

CFD Simulation and Validation of a Redesigned Paediatric Inhaler Spacer

GROUP:
HEALTHCARE 1

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Project Brief

Background:

- Computational Fluid Dynamics is carried out to explore the trajectory of drug particles from the inhaler to the throat. This is performed on a pressurised metered-dose inhaler targeted towards children.

Aims:

- Evaluate the effect of changing the size/shape of the inhaler spacer.
- Analyse the efficiency of the inhaler through the particles that travel to the throat.



Inhaler Spacers and Asthma.

- Metered-Dose Inhaler's (MDIs) are a way of providing a standardized dose of medication during an asthma attack.
- The medicine is typically a corticosteroid or bronchodilator and is absorbed via the lungs.
- A spacer improves the efficiency of the MDI by reducing the amount of medicine wasted in the throat and mouth.
- Spacers do require constant cleaning, with soap and water and there is a misunderstanding regarding the target audience for a spacer – any age can benefit from them.

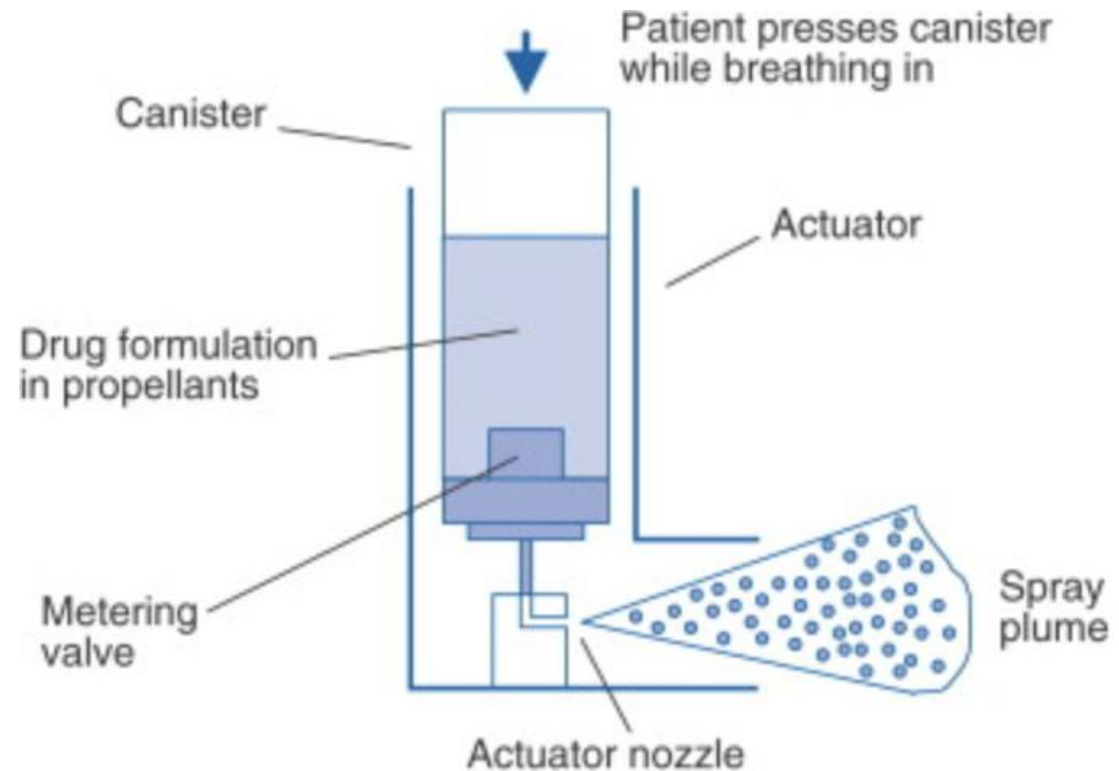
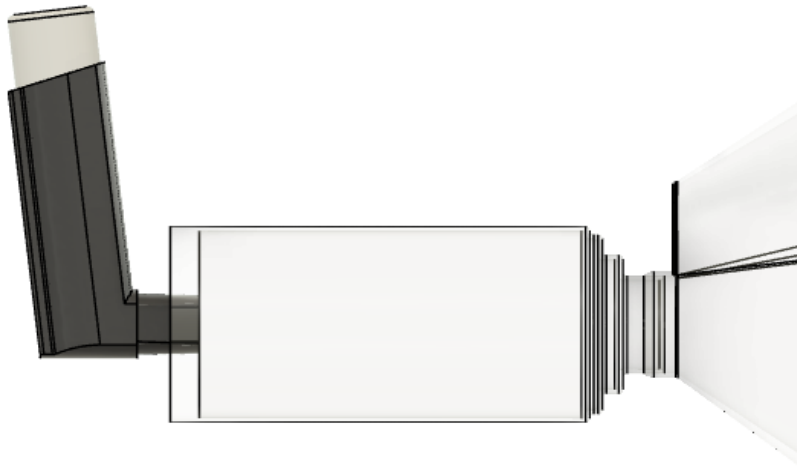


