

15/11/2023

MAGNETISM

- charges in motion \Rightarrow magnetism.
- magnetic materials on an atomic scale $\rightarrow e^-$ orbiting around nucleus + spinning about their axis
- for macroscopic purposes \rightarrow the current loops = magnetic dipoles
- due to random orientation \rightarrow dipole moments cancel off.
- if \vec{B} field applied \rightarrow dipoles align \rightarrow medium magnetically polarized / magnetized.
- electric polarization (\vec{P}) : $\vec{P} \parallel el$ to \vec{E} .
- magnetization depends on materials:
 - ↳ paramagnetic : $\vec{P} \parallel ll$ to \vec{B}
 - ↳ diamagnetic : $-\vec{P} \parallel el$ to \vec{B}
- ferromagnetic : $\vec{P} \parallel el$ to \vec{B} , but if \vec{B} becomes 0, \vec{P} is retained in ferromagnets.
- Anti-ferromagnetic : neighbouring dipoles are opposite.
- ferrimagnetic : \vec{P} is reduced (neighbouring dipoles are oppositely oriented, but not equal in magnitude, so effect is not nullified, but reduced)

Measure of magnetization = M

where M = magnetic moment per unit volume.

$M \rightarrow$ magnetization

\vec{M} (in magnetism) $\equiv \vec{P}$ (in electrostatics)

$$\frac{d\mu_m}{dT} = \vec{M}$$

$$\Rightarrow d\mu_m = \vec{M} dT$$

$$\Rightarrow \boxed{\mu_m = \int_V \vec{M} dV}$$

$$\vec{B} = \vec{\nabla} \times \vec{A}$$

$$\frac{d\mu_E}{dT} = \vec{P}$$

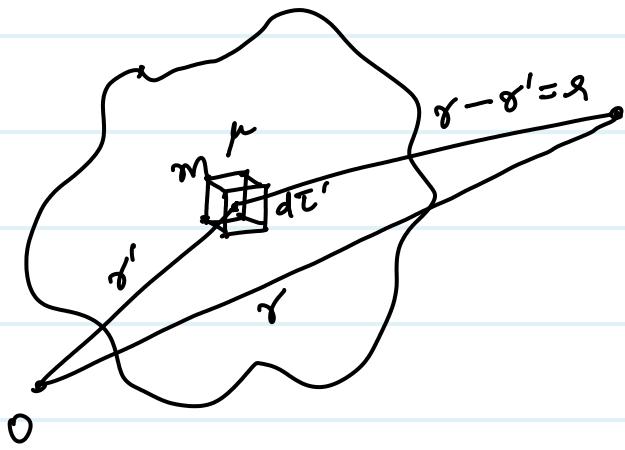
$$\Rightarrow \boxed{\mu_E = \int_V \vec{P} dV} \quad \vec{E} = -\vec{\nabla} V$$

$$\boxed{V_E = K \cdot \frac{\vec{\mu}_E \cdot \hat{r}}{r^2}}$$

$$\vec{A}_m \equiv V_E$$

$$\boxed{\vec{A} = \frac{\mu_0}{4\pi} \cdot \frac{\vec{\mu}_m \times \hat{r}}{r^2}}$$

BOUND CURRENTS



$$d\vec{A}(\gamma) = \frac{\mu_0}{4\pi} \frac{d\vec{m} \times \hat{r}}{r^2}$$

$$d\vec{A}(\gamma) = \frac{\mu_0}{4\pi} \cdot \left(\vec{M} \times \hat{r} \right) d\tau$$

$$\vec{A}(\gamma) = \frac{\mu_0}{4\pi} \int \frac{\vec{M} \times \hat{r}}{r^2} d\tau$$

$$= \frac{\mu_0}{4\pi} \int \vec{M} \times \vec{V} \left(\frac{1}{\lambda} \right) d\tau$$

$$= \frac{\mu_0}{4\pi} \int \left(\frac{1}{\lambda} (\vec{\nabla} \times \vec{M}) - \vec{\nabla} \times \left(\frac{\vec{M}}{\lambda} \right) \right) d\tau'$$

$$= \frac{\mu_0}{4\pi} \int \frac{1}{\lambda} (\vec{\nabla} \times \vec{M}) d\tau'$$

$$- \frac{\mu_0}{4\pi} \int \vec{\nabla} \times \left(\frac{\vec{M}}{\lambda} \right) d\tau'$$

$$= \frac{\mu_0}{4\pi} \int \frac{1}{\lambda} (\vec{\nabla} \times \vec{M}) d\tau'$$

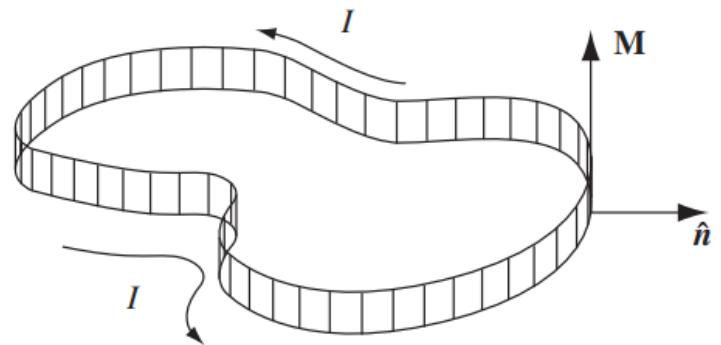
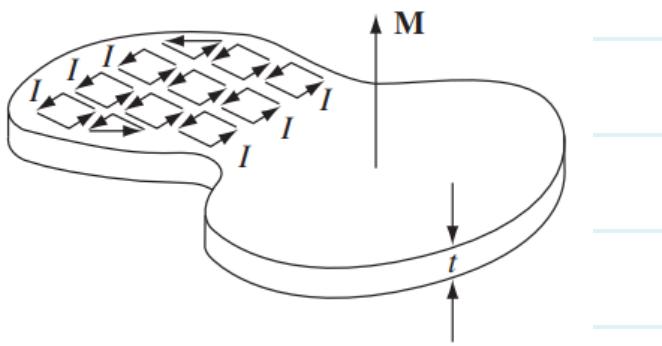
$$+ \frac{\mu_0}{4\pi} \int \frac{1}{\lambda} (\vec{M} \times \vec{da}')$$

