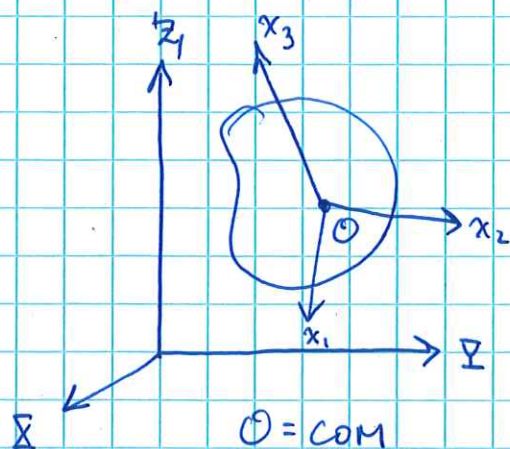


# Summary

04/03/24



$$T = \frac{1}{2} M V^2 + \frac{1}{2} \sum_{ij} I_{ij} \Omega_i \Omega_j$$

$$I_{ij} = \sum m (r^2 \delta_{ij} - x_i x_j)$$

$$L_i = \sum_j I_{ij} \Omega_j$$

$\hookrightarrow \vec{L}$  = ang. mom. w.r.t. O.

• if  $(x_1, x_2, x_3)$  = principal axes:

$$\begin{cases} T_{\text{rot.}} = \frac{1}{2} (I_1 \Omega_1^2 + I_2 \Omega_2^2 + I_3 \Omega_3^2) \\ L_1 = I_1 \Omega_1, L_2 = I_2 \Omega_2, L_3 = I_3 \Omega_3. \end{cases}$$

## Rigid-body EOM

Rigid body = mechanical system w/ 6 DOF.

$$\Rightarrow \text{need 6 EOM} \rightarrow \left. \begin{aligned} \dot{\vec{P}} &= \dots \\ \dot{\vec{L}} &= \dots \end{aligned} \right\} 6 \text{ EOM}$$

$\vec{P}$  = total mom.

$\vec{L}$  = total ang. mom. about COM.

• First EOM:  $\vec{P} = \sum \vec{p}$  (sum over all particles of body).

$$\Rightarrow \dot{\vec{P}} = \sum \dot{\vec{p}} = \sum \vec{f} = \vec{F}$$

$\uparrow$   
 individual forces acting on particles      total force.

$$\Rightarrow \boxed{\dot{\vec{P}} = \vec{F}}$$

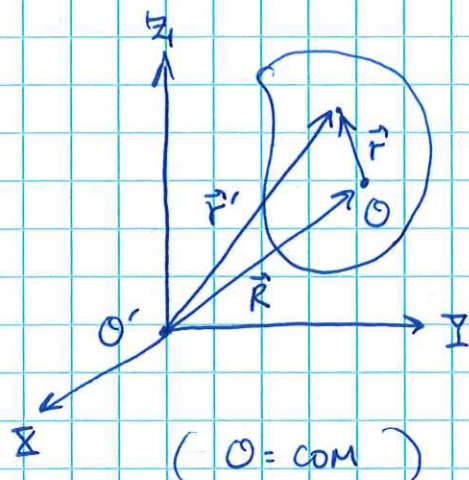
Note:  $\vec{F}$  only includes external forces. internal forces b/w particles of body cancel.



Second EOM:

04/03/24

(2)



$$\vec{L} = \sum \vec{r} \times \vec{p}, \quad \vec{p} = m\vec{v}$$

= ang. mom. about COM O.

$$\vec{L}' = \sum \vec{r}' \times \vec{p}', \quad \vec{p}' = m\vec{v}'$$

= ang. mom. about origin O' of fixed axis.

