

Control Systems

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CONTENTS

1. We are given with a feedback voltage amplifier shown in 1. We can neglect r_o and given with $R_1 + R_2 \gg R_D$.

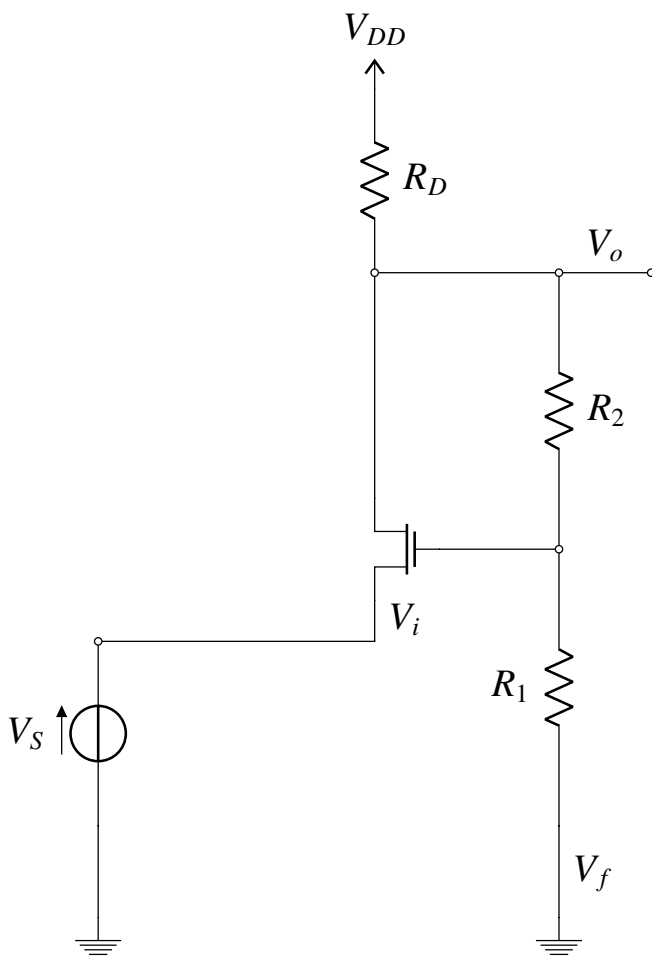


Fig. 1

2. part(a) : We have to find the expressions for G (open loop gain) , H (the feedback factor) and hence the amount of feedback.

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Solution: For this , first we have to draw the Small-Signal Model for the above Circuit, we ground all constant voltage sources and open all constant current sources. All Small-Signal parameters are obtained from DC-Analysis of the circuit. In Small-Signal Analysis a N-MOSFET is modelled as a Current Source with value of current equal to $g_m v_{gs}$ flowing from Drain to Source. Whereas a P-MOSFET is modelled as a Current Source with value of current equal to $g_m v_{sg}$ flowing from Source to Drain.

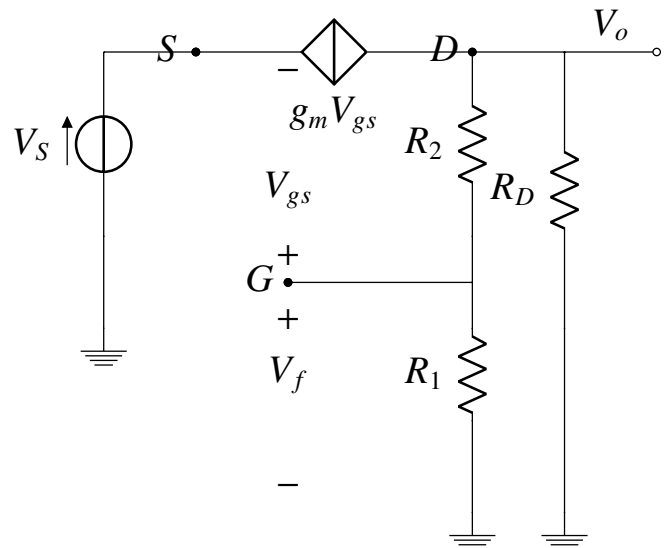


Fig. 2: Small Signal Model

3. For finding open loop gain (G) and the feedback factor (H).

Solution: For finding the open loop gain we have to remove R_2 and R_1 and the gate should be grounded.

4. Finding the open loop gain(G)

Solution:

$$V_o = -g_m V_{gs} * R_D \quad (4.1)$$

$$V_{gs} = -V_S \quad (4.2)$$

$$G = \frac{V_o}{V_S} \quad (4.3)$$

$$G = g_m R_D \quad (4.4)$$

5. Finding the Expression for the feedback factor H .

Solution:

$$H = \frac{V_f}{V_o} \quad (5.1)$$

$$V_f = \frac{R_1}{R_1 + R_2} V_o \quad (5.2)$$

$$H = \frac{R_1}{R_1 + R_2} \quad (5.3)$$

Amount of feedback is defined as : $1 + GH$

$$1 + GH = 1 + \frac{g_m R_D R_1}{R_1 + R_2} \quad (5.4)$$

6. Part(b) : We have to eliminate the feedback by removing R_1 and R_2 and connecting the gate of Q to a constant DC voltage (signal ground). We have to find the expression of the input resistance R_i and the output resistance R_o of the open loop amplifier.

Solution:

When the R_1 and R_2 and gate of Q is connected to a constant DC voltage (signal ground) it becomes a CG(Common gate amplifier) without feedback. We can directly see from the ?? the expression of input resistance R_i and output resistance R_o .

