

# Control Systems

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## CONTENTS

<b>1</b>	<b>Feedback Voltage Amplifier: Series-Shunt</b>	<b>1</b>
<b>2</b>	<b>Feedback Current Amplifier: Shunt-Series</b>	<b>2</b>
2.1	Ideal Case . . . . .	2
2.2	Practical Case . . . . .	4
<b>3</b>	<b>Feedback Current Amplifier: Example</b>	<b>4</b>
<b>4</b>	<b>Feedback Transconductance Amplifier: Series-Series</b>	<b>8</b>

*Abstract*—This manual is an introduction to control systems in feedback circuits. Links to sample Python codes are available in the text.

Download python codes using

svn co <https://github.com/gadepall/school/trunk/control/feedback/codes>

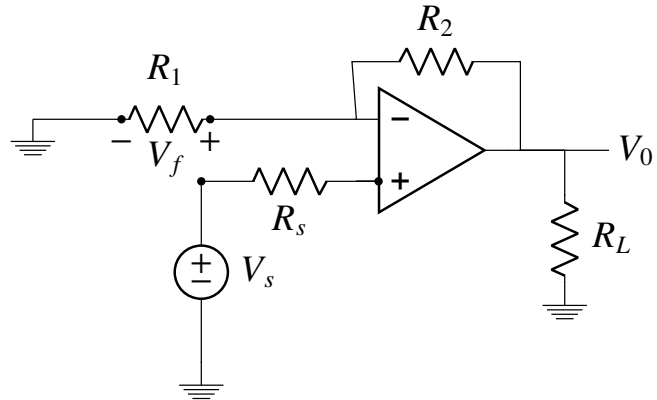


Fig. 1.1.1

Parameter	Value
input resistance	$\infty$
output resistance	<b>0</b>
Input voltage	$V_s$
Output Voltage	$V_o$
Feeding resistance	$R_1$
Feedback resistance	$R_2$
Source resistance	$R_s$
load resistance	$R_L$

TABLE 1.1

## 1 FEEDBACK VOLTAGE AMPLIFIER: SERIES-SHUNT

1.1. Fig. 1.1.1 shows a non-inverting op-amp configuration with parameters described in Table 1.1. Draw the equivalent control system.

**Solution:** See Fig. 1.1.2

1.2. Draw the small signal model for Fig. 1.1.1.

**Solution:** The equivalent circuit of the amplifier is in Fig. 1.2

1.3. Assuming that the operational amplifier has infinite input resistance and zero output resistance, find the *feedback factor*  $H$ .

**Solution:** From Fig. 1.2,

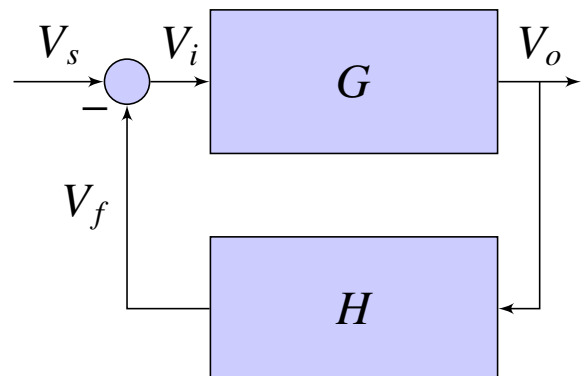


Fig. 1.1.2

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$$V_o = G V_i \quad (1.3.1)$$

$$V_i = V_s - V_f \quad (1.3.2)$$

$$V_f = \frac{R_1}{R_1 + R_2} V_o \quad (1.3.3)$$

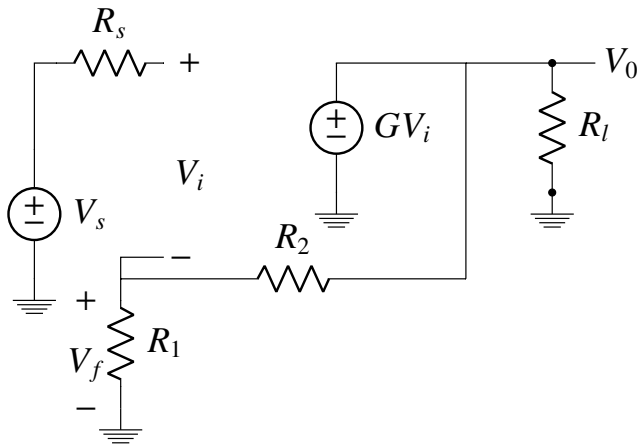


Fig. 1.2

assuming that the current through  $R_s$  is very small. Thus,

$$H = \frac{V_f}{V_o} = \frac{R_1}{R_1 + R_2} \quad (1.3.4)$$

- 1.4. Obtain the closed loop gain  $T$  and summarize your results through a Table.

**Solution:** Table 1.4 provides a summary.

$$T = \frac{V_o}{V_i} = \frac{G}{1 + GH} \quad (1.4.1)$$

$$= \frac{G(R_1 + R_2)}{(R_1 + R_2) + GR_1} \quad (1.4.2)$$

Parameters	Definition	For given circuit
Open loop gain	$G$	$G$
Feedback factor	$H$	$\frac{R_1}{R_1 + R_2}$
Loop gain	$GH$	$G \frac{R_1}{R_1 + R_2}$
Amount of feedback	$1 + GH$	$1 + \frac{GR_1}{R_1 + R_2}$
Closed loop gain	$\frac{G}{1 + GH}$	$\frac{G(R_1 + R_2)}{R_1 + R_2 + GR_1}$

TABLE 1.4

- 1.5. Find the condition under which closed loop gain  $T$  is almost entirely determined by the feedback network.

