## Control Systems

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## **CONTENTS**

1	Feedbac	k Voltage	<b>Amplifier:</b>	Series-	
Shunt			_		1
	1.1	Introduction	1		1
2	Feedback Current Amplifier: Shunt-				
Series					2
	2.1	Introduction	1		2

Abstract—This manual is an introduction to control systems based on GATE problems.Links to sample Python codes are available in the text.

Download python codes using

svn co https://github.com/gadepall/school/trunk/control/codes

- 1 FEEDBACK VOLTAGE AMPLIFIER: SERIES-SHUNT
- 1.1 Introduction
- 1.1.1. Fig. 1.1.1.1 shows a non-inverting op-amp configuration with parameters described in Table 1.1.1. Draw the equivalent control system.

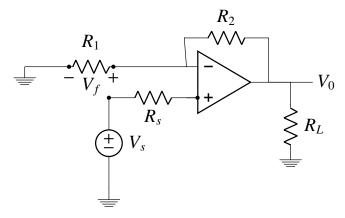


Fig. 1.1.1.1

**Solution:** See Fig. 1.1.1.2

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Parameter	Value
input resistance	$\infty$
output resistance	0
Input voltage	$V_s$
Output Voltage	$V_o$
Feeding resistance	$R_1$
Feedback resistance	$R_2$
Source resistance	$R_s$
load resistance	$R_L$

**TABLE 1.1.1** 

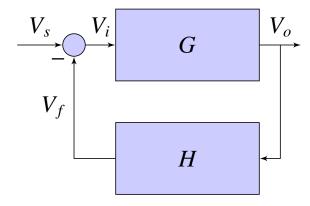


Fig. 1.1.1.2

- 1.1.2. Draw the small signal model for Fig. 1.1.1.1. **Solution:** The equivalent circuit of the amplifier is in Fig. 1.1.2
- 1.1.3. Assuming that the operational amplifier has infinite input resistance and zero output resistance, find the *feedback factor H*.

**Solution:** From Fig. 1.1.2,

$$V_0 = GV_i (1.1.3.1)$$

$$V_i = V_s - V_f (1.1.3.2)$$

$$V_f = \frac{R_1}{R_1 + R_2} V_o (1.1.3.3)$$

assuming that the current through  $R_s$  is very

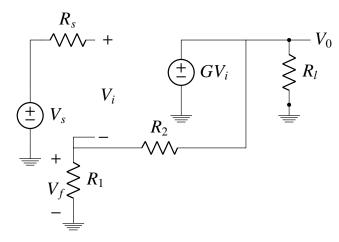


Fig. 1.1.2

small. Thus,

$$H = \frac{V_f}{V_o} = \frac{R_1}{R_1 + R_2} \tag{1.1.3.4}$$

1.1.4. Obtain the closed loop gain T and summarize your results through a Table.

**Solution:** Table 1.1.4 provides a summary.

$$T = \frac{V_0}{V_i} = \frac{G}{1 + GH} \tag{1.1.4.1}$$

$$= \frac{G(R_1 + R_2)}{(R_1 + R_2) + GR_1}$$
 (1.1.4.2)

Parame- ters	Definition	For given circuit
Open loop gain	G	G
Feedback factor	Н	$\frac{R_1}{R_1 + R_2}$
Loop gain	GH	$G^{\frac{R_1}{R_1+R_2}}$
Amount of feedback	1+GH	$1 + \frac{GR_1}{R_1 + R_2}$
Closed loop gain	<u>G</u> 1+ <i>GH</i>	$\frac{G(R_1 + R_2)}{R_1 + R_2 + GR_1}$

**TABLE 1.1.4** 

gain T is almost entirely determined by the feedback network.

**Solution:** If

$$GH \gg 1, \tag{1.1.5.1}$$

$$T \approx \frac{1}{H} = 1 + \frac{R_2}{R_1} \tag{1.1.5.2}$$

1.1.6. If

$$G = 10^4 \tag{1.1.6.1}$$

$$T = 10,$$
 (1.1.6.2)

find H.

**Solution:** From Table 1.1.4

$$T = \frac{G}{1 + GH} = 10 \tag{1.1.6.3}$$

$$\implies H = 0.0999$$
 (1.1.6.4)

1.1.7. Gain Desensitivity: If G decreases by 20%, what is the corresponding decrease in T? Comment.

**Solution:** From From Table 1.1.4, Given

$$T = \frac{G}{1 + GH} \tag{1.1.7.1}$$

$$T = \frac{G}{1 + GH}$$

$$\implies dT = \frac{dG}{(1 + GH)^2}$$
(1.1.7.1)
$$(1.1.7.2)$$

$$\implies \frac{dT}{T} = \frac{1}{1 + GH} \frac{dG}{G}$$
 (1.1.7.3)

From the information available so far,

$$dG = 20\%, G = 10^4, H = 0.0999 \implies \frac{dT}{T} = 0.025\%$$
(1.1.7.4)

using the following code.

## codes/ee18btech11005/ee18btech11005.py

Thus the closed loop gain is almost invariant to a relatively large (20%) variation in the open loop gain G. This is known as gain desensitivity.