$\boxed{\overrightarrow{J}_b = \vec{\nabla} \times \vec{M}}$

 $K_b = \vec{M} \times \hat{n}$

PHYSICAL INTERPRETATION of BOUND CURRENTS

In the last section, we found that the field of a magnetized object is identical to the field that would be produced by a certain distribution of “bound” currents, \mathbf{J}_b and \mathbf{K}_b . I want to show you how these bound currents arise physically. This will be a heuristic argument—the rigorous derivation has already been given. Figure 6.15 depicts a thin slab of uniformly magnetized material, with the dipoles represented by tiny current loops. Notice that all the “internal” currents cancel: every time there is one going to the right, a contiguous one is going to the left. However, at the edge there is *no adjacent loop to do the canceling*. The whole thing, then, is equivalent to a single ribbon of current I flowing around the boundary (Fig. 6.16).



TOTAL CURRENT

$$J = J_b + J_f$$

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc}$$

$$\Rightarrow \int_S (\vec{\nabla} \times \vec{B}) \cdot d\vec{s} = \mu_0 \int_S \vec{J} \cdot d\vec{s}$$

$$\Rightarrow \vec{J} = \frac{1}{\mu_0} (\vec{\nabla} \times \vec{B})$$

$$\therefore \frac{1}{\mu_0} (\vec{\nabla} \times \vec{B}) = J_f + \vec{\nabla} \times \vec{M}$$

$$\Rightarrow \vec{\nabla} \times \left(\frac{1}{\mu_0} \vec{B} \right) - \vec{\nabla} \times \vec{M} = J_f$$

$$\Rightarrow J_f = \vec{\nabla} \times \left(\frac{1}{\mu_0} \vec{B} - \vec{M} \right)$$

$$\therefore J_f = \vec{\nabla} \times \vec{H}; \text{ where}$$

$$\boxed{\vec{H} = \frac{1}{\mu_0} \vec{B} - \vec{M}}$$

$$\vec{\nabla} \times \vec{H} = J_f$$

$$\Rightarrow \int_S (\vec{\nabla} \times \vec{H}) \cdot d\vec{s} = \int_S \vec{J}_f \cdot d\vec{s}$$

$$\Rightarrow \int_L \vec{H} \cdot d\vec{l} = I_{f \text{ enc}}$$

$$\therefore \boxed{\oint \vec{H} \cdot d\vec{l} = I_{f \text{ enc}}}$$

$$\vec{H} = \frac{1}{\mu_0} \vec{B} - \vec{M}$$

$$\Rightarrow \vec{B} = \mu_0 (\vec{H} + \vec{M})$$

for a linear
medium,

$$= \mu_0 (\vec{H} + \chi_m \vec{H})$$

$$= \mu_0 (1 + \chi_m) \vec{H}$$

$$= \mu_0 \mu_r \vec{H}$$

$$\Rightarrow \boxed{\vec{B} = \mu \vec{H}}$$

$$\boxed{\vec{M} = \chi_m \vec{H}}$$

PROBLEM:

$l = 0.25 \text{ m}$, $N = 400$, $I = 15 \text{ A}$
 find \vec{B} , \vec{H} (magnetic field strength).

$$\vec{B} = \mu_0 n \vec{I}$$

$$= 4\pi \times 10^{-7} \times 400 \times 4 \times 15$$

$$= 4\pi \times 400 \times 4 \times 15 \times 10^{-7}$$

$$= 4\pi \times 24000 \times 10^{-7}$$

$$= 96\pi \times 10^{-4}$$

$$\vec{H} = 23952$$

$$\vec{B} = 0.0301 \text{ T}$$

$$\vec{B} = \mu_0 \vec{H} \Rightarrow$$

$$\frac{\vec{B}}{4\pi \times 10^{-7}} = \frac{\vec{H}}{4\pi} = \frac{0.0301}{4\pi} \times 10^7$$

PROBLEM

$$\vec{B} = 0.63 \text{ T}, \quad \vec{H} = 5 \times 10^5 \text{ A/m}$$

- (a) μ (b) χ_m (c) Type of magnetism

$$(a) \quad \vec{B} = \mu \vec{H}$$

$$\Rightarrow \mu = \frac{B}{H} = \frac{0.63}{5} \times 10^{-5} = 1.26 \times 10^{-6}$$

$$(b) \quad \mu_r = \frac{\mu}{\mu_0} = \frac{1.26 \times 10^{-6}}{4\pi \times 10^{-7}} = \frac{1.26}{4\pi} \times 10 = \frac{12.5}{4\pi}$$

