

24/1/24

Interference

Waves

→ Variation (Disturbance) of Physical Quantity that propagates through space.

i.e. Oscillation in space and time

$$y(x, t) = A \sin(kx - \omega t)$$

→ Superposition Theorem:

When two or more waves overlap, the resultant displacement at any instant is the sum of the displacements of each of the individual waves.

Interference: Superposition due to Primary wavefronts.

Diffraction: Superposition due to Secondary wavefronts.

Interference

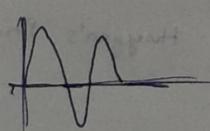
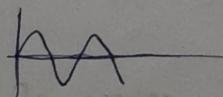
Constructive

$$l_2 - l_1 = m\lambda$$

$$m \in \mathbb{W}$$

(Path difference of any two waves being Integral multiple of wavelength)

- Maxima
- Bright Fringes



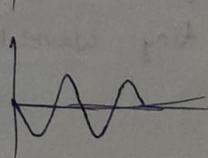
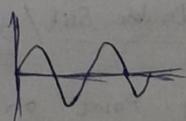
Destructive

$$l_1 - l_2 = (m + \frac{1}{2})\lambda$$

$$m \in \mathbb{W}$$

(Path difference of any two waves being half-Integral multiple of wavelength)

- Minima
- Dark Fringes



$$E_1 = E_0 \sin \theta_1$$

$$E_2 = E_0 \sin \theta_2$$

$$E_0 \sin \theta_3 = \bar{E}_1 + \bar{E}_2 = E_3$$

→ Interference Requirement:

- Need two (or) more waves
- Must have same frequency
- Must be coherent
 - i.e. phase difference should not change with time.
 - ↳ Between the two waves

Note : For sound,

$$l_1 - l_2 = \frac{\lambda}{2}, \frac{3\lambda}{2}, \dots \rightarrow \text{No Sound}$$

$$l_1 - l_2 = \lambda, 2\lambda, \dots \rightarrow \text{Max Sound}$$

[Two speakers @ certain Distance]

For light,

All Sources of Light : Incoherent Sources

(fluctuating @ 10^{14} Hz)

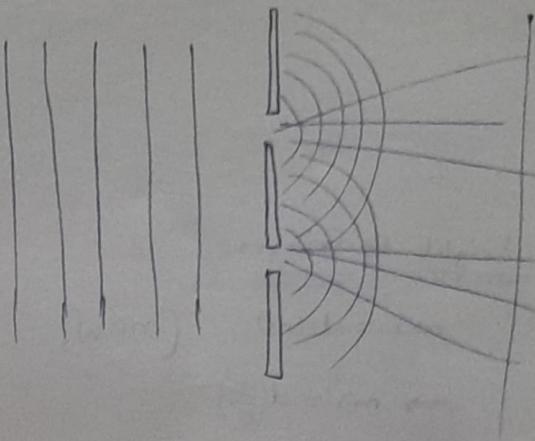
i. We need two waves from the same source taking two different paths

- Two slits
- Reflection ~~Thin Slits~~
(Thin films)
- Diffraction

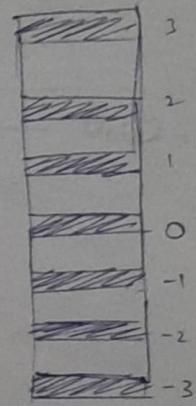
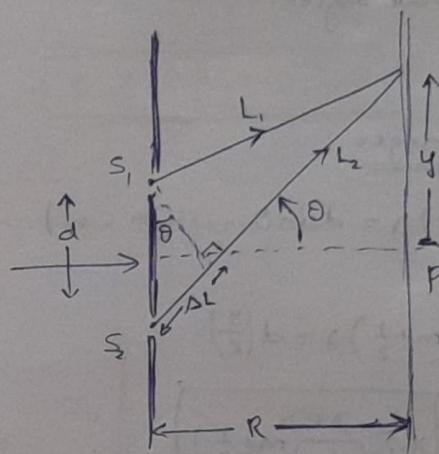
25/1/24

Young's Double Slit / Huygens :

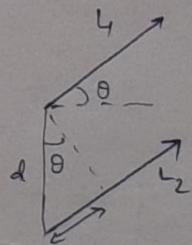
Every Point on a wavefront acts as a source of tiny wavelets that move forward — Huygen's Principle



→ Consider two rays travelling @ an angle θ :



for Infinitely distant screen:



$$\tan \theta = \frac{y}{R}$$

$$\begin{aligned} \Delta y &= d \sin \theta \\ \Delta L &= l_2 - l_1 = d \sin \theta \\ y &= R \tan \theta \end{aligned}$$

$$\Delta L = d \sin \theta = m\lambda$$

$m = 0, \pm 1, \pm 2, \dots$

} Constructive Interference

$$\Delta L = d \sin \theta = (m + \frac{1}{2})\lambda$$

$$m = 0, \pm 1, \pm 2, \dots$$

} Destruction Interference

Central Bright Fringe \Rightarrow Order = 0

For small angles,

$$y = R \tan \theta$$



$$y = R \sin \theta \longrightarrow \text{Bright fringes:}$$

$$m\lambda = d \sin \theta \quad [m \in \mathbb{W}]$$

$$\Rightarrow m\lambda = d \left(\frac{y}{R} \right)$$

$$\Rightarrow \boxed{y = \frac{\lambda R}{d} m}$$

* Note : Only for small angles

$$y = R \sin \theta \longrightarrow \text{Dark fringes:}$$

$$(m + \frac{1}{2})\lambda = d \sin \theta \quad [m \in \mathbb{W}]$$

$$\Rightarrow (m + \frac{1}{2})\lambda = d \left(\frac{y}{R} \right)$$

$$\Rightarrow \boxed{y = \frac{\lambda R}{d} (m + \frac{1}{2})}$$

Q) $R = 1.2 \text{ m}$

$$d = 0.03 \text{ mm}$$

$$m = 2, y = 4.5 \text{ cm}$$

(a) $\lambda = ?$

Soh: $\lambda = \frac{yd}{mR}$

$$\Rightarrow \lambda = \frac{4.5 \times 10^{-2} \times 0.03 \times 10^{-3}}{2 \times 1.2}$$

$$= 562.5 \times 10^{-9} \text{ m}$$

$$\boxed{\therefore \lambda = 562.5 \text{ nm}}$$

(b) $\beta = ? \rightarrow$ Fringe Width: distance b/w two adjacent Maximas or minima

$$\beta = m \left(\frac{\lambda d}{d} \right) = (m+1) \left(\frac{\lambda d}{d} \right)$$

$$= \frac{\lambda d}{d}$$

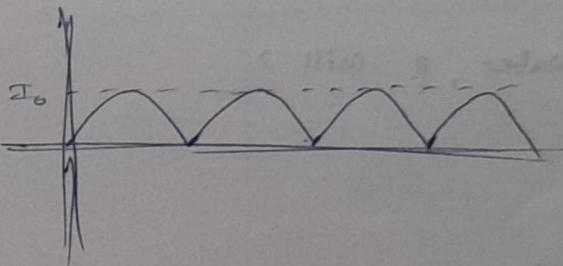
$$\Rightarrow \boxed{\beta = \frac{\lambda d}{d}}$$

$$\therefore \beta = \frac{562.5 \times 10^{-9} \times 1.2}{0.03 \times 10^{-3}}$$

$$= 225 \times 10^2 \times 10^{-6}$$

$$\boxed{\beta = 2.25 \times 10^{-2} \text{ m}} \rightarrow \boxed{\beta = 0.0225 \text{ m}}$$

(c) Intensity Pattern:



Q) $m=2$

$$\theta = 5.4^\circ, \frac{d\lambda}{\lambda} = ?$$

$$\text{Sol: } (m + \frac{1}{2})\lambda = d \sin \theta$$

$$\Rightarrow 2.5 \times \lambda = d \sin(5.4^\circ)$$

$$\Rightarrow \frac{d}{\lambda} = \frac{2.5}{\sin(5.4^\circ)}$$

$$\boxed{\frac{d}{\lambda} = 22.555}$$

$$\boxed{\frac{d}{\lambda} = 16}$$

$$\textcircled{1}) \quad \beta = 0.0240 \text{ m} = y$$

$$\lambda = 475 \text{ nm}$$

$$\sin \theta = k \tan \theta$$

$$\lambda = 611 \text{ nm}, y = ?$$

$$\beta = \frac{\lambda R}{d}$$

$$\Rightarrow \frac{\beta_1}{\lambda_1} = \frac{\beta_2}{\lambda_2}$$

$$\Rightarrow \frac{0.024}{475} = \frac{y}{611} \Rightarrow y = \frac{0.024}{475} \times 611$$

$$\therefore y = 0.03087$$

Q) If placed under water, β will?

