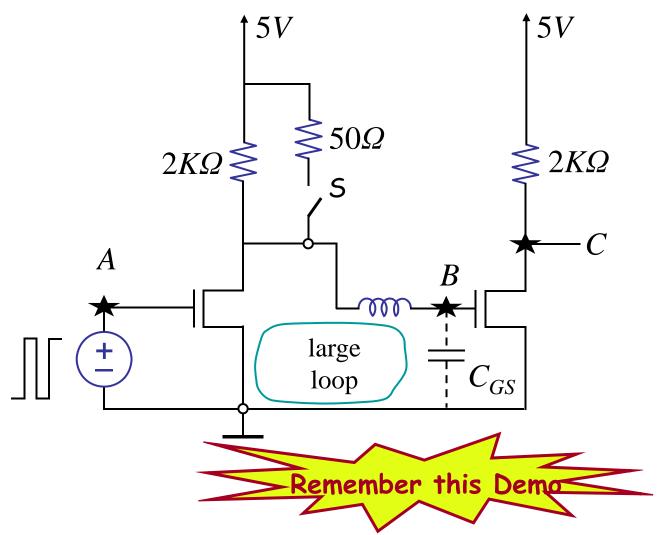


Damped Second-Order Systems

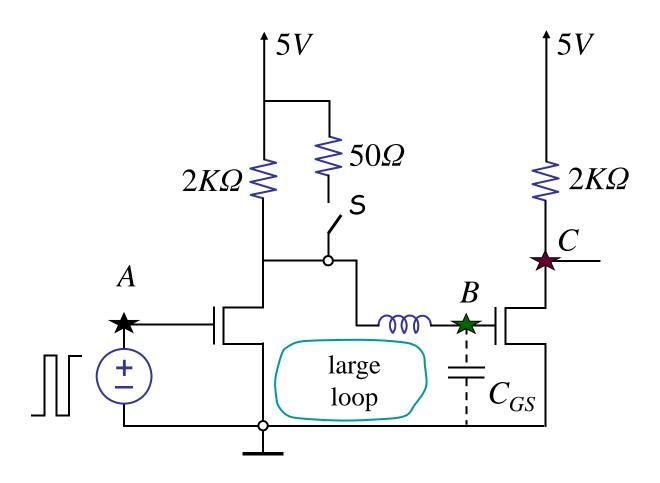
Damped Second-Order Systems

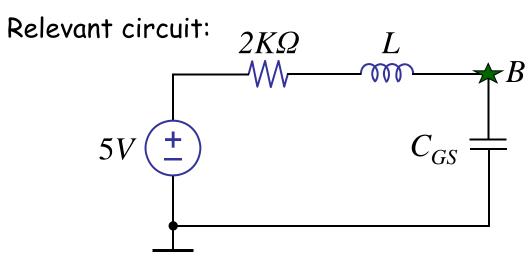


Our old friend, the inverter, driving another. The parasitic inductance of the wire and the gate-to-source capacitance of the MOSFET are shown

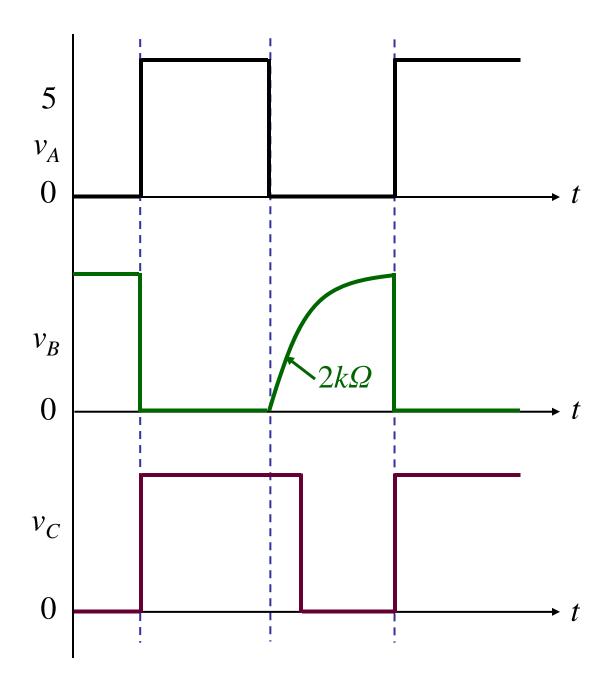
[Review complex algebra appendix in Agarwal & Lang for next class]