Recall that we may write:

$$\vec{L} = \vec{R} \times \vec{P} + \sum \vec{r} \times \vec{p}, \quad \vec{P} = M\vec{V}$$

$$= \vec{R} \times \vec{P} + \vec{L}'$$

$$\Rightarrow \dot{\vec{L}}' = \vec{R} \times \vec{F} + \dot{\vec{L}} \quad (*)$$

On the other hand:  $\dot{\vec{L}}' = \frac{d}{dt} \sum \vec{r}' \times \vec{p}' = \sum \underbrace{\dot{\vec{r}}' \times \vec{p}'}_{=0 \text{ since } \dot{\vec{r}}' \parallel \vec{p}'} + \sum \underbrace{\vec{r}' \times \dot{\vec{p}}'}_{\vec{r}' \times \vec{f}}$

$$= \frac{d}{dt} \sum (\vec{R} + \vec{r}) \times \vec{p} \quad \dot{\vec{r}}' \parallel \vec{p}$$

$$\Rightarrow \dot{\vec{L}}' = \sum \vec{r}' \times \vec{f} = \sum (\vec{R} + \vec{r}) \times \vec{f} = \vec{R} \times \vec{F} + \sum \vec{r} \times \vec{f} \quad (**)$$

Equating (\*) = (\*\*):

$$\dot{\vec{L}} = \sum \vec{r} \times \vec{f} \equiv \vec{K} \quad \text{"torque" about COM.}$$

$$\Rightarrow \boxed{\dot{\vec{L}} = \vec{K}}$$

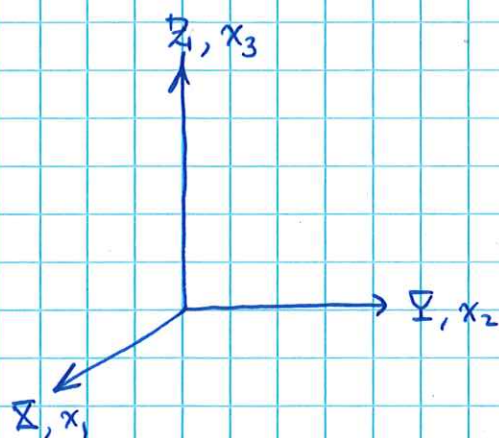
Note:  $\vec{K}$  only includes external forces. internal torques cancel.



Euler angles

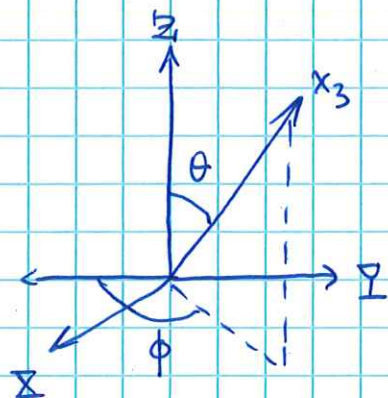
- Euler angles = convenient parametrization of rotn.'l coord.'s in terms of orientation of  $(x_1, x_2, x_3)$  axes w.r.t. fixed  $(\hat{x}, \hat{y}, \hat{z})$  axes.
- Orient  $x_1, x_2, x_3$  in steps, introducing intermediate frames

(0) In the zeroth step,  $x_1, x_2, x_3$  coincide w/  $\hat{x}, \hat{y}, \hat{z}$



~~Frame 0~~

Next we get the orientation of  $x_3$  axis:



\* this definition of  $\phi$  is different from standard azimuthal angle!

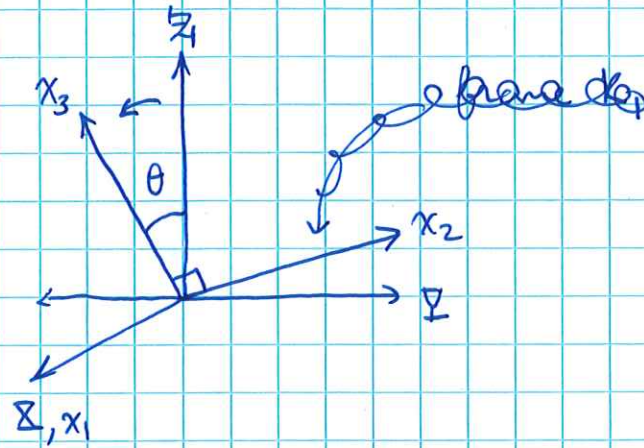
→ this can be achieved by composition of rotations:

$$\hat{x}_3 = R(\hat{z}, \phi) R(\hat{x}, \theta) \hat{z}$$

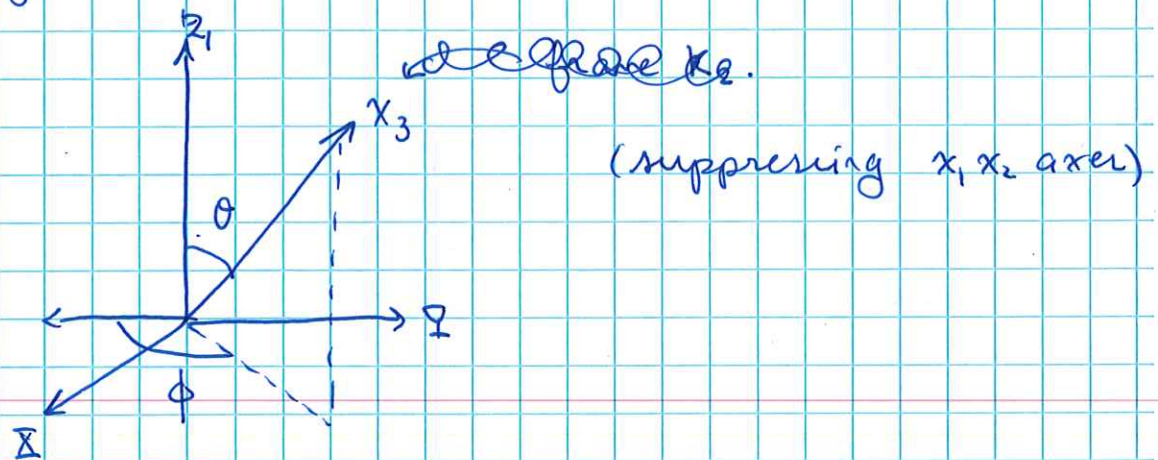
↑ axis-angle parametrization of rotn.'n



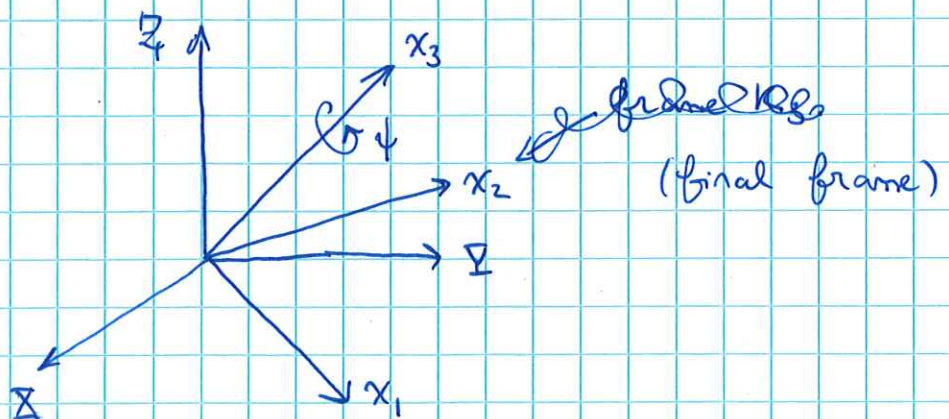
(1) First apply  $R(\hat{x}_1, \theta)$ :



(2) Next apply  $R(\hat{x}_3, \phi)$ :



(3) Once  $x_3$  is right, we have to properly orient  $x_1, x_2$ . This is achieved by appropriate rot.'n in  $x_1, x_2$ -plane; i.e., a rot.'n about  $x_3$  axis  $R(\hat{x}_3, \psi)$ :





$\Rightarrow x_1, x_2, x_3$  properly oriented by sequence of rotations:

$$R = R(\hat{x}_3, \psi) R(\hat{z}, \phi) R(\hat{x}, \theta).$$

$\rightarrow$  we write  $R$  on LHS b/c composition of rotations is itself a rot.<sup>n</sup>.

For a rigid body in motion the angles become fn.'s of  $t$ ; i.e.  $R = R(t)$ .

