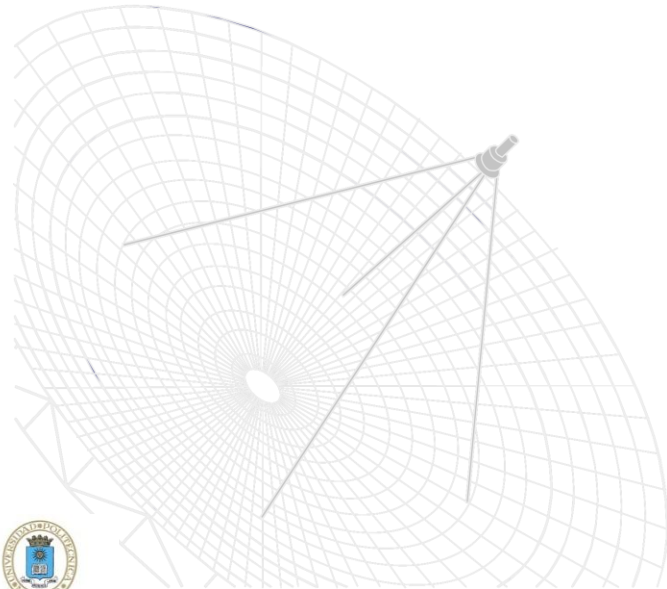


# Master in Space Science and Technology

## Thermal engineering

*Isidoro Martínez*



# Thermal engineering

## •Thermodynamics

### – Basics

- Energy and entropy
- Temperature and thermometry
- Variables: state properties, process functions
- Equations of state, simple processes
- Phase change

### – Applied:

- Mixtures. Humid air (air conditioning)
- Thermochemistry (combustion)
- Heat engines (power generation)
- Refrigeration (cold generation)
- Thermal effects on materials and processes
- Thermofluiddynamic flow 1D...

## •**Heat transfer (conduction, convection, radiation, heat exchangers)**



# Thermodynamics

- **Basic thermodynamics**

- The science of heat and temperature. Work. Energy. Thermal energy.
- Energy and entropy. The isolated system. The traditional Principles
- Generalisation (mass, momentum, energy): the science of assets (conservatives do not disappear) and spreads (conservatives tend to disperse)
- Type of thermodynamic systems (system, frontier, and surroundings)
  - Isolated system:  $\Delta m=0$ ,  $\Delta E=0$
  - Closed system :  $\Delta m=0$ ,  $\Delta E \neq 0$
  - Open system :  $\Delta m \neq 0$ ,  $\Delta E \neq 0$
- Type of thermodynamic variables
  - Intensive or extensive variables
  - State or process variables
- Type of thermodynamic equations
  - Balance equations (conservation laws); e.g.  $\Delta E_{\text{close-sys}} = W + Q$
  - Equations of state (constitutive laws); e.g.  $pV = mRT$
  - Equilibrium laws:  $S(U, V, n_i)_{\text{iso-sys}}(t) \rightarrow S_{\text{max}}$  e.g.  $dS/dU|_{V, n_i} = \text{uniform} \dots$
  - (Kinetics is beyond classical thermodynamics; e.g.  $\vec{q} = -k \nabla T$ )

- **Applied thermodynamics**



# Thermodynamics (cont.)

- **Basic thermodynamics**
- **Applied thermodynamics**
  - Energy and exergy analysis (minimum expense and maximum benefit)
  - Non-reactive mixtures (properties of real mixtures, ideal mixture model...)
  - Hygrometry (humid air applications: drying, humidification, air conditioning...)
  - Phase transition in mixtures (liquid-vapour equilibrium, solutions...)
  - Reactive mixtures. Thermochemistry. Combustion
  - Heat engines
    - Gas cycles for reciprocating and rotodynamic engines
    - Vapour cycles (steam and organic fluid power plants)
  - Refrigeration, and heat pumps
    - Cryogenics (cryocoolers, cryostats, cryopreservation...)
  - Thermal analysis of materials (fixed points, calorimetry, dilatometry...)
  - Non-equilibrium thermodynamics (thermoelectricity, dissipative structures...)
  - Environmental thermodynamics (ocean and atmospheric processes...)

# Balance equations

<u>Magnitude</u>	<u>Accumul</u>		<u>Production</u>	<u>Impermeable flux</u>	<u>Permeable flux</u>
mass	$dm$	=	0	+0	$+\sum dm_e$
momentum	$d(m \vec{v})$	=	$m \vec{g} dt$	$+\vec{F}_A dt$	$+\sum \vec{v}_e dm_e - \sum p_e A_e \vec{n}_e dt$
energy	$d(me)$	=	0	$+dW+dQ$	$+\sum h_{te} dm_e$
entropy	$d(ms)$	=	$dS_{gen}$	$+dQ/T$	$+\sum s_e dm_e$
exergy	$d(m\phi)$	=	$-T_0 dS_{gen}$	$+dW_u + (1-T_0/T)dQ$	$+\sum \psi_e dm_e$

with  $e=u+e_m=u+gz+v^2/2$

$$dW = \int_{IF} F dx = \int_{IF} M d\theta, \quad W_u = W + p_0 \Delta V$$

$$h=u+pv, \quad h_t=h+e_m$$

$$ds=(du+pdv)/T=(dq+de_{mdf})/T, \quad de_{mdf} \geq 0, \quad dS_{gen} \geq 0$$

$$\phi=e+p_0v-T_0s, \quad \psi=h_t-T_0s$$



# Substance data

- **Perfect gas model**

- Ideal gas:  $pV=mRT$  or  $pV=nR_uT$  ( $R=R_u/M$ ,  $R_u=8.3 \text{ J/(mol}\cdot\text{K)}$ )
- Energetically linear in temperature:  $\Delta U=mc_v\Delta T$
- Air data:  $R=287 \text{ J/(kg}\cdot\text{K)}$  and  $c_p=c_v+R=1000 \text{ J/(kg}\cdot\text{K)}$ , or  $M=0.029 \text{ kg/mol}$  and  $\gamma=c_p/c_v=1.4$