- 2 FEEDBACK CURRENT AMPLIFIER: SHUNT-SERIES
- 2.1 Introduction
- 2.1.1. Draw the equivalent control system for the feedback current amplifier shown in 2.1.1.4 **Solution:** See Fig. 2.1.1.5.
- 1.1.5. Find the condition under which closed loop 2.1.2. For the feedback current amplifier shown in 2.1.1.4, draw the Small-Signal Model. Neglect the Early effect in  $Q_1$  and  $Q_2$ .

**Solution:** See Fig. 2.1.2.

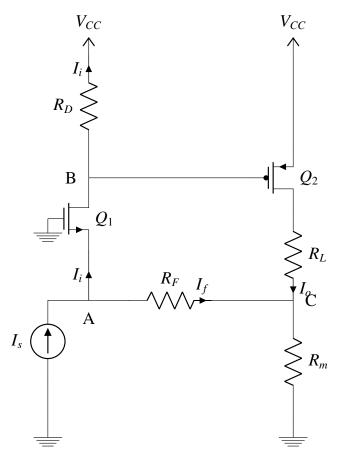
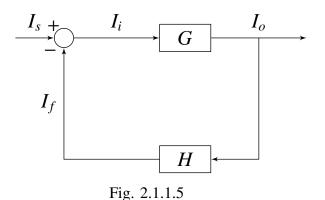


Fig. 2.1.1.4



While drawing a Small-Signal Model, we ground all constant voltage sources and open all constant current sources. All Small-Signal paramters are obtained from DC-Analysis of the circuit. Neglecting Early effect, in Small-Signal Analysis a N-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{gs}$  flowing from Drain to Source. Whereas a P-MOSFET is modelled as a Current Source with value of current equal to  $g_m v_{sg}$  flowing from Source to Drain.

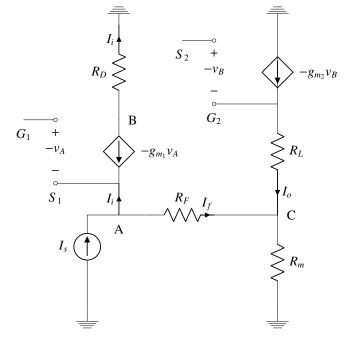


Fig. 2.1.2: Small Signal Model

2.1.3. Describe how the given circuit is a Negetive Feedback Current Amplifier.

**Solution:** For the feedback to be negative,  $I_f$  must have the same polarity as  $I_s$ . To ascertain that this is the case, we assume an increase in  $I_s$  and follow the change around the loop: An increase in  $I_s$  causes  $I_i$  to increase and the drain voltage of  $Q_1$  will increase. Since this voltage is applied to the gate of the p-channel device  $Q_2$ , its increase will cause  $I_o$ , the drain current of  $Q_2$ , to decrease. Thus, the voltage across  $R_M$  will decrease, which will cause  $I_f$  to increase. This is the same polarity assumed for the initial change in  $I_s$ , verifying that the feedback is indeed negative.

2.1.4. Find the Expression for the Open-Loop Gain  $G = \frac{I_o}{I_i}$ , from the Small-Signal Model. in Fig. 2.1.2.

**Solution:** In Small-Signal Model,

$$v_B = I_i R_D (2.1.4.1)$$

$$v_{gs_2} = v_B = I_i R_D (2.1.4.2)$$

In Small-Signal Analysis, P-MOSFET is modelled as a current source where current flows from Source to Drain. So, the value of current flowing from Source to Drain in P-MOSFET is,

$$I_o = -g_{m_2} v_{gs_2} = -g_{m_2} I_i R_D (2.1.4.3)$$

So, the Open-Circuit Gain is

$$G = \frac{I_o}{I_i} = -g_{m_2} R_D (2.1.4.4)$$

2.1.5. Find the Expression of the Feedback Factor  $H = \frac{I_f}{I_o}$ , from Small-Signal Model. **Solution:**  $I_o$  is fed to a current divider formed

**Solution:**  $I_o$  is fed to a current divider formed by  $R_M$  and  $R_F$ .  $R_F$  is a Large Resistance compared to Input resistance of Amplifier and so most of the current flows through it leaving a small current as input to Amplifier. Hence the voltage at point 'A' is very small and is considered,  $v_A \simeq 0$ . So  $R_F$  and  $R_M$  are parallel and Voltage Drop across them is same.

$$(I_o + I_f)R_M \simeq -I_f R_F$$
 (2.1.5.1)

$$\frac{I_f}{I_o} \simeq -\frac{R_M}{R_F + R_M} \tag{2.1.5.1}$$

So, the Feedback Factor,

$$H \equiv \frac{I_f}{I_o} \simeq -\frac{R_M}{R_F + R_M} \tag{2.1.5.3}$$

2.1.6. Find the Expression for the Closed-Loop Gain  $T = \frac{I_0}{I}$ .

**Solution:** From (2.1.4.4) and (2.1.5.3),

$$T = \frac{I_o}{I_s} = \frac{G}{1 + GH} \tag{2.1.6.1}$$

$$= -\frac{g_{m_2}R_D}{1 + g_{m_2}R_D/\left(1 + \frac{R_F}{R_M}\right)}$$
 (2.1.6.2)

$$\implies T = -\frac{g_{m_2} R_D}{1 + g_{m_2} R_D / \left(1 + \frac{R_F}{R_M}\right)} \quad (2.1.6.3)$$