For finding input resistance , output constant voltages are grounded and hence the only current flowing is $g_m V_{gs}$. Hence R_i is :

$$I_{in} = -g_m V_{gs} \quad (6.1)$$

$$V_{in} = V_S \quad (6.2)$$

$$V_S = -V_{gs} \quad (6.3)$$

$$R_i = \frac{V_{in}}{I_{in}} \quad (6.4)$$

$$R_i = \frac{1}{g_m} \quad (6.5)$$

Similarly , for finding output R_o , V_{in} that is V_S will be zero and hence $g_m V_{gs}$ will be zero. Hence only R_D will be left which is the output resistance.

$$R_o = R_D \quad (6.6)$$

7. Part(c) : Using standard circuit analysis that is without using feedback approach we have to find the input resistance R_{if} and output resistance R_{of} and how they relate to R_i and R_o , which we find earlier.

Solution:

We will find them one by one.

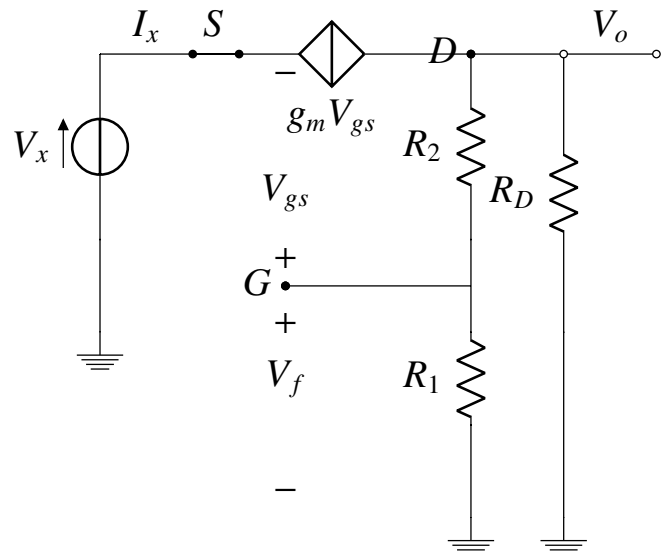


Fig. 7

8. finding expression for R_{if}

Solution:

To obtain R_{if} consider the figure 7 :

We gave test input voltage V_x and current I_x to find the input resistance from the input side to find R_i .

$$R_{if} = \frac{V_x}{I_x} \quad (8.1)$$

$$I_x = -g_m V_{gs} \quad (8.2)$$

$$V_o = I_x R_D \quad (8.3)$$

$$V_f = \frac{V_o R_1}{R_1 + R_2} = \frac{I_x R_D R_1}{R_1 + R_2} \quad (8.4)$$

$$V_x = -V_{gs} + V_f \quad (8.5)$$

$$V_x = \frac{I_x}{g_m} + \frac{I_x R_D R_1}{R_1 + R_2} \quad (8.6)$$

$$\frac{V_x}{I_x} = \frac{1}{g_m} + \frac{R_D R_1}{R_1 + R_2} \quad (8.7)$$

$$\text{rearranging :} \quad (8.8)$$

$$R_{if} = \frac{1}{g_m} \left(1 + \frac{g_m R_D R_1}{R_1 + R_2} \right) \quad (8.9)$$

$$R_{if} = R_i (1 + GH) \quad (8.10)$$

The input impedance is increased by a factor of $(1 + GH)$. R_{if} is related to R_i by :

$$R_{if} = R_i (1 + GH) \quad (8.11)$$

9. finding expression for R_{of}

Solution:

To obtain R_{of} consider the figure ?? :

We gave test input voltage V_x and current I_x from the output side to find the output resistance and made the input constant voltages as zero.

$$R_{of} = \frac{V_x}{I_x} \quad (9.1)$$

$$I_x = g_m V_{gs} \left(\frac{V_x}{R_1 + R_2} \right) + \left(\frac{V_x}{R_D} \right) \quad (9.2)$$

$$V_{gs} = \frac{R_1 V_x}{R_1 + R_2} \quad (9.3)$$

$$I_x = \frac{g_m R_1 V_x}{R_1 + R_2} + \frac{V_x}{R_1 + R_2} + \left(\frac{V_x}{R_D} \right) \quad (9.4)$$

$$I_x = V_x \left(\frac{g_m R_1 + 1}{R_1 + R_2} + \frac{1}{R_D} \right) \quad (9.5)$$

$$R_{of} = \frac{V_x}{I_x} \quad (9.6)$$

$$R_{of} = \frac{1}{\frac{g_m R_1 + 1}{R_1 + R_2} + \frac{1}{R_D}} \quad (9.7)$$

rearranging and multiply both the numerator and denominator by R_D

$$R_{of} = \frac{R_D}{\frac{g_m R_1 R_D}{R_1 + R_2} + 1 + \frac{R_D}{R_1 + R_2}} \quad (9.8)$$

$$\text{since } R_1 + R_2 \gg R_D \implies \frac{R_D}{R_1 + R_2} = 0$$

$$R_{of} = \frac{R_D}{1 + \frac{g_m R_1 R_D}{R_1 + R_2}} \quad (9.9)$$

$$R_{of} = \frac{R_o}{1 + GH} \quad (9.10)$$

The output impedance is decreased by a factor of $(1 + GH)$. R_{of} is related to R_o by :

$$R_{of} = \frac{R_o}{1 + GH} \quad (9.11)$$

The table showing all the expressions we find out in this problem :

G	$g_m R_D$
H	$\frac{R_1}{R_1 + R_2}$
R_i	$\frac{1}{g_m}$
R_o	R_D
R_{if}	$(\frac{1}{g_m})(1 + \frac{g_m R_D R_1}{R_1 + R_2})$
R_{of}	$\frac{R_D}{1 + \frac{g_m R_D R_1}{R_1 + R_2}}$

TABLE 9