$$= 1.0026$$

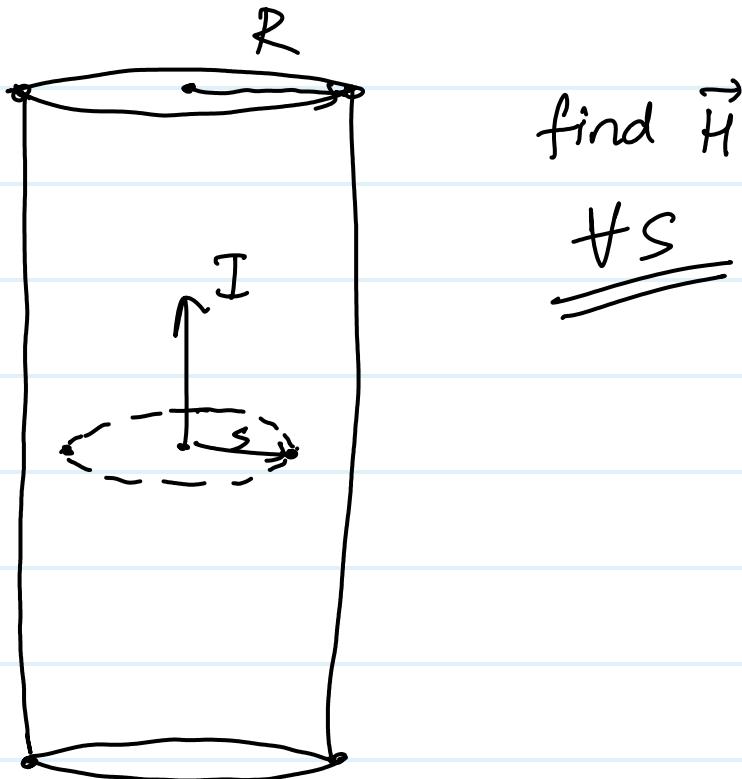
$$1 + \chi_m = \mu_r \Rightarrow \chi_m = \mu_r - 1 = 1.0026 - 1 \\ = 0.0026$$

(c) paramagnetism ($\chi_m > 0$)

$\chi_m < 0 \rightarrow$ diamagnetism

$\chi_m > 0 \rightarrow$ ferromagnetism

PROBLEM



when: $s < R$

$$\int \vec{H} \cdot d\vec{l} = I_{\text{enc}} = \int J_{\text{enc}} \cdot ds = J_{\text{enc}} \int ds$$

$$\Rightarrow H \cdot 2\pi s = \frac{I}{\frac{\pi R^2}{4}} \cdot \pi s^2$$

$$\Rightarrow \boxed{H = \frac{Is}{2\pi R^2} \cancel{\phi}}$$

When $S \geq R$:

$$\int \vec{H} \cdot d\vec{l} = \int \vec{J} \cdot d\vec{s} = \frac{I}{\pi R^2} \cdot \pi R^2 = I$$

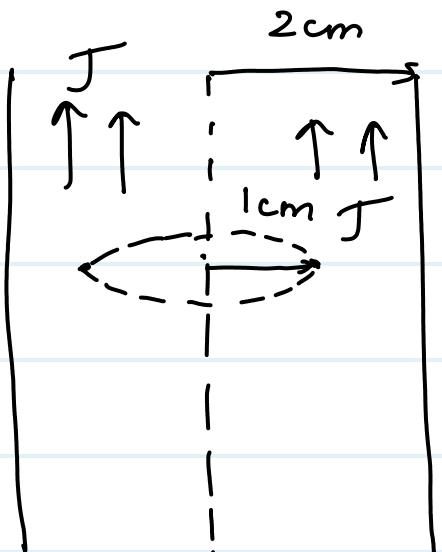
$$\Rightarrow \vec{H} \cdot 2\pi s = I$$

$$\Rightarrow \boxed{\vec{H} = \frac{I}{2\pi s} \hat{\phi}}$$

X ————— X ————— X

~~17/11/2023~~

PROBLEM - 1



$$\begin{aligned} \int \vec{B} \cdot d\vec{l} &= \mu_0 I_{enc} \\ &= \mu_0 \int \vec{J} \cdot d\vec{s} \\ \Rightarrow \vec{B} \cdot 2\pi s &= \mu_0 \cdot J \cdot \pi s^2 \\ \Rightarrow \vec{B} \cdot 2\pi s &= \mu_0 \frac{I}{\pi R^2} \pi s^2 \end{aligned}$$

$$\therefore \vec{B} = \frac{\mu_0 \times 10 \times 1 \times 10^{-2}}{2\pi \times (2 \times 10^{-2})^2}$$

$$\Rightarrow \vec{B} = \frac{\mu_0 I s}{2\pi R^2} \hat{\phi}$$

PROBLEM - 2

∞ - solenoid, n turns/unit length, radius R and current I .

$$\phi = \int_S \vec{B} \cdot d\vec{s} = \oint_L \vec{A} \cdot d\vec{l}$$

$$\Rightarrow \mu_0 n I \cdot \pi R^2 = A \cdot 2\pi R$$

$$\Rightarrow \vec{A} = \frac{\mu_0 n I}{2} s \hat{\phi}$$

$$\Rightarrow \boxed{\vec{A} = \frac{\mu_0 n I}{2} R \hat{\phi}} \quad (s=R)$$

PROBLEM - 3

$$l = 0.25 \text{ m}, \quad N = 400, \quad I = 15 \text{ A}, \quad \chi_m = 3.13 \times 10^{-4}$$

$$\vec{B} = \mu_0 (\vec{H} + \vec{M})$$

$$\vec{B} = \mu n \vec{I}$$

$$n = \frac{400}{0.25}$$

$$= \mu_0 \mu_r n I$$

$$= \underline{\underline{1600}}$$

$$= \mu_0 (1 + \chi_m) n I$$

$$\Rightarrow \vec{B} = \mu_0 (1 + 3 \cdot 13 \times 10^{-4}) \times 400 \times 15 \times 4$$

