#### 1

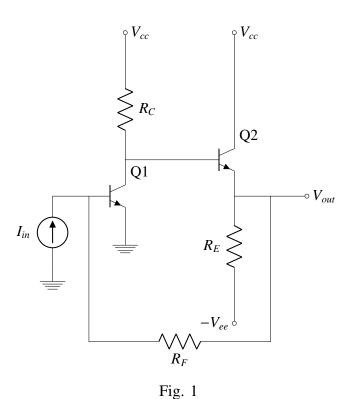
# Trans-Resistance Amplifier

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### **CONTENTS**

For the feedback transresistance amplifier in Fig. , use small-signal analysis to find the open-loop gain G, the feedback H, and the closed loop gain  $G_m$ . Neglect  $r_o$  of each of the transistors and assume  $R_C << \beta_2 R_E$  and  $R_E << R_F$ , and that the feedback causes the signal voltage at the input node to be nearly zero. Evaluate  $/fracV_oI_s$  for the following component values:  $\beta_1 = \beta_2 = 100$ ,  $R_C = R_E = 10k\Omega$  and  $R_F = 100k\Omega$ .

1. Draw the small-signal equivalent of the circuit in Fig.??.



#### **Solution:**

The equivalent circuit is Fig.??

2. Find the expression for the open loop Gain(G) of the system.

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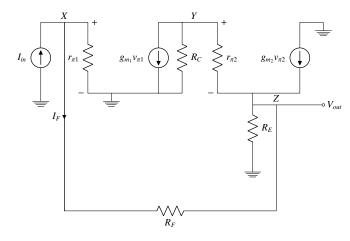


Fig. 1

### **Solution:**

The given system is a cascaded system of  $Q_1$  and  $Q_2$ . The signal flow graph is illustrated in Fig. ??

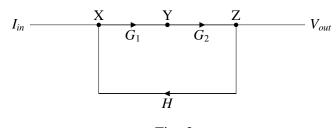


Fig. 2

So, if the gain of  $Q_1$  and  $Q_2$  are  $G_1$  and  $G_2$  respectively, the open-loop gain (G) is given by:

$$G = G_1 G_2 \tag{2.1}$$

 $Q_1$  is in CE(Common-emitter) stage. The input signal is  $I_{in}$ . From fig. ??,

$$I_X = I_{in} \tag{2.2}$$

$$\beta = \frac{I_c}{I_b} \tag{2.3}$$

Applying Kirchoff's Law in the loop connect-

ing Y to ground,

$$\implies V_Y = \beta I_{in} R_C$$
 (2.4)

$$G_1 = \frac{V_{out}}{I_{in}} = \frac{V_Y}{I_X}$$
 (2.5)

$$= \beta R_c \tag{2.6}$$

 $Q_2$  is in emitter follower topology.

$$V_{\pi 2} = V_Y - V_Z \tag{2.7}$$

Applying Kirchoff's Law,

$$\frac{V_Y - V_Z}{r_\pi} + g_{m2} (V_Y - V_Z) = \frac{V_Z}{R_E}$$
 (2.8)

$$\implies \frac{V_Z}{V_Y} = \frac{R_E}{\frac{1}{g_{m2}} + R_E} \tag{2.9}$$

$$\implies G_2 = \frac{R_E}{\frac{1}{g_{m2}} + R_E} \tag{2.10}$$

From (??), the open loop gain (G):

$$G = (\beta_1 R_c) \left( \frac{R_E}{\frac{1}{g_{m2}} + R_E} \right) \tag{2.11}$$

3. Find the feedback factor(H) of the given circuit.

### **Solution:**

From Fig.??, the feedback circuit consists of only a resistor  $R_F$ :

$$\therefore H = \frac{I_F}{V_{out}} = \frac{1}{R_F} \tag{3.1}$$

4. Find the closed loop gain of the system.

### **Solution:**

The closed loop gain of a system is given by:

$$G_L = \frac{G}{1 + GH} \tag{4.1}$$

From (??) and (??). The closed loop gain of the circuit is given by:

$$G_{L} = \frac{(\beta_{1}R_{c})\left(\frac{R_{E}}{\frac{1}{g_{m2}} + R_{E}}\right)}{1 + \frac{(\beta_{1}R_{c})\left(\frac{R_{E}}{\frac{1}{g_{m2}} + R_{E}}\right)}{R_{F}}}$$
(4.2)

$$= \frac{R_F R_C R_E \beta}{\beta R_C R_E + R_F \left(\frac{1}{g_{m2}} + R_E\right)} \tag{4.3}$$

5. Find G,H and  $G_L$  for the given problem. Parameters are summarised in table ??.

Parameters	Value
$V_{cc}$	5 <i>V</i>
$oldsymbol{eta}_1$	100
$eta_2$	100
$R_C$	10 <i>K</i> Ω
$R_E$	10ΚΩ
$R_F$	100ΚΩ

TABLE 5

#### **Solution:**

To calculate the bias values of Q1, Q2. Remove the input and output, the resultant circuit is shown in fig.??

Applying KVL to the circuit, we get:

$$0.7 + I_{b1}R_F + (I_{b1} - (\beta + 1)I_{b2})R_E = -V_{ee}$$
(5.1)

$$0.7 + I_{b1}R_F + 0.7 + (\beta I_{b1} + I_{b2})R_C = V_{cc} \quad (5.2)$$

Solving the above equations, we get:

$$I_{b1} = \frac{\frac{V_{cc} - 1.4}{R_C} - \frac{V_{ee} + 0.7}{R_E(\beta + 1)}}{\frac{R_F + \beta R_C}{R_C} + \frac{R_E + R_F}{R_E(\beta + 1)}}$$
(5.3)

$$= 3.22 * 10^{-6} \tag{5.4}$$

$$I_{b2} = \frac{\frac{V_{cc} - 1.4}{\beta R_C + R_F} + \frac{V_{ee} + 0.7}{R_E + R_F}}{\frac{R_C}{R_E + \beta R_C} + \frac{R_E(\beta + 1)}{R_E + R_E}}$$
(5.5)

we know,

$$g_m = \frac{I_c}{V_T} \tag{5.6}$$

where,  $V_T = 26$ mV, and

$$r_{\pi} = \frac{\beta}{g_m} \tag{5.7}$$

$$\therefore g_{m1} = \frac{\beta I_{b1}}{V_T} \tag{5.8}$$

$$= 0.0123$$
 (5.9)

$$r_{\pi 1} = \frac{\beta}{g_{m1}} \tag{5.10}$$

$$= 8130\Omega \tag{5.11}$$