- **Perfect solid or liquid model**

- Incompressible, undilatable substance:  $V=\text{constant}$  (but beware of dilatations!)
- Energetically linear in temperature:  $\Delta U=mc\Delta T$
- Water data:  $\rho=1000 \text{ kg/m}^3$ ,  $c=4200 \text{ J/(kg}\cdot\text{K)}$

- **Perfect mixture (homogeneous)**

- Ideal mixture  $v = \sum x_i v_i^*$ ,  $u = \sum x_i u_i^*$ ,  $s = \sum x_i s_i^* - R \sum x_i \ln x_i$
- Energetically linear in temperature:  $\Delta U=mc_v\Delta T$

- **Heterogeneous systems**

- Phase equilibria of pure substances (Clapeyron's equation)
- Ideal liquid-vapour mixtures (Raoult's law):  $\frac{x_{v1}}{x_{L1}} = \frac{p_1^*(T)}{p}$
- Ideal liquid-gas solutions (Henry's law):  $\frac{c_{L,s}}{c_{G,s}} = K_{s,cc}^{dis}(T)$

$$\left. \frac{dp}{dT} \right|_{\text{sat}} = \frac{\Delta h}{T \Delta v}$$

- **Real gases. The corresponding state model, and other equations of state.**

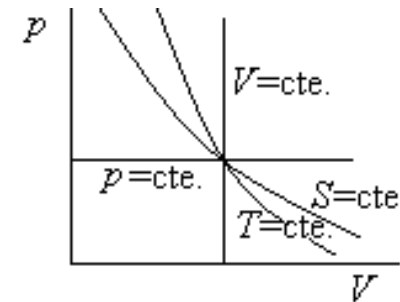


# Thermodynamic processes

- **Adiabatic non-dissipative process of a perfect gas:**

$$dE = dQ + dW \rightarrow dU = -pdV \rightarrow mc_v dT = -\frac{mRT}{V} dV$$

$$\rightarrow \frac{dT}{T} + \frac{R}{c_v} \frac{dV}{V} = 0 \rightarrow T v^{\gamma-1} = \text{cte.}, p v^{\gamma} = \text{cte.}, T/p^{\frac{\gamma-1}{\gamma}} = \text{cte.}$$



- **Fluid heating or cooling**

- At constant volume:  $Q = \Delta U$
- At constant pressure:  $Q = \Delta H = \Delta(U + pV)$

- **Adiabatic gas compression or expansion**

- Close system:  $w = \Delta u = c_v(T_2 - T_1)$
  - Open system:  $w = \Delta h = c_p(T_2 - T_1)$
- $$\eta_c \equiv \frac{w_s}{w} = \frac{h_{2ts} - h_{1t}}{h_{2t} - h_{1t}} \stackrel{\text{PGM}}{=} \frac{(p_{2t}/p_{1t})^{\frac{\gamma-1}{\gamma}} - 1}{T_{2t}/T_{1t} - 1} \quad \eta_T \equiv \frac{w}{w_s} \stackrel{\text{PGM}}{=} \frac{1 - T_{1t}/T_{2t}}{1 - (p_{1t}/p_{2t})^{\frac{\gamma-1}{\gamma}}}$$

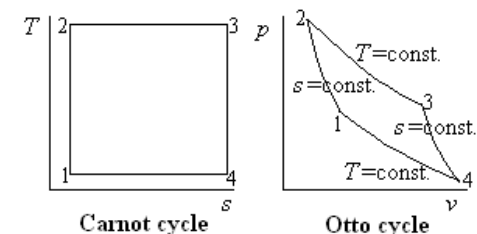
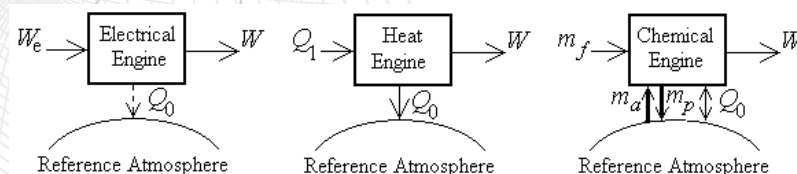
- **Internal energy equation (heating and cooling processes)**