$$\Rightarrow \vec{B} = 6000 \mu_0 (1.000313) \times 4$$

$$= 24000 \mu_0 (1.000313)$$

$$\vec{H} = \frac{\vec{B}}{\mu_0 \mu_r}$$

$$\vec{H} = \frac{\vec{B}}{\mu_0 (1.000313)}$$

$$\frac{1}{\mu_0} \vec{B} = \vec{H} + \vec{M}$$

$$\Rightarrow \vec{M} = \frac{1}{\mu_0} \vec{B} - \vec{H}$$

$$= 24000 (0.000313)$$

$$= 7.512 \text{ A/m}$$

$$= 24,000 \cdot$$

PROBLEM

∞ -ly long cylinder, radius b

$$\vec{M} = b \hat{x} \hat{z}. \quad I_{\text{free}} = 0.$$

find $H_f, T_b, K_b, B_{\text{in}}, B_{\text{out}}$

$$\oint \vec{H} \cdot d\vec{l} = I_{\text{enc}} = 0$$

$$\Rightarrow \boxed{\vec{H} = 0}$$

$$T_b = \vec{V} \times \vec{M}$$

$$= \vec{V} \times (b \hat{x} \hat{z})$$

$$\frac{1}{\rho} \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ 0 & 0 & b \end{vmatrix}$$

$$\frac{1}{\rho} \left(\frac{\partial}{\partial \phi} \hat{i} - \frac{\partial}{\partial z} \hat{j} \right) b \hat{f}$$

$$- \frac{\partial \hat{j}}{\partial \rho} b \hat{f} = - b \hat{f}$$

$$\begin{aligned}
 K_b &= \vec{M} \times \hat{n} = \vec{M} \times \hat{j} \\
 &= b r \hat{z} \times \hat{j} \\
 K_b &= b r \hat{\phi}
 \end{aligned}$$

\vec{B}_{in} :

$$\begin{aligned}
 \vec{B} &= \mu_0 (\vec{H} + \vec{M}) = \mu_0 \vec{M} \\
 &= \mu_0 (0 + b \rho \hat{z}) \\
 \boxed{\vec{B} = \mu_0 b \rho \hat{z}}
 \end{aligned}$$

\vec{B}_{out} :

$$\begin{aligned}
 \vec{B} &= \mu_0 (\vec{M} + \vec{m}) \\
 &= \mu_0 (0 + 0) \\
 \Rightarrow \boxed{\vec{B} = \vec{0}}
 \end{aligned}$$

20/11/2023

BOUNDARY CONDITIONS

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\Rightarrow \int (\vec{\nabla} \cdot \vec{B}) d\tau = 0$$

$$\Rightarrow \int_s \vec{B} \cdot \vec{ds} = 0 \quad \xrightarrow{\quad \text{---} \quad} \quad B_{1,\perp} - B_{2,\perp} = 0$$

$$\Rightarrow \boxed{B_{1,\perp} = B_{2,\perp}}$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

$$\Rightarrow \int_s (\vec{\nabla} \times \vec{B}) \cdot \vec{ds} = \mu_0 \int_s \vec{J} \cdot \vec{ds} = \mu_0 I_{enc}$$

$$\Rightarrow \int_l \vec{B} \cdot \vec{dL} = \mu_0 I_{enc}$$

$$\Rightarrow (B_{1,\parallel\text{rel}} - B_{2,\parallel\text{rel}}) \cdot l = \mu_0 I_{enc}$$

$$\Rightarrow B_{1,\parallel\text{rel}} - B_{2,\parallel\text{rel}} = \mu_0 \frac{I_{enc}}{l} = \mu_0 K$$

$$\boxed{K = \frac{I_{enc}}{l}}$$

$$\therefore \boxed{B_{net\parallel\text{rel}} = \mu_0 K}$$

* NEW *

$\vec{E} \rightarrow$ due to $\vec{B}(t)$: expt. by Faraday.

$\vec{B} \rightarrow$ due to $\vec{E}(t)$: Maxwell.

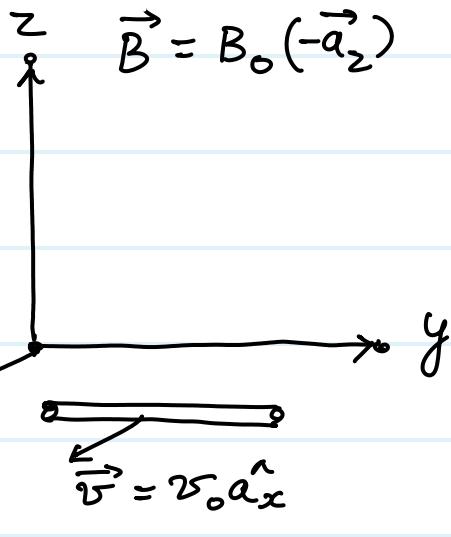
$\vec{B}(t) \rightarrow$ produces emf \rightarrow causes a current in a closed circuit

emf $\rightarrow e$ or $\epsilon \rightarrow$ Voltage generated.

When: • $B = f(t)$

- $V_{\text{circuit}} \neq 0$
- both !! !

