Control Systems

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2.1 Introduction

Abstract—This manual is an introduction to control systems based on GATE problems.Links to sample Python codes are available in the text.

Download python codes using

svn co https://github.com/gadepall/school/trunk/control/codes



1.1 Introduction

1.1.1. Fig. 1.1.1.1 shows a non-inverting op-amp configuration with parameters described in Table 1.1.1. Draw the equivalent control system.

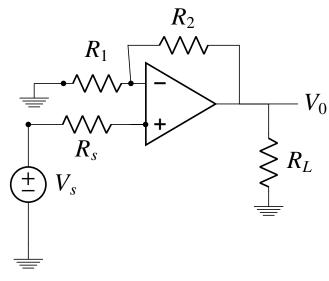
Parameter	Value
input resistance	∞
output resistance	0
Input voltage	V_s
Output Voltage	V_o
Feedback resistance	R_2
load resistance	R_L

TABLE 1.1.1

Solution: See Fig. 1.1.1.2

1.1.2. Draw the small signal model for Fig. 1.1.1.1. **Solution:** The equivalent circuit of the amplifier is in Fig. 1.1.2

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Fig. 1.1.1.1

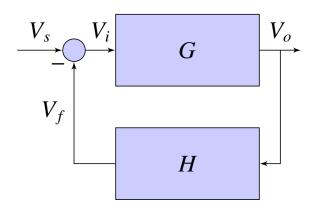


Fig. 1.1.1.2

1.1.3. Assuming that the operational amplifier has infinite input resistance and zero output resistance, find the *feedback factor H*. **Solution:** Let the gain of the operational amplifier be G. From the equivalent circuit, Applying Ohms law,

$$V_0 = G(V_i) (1.1.3.1)$$

and,
$$V_i = V_+ - V_-$$
 (1.1.3.2)

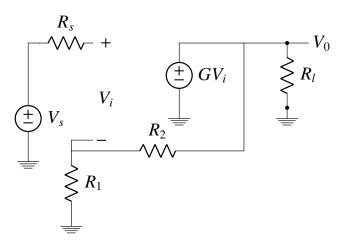


Fig. 1.1.2

Now, Applying voltage dividing rule

$$V_{-} = \left[\frac{R_1}{R_1 + R_2}\right] V_0 \tag{1.1.3.3}$$

Substituting in equ.1.1.3.1

$$V_0 = G(V_+ - \left[\frac{R_1}{R_1 + R_2}\right] V_0) \quad (1.1.3.4)$$

$$\implies V_0 = GV_+ - G\left[\frac{R_1}{R_1 + R_2}\right]V_0 \quad (1.1.3.5)$$

$$G(V_{+}) = V_{0} + G\left[\frac{R_{1}}{R_{1} + R_{2}}\right]V_{0}$$
 (1.1.3.6)

But,

$$V_s = V_+ (1.1.3.7)$$

because, no current flows through resistor.

$$V_0 = G \left[\frac{1}{1 + \frac{GR_1}{R_1 + R_2}} \right] V_s \qquad (1.1.3.8)$$

Gain =
$$\frac{V_0}{V_s} = \left[\frac{G}{1 + \frac{GR_1}{R_1 + R_2}} \right]$$
 (1.1.3.9)

For a negative feedback system,

$$\frac{V_0}{V_i} = \frac{G}{1 + GH} \quad (1.1.3.10)$$

where.,
$$H = \frac{R_1}{R_1 + R_2}$$
 (1.1.3.11)

The equation.1.1.3.1 looks exactly similar to the Gain of a negative feedback system with

- Open loop gain = G
- Loop gain = P
- Amount of feedback = F

- Feedback factor = f
- closed loop gain = T

Parame- ters	Definition	For given circuit
Open loop gain	G	G
Feedback factor	Н	$\frac{R_1}{R_1 + R_2}$
Loop gain	GH	$G^{rac{R_1}{R_1+R_2}}$
Amount of feedback	1+GH	$1 + \frac{GR_1}{R_1 + R_2}$
Closed loop gain	<u>G</u> 1+ <i>GH</i>	$\frac{G(R_1 + R_2)}{R_1 + R_2 + GR_1}$

TABLE 1.1.3

Therefore, So, the feedback factor ...

$$f = H = \frac{R_1}{R_1 + R_2} \tag{1.1.3.12}$$

1.1.4. Find the condition under which closed loop gain T is almost entirely determined by the feedback network. **Solution:** For T to entirely dependent on feedback network, it should be independent on G(open loop gain) T is given by...,

$$T = \frac{G}{1 + \frac{GR_1}{R_1 + R_2}} \tag{1.1.4.1}$$

(1.1.4.2)