Damped Second-Order Systems



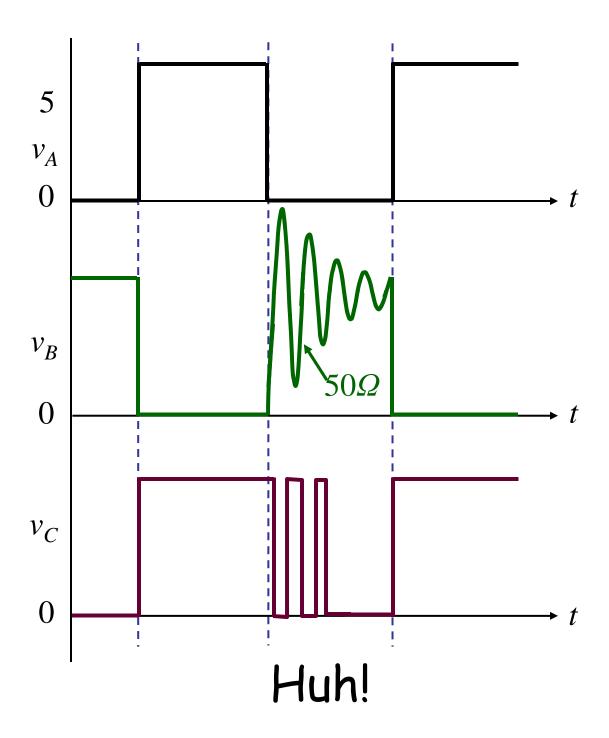


Observed Output $2k\Omega$



Now, let's try to speed up our inverter by closing the switch S to lower the effective resistance

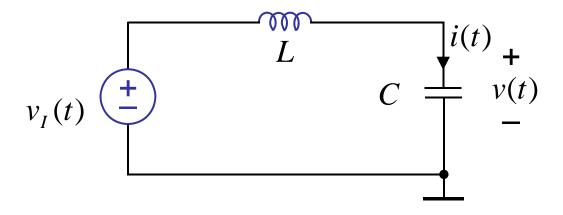
Observed Output $\sim 50\Omega$



6.002 Fall 03

5

In the last lecture, we started by analyzing the simpler LC circuit to build intuition

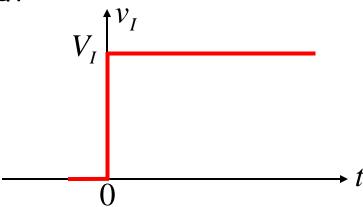


In the last lecture...

We solved

$$\frac{d^2v}{dt^2} + \frac{1}{LC}v = \frac{1}{LC}v_I$$

For input



And for initial conditions

$$v(0) = 0$$
 $i(0) = 0$ [ZSR]

6.002 Fall 03 ₇

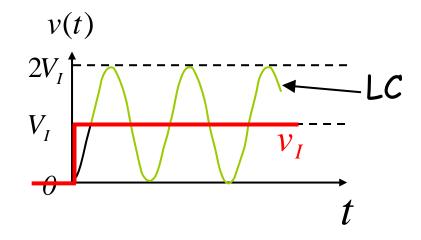
In the last lecture...