Motional \vec{E}



$$\vec{B} = B_0 (-\hat{a}_z)$$

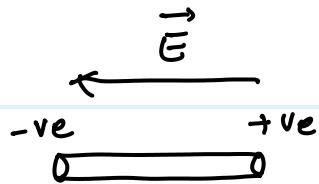
$$\vec{v} = v_0 \hat{a}_x$$

$$\therefore \text{O---O} \rightarrow \begin{matrix} -ve & +ve \end{matrix}$$

$$\vec{F}_q = q (\vec{v} \times \vec{B}) \\ = q (v_0 \hat{a}_x \times B_0 (-\hat{a}_z))$$

$$\vec{F}_q = q v_0 B_0 \hat{y}$$

$$\vec{F}_{-q} = q v_0 B_0 (-\hat{y})$$



\vec{E} produced.

$$\phi = BA$$

$$-\frac{d\phi}{dt} = B \cdot \frac{dA}{dt} = -B \cdot \left(\frac{l \cdot x}{dt} \right) \\ = Bl \cdot v$$

$$\Rightarrow e = -B_0 l v_0$$

$$\Rightarrow \boxed{e_d = -B_0 v_0 l}$$

$$\vec{E} = -B_0 v_0 (-\vec{a}_y)$$

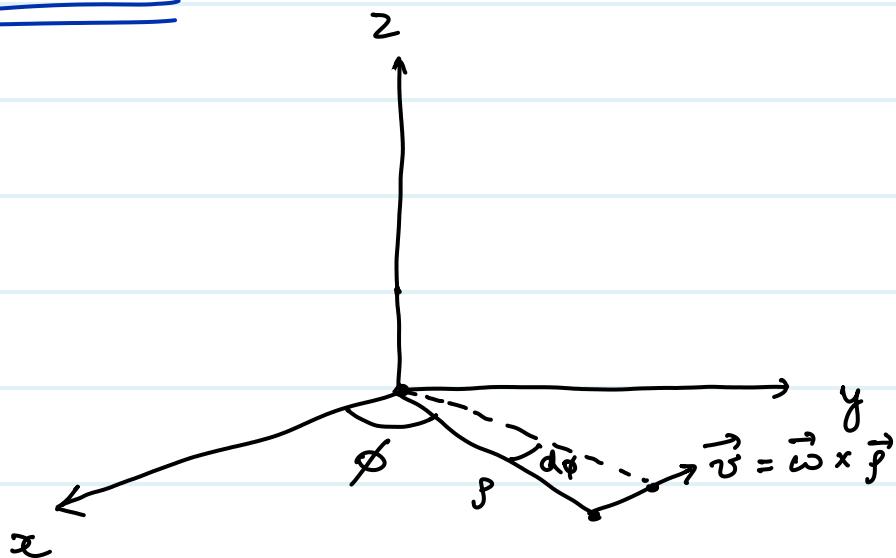
$$= B_0 v_0 \vec{a}_y$$

$$\boxed{\vec{E} = \vec{v} \times \vec{B}}$$

$$e = \frac{dW}{dq} = \frac{F \cdot dl}{q} = q \frac{\vec{E} \cdot \vec{dl}}{q} = \vec{E} \cdot \vec{dl}$$

$$\Rightarrow e = \int \vec{E} \cdot \vec{dl} = \int (\vec{v} \times \vec{B}) \cdot \vec{dl}$$

PROBLEM-1



$$e = \int (\vec{v} \times \vec{B}) \cdot d\vec{l}$$

$$= \int_0^R (B \omega \vec{r}) \cdot d\vec{l} \hat{f}$$

$$= \frac{B \omega \vec{r}^2}{2} \Big|_0^R$$

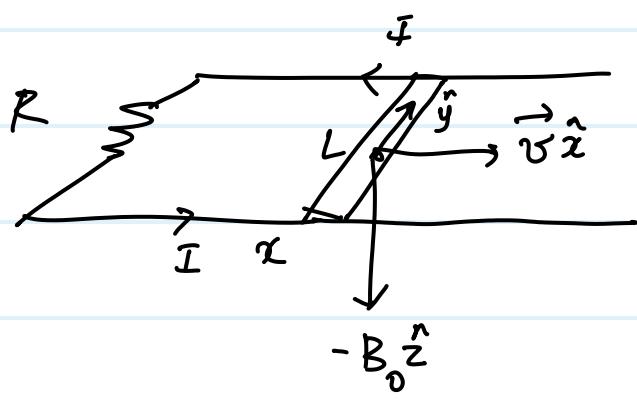
$$= B R^2 \omega / 2 = B l^2 \omega / 2$$

$$\oint (\vec{v} \times \vec{B}) \cdot d\vec{L} + \int_0^L (\vec{v}_r \times \vec{B}) \cdot d\vec{L}$$

$$= - \int_{-L}^0 (B_x \omega) \cdot dx + \int_0^L B_x \omega \cdot dx$$

$$= - \left(\frac{B_0^2 \omega}{2} \right) \Big|_{-L}^0 + \left(\frac{B_0^2 \omega}{2} \right) \Big|_0^L$$

$$= \cancel{\underline{\underline{0}}}$$



$$\phi = \vec{B} \cdot \vec{A}$$

$$\phi = -B_0 A$$

$$R = -\frac{d\phi}{dt} = B_0 \cdot \frac{dA}{dt} = B_0 L \omega$$

$$dW = +i d\vec{B} \cdot d\vec{x}$$

$$=$$

$$i = \frac{e}{R} = \frac{B_0 L \omega}{R}$$

$$F = i (\vec{L} \times \vec{B})$$

$$= \frac{B_0 L \omega}{R} (L \hat{y} \times B_0 (-\hat{z}))$$

$$F = \frac{B_0^2 L^2 \omega}{R} (-\hat{x})$$

23/11/2023

$$\mathcal{E} = \int \vec{E} \cdot d\vec{l} = \int (\nabla \times \vec{E}) \cdot d\vec{s} \quad -\textcircled{1}$$