**Solution:** If

$$GH \gg 1, \quad (1.5.1)$$

$$T \approx \frac{1}{H} = 1 + \frac{R_2}{R_1} \quad (1.5.2)$$

- 1.6. If

$$G = 10^4 \quad (1.6.1)$$

$$T = 10, \quad (1.6.2)$$

find  $H$ .

**Solution:** From Table 1.4

$$T = \frac{G}{1 + GH} = 10 \quad (1.6.3)$$

$$\Rightarrow H = 0.0999 \quad (1.6.4)$$

- 1.7. *Gain Desensitivity:* If  $G$  decreases by 20%, what is the corresponding decrease in  $T$ ? Comment.

**Solution:** From Table 1.4, Given

$$T = \frac{G}{1 + GH} \quad (1.7.1)$$

$$\Rightarrow dT = \frac{dG}{(1 + GH)^2} \quad (1.7.2)$$

$$\Rightarrow \frac{dT}{T} = \frac{1}{1 + GH} \frac{dG}{G} \quad (1.7.3)$$

From the information available so far,

$$dG = 20\%, G = 10^4, H = 0.0999 \Rightarrow \frac{dT}{T} = 0.025\% \quad (1.7.4)$$

using the following code.

```
codes/ee18btech11005/ee18btech11005.py
```

Thus the closed loop gain is almost invariant to a relatively large (20%) variation in the open loop gain  $G$ . This is known as gain desensitivity.

## 2 FEEDBACK CURRENT AMPLIFIER: SHUNT-SERIES

### 2.1 Ideal Case

- 2.1.1. Draw the equivalent control system for the feedback current amplifier shown in 2.1.1.1

**Solution:** See Fig. 2.1.1.2.

- 2.1.1.1. For the feedback current amplifier shown in 2.1.1.1, draw the Small-Signal Model. Neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:** See Fig. 2.1.2.

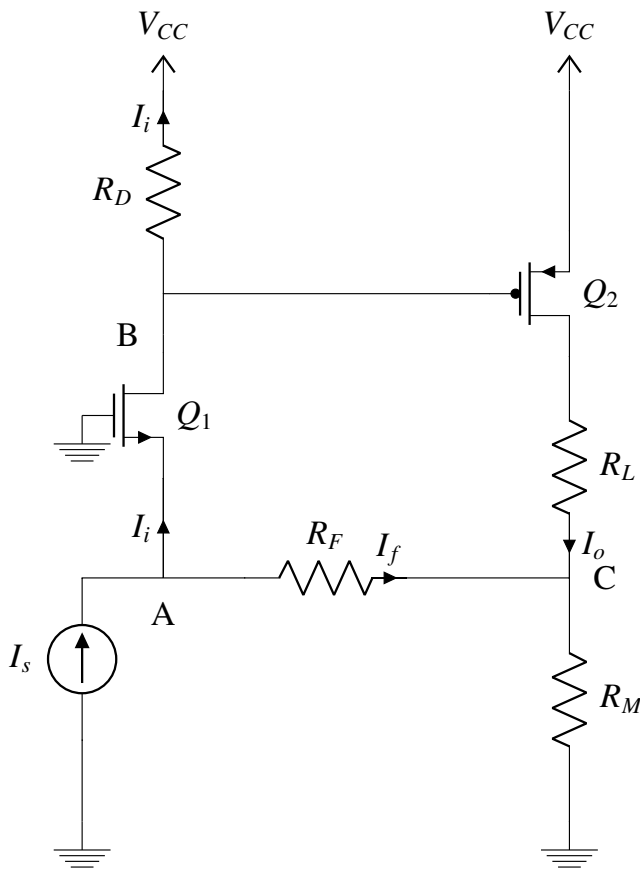


Fig. 2.1.1.1

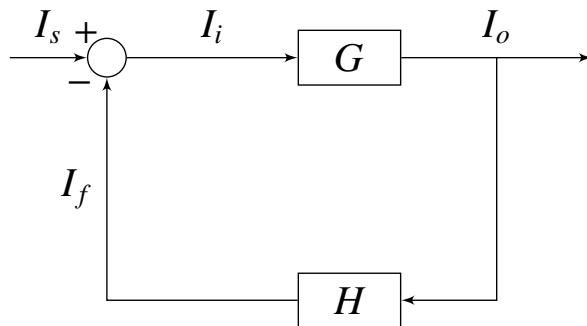


Fig. 2.1.1.2

While drawing a Small-Signal Model, we ground all constant voltage sources and open all constant current sources. All Small-Signal parameters are obtained from DC-Analysis of the circuit. Neglecting Early effect, in Small-Signal Analysis a N-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{gs}$  flowing from Drain to Source. Whereas a P-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{sg}$  flowing from Source to Drain.