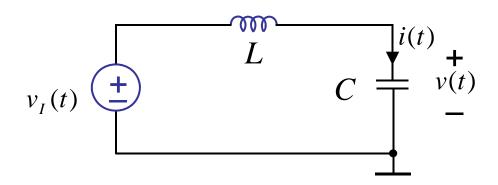
Total solution

$$v(t) = V_I - V_I \cos \omega_O t$$

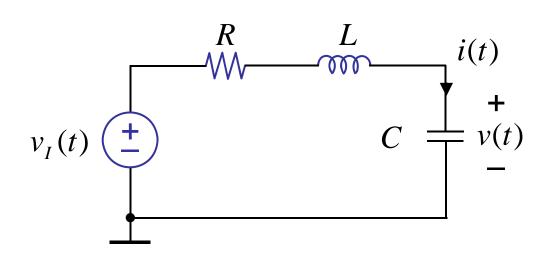
where

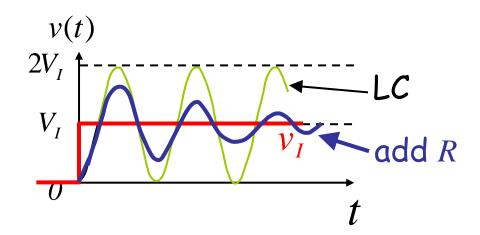
$$\omega_o = \frac{I}{\sqrt{LC}}$$





Today, we will close the loop on our observations in the demo by analyzing the RLC circuit





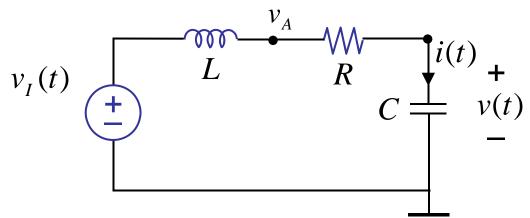
Damped sinusoids with R - remember demo!

See A&L Section 13.6

6.002 Fall 03

9

Let's analyze the RLC network



Node method:

$$v_{A}: \frac{1}{L} \int_{-\infty}^{t} (v_{I} - v_{A}) dt = \frac{v_{A} - v}{R}$$

$$v: \frac{v_{A} - v}{R} = C \frac{dv}{dt}$$

$$\frac{d^2v}{dt^2} + \frac{R}{L}\frac{dv}{dt} + \frac{1}{LC}v = \frac{1}{LC}v_I$$

Recall element rules

L:

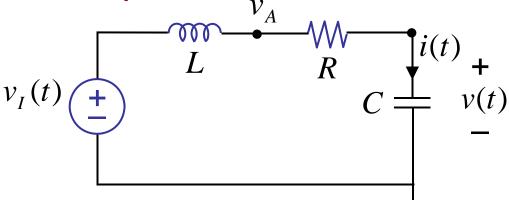
$$v_{L} = L \frac{di}{dt}$$

$$\frac{1}{L} \int_{-\infty}^{t} v_{L} dt = i$$

$$i_C = C \frac{dv_C}{dt}$$

v, i state variables

Let's analyze the RLC network



Node method:

$$v_{A}: \frac{1}{L} \int_{-\infty}^{t} (v_{I} - v_{A}) dt = \frac{v_{A} - v}{R}$$

$$v: \frac{v_{A} - v}{R} = C \frac{dv}{dt}$$

$$\frac{1}{L} (v_{I} - v_{A}) = C \frac{d^{2}v}{dt^{2}}$$

$$\frac{1}{LC} (v_{I} - v_{A}) = \frac{d^{2}v}{dt^{2}}$$

$$v_{A} = RC \frac{dv}{dt} + v$$

$$\frac{1}{LC} (v_{I} - RC \frac{dv}{dt} - v) = \frac{d^{2}v}{dt^{2}}$$

$$\frac{d^{2}v}{dt^{2}} + \frac{R}{L} \frac{dv}{dt} + \frac{1}{LC} v = \frac{1}{LC} v_{I}$$

Solving

Recall, the method of homogeneous and particular solutions:

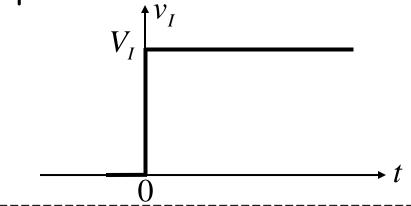
- 1) Find the particular solution.
- Find the homogeneous solution.4 steps
- The total solution is the sum of the particular and homogeneous.
 Use initial conditions to solve for the remaining constants.