Decrease

→ Intensity Pattern:

$$E = E_1 + E_2$$

$$E = E_p \sin(\omega t) + E_p \sin(\omega t + \phi)$$

$$= E_p [\sin(\omega t) + \sin(\omega t + \phi)]$$

$$\left[\Delta \phi = \frac{2\pi}{\lambda} dx \right]$$

$$\therefore E = 2E_p \cos\left(\frac{\phi}{2}\right) \sin\left(\omega t + \frac{\phi}{2}\right)$$

$$ds \sin \theta = \frac{\phi}{2\pi} \rightarrow \text{Path diff}$$

$$\text{Path diff} = \frac{\phi}{2\pi}$$

$$r_2 - r_1 = d \sin \theta = \frac{\lambda f}{2\pi} = \frac{\phi}{k}$$

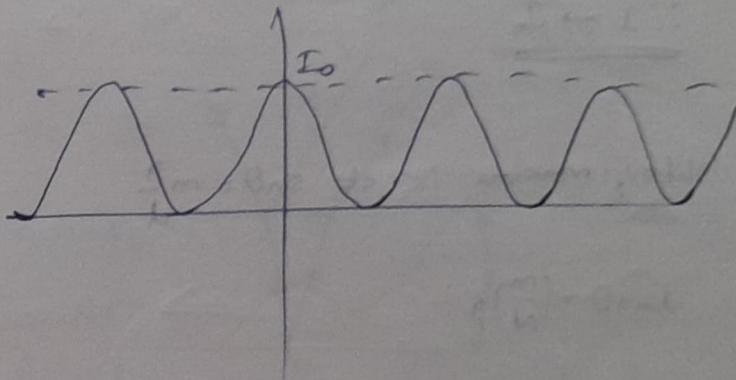
$$\Rightarrow \phi = k d \sin \theta$$

$$I = I_0 \cos^2(\frac{\phi}{2}) = I_0 \cos^2\left(\frac{k d \sin \theta}{2}\right)$$

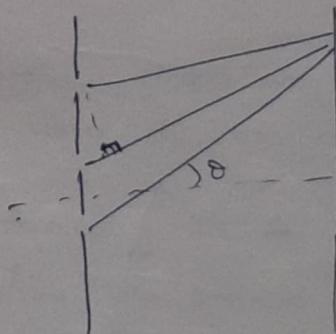
$$\sin \theta \approx \frac{y}{R} \text{ for small } y$$

$$\Rightarrow I_0 \cos^2\left(\frac{k d y}{2R}\right)$$

$$\Rightarrow I_0 \cos^2\left(\frac{\pi d y}{\lambda R}\right)$$



~~Q) 3 Fringes, What Interference~~



Constructive Interference

Ray 1 $\rightarrow I_0$

Combined Intensity = ?

Sol: $E_0 \rightarrow \text{ray } 1, 2, 3$

$$\therefore E_0 + E_0 + E_0 = 3E_0$$

$$I_0 \propto E^2$$

$$I = 9I_0$$

Q) When ray 1 and 2 → Destructive

Intensity - Minimum ?

$$E_0 - E_0 + E_0 = E_0$$

$$\therefore I \rightarrow I_0$$

For many slits, maxima is at $\sin\theta = m\frac{\lambda}{d}$

$$ds\sin\theta = \left(\frac{m}{N}\right)\lambda$$

for N Slits

3/1/24

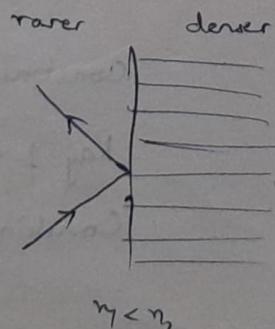
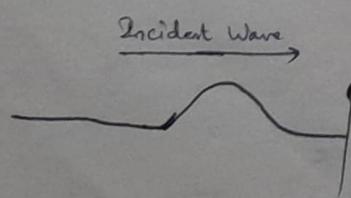
→ Interference of two types:

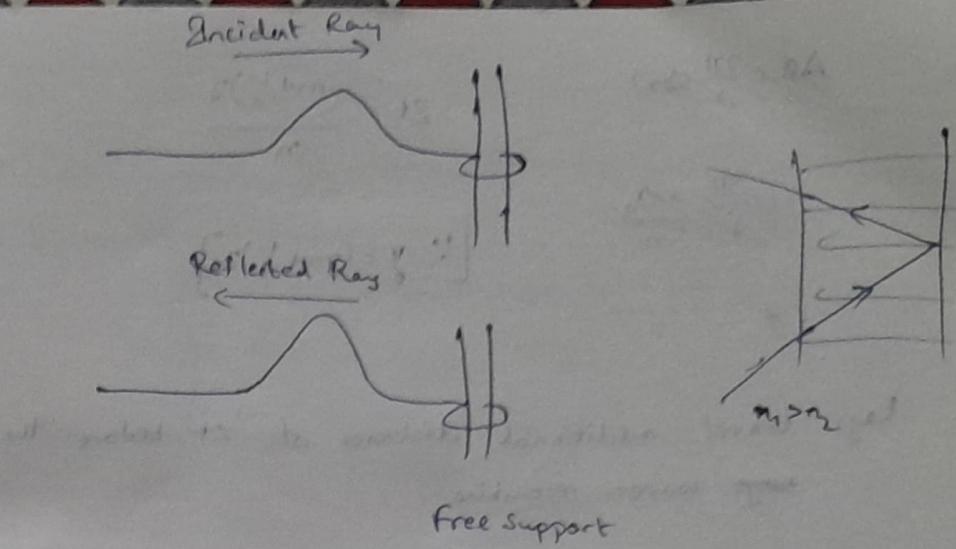
(1) Division of Wavefront

(2) Division of Amplitude

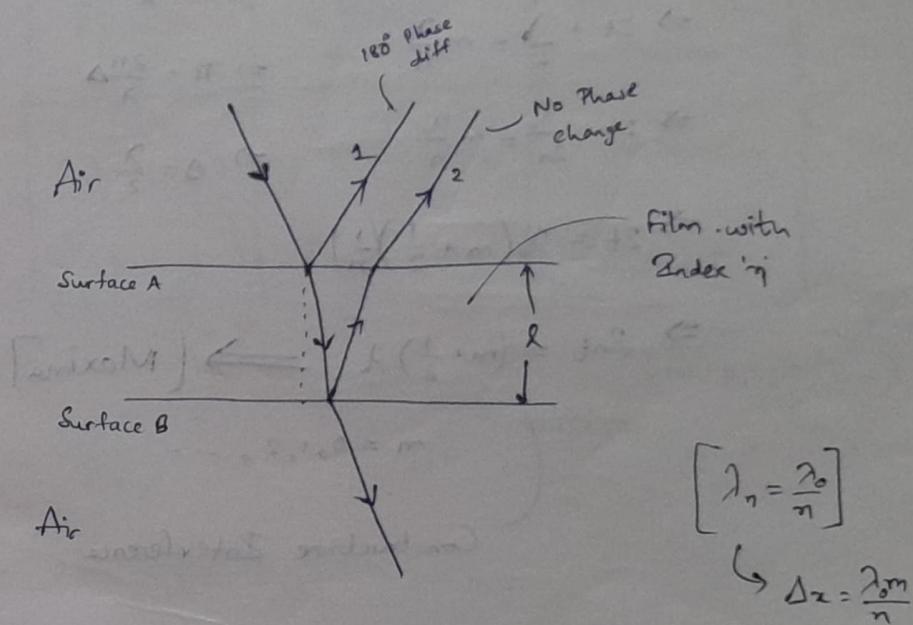
→ Phase change due to Reflection

①





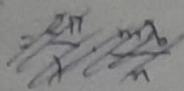
→ Interference in Thin films:



- Interference effects are observed in soap bubbles, oil in water, etc. are examples of this.
- Interference is due to interaction of the waves reflected from both surfaces of the film.
- Ray 1 and Ray 2 give Interference

$$\left[\begin{aligned} \Delta x &= \frac{2\pi}{\lambda} (\Delta n) \\ \Rightarrow \pi &= \frac{2\pi}{\lambda} (\Delta n) \\ \therefore \Delta n &= \frac{\lambda}{2} \end{aligned} \right]$$

$$\Delta\theta = \frac{2\pi}{\lambda} (\Delta x)$$



$$2t = \frac{(m+\frac{1}{2})\lambda}{n}$$

$$[\because y = (m + \frac{1}{2})\lambda_0]$$

Rays travel additional distance of $2t$ before the waves recombine

$$2t + \pi = m \frac{\lambda}{n}$$

$$\phi = \frac{2\pi}{\lambda} \Delta$$

$$\Rightarrow 2t + \frac{\lambda_0}{2} = m \frac{\lambda_0}{n}$$

$$\Rightarrow \pi = \frac{2\pi \Delta}{\lambda}$$

$$\Rightarrow 2t + \frac{\lambda_0}{2n} = m \frac{\lambda_0}{n}$$

$$\Rightarrow \Delta = \frac{\lambda}{2}$$

$$\Rightarrow 2t = \lambda_0 \left(m + \frac{1}{2} \right) \left(\frac{1}{n} \right)$$