Figure 1: Pediatric Inhaler Delivery



Geometry of Initial Design of Inhaler Spacer



Geometry of Initial Design

Dimensions	Value
Length of Spacer	119 mm
Spacer Diameter	48 mm
Mask Insertion Diameter	24 mm



Geometry of Redesigns

Design 1 – Tapered Spacer (Skyler)

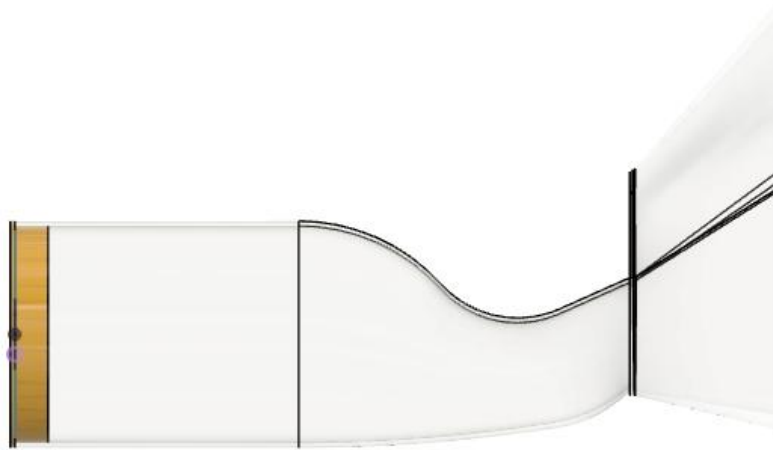


Design 2 – Pear-shaped Spacer (Brandon)

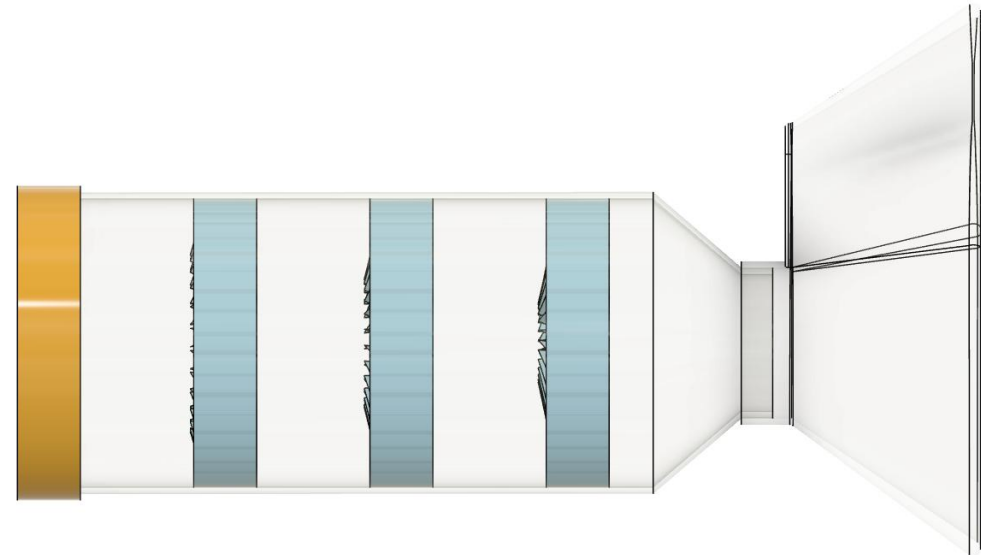


Geometry of Redesigns

Design 3 – Inclined Outlet Spacer (Diljit)