For T to be independent on G.,

$$GH >> 1$$
 (1.1.4.3)

$$G\frac{R_1}{R_1 + R_2} >> 1 \tag{1.1.4.4}$$

$$G >> 1 + \frac{R_2}{R_1} \tag{1.1.4.5}$$

Under such condition...

$$T = \frac{1}{H} \tag{1.1.4.6}$$

$$T = \frac{R_1 + R_2}{R_1} \tag{1.1.4.7}$$

$$T = 1 + \frac{R_2}{R_1} \tag{1.1.4.8}$$

so, the necessary condition for T depend only

on feedback network is

$$G >> T$$
 (1.1.4.9)

1.1.5. If the open loop voltage gain

$$G = 10^4 \tag{1.1.5.1}$$

Find the ratio of R2 and R1 to obtain a closed loop gain of 10. **Solution:** The closed loop gain gain T is given by

$$T = \frac{G}{1 + GH} = \frac{G}{1 + \frac{GR_1}{R_1 + R_2}} = 10$$

(1.1.5.2)

where...,
$$G = 10^4$$
 (1.1.5.3)

$$10 = \frac{10^4}{1 + \frac{10^4}{1 + \frac{R_2}{R_1}}} \tag{1.1.5.4}$$

$$\implies 1 + \frac{R_2}{R_1} = \frac{10^4}{\frac{10^4}{10} - 1} \tag{1.1.5.5}$$

$$1 + \frac{R_2}{R_1} = 10.010 \tag{1.1.5.6}$$

$$\frac{R_2}{R_1} = 9.010\tag{1.1.5.7}$$

1.1.6. What is the amount of feedback in decibels? **Solution:** The value of F in decibals is given by

$$F(dB) = 20\log(F) \qquad (1.1.6.1) \quad 2.1 \text{ Introduction}$$

where...
$$F = 1 + GH$$
 (1.1.6.2)

$$F = \frac{G}{T} \tag{1.1.6.3}$$

where..,
$$G = 10^4$$
 (1.1.6.4) 2.1.2

$$T = 10 (1.1.6.5)$$

$$F(dB) = 20\log(\frac{10^4}{10}) = 20\log(1000)$$
(1.1.6.6)

$$F(dB) = 60dB (1.1.6.7)$$

1.1.7. If G decreases by 20%, what is the corresponding decrease in T? **Solution:** Given

$$G = 10^4 \tag{1.1.7.1}$$

If G decrease by 20% then, the value of G is...

$$G = (1 - 0.2)10^4 \tag{1.1.7.2}$$

$$= 8000 ag{1.1.7.3}$$

For this value of G and,

$$\frac{R_2}{R_1} = 9.010 \tag{1.1.7.4}$$

The value of T can be solved as follows,

$$T = \frac{G}{1 + \frac{G}{1 + \frac{R_2}{R_1}}} \tag{1.1.7.5}$$

$$T = \frac{8000}{1 + \frac{8000}{1 + 0.9010}} \tag{1.1.7.6}$$

$$T = 9.99749 \tag{1.1.7.7}$$

The percentage change in T is..,

$$fractional change = \frac{10 - 9.99749}{10} \quad (1.1.7.8)$$

$$= 2.51x10^{-4} \qquad (1.1.7.9)$$

$$%changeinT = 0.00251$$
 (1.1.7.10)

Therefore T decreases by 0.0025% when G decreases by 20%

1.1.8. Write a python code that can compute closed loop gain,loop gain,amount of feedback given all input parameters. **Solution:** Code to compute different gains.,

codes/ee18btech11005/ee18btech11005.py

2 FEEDBACK CURRENT AMPLIFIER: SHUNT-SERIES

2 TEEDBACK CORRENT AMPLITIES. SHOT

(1.1.6.2) 2.1.1. Draw the equivalent control system for the feedback current amplifier shown in 2.1.1.4 **Solution:** See Fig. 2.1.1.5.

(1.1.6.4) 2.1.2. For the feedback current amplifier shown in (1.1.6.5) 2.1.1.4, draw the Small-Signal Model. Neglect the Early effect in Q_1 and Q_2 .

Solution: See Fig. 2.1.2.

While drawing a Small-Signal Model, we ground all constant voltage sources and open all constant current sources. All Small-Signal paramters are obtained from DC-Analysis of the circuit. Neglecting Early effect, in Small-Signal Analysis a N-MOSFET is modelled as a Current Source with value of current equal to $g_m v_{gs}$ flowing from Drain to Source. Whereas a P-MOSFET is modelled as a Current Source with value of current equal to $g_m v_{sg}$ flowing from Source to Drain.