$$\mathcal{E} = -\frac{d\phi}{dt} = -\int \frac{\partial B}{\partial t} \cdot ds$$

$$\Rightarrow \nabla \times \vec{E} = -\frac{\partial B}{\partial t}$$

$$\nabla \times \vec{H} = \vec{J}_f$$

$$\Rightarrow \vec{\nabla} \cdot (\vec{\nabla} \times \vec{H}) = \vec{\nabla} \cdot \vec{J}_f$$

$$\Rightarrow \vec{\nabla} \cdot (\vec{\nabla} \times \vec{H}) = -\frac{\partial \rho_f}{\partial t}$$

$$\Rightarrow 0 = -\frac{\partial \rho_f}{\partial t} \quad ?? \rightarrow \text{NOT POSSIBLE.}$$

$$\text{So, } \vec{\nabla} \times \vec{H} = \vec{J}_f + \vec{a}$$

$$\Rightarrow \vec{\nabla} \cdot (\vec{\nabla} \times \vec{H}) = \vec{\nabla} \cdot (\vec{J}_f + \vec{a})$$

$$\Rightarrow 0 = \vec{\nabla} \cdot \vec{J}_f + \vec{\nabla} \cdot \vec{a} \Rightarrow$$

$$\boxed{\vec{\nabla} \cdot \vec{a} = \frac{\partial \rho_f}{\partial t}}$$

$$\Rightarrow \vec{\nabla} \cdot \vec{a} = \frac{\partial \vec{\nabla} \cdot \vec{B}}{\partial t} = \vec{\nabla} \cdot \frac{\partial \vec{D}}{\partial t} \Rightarrow \boxed{\vec{a} = \frac{\partial \vec{D}}{\partial t}}$$

MAXWELLS

$$\vec{\nabla} \cdot \vec{D} = \rho \quad ; \quad \vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad ;$$

$$\vec{\nabla} \times \vec{H} = J + \frac{\partial \vec{D}}{\partial t}$$

$$0 = \sigma \vec{E} + \underbrace{\frac{\partial \vec{D}}{\partial t}}_{J_C} \quad \frac{\partial \vec{D}}{\partial t} = \epsilon_0 \epsilon_r \frac{\partial \vec{E}}{\partial t} //$$

PROBLEM : $\sigma = 0.11$, $\epsilon_r = 1.2$ at $t = 5$:

find (i) J_C , (ii) J_D } if $\vec{E} = \cos 0.1t$

$$J_C = \sigma E = 0.11 \cos 0.1t = 0.11 \cos 0.5 //$$

$$J_D = -\frac{1.2 \epsilon_0}{2} \sin 0.5 = -0.6 \epsilon_0 \sin 0.5 //$$

29/11/2023

if $A \rightarrow \text{const}$ & $\phi = f(t) \Rightarrow B = g(t)$

$$V = e = N \frac{d\Phi}{dt}, \quad \lambda = N\Phi; \quad \lambda \rightarrow n(\text{flux linkage})$$

flux current = const(1)

$$\frac{\lambda}{i} = L \Rightarrow \lambda = Li; \quad L \rightarrow \text{self inductance.}$$

$$N\Phi = Li$$

$$\boxed{\Phi \propto i}$$

$$\Rightarrow NBA = Li$$

$$\Rightarrow N\mu_0 n I A = Li$$

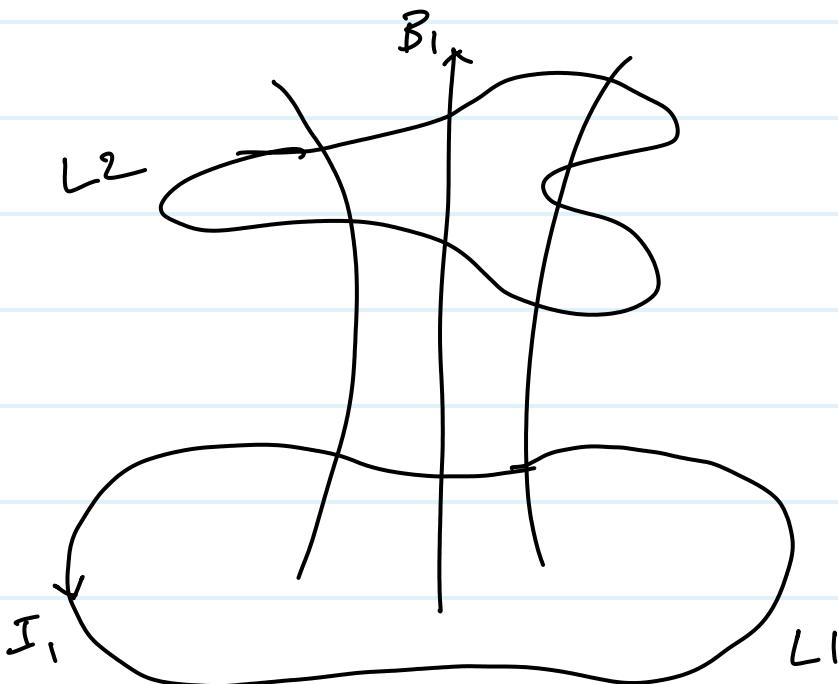
$$\Rightarrow \frac{\mu_0 N^2 A}{l} = L$$

$$\Rightarrow \boxed{L = \frac{\mu_0 N^2 \pi r^2}{l}}$$

$$N_1 = N_2, \quad l_1 = 2l_2, \quad \varrho_1 = \frac{3}{2}\varrho_2$$

$$\frac{L_1}{L_2} = \frac{\mu_0 N_2^2 \pi \left(\frac{3}{2}\varrho_2\right)^2 / 2l_2}{\mu_0 N_2^2 \pi \varrho_2^2 / l_2}$$