Design 4 – Internal Guide Vanes Spacer (Harkirat)



Concept for Redesign 4

Design is inspired by: Stator blades in turbine jet engines

- Usually act to diffuse air, however in some cases they can act as compressors

The geometry of the compressive ring is loosely based on two diagrams below

- Key points:
 - Curved blade > Straight Blade
 - Equally spaced thin blades

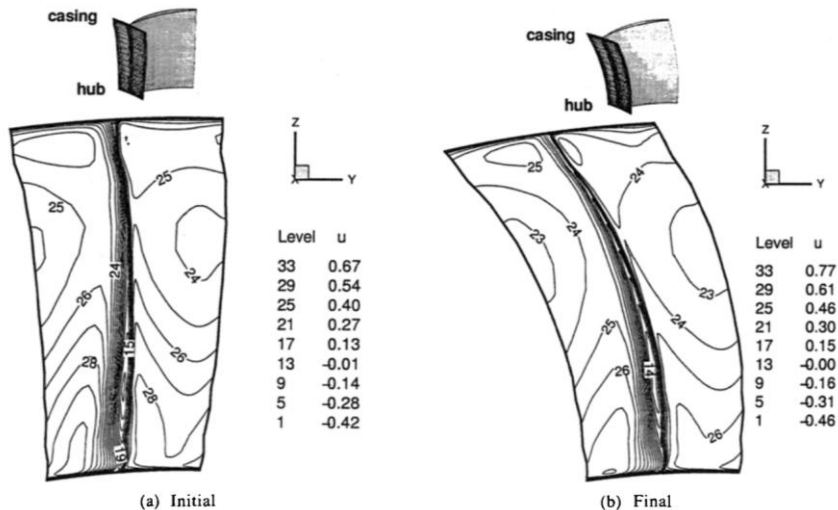


Figure 2: Initial and final designs for a stator blade
(Lee S.Y and Kim K.Y, 2000)

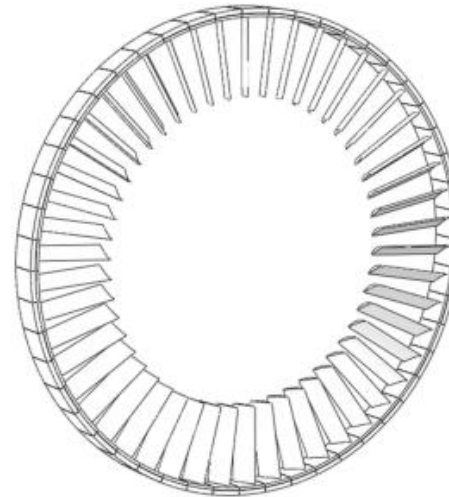


Figure 3: Full circle compressor stator blade ring model
(Ma J, Liu Z, Zhang D and Xie Y, 2023)