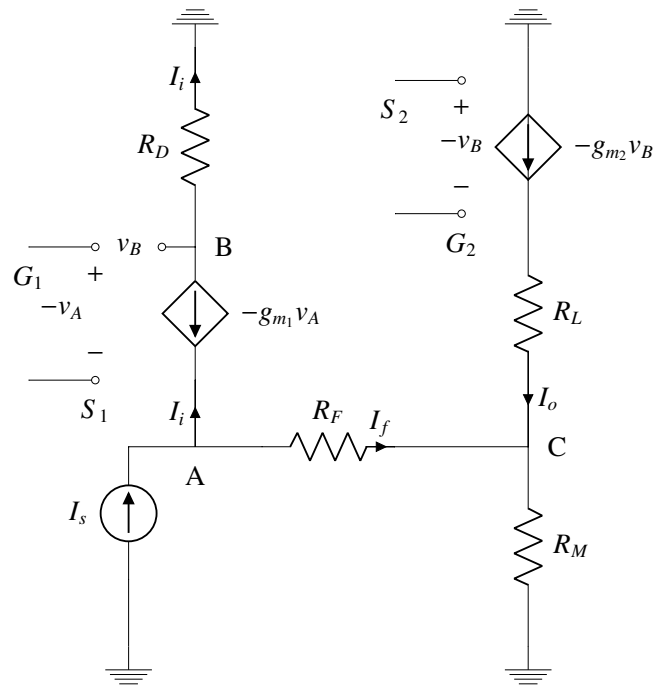


Fig. 2.1.2: Small Signal Model

2.1.3. Write all the node/loop equations using KCL/KVL.

**Solution:** From Figs. 2.1.1.1 and 2.1.2,

$$I_i = \frac{v_B}{R_D} \quad (2.1.3.1)$$

$$I_o = -g_{m2} v_B \quad (2.1.3.2)$$

$$v_C - v_A = -I_f R_F \quad (2.1.3.3)$$

$$v_C = (I_o + I_f) R_M \quad (2.1.3.4)$$

$$I_i = g_{m1} v_A \quad (2.1.3.5)$$

2.1.4. Find the Expression for the Open-Loop Gain  $G$ .

**Solution:** From (2.1.3.1) and (2.1.3.2),

$$G = \frac{I_o}{I_i} = -g_{m2} R_D \quad (2.1.4.1)$$

2.1.5. Find the Expression of the Feedback Factor  $H$ .

**Solution:**

$$H = \frac{I_f}{I_o}, \quad (2.1.5.1)$$

From (2.1.3.3) and (2.1.3.4),

$$(I_o + I_f) R_M - v_A = -I_f R_F \quad (2.1.5.2)$$

$$\Rightarrow (I_o + I_f) R_M + \frac{I_i}{g_{m1}} = -I_f R_F \quad (2.1.5.3)$$

from (2.1.3.5). Dividing by  $I_o$ ,

$$\Rightarrow (1 + H)R_M + \frac{1}{g_{m1}G} = -HR_F \quad (2.1.5.4)$$

upon substituting from (2.1.4.1) and (2.1.5.1). Simplifying further, we obtain

$$\Rightarrow H = \frac{\frac{1}{g_{m1}g_{m2}R_D} - R_M}{R_F + R_M} \quad (2.1.5.5)$$

$$\approx -\frac{R_M}{R_F + R_M} \quad (2.1.5.6)$$

for  $R_M \gg \frac{1}{g_{m1}g_{m2}R_D}$ .

2.1.6. Find the Expression for the Closed-Loop Gain  $T = \frac{I_o}{I_s}$ .

**Solution:** From (2.1.4.1) and (2.1.5.6),

$$T = \frac{I_o}{I_s} = \frac{G}{1 + GH} \quad (2.1.6.1)$$

$$= -\frac{g_{m2}R_D}{1 + g_{m2}R_D / \left(1 + \frac{R_F}{R_M}\right)} \quad (2.1.6.2)$$

## 2.2 Practical Case

2.2.1. Draw the Block Diagram and Circuit Diagram for  $H$ .

**Solution:** The Block Diagram is available in Fig. 2.2.1.1

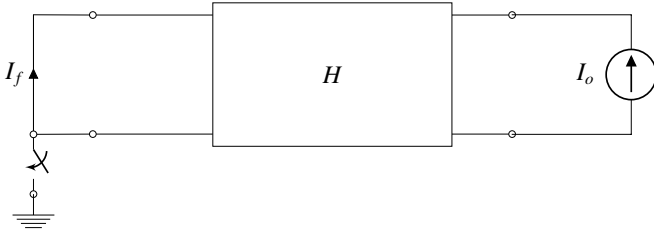


Fig. 2.2.1.1: Feedback Block Diagram

and the corresponding circuit diagram in Fig. 2.2.1.2

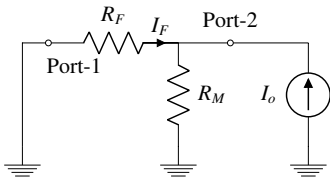


Fig. 2.2.1.2: Feedback Network

2.2.2. Find  $H$  from Fig. 2.2.1.2.

**Solution:** Using current division,

$$\frac{I_f}{I_o} = -\frac{R_M}{R_F + R_M} \quad (2.2.2.1)$$

$$\Rightarrow H = -\frac{R_M}{R_F + R_M} \quad (2.2.2.2)$$

2.2.3. Find  $R_{11}$  and  $R_{22}$  of Feedback Network where  $R_{11}$  is input resistance through Port-1 and  $R_{22}$  is Input Resistance through Port-2.

**Solution:**  $R_{11}$  is calculated by opening the current source at Port-2. Hence,

$$R_{11} = R_F + R_M \quad (2.2.3.1)$$

While calculating  $R_{22}$ , Port-1 should be shorted. Hence,

$$R_{22} = R_F || R_M \quad (2.2.3.2)$$

$$= \frac{R_F R_M}{R_F + R_M} \quad (2.2.3.3)$$

2.2.4. Draw the block diagram and circuit diagram for calculating  $G$ .

**Solution:** See Figs. 2.2.4.1 and 2.2.4.2

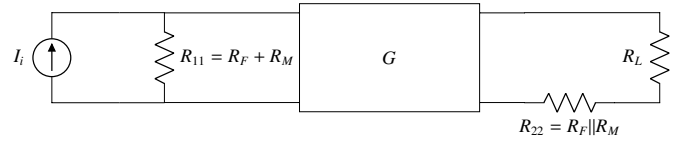


Fig. 2.2.4.1: Open-Loop Block Diagram

2.2.5. Find  $G$ .

**Solution:** The analysis is the same as Problem 2.1.4.

## 3 FEEDBACK CURRENT AMPLIFIER: EXAMPLE

3.1. Consider a Feedback Current Amplifier formed by cascading an Inverting Opamp  $\mu$  with a MOSFET (NMOS). The output current is the Drain Current of the NMOS. Assume that Opamp has an input resistance  $R_{id}$ , an Open Circuit Voltage Gain  $\mu$ , and an output resistance  $r_{o1}$

Identify the type of Feedback Circuit and draw its corresponding Block Diagram Representation

**Solution:** The Feedback Circuit is a Shunt-Series Feedback Current Amplifier.

See Figs. 3.1.3 and 3.1.2 for the block diagram representation.