$$v = v_P(t) + v_H(t)$$

Let's solve

$$\frac{d^2v}{dt^2} + \frac{R}{L}\frac{dv}{dt} + \frac{1}{LC}v = \frac{1}{LC}v_I$$

For input



And for initial conditions

$$v(0) = 0$$
 $i(0) = 0$ [ZSR]

1 Particular solution

$$\frac{d^2v_P}{dt^2} + \frac{R}{L}\frac{dv_P}{dt} + \frac{1}{LC}v_P = \frac{1}{LC}V_I$$

$$v_P = V_I$$
 is a solution.

2 Homogeneous solution

Solution to
$$\frac{d^2v_H}{dt^2} + \frac{R}{L}\frac{dv_H}{dt} + \frac{1}{LC}v_H = 0$$

Recall, v_H : solution to homogeneous equation (drive set to zero)

Four-step method:

$$v_H = Ae^{st} \qquad , A, s = ?$$

- B Form the characteristic equation f(s)
- \bigcirc Find the roots of the characteristic equation S_1, S_2
- (D) General solution

$$v_H = A_1 e^{s_1 t} + A_2 e^{s_2 t}$$

(2) Homogeneous solution

Solution to
$$\frac{d^2v_H}{dt^2} + \frac{R}{L}\frac{dv_H}{dt} + \frac{1}{LC}v_H = 0$$

(A) Assume solution of the form

$$v_H = Ae^{st} \qquad , A, s = ?$$

so,
$$As^2e^{st} + \frac{R}{L}Ase^{st} + \frac{1}{LC}Ae^{st} = 0$$

B
$$s^2 + \frac{R}{L}s + \frac{1}{LC} = 0$$
 characteristic equation
$$s^2 + 2\alpha s + \omega^2_o = 0$$

$$\omega_o = \sqrt{\frac{1}{LC}}$$

$$\alpha = \frac{R}{2L}$$

Roots
$$s_{I} = -\alpha + \sqrt{\alpha^{2} - \omega_{o}^{2}}$$

$$s_{2} = -\alpha - \sqrt{\alpha^{2} - \omega_{o}^{2}}$$

(D) General solution

$$v_{H} = A_{1}e^{\left(-\alpha + \sqrt{\alpha^{2} - \omega^{2}_{o}}\right)t} + A_{2}e^{\left(-\alpha - \sqrt{\alpha^{2} - \omega^{2}_{o}}\right)t}$$

(3) Total solution

$$v(t) = v_P(t) + v_H(t)$$

$$v(t) = V_I + A_1 e^{\left(-\alpha + \sqrt{\alpha^2 - \omega_o^2}\right)t} + A_2 e^{\left(-\alpha - \sqrt{\alpha^2 - \omega_o^2}\right)t}$$

and unknowns from initial conditions.

$$v(\theta) = 0: \quad 0 \neq V_I + A_I + A_I$$

$$i(0) = 0:$$

$$i(t) = C \frac{dv}{dt}$$

$$= CA_1 \left(-\alpha + \sqrt{\alpha^2 - \omega^2_o}\right)^{\left(-\alpha + \sqrt{\alpha^2 - \omega^2_o}\right)t} +$$

$$\mathcal{L}A_2 \left(-\alpha - \sqrt{\alpha^2 - \omega^2_o}\right)^{\left(-\alpha + \sqrt{\alpha^2 - \omega^2_o}\right)t}$$

So,
$$0 = A_1 \left(-\alpha + \sqrt{\alpha^2 - \omega^2} \right) + A_2 \left(-\alpha - \sqrt{\alpha^2 - \omega^2_{jo}} \right)$$

Mathematically: solve for unknowns, done.