$$= \frac{9}{4} \times \frac{1}{2} = \frac{9}{8} //$$



$$\Phi_2 = \int \vec{B}_1 \cdot d\vec{s}_2 = M_{21} I_1$$

$$\vec{B} = \frac{\mu_0}{4\pi} \oint \frac{Idl \times \hat{r}}{r^2}$$

$$\left. \begin{aligned} W &= -\mathcal{E} q \\ \Rightarrow \frac{dW}{dt} &= -\mathcal{E} \frac{dq}{dt} \\ \frac{dW}{dt} &= -\mathcal{E} i \end{aligned} \right\} \rightarrow \begin{array}{l} \text{work} \\ \text{done against emf.} \end{array}$$

$$\mathcal{E} = -\frac{d\phi}{dt} = -L \frac{di}{dt}$$

$$\Rightarrow \frac{dW}{dt} = \left(L \frac{di}{dt} \right) i \Rightarrow dW = L i di \Rightarrow \boxed{W = \frac{1}{2} L i^2}$$

$$W = \frac{\mu_0}{2} \int H^2 dt \equiv \frac{\mathcal{E}_0}{2} \int E^2 dt$$

$$= \frac{1}{2\mu_0} \int B^2 dt$$

$\therefore \frac{L}{l} = 0.0064 \text{ H/m}$

$1600\pi\mu_0$
 $= 1600 \times 3.14 \times 4\pi \times 10^{-7}$

$$r = 20 \text{ cm}, \quad n = 200$$

$$L = \frac{\mu_0 N^2 A}{l} = (1600 \times 9.8 \times 4\pi \times 10^{-7})$$

$$\frac{20}{100} = \frac{400}{10000}$$

$$\frac{L}{l} = \frac{\mu_0 n^2 A}{l} = \frac{\mu_0 \times 40000 \times \pi \frac{400}{10000}}{l} = \frac{\mu_0 n \cdot n l A}{l} = \mu_0 n^2 A l$$

$$\vec{H} = H_0 \sin \theta \vec{a}_y \quad , \quad \theta = \omega t - \beta z$$

find (a) disp. current density (b) \vec{E} field intensity

$$\vec{\nabla} \times \vec{H} = J_C + J_D$$

$$\begin{vmatrix} \vec{a}_x & \vec{a}_y & \vec{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & H_0 \sin(\omega t - \beta z) & 0 \end{vmatrix} = 0 + \frac{\partial D}{\partial t}$$

$$\left(\frac{\partial}{\partial z} \vec{a}_x - \cancel{\frac{\partial}{\partial x} \vec{a}_z} \right) H_0 \sin(\omega t - \beta z) = \frac{\partial D}{\partial t}$$

$$\Rightarrow +H_0 \beta \cos(\omega t - \beta z) = \frac{\partial D}{\partial t}$$

$$\Rightarrow +\frac{H_0 \beta \sin(\omega t - \beta z)}{\omega} \vec{a}_z = \vec{D}$$

$$\vec{E} = \frac{\vec{D}}{\epsilon_0} = \frac{H_0 \beta}{\omega \epsilon_0} \sin(\omega t - \beta z) \vec{a}_z //$$

01/12/2023

POYNTING THEOREM

$$\vec{F} = q(\vec{E} + \vec{u} \times \vec{B})$$

$$\vec{F} \cdot \vec{u} = P = q(\vec{E} + \vec{u} \times \vec{B}) \cdot \vec{u} = q(\vec{u} \cdot \vec{E})$$

$$dP = dq(\vec{u} \cdot \vec{E})$$

$$dP = \int_V d\tau (\vec{u} \cdot \vec{E})$$

$$\frac{dP}{d\tau} = \rho_V (\vec{u} \cdot \vec{E})$$

$$= (\rho_V \vec{u}) \cdot \vec{E} = \vec{J} \cdot \vec{E}$$

$$\Rightarrow \frac{dP}{d\tau} = \vec{J} \cdot \vec{E} = \bar{P} \quad (\bar{P} \rightarrow \text{power dens.})$$

* DERIVE POYNTING THEOREM LATER *

EXAMPLE : $\vec{E}(t) = E \cos(\omega t - kz) \vec{\alpha}_x \text{ V/m}$

(a) $\vec{\nabla} \times \vec{E} = -\frac{\partial B}{\partial t}$

$$\begin{aligned}\vec{\nabla} \times \vec{E} &= \vec{\nabla} \times (E \cos(\omega t - kz) \vec{\alpha}_x) \\ &= E \cdot \vec{\nabla} \times (\cos(\omega t - kz) \vec{\alpha}_x)\end{aligned}$$

$$E \cdot \begin{vmatrix} \vec{\alpha}_x & \vec{\alpha}_y & \vec{\alpha}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \cos(\omega t - kz) & 0 & 0 \end{vmatrix}$$

$$\begin{aligned}&= E \cos(\omega t - kz) \left(\frac{\partial}{\partial z} \vec{\alpha}_y - \cancel{\frac{\partial}{\partial y} \vec{\alpha}_z} \right) \\ &= +E \frac{\partial \cos(\omega t - kz)}{\partial z} \vec{\alpha}_y\end{aligned}$$

$$+ \frac{\partial B}{\partial t} = +KE \sin(\omega t - kz) \hat{y}$$

$$B = \int KE \sin(\omega t - kz) dt$$

$$= \frac{KE}{\omega} \cos(\omega t - kz) \vec{\alpha}_y$$

$$H = -\frac{KE}{\mu\omega} \cos(\omega t - kz) \vec{\alpha}_y$$

(b) $\vec{S} = \vec{E} \times \vec{H} = \vec{\alpha}_x \times \vec{\alpha}_y = \vec{\alpha}_z$