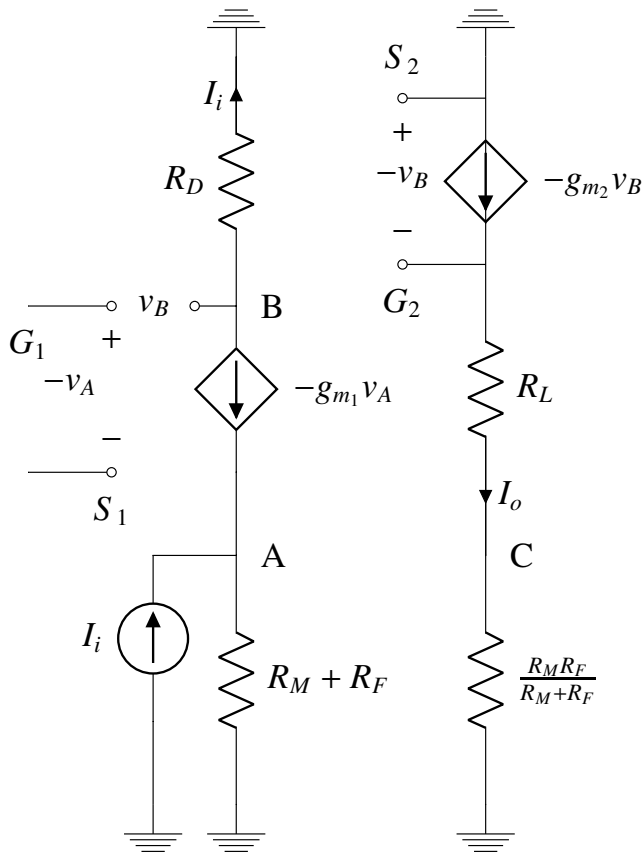


Fig. 2.2.4.2: Open-Loop Network

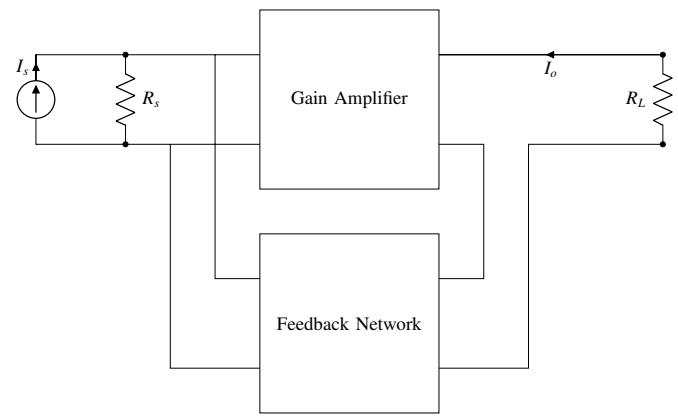


Fig. 3.1.2: Shunt Series Amplifier Block Diagram

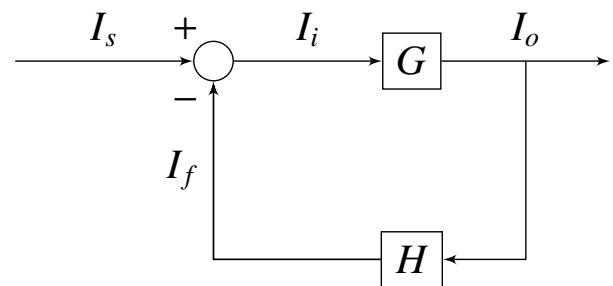


Fig. 3.1.3: Block Diagram

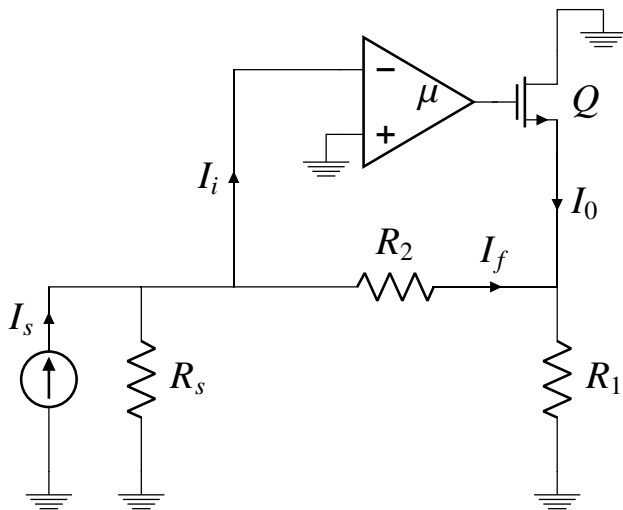


Fig. 3.1.1: Complete Circuit

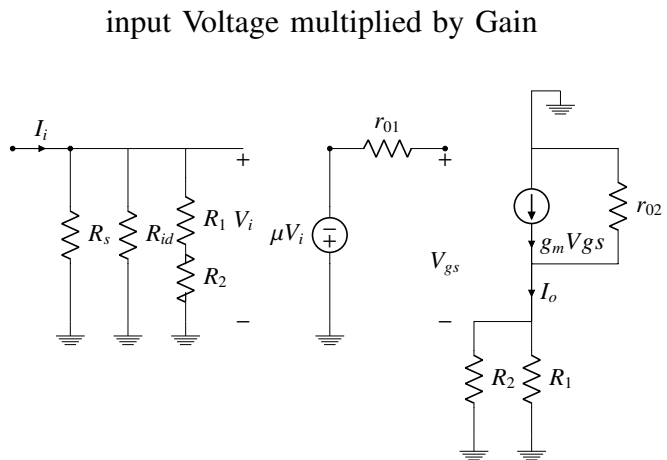


Fig. 3.2: Small Signal Model

3.2. Represent the given circuit using a Small Signal Equivalent Model.

**Solution:** See Fig. 3.2.

To draw Small Signal Equivalent model,

- Replace MOSFET with Current Source and Resistance in parallel with it.
- Replace Opamp with Voltage Source of the

3.3. Describe the resistances involved in the circuit

**Solution:** See Table 3.3

3.4. Draw the Block Diagram for  $H$ , with the corresponding Circuit.

**Solution:** See Figs. 3.4 and 3.4

3.5. Find the Feedback Gain  $H$ . **Solution:** In Fig. 3.4,  $I_f$  is the current in  $R_2$

$$\Rightarrow H = \frac{I_f}{I_o} = -\frac{R_1}{R_1 + R_2} \quad (3.5.1)$$

Resistance	Description
$R_i$	Total Input Resistance
$R_{out}$	Total Output Resistance
$R_{id}$	Input resistance of Opamp
$r_{o1}$	Output resistance of Opamp
$r_{o2}$	Output resistance of MOSFET
$R_i$	Input resistance of Open Loop