Let's stare at this a while longer...

$$v(t) = V_I + A_1 e^{-\alpha t} e^{\left(\sqrt{\alpha^2 - \omega_o^2}\right)t} + A_2 e^{-\alpha t} e^{\left(-\sqrt{\alpha^2 - \omega_o^2}\right)t}$$

3 cases:

$$\alpha > \omega_o \quad \text{Overdamped}$$

$$v(t) = V_I + A_1 e^{-\alpha_1 t} + A_2 e^{-\alpha_2 t}$$

$$\alpha < \omega_o$$
 Underdamped

$$\begin{aligned} v(t) &= V_I + A_1 e^{-\alpha t} e^{\left(j\sqrt{\omega^2_o - \alpha^2}\right)t} + A_2 e^{-\alpha t} e^{\left(-j\sqrt{\omega_o^2 - \alpha^2}\right)t} \\ &= V_I + A_1 e^{-\alpha t} e^{j\omega_d t} + A_2 e^{-\alpha t} e^{-j\omega_d t} \begin{vmatrix} \omega_d &= \sqrt{\omega^2_o - \alpha^2} \\ \omega_d &= \sqrt{\omega^2_o - \alpha^2} \end{vmatrix} \\ &= V_I + K_1 e^{-\alpha t} \cos \omega_d t + K_2 e^{-\alpha t} \sin \omega_d t \end{vmatrix} e^{j\omega_d t} = \cos \omega_d t + j \sin \omega_d t \end{aligned}$$

$$\alpha = \omega_o$$
 Critically damped Later...

Let's stare at underdamped a while longer...

$$\alpha < \omega_o$$
 Underdamped contd...

$$\begin{aligned} v(t) &= V_I + K_1 e^{-\alpha t} \cos \omega_d t + K_2 e^{-\alpha t} \sin \omega_d t \\ v(0) &= 0: \quad K_1 = -V_I \\ i(0) &= 0: \quad i(t) = C \frac{dv}{dt} \\ &= -CK_1 \alpha e^{-\alpha t} \cos \omega_d t - CK_2 \omega_d e^{-\alpha t} \sin \omega_d t \\ &- CK_1 \alpha e^{-\alpha t} \sin \omega_d t + CK_2 \omega_d e^{-\alpha t} \cos \omega_d t \\ 0 &= -K_1 \alpha + K_2 \omega_d \\ K_2 &= -\frac{V_1 \alpha}{\omega_d} \end{aligned}$$

$$v(t) = V_I - V_I e^{-\alpha t} \cos \omega_d t - V_I \frac{\alpha}{\omega_d} e^{-\alpha t} \sin \omega_d t$$

19

Note: For
$$R=0\Longrightarrow \alpha=0$$

$$v(t)=V_I-V_I\cos\omega_o t$$
 Same as LC as expected

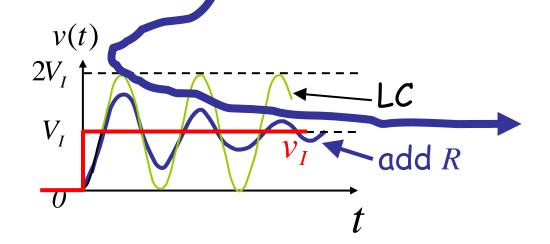
Let's stare at underdamped a while longer...

 $\alpha < \omega_o$ Underdamped contd...

$$v(t) = V_I - V_I e^{-\alpha t} \cos \omega_d t - V_I \frac{\alpha}{\omega_d} e^{-\alpha t} \sin \omega_d t$$

Remember, scaled sum of sines (of the same frequency) are also sines! -- Appendix B.7

$$v(t) = V_I - V_I \frac{\omega_d}{\omega_d} e^{-\alpha t} \cos \left(\omega_d t - \tan^{-1} \frac{\alpha}{\omega_d} \right)$$