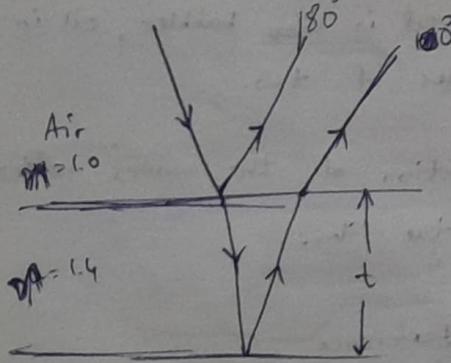
$$\Rightarrow 2nt = \left(m + \frac{1}{2} \right) \lambda \quad \Rightarrow [\text{Maxima}]$$

$$m = 0, 1, 2, \dots$$

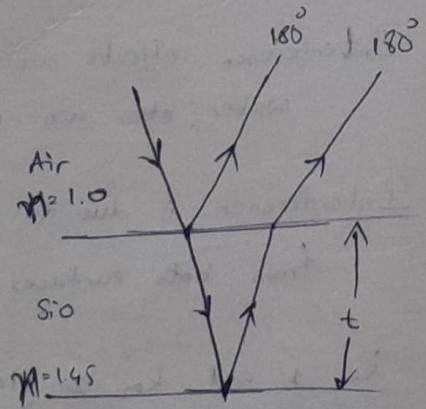
Constructive Interference

1/2/24

(g)



$$n = 1.33$$



$$n = 3.50$$

$$2nt = \left(m + \frac{1}{2} \right) \lambda$$

$$2nt = m \lambda_0$$

→ Problem Solving for Thin films,

- Identify the thin film causing the Interference
- Determine refractive Index
 - (to find which is rare and dense)
 - (to find δ, ϕ)
- Determine Phase reversal ($\theta_{\text{on}}, \theta_{\text{on},2}$)

<u>Equation</u>	1 Phase Reversal	$\theta_{\text{on}} / 2$ Phase Reversal
$2nt = (m + \frac{1}{2})\lambda$	Constructive	Destructive
$2nt = m\lambda$	Destructive	Constructive
...	vacuum	$(m: 0, 1, 2, \dots)$

(OR)

$$2t = (m + \frac{1}{2})\lambda_{\text{film}}$$

$$2t = m\lambda_{\text{film}}$$

Q) Soap film - refractive Index 'n'

↳ Air on both sides

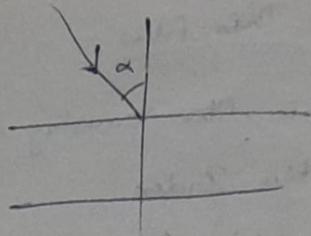
One Region - Yellow - Destructive, Removed blue ($\lambda_{\text{vac.}} = 469 \text{ nm}$)

Second Region - Magenta - Destructive, Removed Green ($\lambda_{\text{vac.}} = 555 \text{ nm}$)

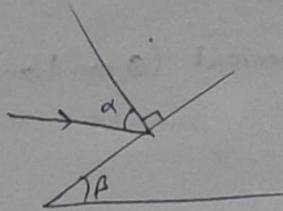
Thickness 't'

$$\frac{t_{\text{magenta}}}{t_{\text{yellow}}} = ?$$

4/2/24



$$2nt \cos \alpha = (m + \frac{1}{2})\lambda$$



$$2nt \cos(\alpha + \beta) = (m + \frac{1}{2})\lambda$$

Sol: Light falls \rightarrow Normal to surface $\Rightarrow 2t + \text{Addition due to reflection} \equiv m\lambda_{\text{film}}$

$$\therefore 2t + \frac{m\lambda_{\text{film}}}{2} = m\lambda_{\text{film}}$$

$$\left. \begin{aligned} \Delta \ell &= (m + \frac{1}{2})\lambda \\ m &: 0, 1, 2, \dots \end{aligned} \right\}$$

$$\Rightarrow 2t = \frac{m\lambda_{\text{film}}}{2}$$

$$\Rightarrow \frac{t_1}{t_2} = \frac{\lambda_{\text{film}_1}}{\lambda_{\text{film}_2}}$$

$$\left[\lambda_{\text{film}} = \frac{\lambda_{\text{vacuum}}}{n} \right]$$

$$\left[t = \frac{\lambda_{\text{vacuum}}}{2n} \right]$$

$$\frac{t_{\text{magenta}}}{t_{\text{yellow}}} = \frac{\lambda_{\text{film(magenta)}}}{\lambda_{\text{film(yellow)}}} = \frac{555}{969}$$

(Q) Orange light ($\lambda_{\text{vac.}} = 611 \text{ nm}$)

Soap film, $n = 1.33$, Air on both sides

Light strikes normal to surface

$t_{\text{min}} = ?$ for constructive interference

Sol:

$$2t = 2t + \frac{m\lambda_{\text{film}}}{2}$$

$$\left(\Delta \ell = m\lambda \quad m: 0, 1, 2, \dots \right)$$

$$2t + \frac{1}{2}\lambda_{\text{film}} = \lambda_{\text{film}}, 2\lambda_{\text{film}}, \dots$$

$$\Rightarrow \left[2t = (m + \frac{1}{2})\lambda_{\text{film}} \right] \quad m: 0, 1, 2, \dots$$

$$\left[\lambda_{\text{film}} = \frac{\lambda_{\text{vacuum}}}{n} \right]$$

$$2t = (0 + \frac{1}{2})\lambda_{\text{film}}$$

$$\Rightarrow 2t = \frac{1}{2} \times \frac{611}{n(1.33)}$$

$$\boxed{\therefore t = 115 \text{ nm}} \rightarrow t = 115 \times 10^{-9} \text{ m} \\ = 1.15 \times 10^{-7} \text{ m}$$

$$\boxed{\therefore t = 115 \times 10^{-3} \text{ pm}}$$

(a) yellow ($\lambda_{\text{vac.}} = 580 \text{ nm}$) and violet ($\lambda_{\text{vac.}} = 410 \text{ nm}$)

Falls Perpendicular

$$n_{\text{gasoline}} = 1.40$$

$$n_{\text{water}} = 1.33$$

$$t_{\min} = ? \quad \text{for (a) yellow} \quad \left. \begin{array}{l} \text{(b) violet} \\ \text{destructive} \end{array} \right\}$$

Sol.

$$2t + \frac{m\lambda_{\text{film}}}{2} = \frac{m\lambda_{\text{film}}}{2}, \frac{3m\lambda_{\text{film}}}{2}, \frac{5m\lambda_{\text{film}}}{2}, \dots$$

$$\Rightarrow 2t = 0, m\lambda_{\text{film}}, 2m\lambda_{\text{film}}, \dots$$

$$\left[\begin{array}{l} 2t = m\lambda_{\text{film}} \\ \Rightarrow t = \frac{m\lambda_{\text{vac}}}{2n} \end{array} \right]$$

$$(a) t = \frac{1}{2} \times \frac{580}{1.40} = 210 \text{ nm}$$

$$\left[\begin{array}{l} 2t = \lambda_{\text{film}} \\ t = \frac{\lambda_{\text{vacuum}}}{2n} \end{array} \right]$$

$$(b) t = \frac{1}{2} \times \frac{410}{1.40} = 150 \text{ nm}$$

9/2/24

Q) bubble - Thin, Soapy Film

looks blue @ normal incidence

$$t = ?$$

$$n_{\text{film}} = 1.35$$

$$\lambda_{\text{blue}} = 400 \text{ nm}$$

Sol:

$$2t = \lambda_{\text{film}}$$

$$\Rightarrow 2t = \frac{\lambda_{\text{vac}}}{2n}$$

$$2t = \frac{(m + \frac{1}{2}) \lambda_{\text{blue}}}{n_{\text{film}}} = \frac{\lambda_{\text{blue}}}{2n_{\text{film}}}$$

$$2t = \frac{400}{2 \times 1.35} \times \frac{1}{2}$$

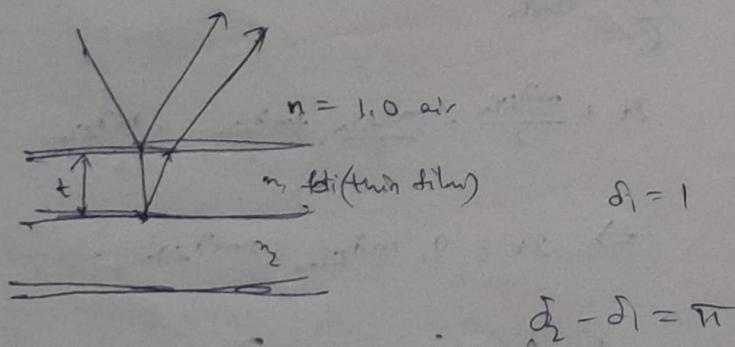
$$\boxed{2t = 74 \text{ nm}}$$

Q) Blue light $\lambda_0 = 500 \text{ nm}$

incident on glass ($n_1 = 1.5$)

cover slip ($t = 167 \text{ nm}$)

floating on top of water ($n_2 = 1.3$)