$(\theta, \phi, \psi) = \text{Euler angles}$

$$0 \leq \theta \leq \pi$$

$$0 \leq \phi < 2\pi$$

$$0 \leq \psi < 2\pi$$

A pt.  $\vec{r}$  in the rigid body is similarly specified  $\vec{r}(t) = R(t) \vec{r}_0$  where  $\vec{r}_0 = \text{location of that pt. in the reference orientation.}$

It is sometimes more convenient to express  $R$  in terms of rotations purely about fixed space axes. Using properties of rotation matrices it can be shown that:

$$R = R(\hat{z}, \phi) R(\hat{x}, \theta) R(\hat{z}, \psi).$$

┌ "ZXZ" parametrization. Note: there are (many) other parametrizations in the literature. └



Now we would like to express the Lagrangian  $L$  in terms of the generalized coord.'s  $q = (\theta \phi \psi)$  & generalized velocities  $\dot{q} = (\dot{\theta} \dot{\phi} \dot{\psi})$ .

Start w/ kinetic energy:

$$T = \frac{1}{2} (I_1 \Omega_1^2 + I_2 \Omega_2^2 + I_3 \Omega_3^2).$$

→ express comp.'s of ang. velocity  $(\Omega_1, \Omega_2, \Omega_3)$  in terms of Euler angles.

To do this we'll need two facts about rotations:

(1) for infinitesimal rot.'n  $R(\hat{n}, \epsilon)$  ( $\epsilon \ll 1$ ):

~~$$R(\hat{n}, \epsilon) \vec{r} = \vec{r} + \epsilon \hat{n} \times \vec{r}$$~~

$$R(\hat{n}, \epsilon) \vec{r} = \vec{r} + \epsilon \hat{n} \times \vec{r}$$

$$(2) R(\vec{a} \times \vec{b}) = (R\vec{a}) \times (R\vec{b}).$$

i.e., rot.'n of cross product of two vec.'s

= cross product of the rotated vec.'s.

[Note: Only true for "proper rotations"

$$\text{w/ } \det R = +1$$



• Now consider the motion of a pt.  $\vec{r}(t) = R(t) \vec{r}_0$  in the rigid body.

Suppose in time  $dt$  angle  $\psi$  changes  $\psi(t+dt) = \psi(t) + \dot{\psi} dt$ .

$$\begin{aligned} \Rightarrow \vec{r}(t+dt) &= R(t+dt) \vec{r}_0 = R(\hat{z}, \phi) R(\hat{x}, \theta) \underbrace{R(\hat{z}, \psi + \dot{\psi} dt)}_{\substack{\text{composition of two} \\ \text{rotations}}} \vec{r}_0 \\ &= R(\hat{z}, \psi) R(\hat{z}, \dot{\psi} dt) \vec{r}_0 \quad (\text{composition of two rotations}). \\ &= R(\hat{z}, \psi) (\vec{r}_0 + \dot{\psi} dt \hat{z} \times \vec{r}_0) \quad \downarrow \dot{\psi} dt = \text{small angle.} \end{aligned}$$

$$\begin{aligned} \Rightarrow \vec{r}(t+dt) &= R(\hat{z}, \phi) R(\hat{x}, \theta) R(\hat{z}, \psi) (\vec{r}_0 + \dot{\psi} dt \hat{z} \times \vec{r}_0) \quad \downarrow \text{Prop. (2)} \\ &= \vec{r}(t) + \dot{\psi} dt [ \cancel{R(\hat{z}, \phi) R(\hat{x}, \theta)} (R(\hat{z}) \times \vec{r}) ] \quad \downarrow R\hat{z} = \hat{x}_3 \\ &= \vec{r}(t) + \dot{\psi} dt \hat{x}_3 \times \vec{r}(t). \end{aligned}$$

$$\& \vec{r}(t+dt) = \vec{r}(t) + \vec{v} dt$$

$$\Rightarrow \vec{v} = \dot{\psi} \hat{x}_3 \times \vec{r}$$

And recall the ~~angle~~ angular vel.  $\vec{\Omega}$  was defined according to:

$$\vec{v} = \vec{\Omega} \times \vec{r}$$

$$\Rightarrow \vec{\Omega} = \dot{\psi} \hat{x}_3$$

• The same exercise can be repeated for  $\theta$  &  $\phi$ . The result is that the ang. vel. is the vector sum:

$$\boxed{\vec{\Omega} = \dot{\phi} \hat{z} + \dot{\theta} R(\hat{z}, \phi) \hat{x} + \dot{\psi} \hat{x}_3}$$