$$\Delta U \equiv \Delta E - \Delta E_m = Q + E_{mdf} - \int p dV$$

- **One-dimensional flow at steady state**

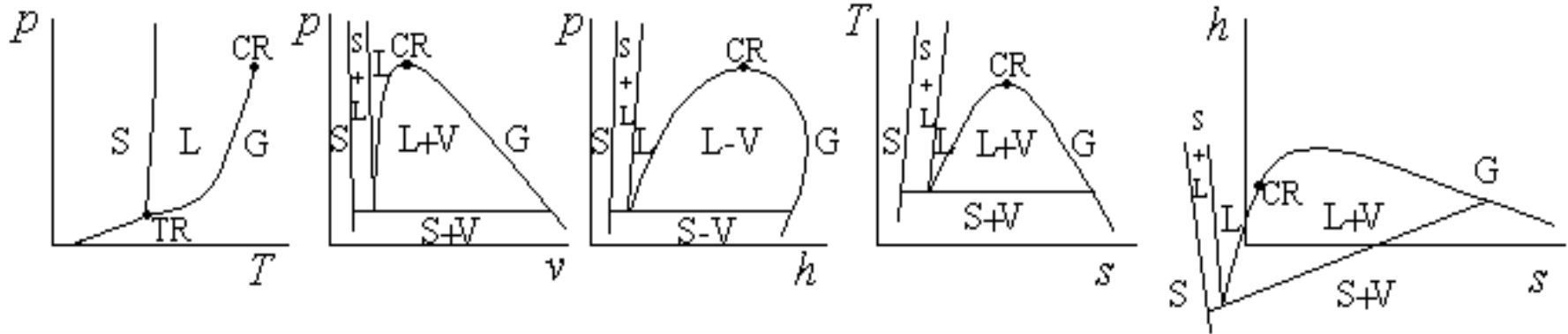
$$\dot{m}_{in} = \dot{m}_{out} = \rho v A = \rho \dot{V} \quad \Delta h = w + q \quad w = \int \frac{dp}{\rho} + \Delta e_m + e_{mdf}$$

- **Thermodynamic processes in engines**





# Phase diagrams (pure substance)



- Normal freezing and boiling points ( $p_0=100$  kPa)
- Triple point (for water  $T_{TR}=273.16$  K,  $p_{TR}=611$  Pa)
- Critical point (for water  $T_{CR}=647.3$  K,  $p_{CR}=22.1$  MPa)
- Clapeyron's equation (for water  $h_{SL}=334$  kJ/kg,  $h_{LV}=2260$  kJ/kg)

$$\left. \frac{dp}{dT} \right|_{sat} = \frac{h_V - h_L}{T(v_V - v_L)} \xrightarrow{v_V \gg v_L, v_V = RT/p, h_{LV} = const} \ln\left(\frac{p}{p_0}\right) = \frac{-h_{LV}}{R} \left( \frac{1}{T} - \frac{1}{T_0} \right)$$



# Thermometry

- **Temperature, the thermal level of a system, can be measured by different primary means:**

- The ideal-gas, constant-volume thermometer
- The acoustic gas thermometer
- The spectral radiation thermometer
- The total radiation thermometer
- The electronic noise thermometer

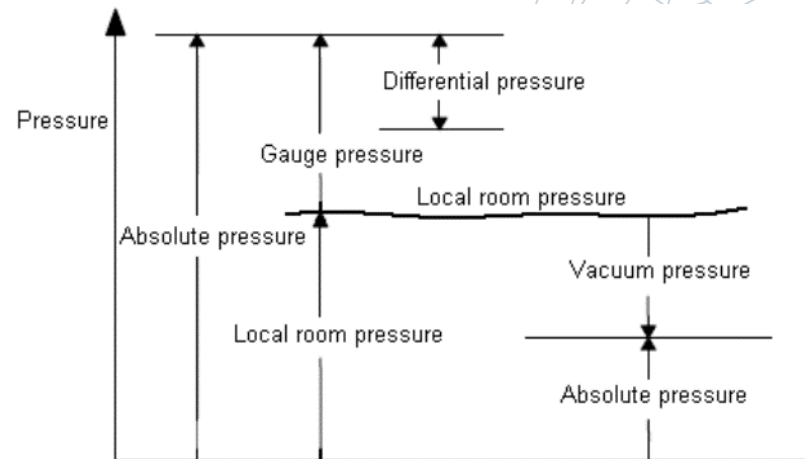
$$\frac{T}{T_{TPW}} \equiv \lim_{p \rightarrow 0} \frac{pV}{(pV)_{TPW}}$$

$$\frac{T}{T_{TPW}} \equiv \lim_{\varepsilon \rightarrow 1} \left( \frac{M}{M_{TPW}} \right)^{1/4}$$

- **The temperature unit is chosen such that  $T_{TPW} \equiv 273.16 \text{ K}$**
- **The Celsius scale is defined by  $T/^{\circ}\text{C} \equiv T/\text{K} - 273.15$**
- **Practical thermometers:**
  - Thermoresistances (e.g. Pt100, NTC)
  - Thermocouples (K, J...).

# Piezometry

- Pressure (normal surface force per unit normal area), is a scalar magnitude measured by difference (in non-isolated systems; recall free-body force diagrams).
- Gauge and absolute pressure:



- Pressure unit (SI) is the pascal,  $1 \text{ Pa} \equiv 1 \text{ N/m}^2$  ( $1 \text{ bar} \equiv 100 \text{ kPa}$ )
- Hydrostatic equation:
 
$$\frac{dp}{dz} = -\rho g \rightarrow \begin{cases} \xrightarrow{\text{PLM}} & p = p_0 - \rho g (z - z_0) \\ \xrightarrow{\text{PGM}} & \frac{dp}{dz} = -\frac{p}{RT} g \end{cases}$$
- Vacuum (practical limit is about  $10^{-8} \text{ Pa}$ )
- Pressure sensors: U-tube, Bourdon tube, diaphragm, piezoelectric...