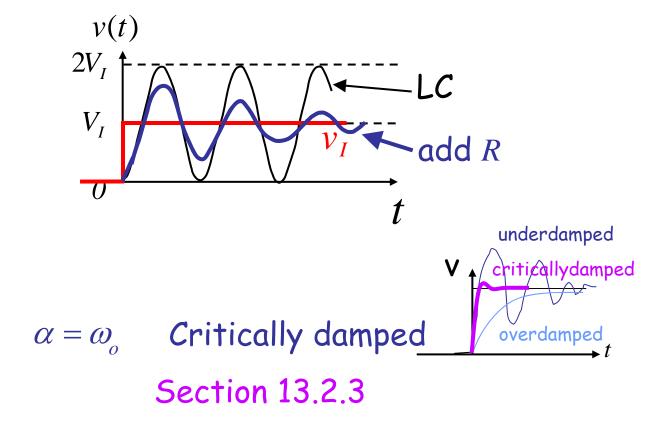
20

 $\alpha < \omega_o$ Underdamped contd...

$$v(t) = V_I - V_I e^{-\alpha t} \cos \omega_d t - V_I \frac{\alpha}{\omega_d} e^{-\alpha t} \sin \omega_d t$$

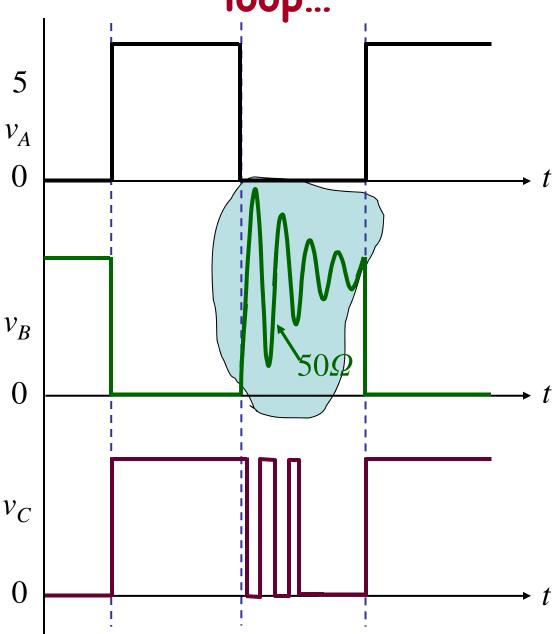
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$$v(t) = V_I - V_I \frac{\omega_o}{\omega_d} e^{-\alpha t} \cos \left(\omega_d t - \tan^{-1} \frac{\alpha}{\omega_d} \right)$$



21

Remember this? Closed the loop...

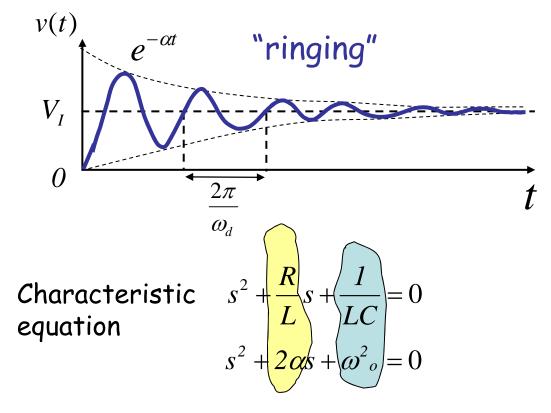


See example 12.9 on page 664 of the A&L textbook for inverter-pair analysis

Intuitive Analysis

See Sec. 12.7 of A&L textbook

Underdamped
$$v(t) = V_I - V_I \frac{\omega_o}{\omega_d} e^{-\alpha t} \cos \left(\omega_d t - \tan^{-1} \frac{\alpha}{\omega_d} \right)$$



Oscillation frequency $\omega_{d} = \sqrt{\omega_{o}^{2} - \alpha}$

$$\omega_d = \sqrt{\omega_o^2 - \alpha^2}$$

 α : Governs rate of decay

 $V_{\scriptscriptstyle I}$: Final value

v(0): Initial value

 $Q = \frac{\omega_o}{2\alpha}$: Quality factor (approximately the number of cycles of ringing)

Fall 03 6.002

Intuitive Analysis

See Sec. 12.7 of A&L textbook