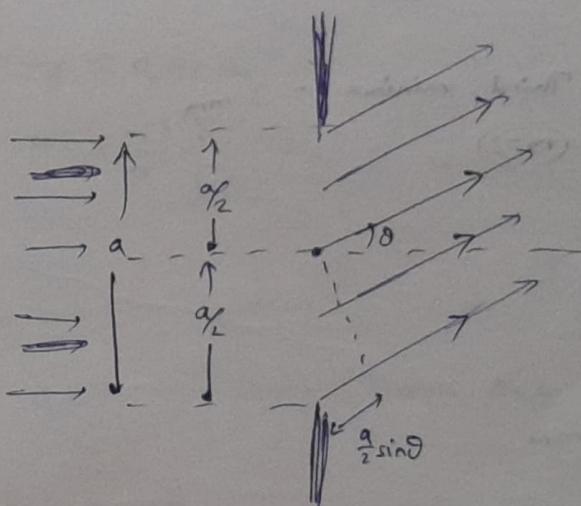


$$\text{if } n_2 > n \Rightarrow d_2 - d_1 = 0 / 2n$$

→ Diffraction:

- " A single slit placed between a distant light source and a screen produces a diffraction pattern.
- " Sharp Edges create diffraction pattern.
(Sharpness is comparable to wavelength of light)
- Intensity keeps decreasing maxima by maxima.
 - Consists broad, Intense central band.
 - Less Intensity Secondary band ~ Secondary Maxima
 - Series of Dark bands ~ Minima
 - Cannot be explained by Geometric Optics.

7/2/24



$$\sin \theta_{\text{dark}} = \frac{m\lambda}{a} \quad (m = \pm 1, \pm 2, \dots)$$

[Destructive Interference]

$$\begin{cases}
 \sin \theta = 2\lambda/a \\
 \sin \theta = \lambda/a \\
 \sin \theta = 0 \\
 \sin \theta = -\lambda/a \\
 \sin \theta = -2\lambda/a
 \end{cases}$$

$$q) \lambda = 500 \text{ nm}$$

$$a = 50 \mu\text{m}$$

$$D = 50 \text{ cm}$$

$$\Delta\theta = \gamma_a$$

$$\Delta y = L \Delta\theta$$

$$= \frac{(50 \times 10^{-4})(500 \times 10^{-9})}{50 \times 10^{-6}}$$

$$= 5 \text{ mm}$$

$$q) D = 50 \text{ cm}$$

$$\lambda = 680 \text{ nm}$$

dist. b/w first & third minima = 3 mm

$$(m=1) \quad (m=3)$$

~~cancel~~

$$a = ?$$

$$\underline{\text{Sol}} : \frac{3\lambda}{a} - \frac{\lambda}{a} = 3 \text{ mm}$$

$$\Rightarrow \frac{2\lambda}{a} = 3 \text{ mm}$$

$$\Rightarrow a = \frac{2\lambda}{3 \times 10^{-3}}$$

$$\therefore a = 4.53 \times 10^{-4} \text{ m}$$

$$\boxed{\therefore a = 0.453 \text{ mm}}$$

$$\textcircled{1} \quad \lambda = 610 \text{ nm}$$

$$a = 0.2 \text{ mm}$$

$$D = 1.5 \text{ m}$$

Width of Central Maxima?

Sol:

$$\frac{2\lambda}{a} = \frac{2 \times 610 \times 10^{-9}}{0.2 \times 10^{-3}}$$

$$= 0.0061 \text{ m}$$

$$= 6.1 \text{ mm}$$

$$y = \frac{a m \lambda}{D}$$

$$\Rightarrow 2y \approx 0.92 \text{ cm}$$

$$\left[y = a \frac{m \lambda}{D} \right]$$

$$\textcircled{2} \quad \lambda = 687 \text{ nm}$$

$$a = 0.75 \text{ mm}$$

$$D = ?$$

$$\frac{2\lambda}{a} = 1.7 \text{ mm}$$

Sol:

$$\sin \theta_{\text{dark}} = \frac{2\lambda}{a}$$

$$y = a \frac{m \lambda}{D}$$

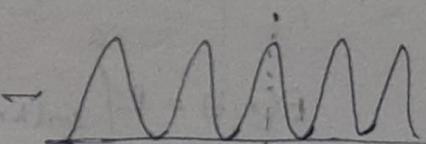
$$\Rightarrow a = \frac{y D}{m \lambda}$$

$$\Rightarrow a \approx 0.93 \text{ cm}$$

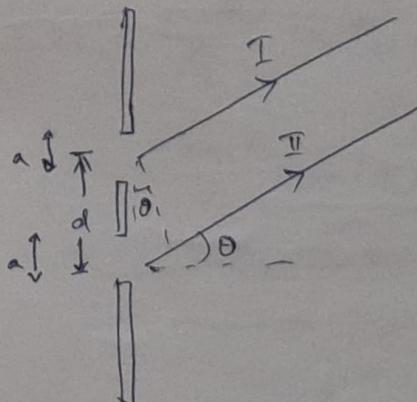
8/2/24

→ Double Slit Diffraction:

~~sh~~ $a < \lambda \rightarrow$ Young's Double slit

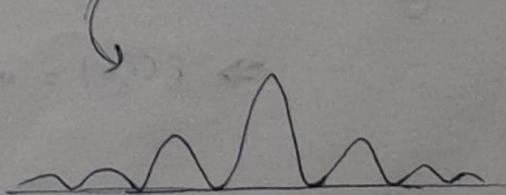


(Interference)

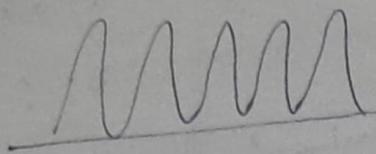


Single slit ($d=0$)

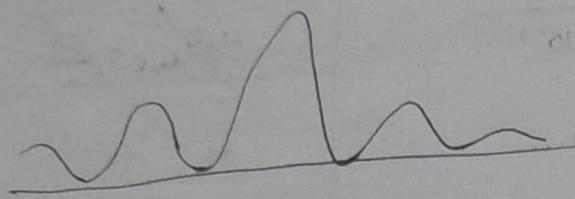
[Diffraction]



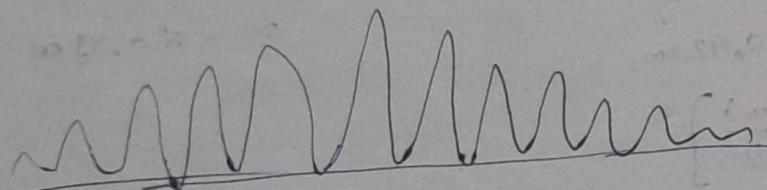
$a < \lambda$ — Double Slit Interference



$a > \lambda$ — Single Slit

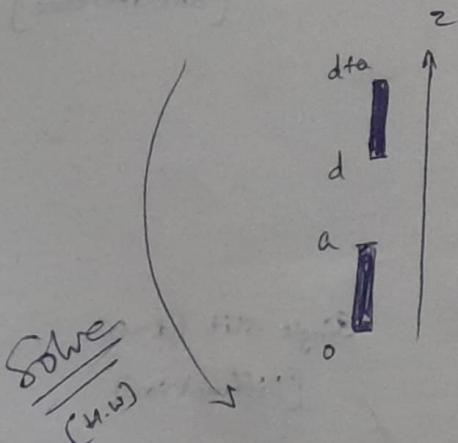


$a > \lambda$ — Double Slit



$$E(r, t) = E_0 \int_0^a \sin(kr - wt + kz \sin\theta) dz + E_0 \int_d^{d+a} \sin(kr + wt + kz \sin\theta) dz$$

$(\phi = kaz + \theta)$



$$\Rightarrow E(r, t) = a \frac{\sin(\phi_2)}{\phi_2} \sin(kr - wt + \delta + \phi_2/2)$$

$$+ a \frac{\sin(\phi_2)}{\phi_2} \sin(kr - wt + \delta + \phi_2/2 + \delta)$$

$$\int_0^a \sin(kr - wt + k_z z \sin\theta) dz$$

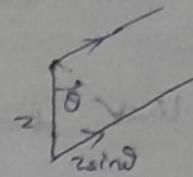
$$= \left[\frac{-\cos(kr - wt + k_z z \sin\theta)}{-k_z \sin\theta} \right]_0^a$$

$$= \frac{1}{k_z \sin\theta} \left[\cos(kr - wt) - \cos(kr - wt + a k_z \sin\theta) \right]$$