# Questions

(Only one answer is correct)

1. **The mass of air in a 30 litre vessel at 27 °C and a gauge pressure of 187 kPa is about?**
  - a) 1 g
  - b) 10 g
  - c) 100 g
  - d) 1000 g..
2. **When a gas in a 30 litre rigid vessel is heated from 50 °C to 100 °C, the pressure ratio: (final/initial):**
  - a) Doubles
  - b) Is closer to 1 than to 2.
  - c) Depends on initial volume
  - d) Depends on heating speed
3. **Liquids:**
  - a) Cannot be compressed
  - b) Cannot be heated by compression
  - c) Heat a little bit when compressed, but volume remains the same
  - d) Heat up and shrink when compressed
4. **The critical temperature of any gas is:**
  - a) The temperature below which the gas cannot exist as a liquid
  - b) -273.16 °C
  - c) The temperature above which the gas cannot be liquefied
  - d) The temperature at which solid, liquid, and gas coexist
5. **In a refrigerator, the amount of heat extracted from the cold side:**
  - a) Cannot be larger than the work consumed
  - b) Cannot be larger than the heat rejected to the hot side
  - c) Is inversely proportional to the temperature of the cold side
  - d) Is proportional to the temperature of the cold side.

# Questions

(Only one answer is correct)

6. **Which of the following assertions is correct?**
  - a) Heat is proportional to temperature
  - b) Heat is a body's thermal energy
  - c) Net heat is converted to net work in a heat engine
  - d) The algebraic sum of received heats in an interaction of two bodies must be null.
7. **The variation of entropy in a gas when it is compressed in a reversible way is:**
  - a) Less than zero
  - b) Equal to zero
  - c) Greater than zero
  - d) It depends on the process.
8. **The volumetric coefficient of thermal expansion:**
  - a) Is always positive
  - b) Is dimensionless
  - c) Is different in the Kelvin and Celsius temperature scales
  - d) Is three times the linear coefficient value.
9. **It is not possible to boil an egg in the Everest because:**
  - a) The air is too cold to boil water
  - b) Air pressure is too low for stoves to burn
  - c) Boiling water is not hot enough
  - d) Water cannot be boiled at high altitudes.
10. **When a combustion takes place inside a rigid and adiabatic vessel:**
  - a) Internal energy increases
  - b) Internal energy variation is null
  - c) Energy is not conserved
  - d) Heat flows out.



# Exercises

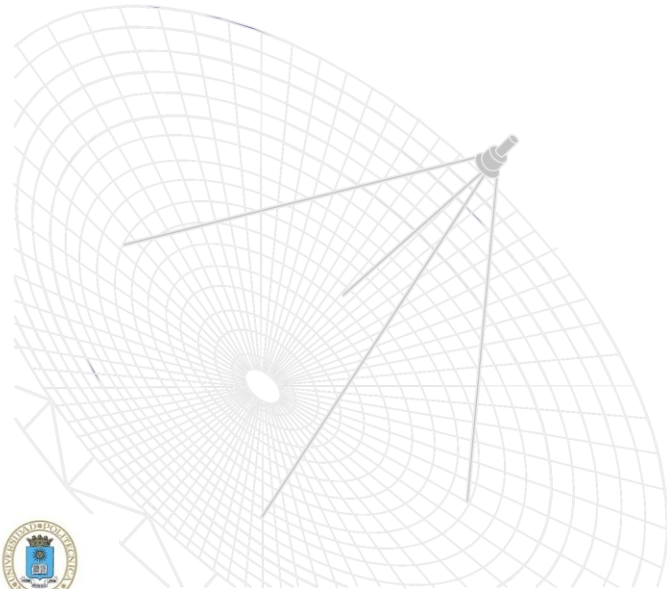
1. **A U-tube is made by joining two 1 m vertical glass-tubes of 3 mm bore (6 mm external diameter) with a short tube at the bottom. Water is poured until the liquid fills 600 mm in each column. Then, one end is closed. Find:**
  1. The change in menisci height due to an ambient pressure change,  $(\partial z / \partial p_{\text{amb}})$ , with application to  $\Delta p = 1$  kPa.
  2. The change in menisci height due to an ambient temperature change,  $(\partial z / \partial T_{\text{amb}})$ , with application to  $\Delta T = 5$  °C.
2. **An aluminium block of 54.5 g, heated in boiling water, is put in a calorimeter with 150 cm<sup>3</sup> of water at 22 °C, with the thermometer attaining a maximum of 27.5 °C after a while. Find the thermal capacity of aluminium.**
3. **How many ice cubes of 33 g each, at -20 °C, are required to cool 1 litre of tea from 100 °C to 0 °C?**
4. **Carbon dioxide is trapped inside a vertical cylinder 25 cm in diameter by a piston that holds internal pressure at 120 kPa. The plunger is initially 0.5 m from the cylinder bottom, and the gas is at 15 °C. Thence, an electrical heater inside is plugged to 220 V, and the volume increases by 50% after 3 minutes. Neglecting heat losses through all walls, and piston friction, find:**
  1. The energy balance for the gas and for the heater.
  2. The final temperature and work delivered or received by the gas.
5. **Find the air stagnation temperature on leading edges of an aircraft flying at 2000 km/h in air at -60 °C.**



# Master in Space Science and Technology

## Thermal engineering

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# Thermal engineering

## •Thermodynamics

- Basic (energy and entropy, state properties, state equations, simple processes, phase changes)
- Applied (mixtures, liquid-vapour equilibrium, air conditioning, thermochemistry, power and cold generation, materials processes)

## •Heat transfer

- Thermal conduction (solids...)
- Thermal convection (fluids...)
- Thermal radiation (vacuum...)
- Heat exchangers
- Heat generation (electrical heaters...)
- Thermal control systems
- Combined heat and mass transfer (evaporative cooling, ablation...)