$R_o$	Output resistance of Open Loop
$R_{if}$	Input resistance of Feedback
$R_{of}$	Output resistance of Feedback
$R_s$	Resistance of Current Source

TABLE 3.3

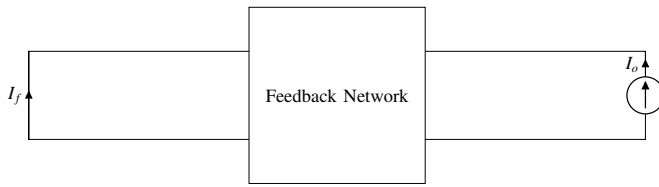


Fig. 3.4: Feedback Block

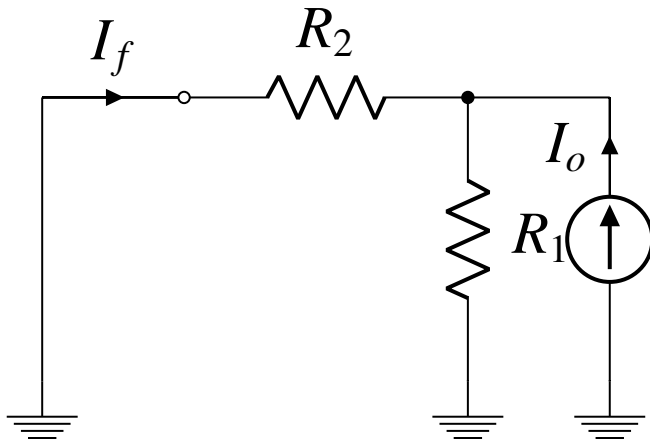


Fig. 3.4: Feedback Circuit

3.6. Find  $R_{11}$  and  $R_{22}$ .

**Solution:** From Fig. 3.4,

$$R_{11} = R_1 + R_2 \quad (3.6.1)$$

From Feedback Circuit,  $R_{22}$  is resistance obtained by shorting Feedback Network

$$R_{22} = R_1 \parallel R_2 \quad (3.6.2)$$

3.7. Draw the Block Diagram for  $G$ , with the corresponding Circuit.

**Solution:** See Figs. 3.7.1 and 3.7.2

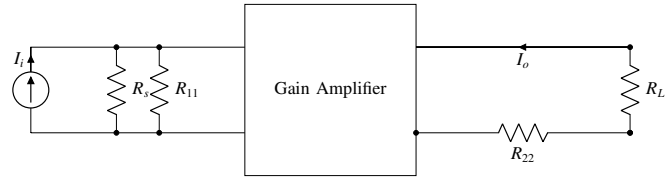


Fig. 3.7.1: Gain Block

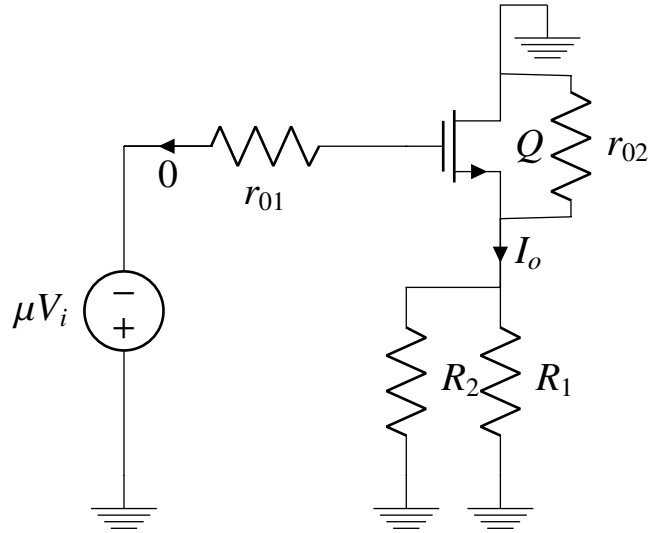


Fig. 3.7.2: Gain Circuit

3.8. Find the Gain  $G$ .

**Solution:** In Fig. 3.7.2,

$$R_i = R_s \parallel R_{id} \parallel (R_1 + R_2) \quad (3.8.1)$$

$$V_i = I_i R_i \quad (3.8.2)$$

$$I_o = -\mu V_i \frac{1}{1/g_m + (R_1 \parallel R_2 \parallel r_{o2})} \frac{r_{o2}}{r_{o2} + (R_1 \parallel R_2)} \quad (3.8.3)$$

$$G = \frac{I_o}{I_i} = -\mu \frac{R_i}{1/g_m + (R_1 \parallel R_2 \parallel r_{o2})} \frac{r_{o2}}{r_{o2} + (R_1 \parallel R_2)} \quad (3.8.4)$$