How $k_z z \sin\theta = \phi$?
 Sol:

$$\sin(kr - wt + \phi)$$

$$\phi = \frac{2\pi}{\lambda} \Delta$$



$$\therefore \phi = \frac{2\pi}{\lambda} z \sin\theta$$

$$\left[\frac{2\pi}{\lambda} = k \right]$$

$$\Rightarrow \phi = k_z z \sin\theta$$

9/2/24

$$E(r, t) = E_m a \frac{\sin(\phi_{1/2})}{\phi_{1/2}} \left[\sin(A) + \sin(A + \delta) \right]$$

$$\left. \begin{aligned} A &= kr - wt + \phi_{1/2} \\ \phi &= k_z z \sin\theta \\ \delta &= k_d z \sin\theta \end{aligned} \right]$$

$$\left. \begin{aligned} &\frac{0}{0} \\ &\text{let } z = \infty \\ &= \frac{x}{x} \\ &= 1 \end{aligned} \right]$$

$$= 2 E_m a \frac{\sin(\phi_{1/2})}{\phi_{1/2}} \cos(\phi_{1/2}) \sin(A + \delta_{1/2})$$

$$= \underbrace{\left[2 E_m a \frac{\sin(\phi_{1/2})}{\phi_{1/2}} \cos(\phi_{1/2}) \right]}_{\text{Amplitude}} \sin(kr - wt + \phi_{1/2} + \delta_{1/2})$$

Amplitude

→ Intensity:

$$\overline{P} = \overline{I}$$

$$I = I_0 \cdot \left(\frac{\sin(\phi_{1/2})}{\phi_{1/2}} \right)^2 \left(\cos^2\left(\frac{\delta}{2}\right) \right)$$

$$\phi = ka \sin \theta$$

$$\delta = kd \sin \theta$$

limit $a \rightarrow 0$	$I = I_0 (\cos \frac{\delta}{2})^2$	Young's Double Slit
limit $d \rightarrow 0$	$I = I_0 \left(\frac{\sin(\frac{\delta}{2})}{(\frac{\delta}{2})} \right)^2$	Single Slit

Note :

$$\boxed{\frac{\phi}{\delta} = \frac{a}{d}}$$

$$(A) \text{ Amplitude : } 2E_m a \left(\frac{\sin \frac{\phi_2}{2}}{\frac{\phi_2}{2}} \right) \cos \left(\frac{\phi_2}{2} \right)$$

$$A^2 = 4E_m^2 a^2 \left(\frac{\sin \frac{\phi_2}{2}}{\frac{\phi_2}{2}} \right)^2 \cos^2 \left(\frac{\phi_2}{2} \right)$$

$$I = I_0 \left(\frac{\sin \frac{\phi_2}{2}}{\frac{\phi_2}{2}} \right)^2 \cos^2 \left(\frac{\phi_2}{2} \right)$$

Proof:

$$\lim_{a \rightarrow 0} I = \lim_{a \rightarrow 0} I_0 \left(\frac{\sin \frac{\phi_2}{2}}{\frac{\phi_2}{2}} \right)^2 \cos^2 \left(\frac{\phi_2}{2} \right)$$

$$= \lim_{a \rightarrow 0} I_0 \left(\frac{\sin \left(\frac{ka \sin \theta}{2} \right)}{\left(\frac{ka \sin \theta}{2} \right)} \right)^2 \cos^2 \left(\frac{\phi_2}{2} \right)$$

$$= I_0 \cos^2 \left(\frac{\phi_2}{2} \right)$$

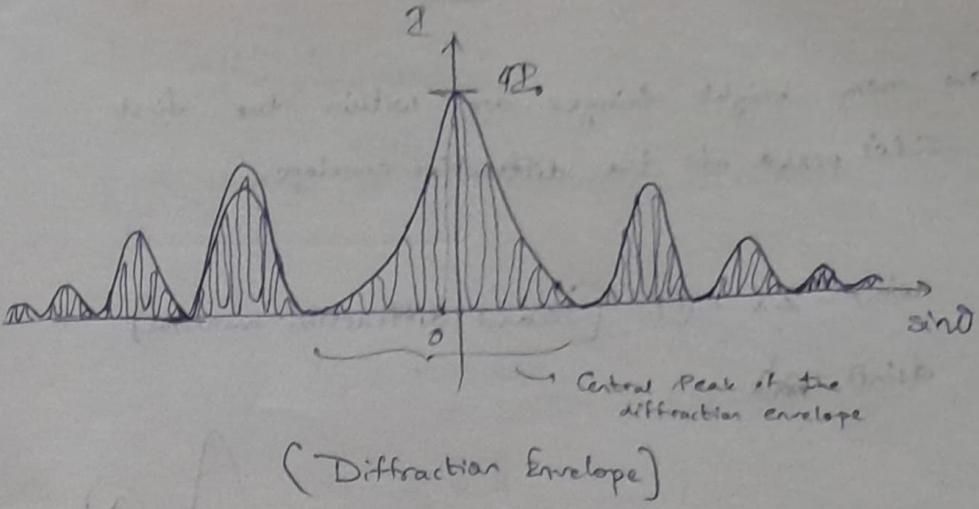
$$I = I_0 \left(\frac{\sin \frac{\phi_2}{2}}{\frac{\phi_2}{2}} \right)^2 \cos^2 \left(\frac{\phi_2}{2} \right)$$



Diffracton
Envelope

Two slit

Interference



13/2/24

Q) $\lambda = 405 \text{ nm}$

$d = 19.44 \mu\text{m}$ (centre to centre - slit separation)

$a = 9.050 \text{ mm}$ (slit width)

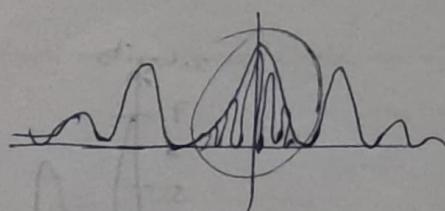
Q) How many bright fringes are within the central Peak of the diffraction envelope?

Sol:

$$m = \pm 1 \rightarrow a \sin \theta = m \lambda$$

$$\begin{cases} \text{Central} \\ \text{Peak limit} \end{cases} \quad \begin{cases} \text{Diffraction} \\ \text{envelope} \end{cases}$$

$$\Rightarrow a \sin \theta = \lambda \quad \text{--- (1)}$$



$$d \sin \theta = m \lambda \quad \text{--- (2)}$$

$$\Rightarrow m = \frac{d}{a} \quad [\text{from } (2)/(1)]$$

$$\Rightarrow m = \frac{19.44 \times 10^{-6}}{4.05 \times 10^{-3}} = 4.8$$

$$\boxed{\therefore m = 4.8}$$

$$\Rightarrow 2m = 9.6$$

$\therefore 9$ fringes

$$[9.6] = 9$$

$\Rightarrow 9$ fringes

i.e. $0, \pm 1, \pm 2, \pm 3, \pm 4$

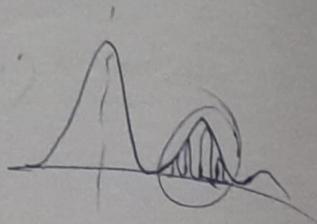
Q2) How many bright fringes are within the first side's peak of the diffraction envelope.

Sol: $a \sin \theta = m\lambda \rightarrow ①$ [Second diffraction minima]

$$d \sin \theta = \frac{m}{n} \lambda - ②$$

$$\Rightarrow m' = \frac{2d}{\lambda} = 9.6$$

$$\boxed{\therefore m = 9.6}$$



$m' = 5, 6, 7, 8, 9$ lie within the side's peak

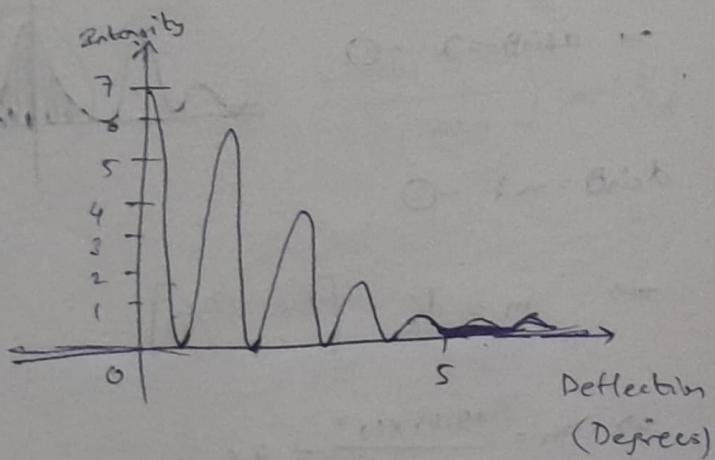
$\therefore 5$ fringes

Q) $\lambda = 440 \text{ nm}$

double slit

Q(a) Slit width = ?