# Heat transfer

- **What is heat (i.e. heat flow, heat transfer)?**

- First law: *heat is non-work energy-transfer through an impermeable surf.*

$$Q \equiv \Delta E - W = \Delta E + \int p dV - W_{dis} = \Delta H - \int V dp - W_{dis} = (mc\Delta T)_{PIS, non-dis}$$

- Second law: heat tends to equilibrate the temperature field.

$$\dot{s}_{gen} = \frac{-\nabla T \cdot \vec{q}}{T^2}$$

- **What is heat flux (i.e. heat flow rate, heat transfer rate)?**

$$\dot{Q} \equiv \frac{dQ}{dt} = mc \left. \frac{dT}{dt} \right|_{PSM, non-dis} \equiv KA\Delta T$$

- **Heat transfer is the flow of thermal energy driven by thermal non-equilibrium (i.e. the effect of a non-uniform temperature field), commonly measured as a heat flux (vector field).**

# Heat transfer modes

- How is heat flux density modelled?

$$\dot{q} \equiv \frac{\dot{Q}}{A} = K \Delta T \begin{cases} \text{conduction} & \vec{\dot{q}} = -k \nabla T \\ \text{convection} & \dot{q} \equiv h(T - T_{\infty}) \\ \text{radiation} & \dot{q} = \varepsilon \sigma (T^4 - T_{\infty}^4) \end{cases}$$

- The 3 ways to change  $\dot{Q}$ :  $K$ ,  $A$ , and  $\Delta T$ .
- $K$  is thermal conductance coeff. (or heat transfer coeff.),  $k$  is conductivity,  $h$  is convective coeff.,  $\varepsilon$  is emissivity.
- Field or interface variables?
- Vector or scalar equations?
- Linear or non-linear equations?
- Material or configuration properties?
- Which emissivity? This form only applies to bodies in large enclosures.

# Heat conduction

- **Physical transport mechanism**

- Short-range atomic interactions (collision of particles in fluids, or phonon waves in solids), supplemented with free-electron flow in metals.

- **Fourier's law (1822)**

$$\vec{q} = -k\nabla T$$

- **Heat equation**

$$\left. \frac{dH}{dt} \right|_p = \dot{Q} \rightarrow \int_V \rho c \frac{\partial T}{\partial t} dV = - \int_A \vec{q} \cdot \vec{n} dA + \int_V \phi dV = - \int_V \nabla \cdot \vec{q} dV + \int_V \phi dV$$
$$\xrightarrow{V \rightarrow 0} \rho c \frac{\partial T}{\partial t} = -\nabla \cdot \vec{q} + \phi \stackrel{\nabla k=0}{=} k \nabla^2 T + \phi, \quad \text{or} \quad \frac{\partial T}{\partial t} = a \nabla^2 T + \frac{\phi}{\rho c}$$

- with the initial and boundary conditions particular to each problem.

# Thermal conductivity

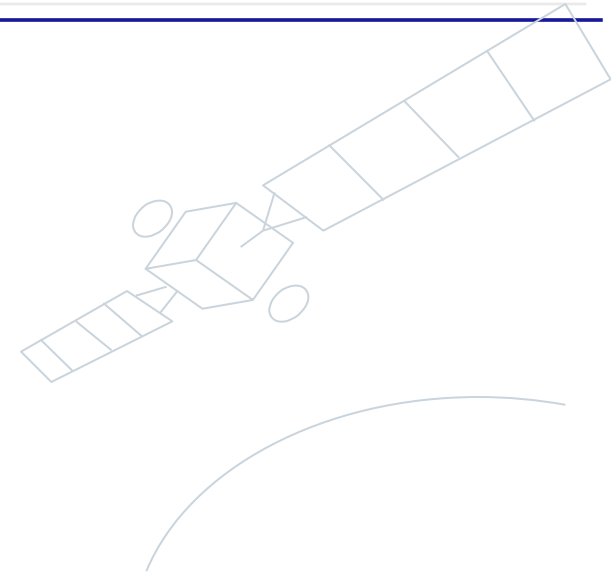
Table 1. Representative thermal conductivity values

	$k$ [W/(m·K)]	Comments
Order of magnitude for solids	$10^2$ (good conductors) 1 (bad conductors)	In metals, Lorentz's law (1881), $k/(\sigma T)=\text{constant}$
Aluminium	200	Duralumin has $k=174$ W/(m·K), increasing to $k=188$ W/(m·K) at 500 K.
Iron and steel	50 (carbon steel) 20 (stainless steel)	Increases with temperature. Decreases with alloying
Order of magnitude for liquids	1 (inorganic) 0.1 (organic)	Poor conductors (except liquid metals).
Water	0.6	Ice has $k=2.3$ W/(m·K),
Order of magnitude for gases	$10^{-2}$	Very poor thermal conductors. KTG predicts $k/(\rho c) \equiv a = D_i = v \approx 10^{-5}$ m <sup>2</sup> /s
Air	0.024	Super insulators must be air evacuated.