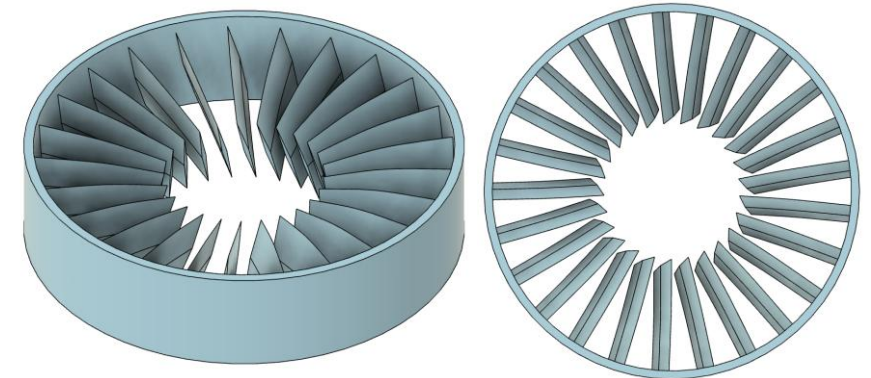


Figure 4: Isometric and top view of the guide vanes CAD render

Mouth Anatomy

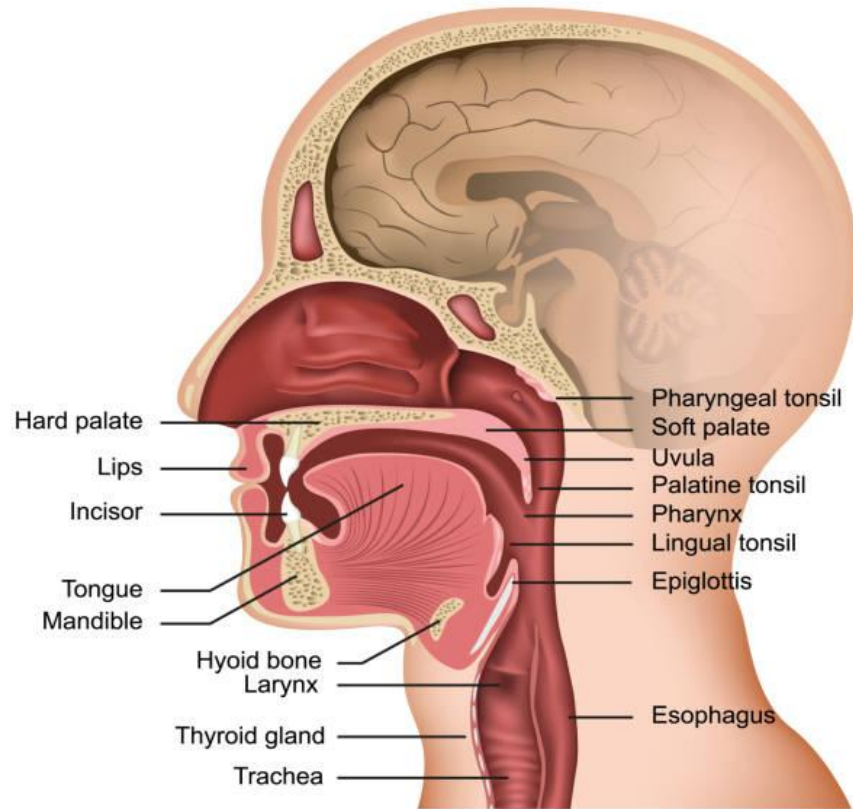
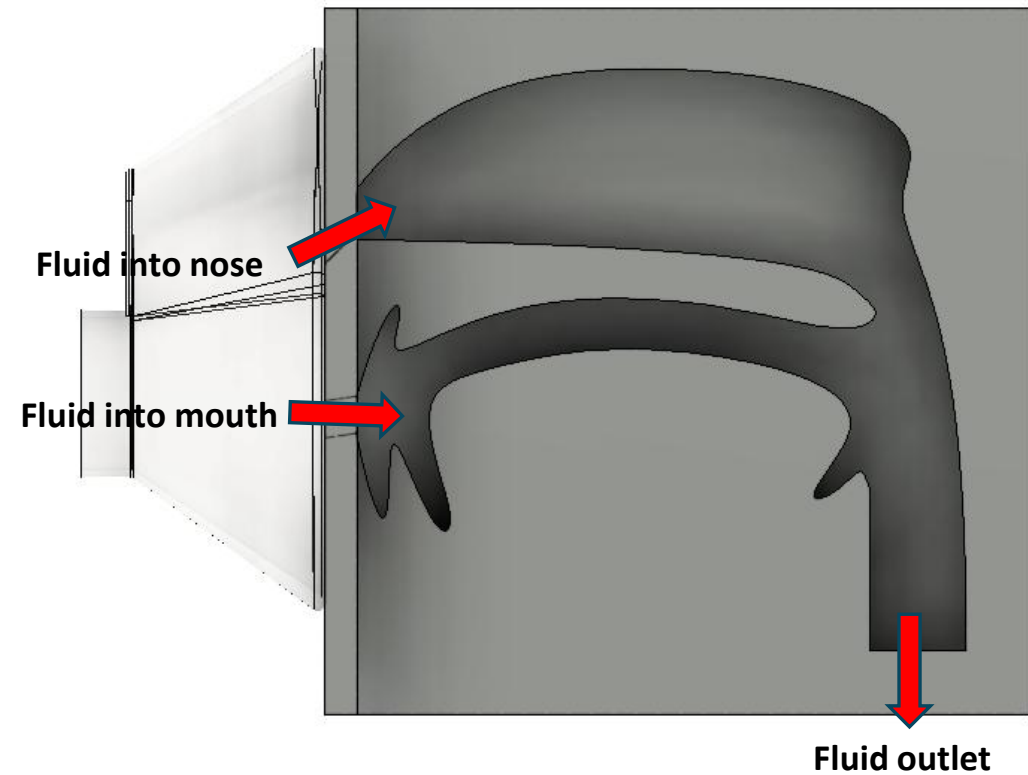