We use the approximation

$$1/g_m \ll (R_1 \parallel R_2 \parallel r_{o2}) \quad (3.8.5)$$

This is because the  $\frac{1}{g_m}$  is in order of few  $\Omega$ s but,  $R_1$ ,  $R_2$  and  $r_{o2}$  are in order of k $\Omega$ s

$$G = -\mu \frac{R_i}{R_1 \parallel R_2} \quad (3.8.6)$$

3.9. Calculate Loop Gain GH

**Solution:**

$$GH = \mu \frac{R_i}{\frac{1}{g_m} + (R_1 \parallel R_2 \parallel r_{o2})} \frac{r_{o2}}{r_{o2} + (R_1 \parallel R_2)} \frac{R_1}{R_1 + R_2} \quad (3.9.1)$$

$$\Rightarrow GH \simeq \mu \frac{R_i}{R_1 \parallel R_2} \frac{R_1}{R_1 + R_2} = \mu \frac{R_i}{R_2} \quad (3.9.2)$$

3.10. If loop gain is large, find approximate expression for closed loop gain  $T$

**Solution:** Given,

$$GH \gg 1 \quad (3.10.1)$$

$$T = \frac{G}{1 + GH} \simeq \frac{1}{H} \quad (3.10.2)$$

$$T \simeq \frac{1}{H} = - \left( 1 + \frac{R_2}{R_1} \right) \quad (3.10.3)$$

3.11. Give expressions for  $R_{if}$ ,  $R_{in}$

$$R_{if} = R_i / (1 + GH) \quad (3.11.1)$$

$$\Rightarrow \frac{1}{R_{if}} = \frac{1}{R_i} + \frac{\mu}{R_2} \quad (3.11.2)$$

$$\Rightarrow R_{if} = R_i \parallel \frac{R_2}{\mu} \quad (3.11.3)$$

Substituting the value of  $R_i$ ,

$$R_{if} = R_s \parallel R_{id} \parallel (R_1 + R_2) \parallel \frac{R_2}{\mu} \quad (3.11.4)$$

$$R_{if} = R_s \parallel R_{in} \quad (3.11.5)$$

$$\Rightarrow R_{in} = R_{id} \parallel (R_1 + R_2) \parallel \frac{R_2}{\mu} \quad (3.11.6)$$

$$R_{in} \simeq \frac{R_2}{\mu} \quad (3.11.7)$$

3.12. Give expressions for  $R_o$ ,  $R_{of}$ ,  $R_{out}$

**Solution:**

$$R_o = r_{o2} + (R_1 \parallel R_2) + (g_m r_{o2})(R_1 \parallel R_2) \quad (3.12.1)$$

$$\Rightarrow R_o \simeq g_m r_{o2} (R_1 \parallel R_2) \quad (3.12.2)$$

$$R_{of} = R_o (1 + GH) \simeq GHR_o \quad (3.12.3)$$

$$R_{of} \simeq \mu \left( \frac{R_i}{R_2} \right) (g_m r_{o2}) (R_1 \parallel R_2) \quad (3.12.4)$$

$$R_{out} = R_{of} = \mu \frac{R_i}{R_1 + R_2} (g_m r_{o2}) R_1 \quad (3.12.5)$$

3.13. Given the following values

Parameter	Value
$\mu$	1000
$R_s$	$\infty$
$R_{id}$	$\infty$
$r_{o1}$	$1k\Omega$
$R_1$	$10k\Omega$
$R_2$	$90k\Omega$
$g_m$	$5mA/V$
$r_{o2}$	$20k\Omega$

TABLE 3.13

Find numerical value of  $R_i$  and use it to find the value of  $G$

**Solution:** Using the given numerical values on the previously obtained equations, we obtain:

$$R_i = \infty \parallel \infty \parallel (10 + 90) = 100k\Omega \quad (3.13.1)$$

$$G = -1000 \frac{100}{10 \parallel 90} = -11.11 \times 10^3 \quad (3.13.2)$$

3.14. Check the validity of the approximation that we use to neglect  $1/g_m$

**Solution:**

$$1/g_m = 0.2k\Omega \ll (10 \parallel 90 \parallel 20)k\Omega = 6.2k\Omega \quad (3.14.1)$$