# Simple heat conduction cases

- **One-dimensional steady cases**

- Planar  $\dot{Q} = kA \frac{T_1 - T_2}{L_{12}}$
- Cylindrical  $\dot{Q} = k2\pi L \frac{T_1 - T_2}{\ln \frac{R_2}{R_1}}$
- Spherical  $\dot{Q} = k4\pi R_1 R_2 \frac{T_1 - T_2}{R_2 - R_1}$



- **Composite wall (planar multilayer)**

$$\dot{q} = K\Delta T = k_{12} \frac{T_2 - T_1}{L_{12}} = k_{23} \frac{T_3 - T_2}{L_{23}} = \dots = \frac{T_n - T_1}{\sum \frac{L_i}{k_i}} \Rightarrow K = \frac{1}{\sum \frac{L_i}{k_i}}$$

- **Unsteady case. Relaxation time:**

$$\Delta t = mc\Delta T / \dot{Q} \quad \left\{ \begin{array}{l} \Delta t = \frac{\rho c L^2}{k} \quad Bi \gg 1 \\ \Delta t = \frac{\rho c V}{hA} \quad Bi \ll 1 \end{array} \right. \quad Bi \equiv \frac{hL}{k_s}$$



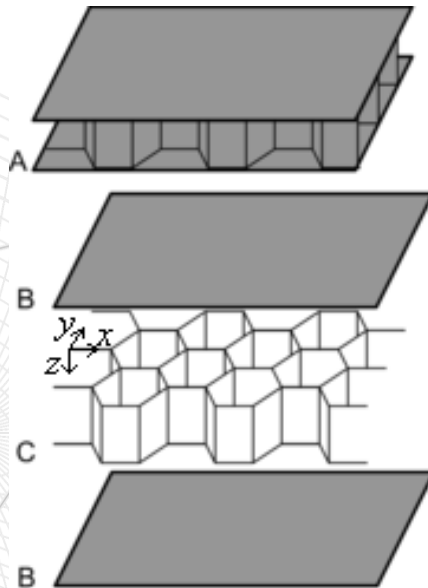
# Multiple path in heat conduction

- **Multidimensional analysis**

- Analytical, e.g. separation of variables, conduction shape factors,
- Numerical, finite differences, lumped network, finite elements

- **Parallel thermal resistances**

- Example: honeycomb panel made of ribbon (thickness  $\delta$ ), cell size  $s$ :



$$\left. \begin{aligned} \dot{Q}_x &= k F_x A_x \frac{\Delta T_x}{L_x} & \text{with } F_x &= \frac{3}{2} \frac{\delta}{s} \\ \dot{Q}_y &= k F_y A_y \frac{\Delta T_y}{L_y} & \text{with } F_y &= \frac{\delta}{s} \\ \dot{Q}_z &= k F_z A_z \frac{\Delta T_z}{L_z} & \text{with } F_z &= \frac{8}{3} \frac{\delta}{s} \end{aligned} \right\}$$

# Heat convection

- **Newton's law and physical mechanism**

$$\dot{q} \equiv h(T - T_{\infty}) = -k \nabla_n T \rightarrow h \Delta T \approx k \frac{\Delta T}{\delta} \rightarrow Nu \equiv \frac{hL}{k} = f(Re, Pr...)$$

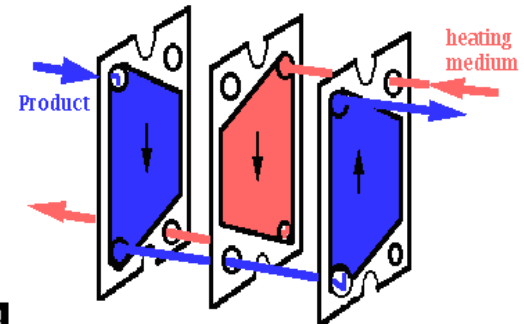
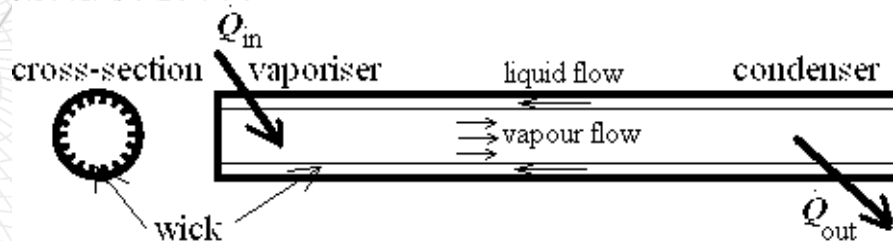
- e.g. in air flow,  $h = a + b v_{\text{wind}}$ , with  $a = 3 \text{ W}/(\text{m}^2 \cdot \text{K})$  and  $b = 3 \text{ J}/(\text{m}^3 \cdot \text{K})$
- e.g. plate ( $< 1 \text{ m}$ ) at rest,  $h = a(T - T_{\infty})^{1/4}$ , with  $a \sim 2 \text{ W}/(\text{m}^2 \cdot \text{K}^{5/4})$  (1,6 upper, 0.8 lower, 1.8 vert.)

- **Classification of heat convection problems**

- By time change: steady, unsteady (e.g. onset of convection)
- By flow origin: forced (flow), natural (thermal, solutal...)
- By flow regime: laminar, turbulent
- By flow topology: internal flow, external flow
- By flow phase: single-phase or multi-phase flow

- **Heat exchangers (tube-and-shell, plates...)**

- **Heat pipes**





# Heat radiation

- **Heat radiation (thermal radiation)**

- It is the transfer of internal thermal energy to electromagnetic field energy, or viceversa, modelled from the basic black-body theory. Electromagnetic radiation is emitted as a result of the motion of electric charges in atoms and molecules.