(c) $S = \frac{-KE^2}{\mu\omega} \cos(\omega t - kz) \cdot E \cos(\omega t - kz) \hat{z} = \underline{\underline{\frac{-KE^2}{\mu\omega} \cos^2(\omega t - kz) \hat{z}}} = S$

$$\frac{-KE^2}{\mu\omega} \int_0^T \cos^2(\omega t - kz) dt$$

T

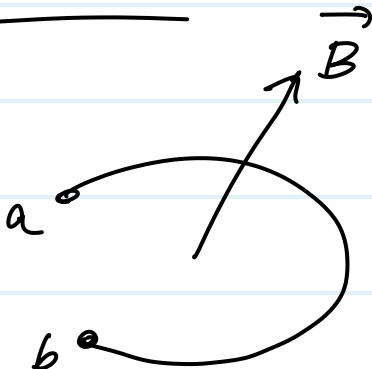
$$\begin{aligned}
 &= \frac{-KE^2}{\mu\omega T} \left[\frac{1}{2} \int_0^T \cos(2\omega t - 2kz) dt + \frac{1}{2} \int_0^T \sin(2\omega t - 2kz) dt \right] \\
 &= \frac{-KE^2}{\mu\omega T} \left[\frac{1}{4} \sin(2\omega t - 2kz) \Big|_0^T + \frac{T}{2} \right] \\
 &= \frac{-KE^2}{\mu\omega T} \left[\frac{1}{2} T \right] = \underline{\underline{\frac{-KE^2}{2\mu\omega}}}
 \end{aligned}$$

$$\cos^2 x = \frac{\cos 2x + 1}{2}$$

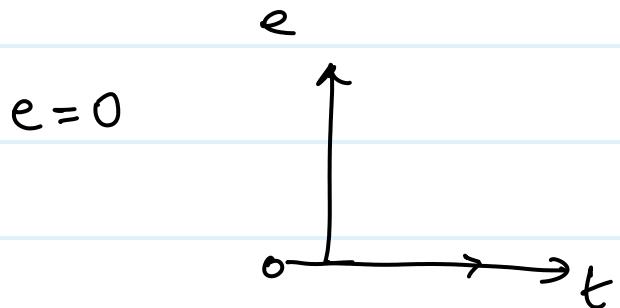
$$\therefore |P_{avg}| = \frac{KE^2}{2\mu\omega}$$

\vec{B} and \vec{e}

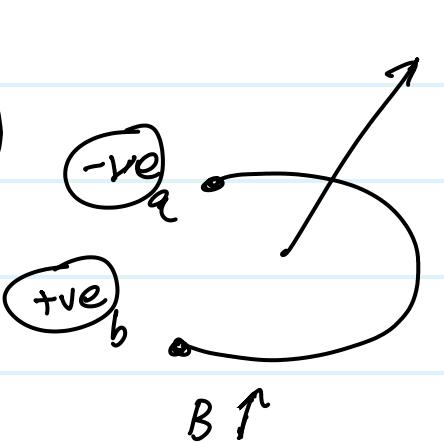
(i)



B is const.



(ii)

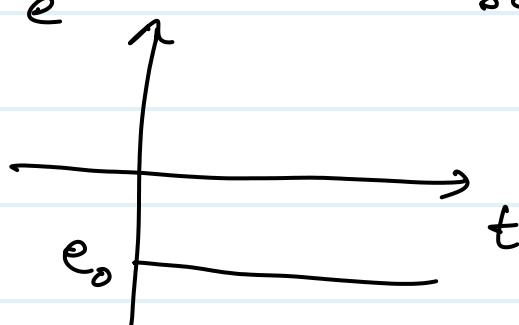


$B \uparrow$

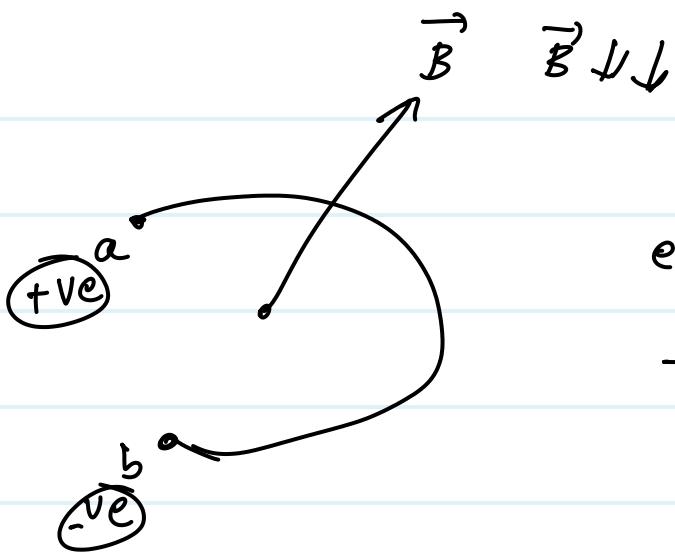
$$-e = \frac{d\phi}{dt} = A \left[\frac{dB}{dt} \right]$$

→ const. (+ve)

$\therefore e \rightarrow -ve$



(iii)



$$e = - \left(\frac{d\vec{B}}{dt} \right) A$$

, -ve
∴, $e = +ve$