Q(b) Slit separation = ?



Sol: $a \sin \theta = m\lambda$

$$\begin{aligned} m &= 4 \\ \lambda &= 440 \text{ nm} \end{aligned} \quad \left\{ \Rightarrow a = \frac{m\lambda}{\sin(5^\circ)} = \frac{4 \times 440 \times 10^{-9}}{\sin(5^\circ)}$$

$$I = I_0 \left(\frac{\sin(\phi/2)}{\phi/2} \right)^2 \cos^2(\phi/2)$$

First Minima of Diffraction $\rightarrow \theta \approx 5^\circ$

$$\Rightarrow \cancel{\frac{5\pi}{180}}$$

$$\phi/2 = \pi \sin \theta/2$$

$$\Rightarrow \phi/2 = \pi$$

$$\therefore a = \lambda \sin \theta \Rightarrow a = 5.048 \mu m$$

First Maxima of Interference $\rightarrow \theta \approx 1.25^\circ$

$$\phi/2 = \pi$$

$$\Rightarrow d = \lambda \sin \theta \Rightarrow d = 20.2 \mu m$$

14/2/24

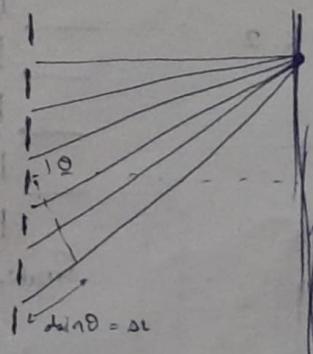
Diffraction Grating:

- An arrangement of many slits
- Assumptions :
 - (1) The slits are Narrow (Each one produces single wave)
 - (2) The screen is very far

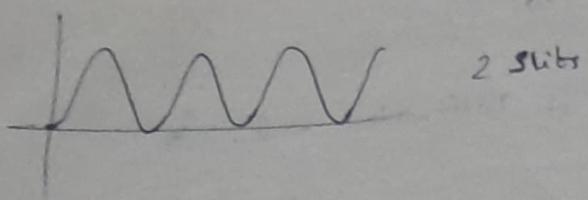
- For two adjacent slits :

$$\Delta L = d \sin \theta$$

Constructive :
 $d \sin \theta = m\lambda$
 $[m \in \mathbb{W}]$



No 'O' Intensity in this case



2 slits

$$\text{Ex. } \lambda = 630 \text{ nm}$$

$$h = 0.15 \text{ m}$$

↳ Diffraction slits are separated by

$$W = 2 \text{ m}$$

↳ distance of screen from the grating

Find 'd',

↳ distance b/w slits in the grating

Sol:

$$ds \sin \theta = m \lambda$$

$$\Rightarrow d = \frac{m \lambda}{\sin \theta}$$

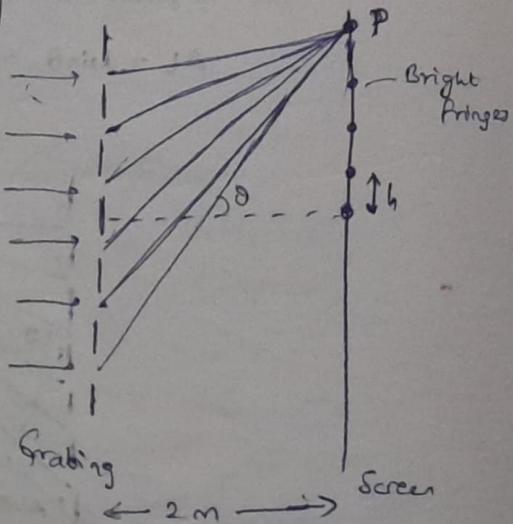
$$\Rightarrow d = \frac{630 \times 10^{-9}}{0.15} \times 2$$

$$= 8400 \times 10^{-9}$$

$$= 8.4 \mu\text{m}$$

$$\boxed{\therefore d = 8.4 \mu\text{m}}$$

$$\left[\sin \theta = \frac{y}{D} = \frac{h}{W} \right]$$



(OR)

$$\tan \theta = \frac{h}{w}$$

$$\Rightarrow \theta = \tan^{-1}\left(\frac{h}{w}\right) \text{ rad}$$

Convert into degrees

$$\pi^c = 180^\circ$$

$$1^\circ = \frac{180}{\pi}$$

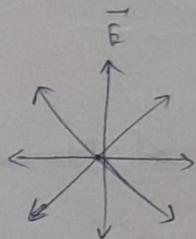
$$\tan^{-1}\left(\frac{h}{w}\right)^c = \frac{180}{\pi} \times \tan^{-1}\left(\frac{h}{w}\right)$$

$$\sin \theta = m \lambda \Rightarrow \sin \theta = \lambda$$

$$\Rightarrow d = \frac{\lambda}{\sin(\tan^{-1}(h/w))}$$

20/2/24

Polarisation



Unpolarised Light
(Daily life)



Linearly
Polarised Light
(Lasers)

Planar Wavefronts

(Plane Polarised Light)

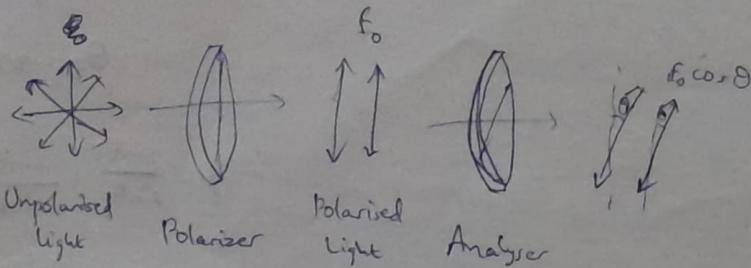
Polarisation can be obtained by

(1) Absorption

(2) Reflection

(3) Selection

(1) Absorption:



$$I = I_0 \cos^2 \theta : \text{Malus' Law}$$

Before Analyser

After Analyser

(2) Reflection:

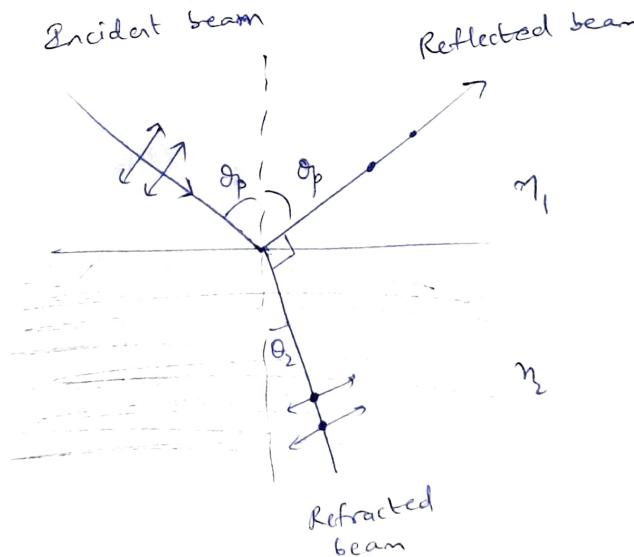
Angle: 0 or 90° ,

After passing through a medium and gets reflected ~~off~~ from a surface,

Reflected beam is unpolarised.

Angle - b/w 0° and 90° - some degree of Polarisation

Particular Angle: Completely Polarised



$$\theta_p + 90^\circ + \theta_2 = 180^\circ$$

$$\theta_2 = 90^\circ - \theta_p$$

$$\eta = \frac{\sin \theta_1}{\sin \theta_2} = \frac{\sin \theta_p}{\sin \theta_2} = \frac{\sin \theta_p}{\cos \theta_p}$$

$$\therefore \eta = \frac{\sin \theta_p}{\cos \theta_p} = \tan \theta_p$$

Q) Light - Intensity I_0

Polarised parallel to Transmission axes of a Polariser
& is incident on an Analyser

(a) Transmission axis of Analyser makes 45° with axis of Polariser

$$\underline{\text{Soln}} \quad I_0 = I_0$$

$$I = \frac{I_0}{2}$$

(b) Angle for which $\frac{I}{I_0} = \frac{1}{3}$

$$I = I_0 \cos^2 \theta$$

$$\Rightarrow \frac{I_0}{3} = I_0 \cos^2 \theta$$

$$\Rightarrow \cos^2 \theta = \frac{1}{3}$$

$$\cos \theta = \frac{1}{\sqrt{3}} \Rightarrow \cos^{-1}\left(\frac{1}{\sqrt{3}}\right) = \theta$$

13/3/24

LASERS

→ LASER:

L : Light

A : Amplification by

S : Stimulated

E : Emission of

R : Radiation

→ LASER: Photons are in Phase

↳ Emits coherent source

Population:

no. of atoms per unit vol.
that occupy a given energy
state. (N)



1 ←
(Ground state)

Note $-E/kT$

[k : Boltzmann's constant]

Atoms tend to be at lowest ~~energy~~ possible
energy level

$$N = N_0 \cdot e^{-E/kT}$$

At temp. above 0 K:

- Atoms have some thermal energy.
- Distribute themselves among available energy levels according to their energy.