- **Blackbody radiation**

- Radiation within a vacuum cavity
  - Radiation temperature (equilibrium with matter)
  - Photon gas (wave-particle duality, carriers with zero rest mass,  $E=h\nu$ ,  $p=E/c$ )
  - Isotropic, unpolarised, incoherent spatial distribution
  - Spectral distribution of photon energies at equilibrium ( $E=\text{const.}$ ,  $S=\text{max.}$ )
- Radiation escaping from a hole in a cavity
  - Blackbody emission

$$M_{\lambda} = \frac{2\pi hc^2}{\lambda^5 \left[ \exp\left(\frac{hc}{k\lambda T}\right) - 1 \right]} \quad \left\{ \begin{array}{l} M = \int_0^{\infty} M_{\lambda} d\lambda = \sigma T^4 \quad \sigma = 5.67 \cdot 10^{-8} \frac{\text{W}}{\text{m}^2 \cdot \text{K}^4} \\ \lambda|_{M_{\lambda}=\text{max}} = \frac{C}{T} \quad C = 0.003 \text{ m} \cdot \text{K} \end{array} \right.$$

# Thermo-optical properties

- **Propagation through real media**

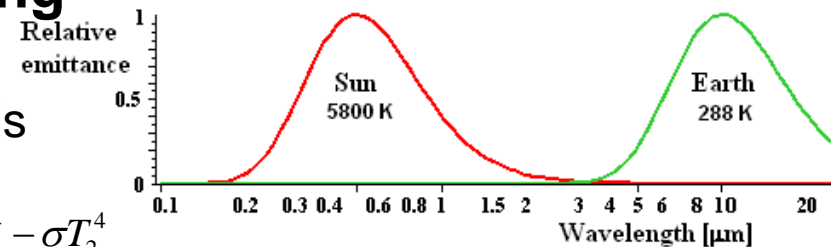
- Attenuation by absorption and scattering (Rayleigh if  $d \ll \lambda$ , Mie if  $d \geq \lambda$ )

- **Properties of real surfaces**

- Partial absorption ( $\alpha$ ), reflectance ( $\rho$ ), emissivity ( $\varepsilon$ ), and, in some cases, transmittance ( $\tau$ ). Energy balance:  $\alpha + \rho + \tau = 1$ .
- Directional and spectral effects (e.g. retroreflective surfaces, selective glasses...)
- Detailed equilibrium: Kirchhoff's law (1859),  $\alpha_{\lambda\beta\theta T} = \varepsilon_{\lambda\beta\theta T}$ , but usually  $\alpha \neq \varepsilon$

- **Spectral and directional modelling**

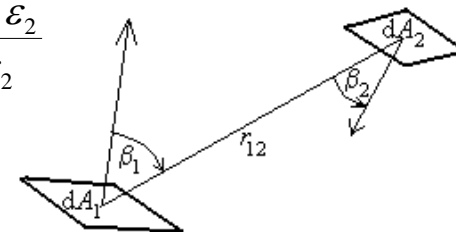
- Two-spectral-band model:
- Diffuse (cosine law) or specular models



- **Radiative coupling**

- e.g. planar infinite surfaces:  $\dot{q}_{12} = \frac{\sigma T_1^4 - \sigma T_2^4}{\frac{1 - \varepsilon_1}{\varepsilon_1} + 1 + \frac{1 - \varepsilon_2}{\varepsilon_2}}$

- **View factors**  $F_{12} = \frac{1}{\pi A_1} \int_{A_2} \int_{A_1} \frac{\cos \beta_1 \cos \beta_2}{r_{12}^2} dA_1 dA_2$



# Heat transfer goals

- **Analysis**

- Find the heat flux for a given set-up and *temperature* field

- e.g.  $\dot{Q} = kA(T_1 - T_2) / L$

- Find the temperature corresponding to a given heat flux and set-up

- e.g.  $T_1 = T_2 + \dot{Q}L / (kA)$

- **Design**

- Find an appropriate material that allows a prescribed heat flux with a given *T*-field in a given geometry

- e.g.  $k = \dot{Q}L / (A\Delta T)$

- Find the thickness of insulation to achieve a certain heat flux with a given *T*-field in a prescribed geometry

- e.g.  $L = kA(T_1 - T_2) / \dot{Q}$

- **Control**

- To prevent high temperatures, use insulation and radiation shields, or use heat sinks and coolers.
  - To prevent low temperatures, use insulation and radiation shields, or use heaters.
  - To soften transients, increase thermal inertia (higher thermal capacity, phase change materials).