Now compute components. Notation  $\begin{cases} R_1 = R(\hat{z}, \phi) \\ R_2 = R(\hat{x}, \theta) \\ R_3 = R(\hat{z}, \psi) \end{cases}$

$$\Omega_1 = \hat{x}_1 \cdot \vec{\Omega} = \dot{\phi} \hat{x}_1 \cdot \hat{z} + \dot{\theta} \hat{x}_1 \cdot (R_1 \hat{x}) \quad (\hat{x}_1 \cdot \hat{x}_3 = 0)$$

$$\begin{aligned} &= \dot{\phi} (R_1 R_2 R_3 \hat{x}) \cdot \hat{z} + \dot{\theta} (R_1 R_2 R_3 \hat{x}) \cdot (R_1 \hat{x}) \quad \hookrightarrow (R\vec{a}) \cdot \vec{b} = \vec{a} \cdot (R^{-1}\vec{b}) \\ &= \dot{\phi} (R_2 R_3 \hat{x}) \cdot \hat{z} + \dot{\theta} (R_2 R_3 \hat{x}) \cdot \hat{x} \\ &= \dot{\phi} (R_3 \hat{x}) \cdot (R_2^{-1} \hat{z}) + \dot{\theta} (R_3 \hat{x}) \cdot (R_2^{-1} \hat{x}) \\ &= \dot{\phi} (\cos\psi \hat{x} + \sin\psi \hat{y}) \cdot (\cos\theta \hat{z}_1 + \sin\theta \hat{y}) \\ &\quad + \dot{\theta} (\cos\psi \hat{x} + \sin\psi \hat{y}) \cdot \hat{x} \\ &= \dot{\phi} \sin\theta \sin\psi + \dot{\theta} \cos\psi \end{aligned}$$

$$\begin{aligned} \Omega_2 = \hat{x}_2 \cdot \vec{\Omega} &= \dot{\phi} \hat{x}_2 \cdot \hat{z} + \dot{\theta} \hat{x}_2 \cdot (R_1 \hat{x}) \\ &= \dot{\phi} (R_2 R_3 \hat{y}) \cdot \hat{z} + \dot{\theta} (R_2 R_3 \hat{y}) \cdot \hat{x} \\ &= \dot{\phi} (\cos\psi \hat{y} - \sin\psi \hat{x}) \cdot (\cos\theta \hat{z}_1 + \sin\theta \hat{y}) \\ &\quad + \dot{\theta} (\cos\psi \hat{y} - \sin\psi \hat{x}) \cdot \hat{x} \\ &= \dot{\phi} \sin\theta \cos\psi - \dot{\theta} \sin\psi \end{aligned}$$

$$\begin{aligned} \Omega_3 = \hat{x}_3 \cdot \vec{\Omega} &= \dot{\phi} \hat{x}_3 \cdot \hat{z} + \dot{\theta} \hat{x}_3 \cdot (R_1 \hat{x}) + \dot{\psi} \\ &= \dot{\phi} (R_2 \hat{z}) \cdot \hat{z} + \dot{\theta} (R_2 \hat{z}) \cdot \hat{x} + \dot{\psi} \\ &= \dot{\phi} \cos\theta + \dot{\psi} \end{aligned}$$

 $\Rightarrow$ 

$$\begin{aligned} \Omega_1 &= \dot{\phi} \sin\theta \sin\psi + \dot{\theta} \cos\psi \\ \Omega_2 &= \dot{\phi} \sin\theta \cos\psi - \dot{\theta} \sin\psi \\ \Omega_3 &= \dot{\phi} \cos\theta + \dot{\psi} \end{aligned}$$

$$\begin{aligned} \rightarrow T &= T(\phi, \psi, \theta, \dot{\phi}, \dot{\psi}) \\ &= T(\mathbf{q}, \dot{\mathbf{q}}) \end{aligned}$$