At $T = 0$ K:

All atoms are in the ground state.

Note:

Population at each energy level decreases with increase in energy level.

→ Boltzmann's Equation:

$$\underline{N_1 = k e^{-E_1/kT}} \quad \& \quad \underline{N_2 = k e^{-E_2/kT}}$$

$$\frac{N_1}{N_2} = e^{-(E_2 - E_1)/kT}$$

$$\boxed{\therefore N_2 = N_1 \cdot e^{-\Delta E/kT}} \quad ; \quad \Delta E = E_2 - E_1$$

Relative Population

Depends on two factors - (i) Energy Diff.
 $(E_2 - E_1)$

(ii) Temperature
(T)

At lower temps., All atoms - Ground ~~floor~~ State

At higher temps., ~~All~~ Some atoms - Higher state

Limiting Cases :

$$E_2 - E_1 \rightarrow 0 \Rightarrow N_2 - N_1 \approx 0 \Rightarrow \underline{\underline{N_1 = N_2}}$$

$$T \rightarrow \infty \Rightarrow N_2 = N_1$$

\therefore Material in Thermal equilibrium \rightarrow Population of higher states cannot exceed the population of lower states

For Lasing Action - More than 2 energy levels

14/3/24

Simple Absorption : When energy is available $n=1$ to $n=2$

Excitation : Induced / stimulated absorption

De-excitation : Spontaneous emission

$$\hbar\nu = E_2 - E_1$$

↳ Monotwisted

Lifetime of excited state = μs or ms

Lasing Action \uparrow Lifetime \uparrow

→ Properties of laser, also depend on material & setup (design)

Lasers - mW

High-Power lasers - kW

→ Stimulated Emission:

① Absorption:

$$\text{Rate of Absorption} = B_{12} \cdot f(v) \cdot N_1 \quad \text{--- (1)}$$

$$[A + h\nu = A^{\ddagger}]$$

N_1 : Population at lower level N_1

$f(v)$: Energy density of incident light

B_{12} : Proportionality constant ~~for~~

(Einstein coefficient for induced Absorption)

→ Indicates probability of an induced transition from Level 2-1.

② Spontaneous Emission:

$$\text{Rate of Spt. Emission} = A_{21} \cdot N_2$$

A_{21} : Einstein coeff. for spt. emission and is a function of frequency and properties of material.

$$A_{21} = 1/\tau_{sp} \quad \text{--- (2)} \quad [\tau_{sp}: \text{Lifetime of spt. emission}]$$

Important features:

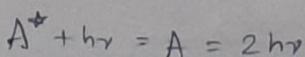
- (1) No outside control
[No stimulus]
- (2) Probabilistic in nature
- (3) Incoherent
- (4) Non-Monochromatic
[Will be monochromatic, if there is a film]
(Still Incoherent)
- (5) Lack of Directionality

$$\underline{\underline{P_{\text{total}} = NI}}$$

18/3/24

④ Stimulated Emission:

- Most important for lasers
- When no. of e^- in higher energy is more.



$$R_{st} = B_{21} \cdot P(v) \cdot N_2 - \textcircled{?}$$

B_{21} — Einstein coefficient for stimulated emission.

Important Features:

- (1) Controlled from outside
- (2) Same freq., same phase & same phase of Polarisation
- (3) Coherent
- (4) Monochromatic
- (5) Directional

Note: All these are properties of Laser as well

→ Light Amplification:

- Multiplication of Photons
- All in same phase & travel in same direction

$$I_{\text{total}} = N^2 I$$

Intensity of Stimulated Photons

→ Steady State Condition:

$$\text{Rate of Absorption} = \text{Rate of Spontaneous emission} + \text{Rate of Stimulated emission}$$

i.e. Thermal Equilibrium

Φ Einstein Relations

$$@ \text{Thermal eq, Rate of Absorption} = \text{Rate of Emission}$$

$$\beta_{12} p(v) \cdot N_1 = A_{21} N_2 + \beta_{21} p(v) N_2$$

$$\Rightarrow p(v) \cdot [B_{21} N_1 - B_{12} N_2] = A_{21} N_2$$

$$\boxed{\therefore p(v) = \frac{A_{21} \cdot N_2}{B_{21} \cdot N_1 - B_{12} \cdot N_2}}$$

Can be known from Planck's Law

$$p(v) = \frac{A_{21}/B_{12}}{N_1/N_2 - B_{21}/B_{12}}$$

$$\text{As } \frac{N_1}{N_2} = e^{\frac{(E_2 - E_1)/h\nu}{kT}} = e^{\frac{h\nu}{kT}}$$

$$\therefore p(v) = \frac{A_{21}}{B_{12}} \left[\frac{1}{e^{hv/kT} - \frac{B_{21}}{B_{12}}} \right]$$

Must be identical to Black body Radiation
 & be consistent to with Planck's Law of
 Radiation Law.

→ Conditions for Large Stimulated Emissions:

Key to Laser Action - Existence of Stimulated Emission

$$\frac{B_{21}}{A_{21}} = \frac{B_{12}}{A_{12}} = \frac{e^3}{8\pi h\nu^3 \mu}$$

$$R_1 = \frac{1}{e^{hv/kT} - 1}$$

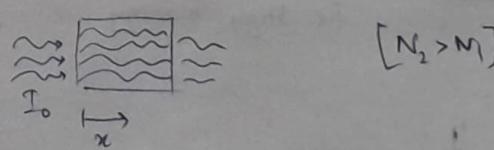
$$R_2 = \frac{\text{Stimulated Transitions}}{\text{Absorption Transitions}} = \frac{B_{21} p(v) \cdot N_2}{B_{12} \cdot p(v) \cdot N_1}$$

$$\text{As } B_{21} = B_{12} \Rightarrow R_2 = \frac{N_2}{N_1}$$

Lifetime in excited state $\uparrow \Rightarrow$ Better Material for Laser

$$I = I_0 \cdot e^{-\alpha x}$$

↪ Intensity inside the material



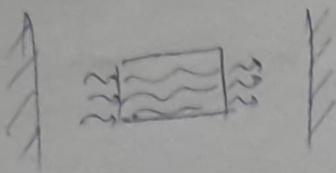
Gain Coefficient - γ $[\gamma > 0]$

$$I = I_0 e^{\gamma x} \quad [N_2 > N_1]$$

$\hookrightarrow \alpha \rightarrow -ve$

$N_1 > N_2 \Rightarrow \alpha > 0$ Always

[γ : Gain coeff. per unit length]



$$\gamma = (N_2 - N_1) \frac{B_{12} h\nu}{V} \rightarrow \text{Conditions of Amplification}$$

$\gamma > 0$ when $N_2 > N_1$

Population inversion:

16/4/24

$\text{Ar}^+ \Rightarrow$ Electronic Transitions

$\text{CO}_2 \Rightarrow$ Vibrational levels

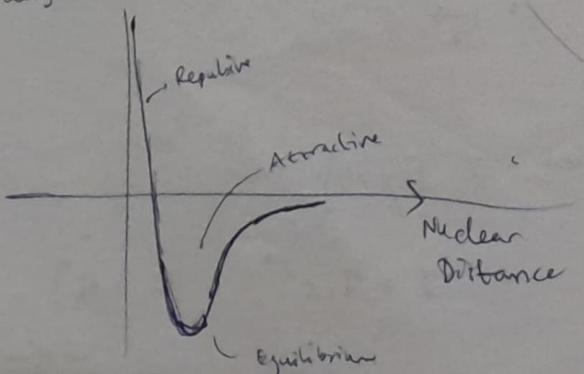
$\text{CO}_2 \Rightarrow \text{O=C=O}$

$E_{\text{rotation}} < E_{\text{transitional}} < E_{\text{electronic}}$

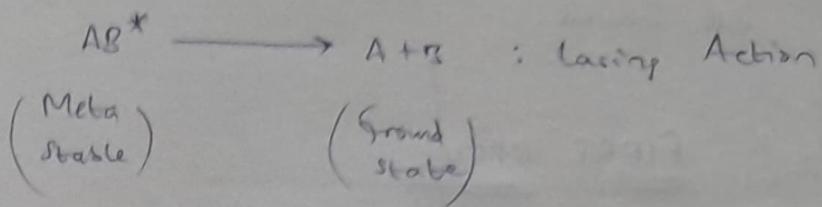
17/4/24

Excimer Laser — UV Laser
i.e. High Energy

P.E. diagram:



No Cavity Mirrors required.



UV Lasers used mostly in Photolithography.