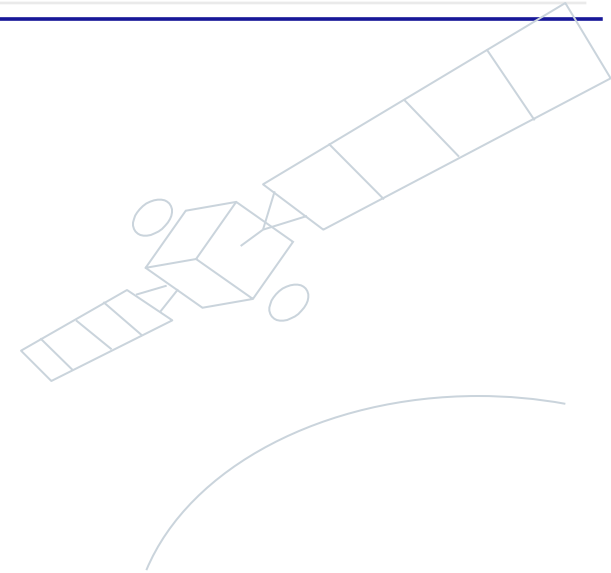


# Application to electronics cooling

- All active electrical devices at steady state must evacuate the energy dissipated by Joule effect (i.e. need of heat sinks).
- Most electronics failures are due to overheating (e.g. for germanium at  $T > 100\text{ }^{\circ}\text{C}$ , for silicon at  $T > 125\text{ }^{\circ}\text{C}$ ).
- At any working temperature there is always some dopant diffusion at junctions and bond-material creeping, causing random electrical failures, with an event-rate doubling every  $10\text{ }^{\circ}\text{C}$  of temperature increase. Need of thermal control.
- Computing power is limited by the difficulty to evacuate the energy dissipation (a Pentium 4 CPU at 2 GHz in  $0.18\text{ }\mu\text{m}$  technology must dissipate 76 W in an environment at  $40\text{ }^{\circ}\text{C}$  without surpassing  $75\text{ }^{\circ}\text{C}$  at the case,  $125\text{ }^{\circ}\text{C}$  at junctions).
- Modern electronic equipment, being powerfull and of small size, usually require liquid cooling (e.g. heat pipes).

# Thermal modelling

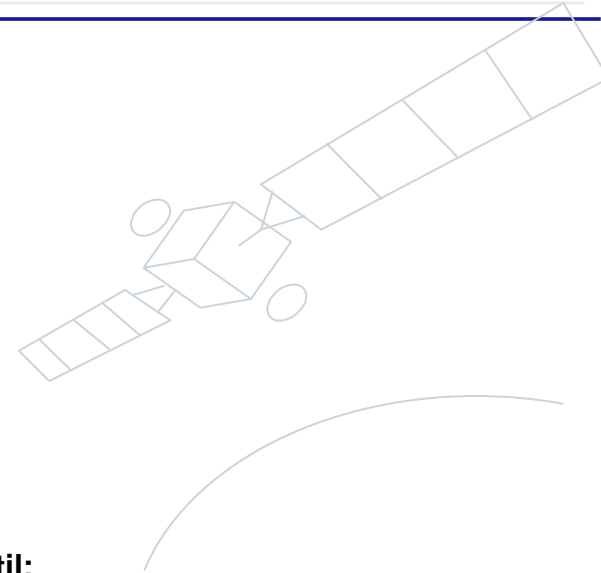
- **Modelling the geometry**
- **Modelling the material properties**
- **Modelling the transients**
- **Modelling the heat equation**
- **Mathematical solution of the model**
  - Analytical solutions
  - Numerical solutions
- **Analysis of the results**
- **Verification planning (analytical checks and testing)**
- **Feedback**



# Questions

(Only one answer is correct)

1. **The steady temperature profile in heat transfer along a compound wall:**
  - a) Has discontinuities
  - b) Must have inflexion points
  - c) Must be monotonously increasing or decreasing
  - d) Must have a continuous derivative.
2. **If the temperature at the hot side of a wall is doubled:**
  - a) Heat flow through the wall doubles
  - b) Heat flow through the wall increases by a factor of 4
  - c) Heat flow through the wall increases by a factor of 8
  - d) None of the above.
3. **When a piece of material is exposed to the sun, its temperature rises until:**
  - a) It loses and gains heat at the same rate
  - b) The heat absorbed equals its thermal capacity
  - c) It reflects all the energy that strikes it
  - d) No more heat is absorbed.
4. **A certain blackbody at 100 °C radiates 100 W. How much radiates at 200 °C?**
  - a) 200 W
  - b) 400 W
  - c) 800 W
  - d) None of the above.
5. **When two spheres, with same properties except for their radius, are exposed to the Sun and empty space:**
  - a) The larger one gets hotter
  - b) The larger one gets colder
  - c) The larger one gets hotter or cooler depending on their emissivity-to-absorptance ratio
  - d) None of the above.





# Exercises

1. **A small frustrum cone 5 cm long, made of copper, connects two metallic plates, one at 300 K in contact with the smallest face, which is 1 cm in diameter, and the other at 400 K, at the other face, which is 3 cm in diameter. Assuming steady state, quasi-one-dimensional flow, and no lateral losses, find:**
  - The temperature profile along the axis.
  - The heat flow rate.
2. **An electronics board  $100 \cdot 150 \cdot 1 \text{ mm}^3$  in size, made of glass fibre laminated with epoxy, and having  $k=0.25 \text{ W/(m}\cdot\text{K)}$ , must dissipate 5 W from its components, which are assumed uniformly distributed. The board is connected at the largest edges to high conducting supports held at 30 °C. Find:**
  1. The maximum temperature along the board, if only heat conduction at the edges is accounted for (no convection or radiation losses).
  2. The thickness of a one-side copper layer (bonded to the glass-fibre board) required for the maximum temperature to be below 40 °C above that of the supports.
  3. The transient temperature field, with and without a convective coefficient of  $h=2 \text{ W/(m}^2\cdot\text{K)}$ .
3. **Find the required area for a vertical plate at 65 °C to communicate 1 kW to ambient air at 15 °C.**
4. **Consider two infinite parallel plates, one at 1000 °C with  $\varepsilon=0.8$  and the other at 100 °C with  $\varepsilon=0.7$ . Find:**
  - The heat flux exchanged.
  - The effect of interposing a thin blackbody plate in between.
5. **Find the steady temperature at 1 AU, for an isothermal blackbody exposed to solar and microwave background radiation, for the following geometries: planar one-side surface (i.e. rear insulated), plate, cylinder, sphere, and cube.**

(END)



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