(1.1.7.3) 2.1.3. Describe how the given circuit is a Negetive Feedback Current Amplifier.

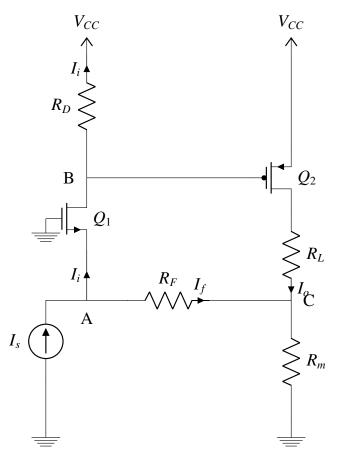
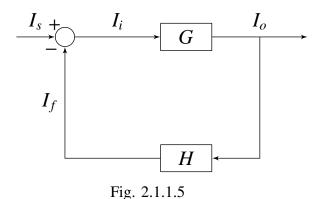


Fig. 2.1.1.4



Solution: For the feedback to be negative, I_f must have the same polarity as I_s . To ascertain that this is the case, we assume an increase in I_s and follow the change around the loop: An increase in I_s causes I_i to increase and the drain voltage of Q_1 will increase. Since this voltage is applied to the gate of the p-channel device Q_2 , its increase will cause I_o , the drain current of Q_2 , to decrease. Thus, the voltage across R_M will decrease, which will cause I_f to increase. This is the same polarity assumed

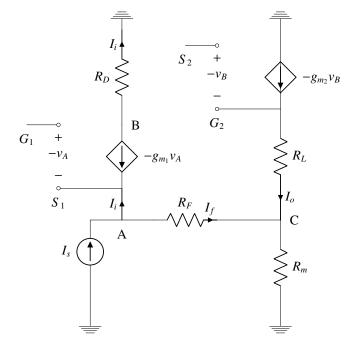


Fig. 2.1.2: Small Signal Model

for the initial change in I_s , verifying that the feedback is indeed negative.

2.1.4. Find the Expression for the Open-Loop Gain $G = \frac{I_0}{I_i}$, from the Small-Signal Model. in Fig. 2.1.2.

Solution: In Small-Signal Model,

$$v_B = I_i R_D (2.1.4.1)$$

$$v_{gs_2} = v_B = I_i R_D (2.1.4.2)$$

In Small-Signal Analysis, P-MOSFET is modelled as a current source where current flows from Source to Drain. So, the value of current flowing from Source to Drain in P-MOSFET is,

$$I_o = -g_{m_2} v_{gs_2} = -g_{m_2} I_i R_D (2.1.4.3)$$

So, the Open-Circuit Gain is

$$G = \frac{I_o}{I_i} = -g_{m_2} R_D (2.1.4.4)$$

in I_s and follow the change around the loop: 2.1.5. Find the Expression of the Feedback Factor An increase in I_s causes I_i to increase and the $H = \frac{I_f}{L}$, from Small-Signal Model.

Solution: I_o is fed to a current divider formed by R_M and R_F . R_F is a Large Resistance compared to Input resistance of Amplifier and so most of the current flows through it leaving a small current as input to Amplifier. Hence the voltage at point 'A' is very small and is

considered, $v_A \simeq 0$. So R_F and R_M are parallel and Voltage Drop across them is same.

$$(I_o + I_f)R_M \simeq -I_f R_F$$
 (2.1.5.1)

$$\frac{I_f}{I_o} \simeq -\frac{R_M}{R_F + R_M}$$
 (2.1.5.2)

So, the Feedback Factor,

$$H \equiv \frac{I_f}{I_o} \simeq -\frac{R_M}{R_F + R_M} \tag{2.1.5.3}$$

2.1.6. Find the Expression for the Closed-Loop Gain $T = \frac{I_o}{I_s}$. **Solution:** From (2.1.4.4) and (2.1.5.3),

$$T = \frac{I_o}{I_s} = \frac{G}{1 + GH} \tag{2.1.6.1}$$

$$= -\frac{g_{m_2}R_D}{1 + g_{m_2}R_D/\left(1 + \frac{R_F}{R_M}\right)}$$
 (2.1.6.2)

$$\implies T = -\frac{g_{m_2} R_D}{1 + g_{m_2} R_D / \left(1 + \frac{R_F}{R_M}\right)} \quad (2.1.6.3)$$