

1) $I-\phi 230V$

25A Type B MCB

PVC 1/c copper

$$S_{ph} = 4\text{mm}^2, S_{CPC} = 2.5\text{mm}^2$$

$$L = 30\text{m}$$

$$Z_E = 5\Omega$$

$$R_A = 2\Omega$$

a) Shock protection $\Rightarrow Z_s \leq Z_{smax}$

$$Z_{smax} = 230/125 = 1.84\Omega \text{ CP5 Type B MCB graph, pg 196}$$

CP5 Table 17A pg 222

$$\begin{aligned} Z_s &= Z_E + 1.38 [R_1 + R_2] \times 10^3 \times L \\ &= 5 + 1.38 [12.02] \times 10^3 \times 30 \\ &= 5.497628\Omega \end{aligned}$$

Since $Z_s > Z_{smax} \therefore$ does not complies with shock protection requirement X

b) $I_f = V/Z_s$

$$= 230/5.497628$$

$$= 41.84A \text{ } \cancel{\text{X}}$$

c) $k = 115 \text{ } \cancel{\text{A}} \text{ copper PVC @ } 70^\circ\text{C}$

thermal constraints of CPC $\Rightarrow S_{CPC}^2 k^2 \geq I_f^2 t$

$$t = 700s \text{ CP5 Type B MCB graph, pg 196}$$

Check:

$$S_{CPC}^2 k^2 \geq I_f^2 t$$

$$(2.5)^2 \times (115)^2 \geq (41.84)^2 \times (700)$$

$$82656 \geq 1225410 \text{ (false)}$$

\therefore The size of CPC is unable to meet the thermal constraints requirement. X

d) V_t without bonding $\Rightarrow I_f \times (R_z + R_A)$

$$R_z = 1.38 \times [R_z'] \times 10^{-3} \times L$$

$$R_z' = [r] / 2 \quad \text{Assume the cable is in the wall.}$$

$T = 18 \quad \text{CP5 Table 4D1B, col. 3, pg 218}$

$$\Rightarrow R_z = 1.38 \times \left[\frac{18}{2} \right] \times 10^{-3} \times 30 \\ = 0.3726 \Omega$$

$$V_t = 41.84 \times [2 + 0.3726] \\ = 99.27 V$$

Assume human body impedance under dry condition = 100 k Ω ,
 $I_b = V_t / 100k = 0.9927 mA$

Under "Consequences on the individual" graph, I_b is located in AC-2.
Under AC-2 region, there is usually no harmful physiological effects. $\cancel{\text{X}}$

e) V_t with bonding $\Rightarrow I_f \times (R_z)$

$$V_t = (41.84) \times (0.3726) \\ = 15.58 V$$

Comparing both V_t result, we can conclude that bonded equipment have lower touch voltage which can reduce the risk of a person when touching the faulted equipment. $\#$

2a) 3-Ø 400V

2 set 11C PVC copper cable

flat & touching on a horizontal cable tray

Max demand 1400A

temperature 35°C

Since 2 sets, assume identical set with each carrying 700A

$$I_Z \geq I_n / (C_a \times C_i \times C_g), I_n = 700A$$

$$C_i = 1, C_a = 0.94, C_g = 0.9$$

CP5 Table 4C1 CP5 Table 4B1

$$I_Z = 700 / (1 \times 0.94 \times 0.9)$$
$$= 827A$$

$$I_{tab} = 892A \Rightarrow S = 630 \text{ mm}^2$$

CP5 Table 4D1A, Col 9, pg 217

b) $V_{d\max} = 1.5\% \text{ of } 400V$
 $= 6V$

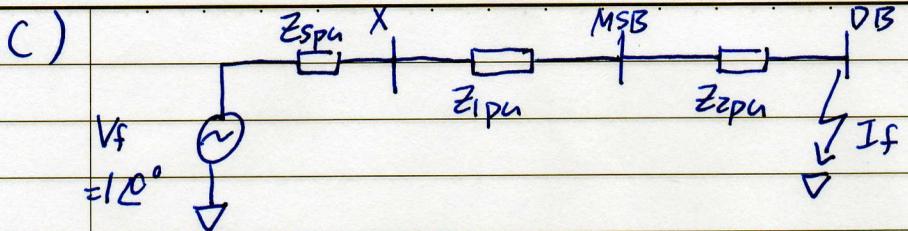
$$V_d = [r \cos \theta + X \sin \theta] \times 10^{-3} \times L \times I_{SL}$$
$$\theta = \cos^{-1}(0.85) = 31.8^\circ, L = 30m, I_{SL} = 150A$$