Hence, we can see that our approximation is valid

3.15. Find the value of feedback gain  $H$  and open loop gain  $GH$

**Solution:**

$$H = -\frac{R_1}{R_1 + R_2} = -\frac{10}{10 + 90} = -0.1 \quad (3.15.1)$$

$$GH = 1111 \gg 1 \quad (3.15.2)$$

3.16. Find the approximate value of closed loop gain  $T$

**Solution:**

$$T \simeq \frac{1}{H} = -\frac{1}{0.1} = -10 \quad (3.16.1)$$

3.17. Find the values of  $R_{in}$  and  $R_{out}$

**Solution:**

$$R_{in} = \frac{R_2}{\mu} = \frac{90k\Omega}{1000} = 90\Omega \quad (3.17.1)$$

$$R_o = g_m r_{o2} (R_1 \parallel R_2) = 5 \times 20(10 \parallel 90) = 900k\Omega \quad (3.17.2)$$

$$R_{out} = (1 + GH)R_o = 1112 \times 900 \simeq 1000M\Omega \quad (3.17.3)$$

Parameter	Value
$R_i$	$100k\Omega$
$1/g_m$	$200\Omega$
$G$	$-1.11 \times 10^4$
$H$	$-0.1$
$GH$	$1111$
$T$	$-10$
$R_{in}$	$90\Omega$
$R_o$	$900k\Omega$
$R_{out}$	$1000M\Omega$

TABLE 3.17

3.18. Verify the above calculations using a Python code.

**Solution:**

codes/ee18btech11021/ee18btech11021\_calc.py

#### 4 FEEDBACK TRANSCONDUCTANCE AMPLIFIER: SERIES-SERIES

4.1. Part of the circuit of the MC1553 Amplifier is shown in circuit1 in Fig. 4.1.1 with values of

various parameters given in Table 4.1. Draw the equivalent block diagrams.

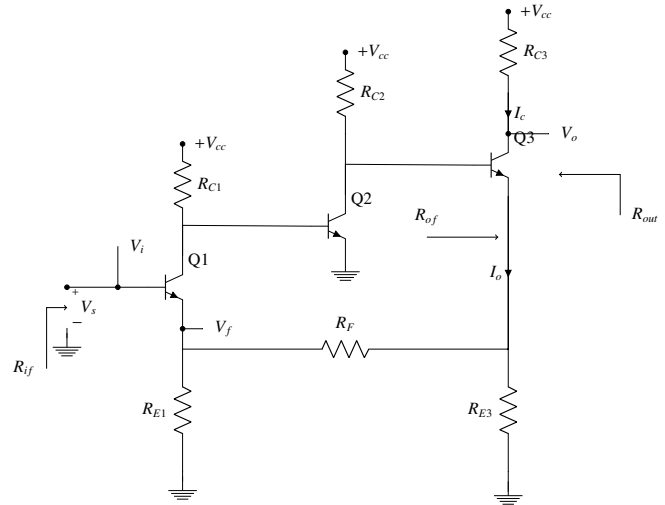


Fig. 4.1.1

Parameter	Value
$R_{C1}$	$9k\Omega$
$R_{E1}$	$100\Omega$
$R_{C2}$	$5k\Omega$
$R_F$	$640\Omega$
$R_{E2}$	$100\Omega$
$R_{C3}$	$600\Omega$
$h_{fe}$	<b>100</b>
$r_o$	$\infty\Omega$
$I_{C1}$	<b>0.6mA</b>
$I_{C2}$	<b>1mA</b>
$I_{C3}$	<b>4mA</b>
$r_{e1}$	$41.7\Omega$
$r_{\pi2}$	$2.5k\Omega$
$\alpha_1$	<b>0.99</b>
$g_{m2}$	<b>40mA/V</b>
$r_{e3}$	$6.25\Omega$
$r_{o3}$	$25k\Omega$
$r_{\pi3}$	$625\Omega$

TABLE 4.1: parameters

**Solution:** The block diagrams are available in Figs. 4.1.2 and 4.1.3.

4.2. Draw the block diagram and equivalent circuit for  $H$  for Fig. 4.1.3.



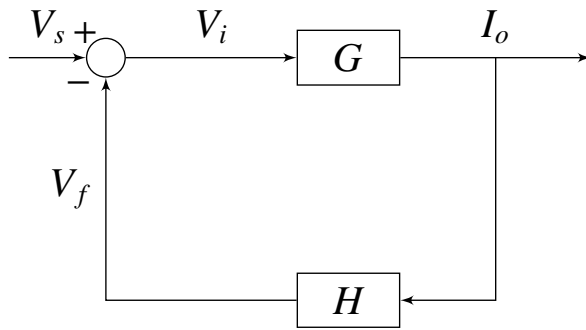


Fig. 4.1.2: block diagram

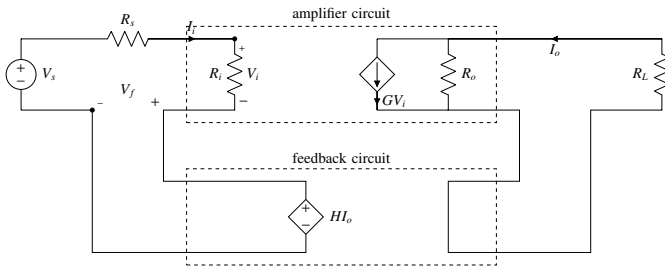


Fig. 4.1.3: Feedback Transconductance Amplifier

**Solution:** Fig. 4.2.1 gives the required block diagram

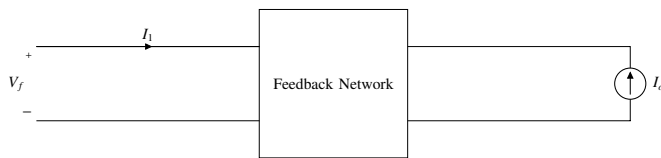


Fig. 4.2.1: Feedback circuit block diagram

$$H = \frac{V_f}{I_o} \Big|_{I_i=0} \quad (4.2.1)$$

and the equivalent  $H$  circuit is available in Fig. 4.2.2.

