}(j1)| = \left| \frac{1}{1 + \frac{2}{2+j4}} \right| = 0.79$



Thus, the closed-loop system is 40% less sensitive than open-loop system when at steady-state, and 21% less sensitive than the open-loop system for low frequencies (< 1 rad/s). For high frequencies, the sensitivity of the closed-loop system approaches 1, the same as that of the open-loop system.

It's interesting to note that for this problem, the sensitivity of the closed-loop system is higher than that of the open-loop system for certain range of frequencies (> 2 rad/s)!