$$r = 0.56, X = 0.25$$

CP5 Table 4D1B, Col 6, pg 218

$$V_d = [0.56 \cos(31.8^\circ) + 0.25 \sin(31.8^\circ)] \times 10^{-3} \times 30 \times 150$$
$$= 2.735V$$

Since $V_d < V_{d\max}$ ∴ the cable comply with the voltage drop requirement.



$$S_b = 1000 \text{ MVA}$$

$$V_{b1} = 22 \text{ kV}, V_{b2} = 400 \text{ V}$$

$$Z_{b2} = 0.00016 \Omega$$

$$I_{b2} = 1.443 \text{ MA}$$

$$Z_{spn} = j0.05$$

CP5 Table 4DIB, Col 8, Pg 218

$$\begin{aligned} Z_{ipn} &= [(R+jX) \times 10^3 \times L_1] / [2 \times \sqrt{3} \times Z_{b2}] \\ &= [(0.072+j0.21) \times 10^3 \times 20] / [2 \times \sqrt{3} \times 0.00016] \\ &= 8.011 \angle 71^\circ \end{aligned}$$

CP5 Table 4DIB, Col 6, Pg 218

$$\begin{aligned} Z_{2pn} &= [(R+jX) \times 10^3 \times L_2] / [\sqrt{3} \times Z_{b2}] \\ &= [(0.56+j0.25) \times 10^3 \times 30] / [\sqrt{3} \times 0.00016] \\ &= 66.39 \angle 24.1^\circ \end{aligned}$$

$$\begin{aligned} I_f &= V_f / [Z_{spn} + Z_{ipn} + Z_{2pn}] \\ &= 0.01386 \angle -28.8^\circ \end{aligned}$$

$$\begin{aligned} |I_{\text{actual}}| &= 0.01386 \times I_{b2} \\ &= 20 \text{ kA} \end{aligned}$$

3a) Risk due to lightning to the building structure resulting physical damage.
(S1) (D2)

$$\Rightarrow R_B = N_D \times P_B \times r_p \times h_z \times r_f \times L_f$$

$$\Rightarrow N_D = N_g \times A_d \times C_d \times 10^6$$

$$\Rightarrow A_d = [L \times W] + [6H(L+W)] + [9\pi H^2]$$

$$A_d = [40 \times 20] + [6 \times 25 \times (40+20)] + [9\pi \times (25)^2]$$
$$= 27471$$

$$N_g = 25 \text{ (NTU)}$$

$$C_d = 1 \text{ (point (iv))}$$

$$\Rightarrow N_D = 0.686775$$

$$P_B = 1 \text{ (point (iii))}$$

$$r_p = 1 \text{ (point (ii))}$$

$$h_z = 2 \text{ (70 staff)}$$

$$r_f = 10^3 \text{ (point (ii))}$$

$$L_f = 10^1 \text{ (office building)}$$

$$\Rightarrow R_B = 1.37355 \times 10^{-4} \text{ } \cancel{\text{x}}$$

b) $R_B > R_{tol.} \Rightarrow 1.37355 \times 10^{-4} > 1 \times 10^{-5}$

We assume certain factor to remain the same due to constraint such as location and building size. (A_d, C_d, N_g, h_z, r_f & L_f remain the same)

Method 1: Install LPS of Class 2 or higher. $\cancel{\text{x}}$

Method 2: Install LPS of Class 3 or higher in addition to provision of fire extinguishers. $\cancel{\text{x}}$

Method 3: Install LPS of Class 4 or higher in addition to provision of fixed automatically operated extinguishing installations. $\cancel{\text{x}}$

The method is chosen such that $R_B \text{ new} < 10^{-5}$