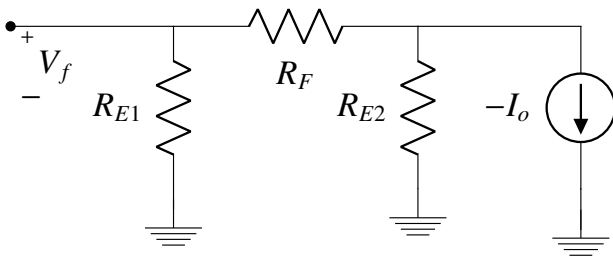


Fig. 4.2.2: H circuit

**Solution:** From Fig. 4.2.2,

$$H = \frac{V_f}{I_o} = \frac{R_{E1}R_{E2}}{R_{E2} + R_F + R_{E1}} \quad (4.3.1)$$

4.4. Find  $R_{11}$  and  $R_{22}$  from Figs. 4.4 and 4.2.2

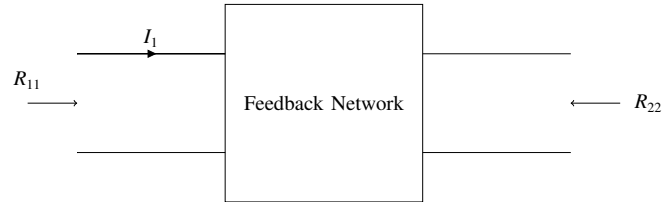


Fig. 4.4: feedback network

**Solution:**

$$R_{11} = R_{E1} || (R_F + R_{E2}) \quad (4.4.1)$$

$$R_{22} = R_{E2} || (R_F + R_{E1}) \quad (4.4.2)$$

4.5. Draw the block diagram and equivalent circuit for  $G$ .

**Solution:** The required block diagram is available in Fig. 4.5 and the equivalent circuit in

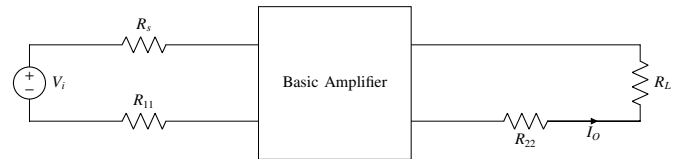


Fig. 4.5: Amplifier circuit block diagram

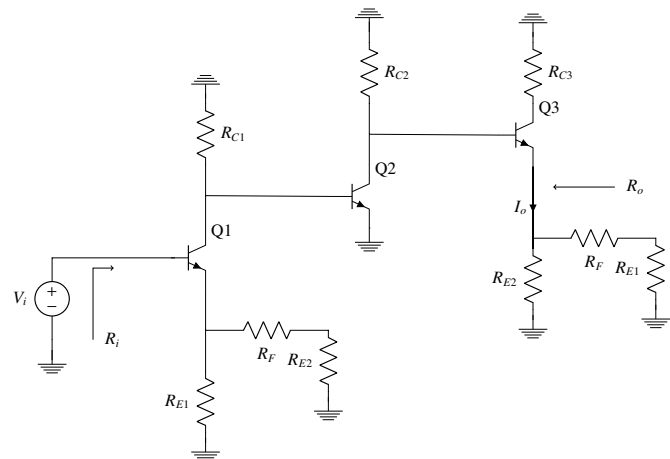


Fig. 4.5: G circuit

4.3. Find the feedback Factor  $H$

4.6. Find  $G$ 

**Solution:** To find  $G = \frac{I_0}{V_i}$  we determine the gain of first stage, this is written by inspection as-

$$\frac{V_{c1}}{V_i} = \frac{-\alpha(R_{c1} || r_{\pi 2})}{r_{e1} + (R_{E1} || (R_F + R_{E2}))} \quad (4.6.1)$$

Next, we determine the gain of the second stage, which can be written by inspection (noting that  $V_{b2} = V_{c1}$ ) as

$$\frac{V_{c2}}{V_{c1}} = -g_{m2} R_{c2} || (h_{fe} + 1) [r_{e3} + (R_{E2} || (R_F + R_{E1}))] \quad (4.6.2)$$

Finally, for the third stage we can write by inspection

$$\frac{I_0}{V_{c2}} = \frac{I_{e3}}{V_{b3}} = \frac{1}{r_{e3} + (R_{E2} || (R_F + R_{E1}))} \quad (4.6.3)$$

4.7. Find closed loop gain  $T$  and Voltage Gain  $V_o/V_s$  numerically.

**Solution:**

$$T = \frac{I_0}{V_s} = \frac{G}{1 + GH} = \frac{20.7}{1 + 20.7 \times 11.9} = 83.7 \text{ mA/V} \quad (4.7.1)$$

## 4.8. Now assume Loop gain is large and find approximate expression for closed loop gain

$$T = \frac{I_0}{V_s}$$

**Solution:** When  $GH \gg 1$ ,

$$T \approx \frac{I_0}{V_s} \approx \frac{1}{H} \quad (4.8.1)$$

$$= \frac{1}{11.9} = 84 \text{ mA/V} \quad (4.8.2)$$

$$\frac{I_c}{V_s} \approx \frac{I_0}{V_s} = 84 \text{ mA/V} \quad (4.8.3)$$

which we note is very close to the approximate value found in (4.7.1)

## 4.9. Tabulate all your results.

**Solution:** See Table 4.9.

## 4.10. Write a code for doing calculations and verify the values obtained in 4.9

**Solution:** The following code does all the calculations of above equations to give parameters in 4.9

```
codes/ee18btech11007/circuit_calc.py
```

Parameter	Value
<b>G</b>	<b>20.7A/V</b>
<b>H</b>	11.9Ω
<b>T</b>	<b>83.7mA/V</b>
$V_o/V_s$	<b>-50.2V/V</b>
$R_{in}$	3.38MΩ
$R_{out}$	2.19MΩ
$R_{of}$	35.6kΩ

TABLE 4.9: calculated parameters