Ground State - Monomers (A + B)

~~18/12/24~~ Chemical Lasers :

NOT IN SYLLABUS

Dye Lasers

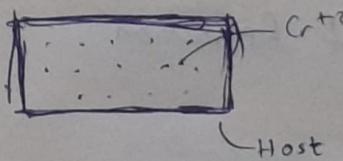
Dye : Fluorescent

Singlet & Triplet — According to spin, states
 $(2s+1, s=0)$ $(2s+1, s=1)$

Singlet $\xrightarrow{\text{Transition}}$ Singlet

Triplet $\xrightarrow{\text{Transition}}$ Triplet

Singlet $\xrightarrow[\text{Not Possible}]{\text{Transition}}$ Triplet



Lasing Action : Dye

Solid State Lasers - singular Wavelength

Gas Laser - 3-4 wavelengths

Dye lasers - 320 nm \rightarrow 1000 nm
(UV) (FIR)

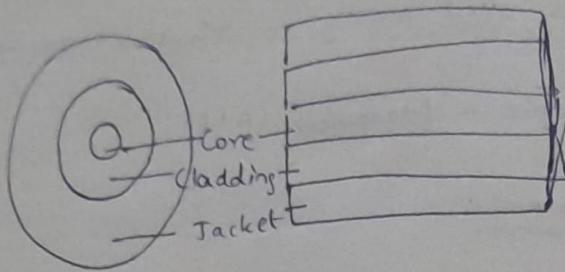
Note :

Hazardous to Human health

Pumps High Energy - Less Visibility
but Coherent.

23/4/24

FIBRE OPTICS



Fiber cross
section

Optical Fibre Material — Glass/Plastic

Imp:

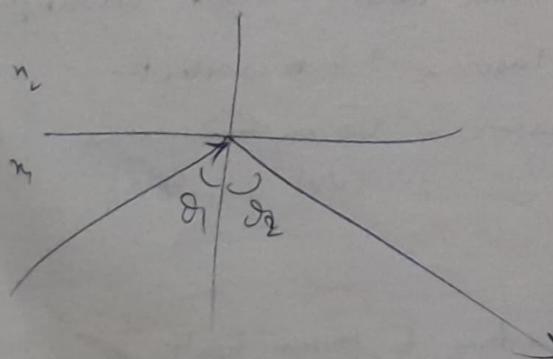
TIR: Snell's Law

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

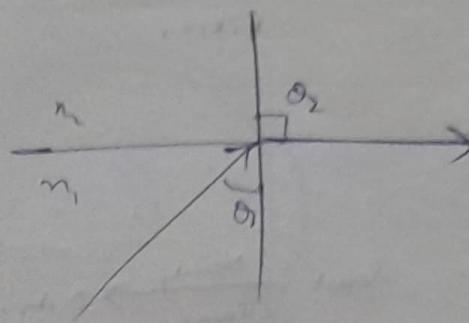
[Relation b/w
Core & Cladding]

Angle of Refraction

(i) Angle of Incidence > Critical Angle

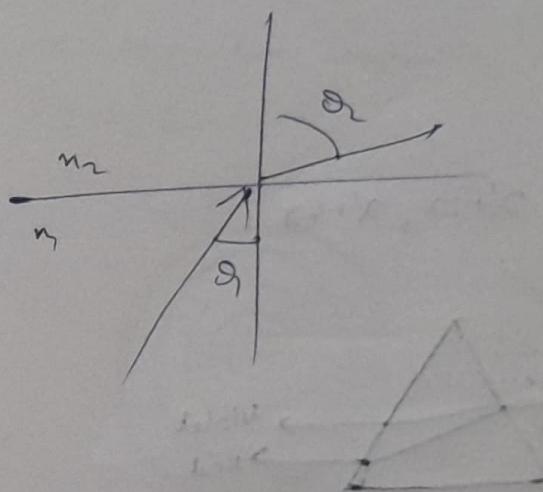


(ii) Angle of Incidence = Critical Angle



(iii) Angle of Incidence < Critical Angle

Min. angle for TIR



→ Numerical Aperture:

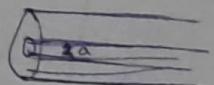
Solid Angle within which if light falls,
TIR occurs

$$NA = \sqrt{n_1^2 - n_2^2} = \sin \theta_a$$

$$V = 2\pi \cdot \frac{NA}{2} a$$

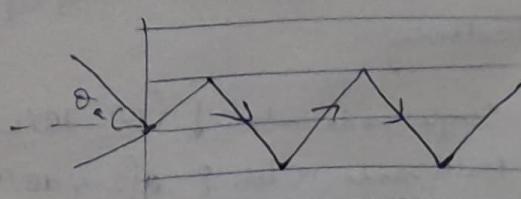
a: Core Radius

$$\text{Angle of Acceptance} = 2\sqrt{n_1^2 - n_2^2}$$

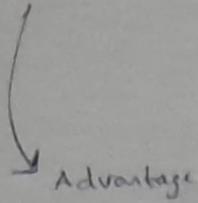


24/4/24

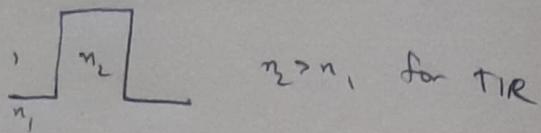
Refractive Index changes step-by-step : Step-Index fibre



Graded Index Fibre : less Dispersion in multi mode compared to the step-index fibre.

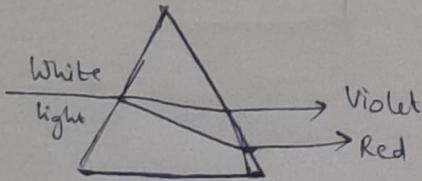


Single mode : Input $\xrightarrow[\text{Nearby}]{\text{same}}$ Output
[slight diff. in diameter]

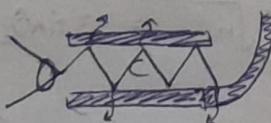
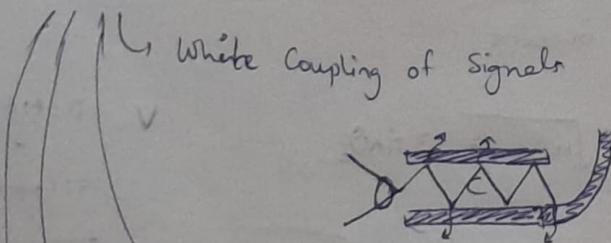


→ Dispersion:

$$\lambda \rightarrow \lambda' + 2\lambda, \lambda' + 4\lambda$$



→ Losses:



-) Escaping light through Cladding (leakage)
most of the time & because of Bending
-) After long distance, Signal becomes weak
 \therefore Signal needs Amplifying
-) Scattering

Single mode - loss \downarrow [0-4 dB/km] (Dispersion)

Multi mode - loss \uparrow a [2-4 dB/km]

- Bending ~~because~~ losses because light falls beyond critical angle and light goes to cladding \therefore loss.

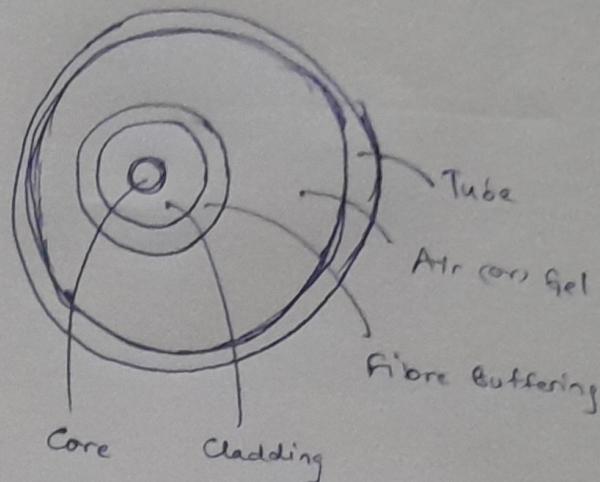


Fig. (a) Loose - Tube Construction

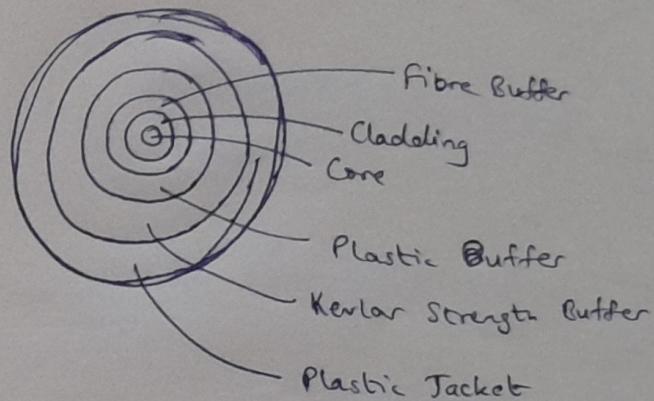


Fig. (b) Tight - buffer Construction