Figure 5: Mouth and Tongue Anatomy



Direction of Fluid Into and Out of the Cavity of Mouth and Nose.

Regulations

- The National Institute for Health and Care Excellence (NICE) guideline emphasises the importance of using Pressure Metered Dose Inhalers with a spacer device for young children.
- They also highlight the need to select the right device to ensure consistent drug dosing.



Fluid and Material Properties

- Due to insufficient information around the properties of salbutamol except density, air properties from Ansys Fluent are used to replace the missing ones.

Property	Salbutamol / Air
Density	1.07 kg/m ³
Specific Heat	1006.43 J/kgK
Thermal Conductivity	0.0242 W/mK
Dynamic Viscosity	1.7894 x 10 ⁻⁵ kg/ms

Property	Polycarbonate
Density	63.987 kg/m ³
Specific Heat	1198.5
Thermal Conductivity	0.034606 W/mK



Governing Equations

- Assuming that density is constant: $\nabla \cdot (\rho \vec{v}) \equiv \rho \nabla \cdot \vec{v} + \vec{v} \cdot \nabla \rho$
- Assuming that momentum is constant:
 - x-component: $\frac{\partial(\rho u)}{\partial t} + \nabla \cdot (\rho u \vec{V}) = -\frac{\partial p}{\partial x} + \frac{\partial \tau_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} + \rho f_x$
 - y-component: $\frac{\partial(\rho v)}{\partial t} + \nabla \cdot (\rho v \vec{V}) = -\frac{\partial p}{\partial y} + \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} + \rho f_y$
 - z-component: $\frac{\partial(\rho w)}{\partial t} + \nabla \cdot (\rho w \vec{V}) = -\frac{\partial p}{\partial z} + \frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z} + \rho f_z$

- Energy is conserved:

$$\begin{aligned}
 & \frac{\partial}{\partial t} \left[\rho \left(e + \frac{V^2}{2} \right) \right] + \nabla \cdot \left[\rho \left(e + \frac{V^2}{2} \right) \vec{V} \right] \\
 &= \rho \dot{q} + \frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) \\
 &+ \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) - \frac{\partial(u p)}{\partial x} - \frac{\partial(v p)}{\partial y} - \frac{\partial(w p)}{\partial z} + \frac{\partial(u \tau_{xx})}{\partial x} \\
 &+ \frac{\partial(u \tau_{yx})}{\partial y} + \frac{\partial(u \tau_{zx})}{\partial z} + \frac{\partial(v \tau_{xy})}{\partial x} + \frac{\partial(v \tau_{yy})}{\partial y} \\
 &+ \frac{\partial(v \tau_{zy})}{\partial z} + \frac{\partial(w \tau_{xz})}{\partial x} + \frac{\partial(w \tau_{yz})}{\partial y} + \frac{\partial(w \tau_{zz})}{\partial z} + \rho \vec{f} \cdot \vec{V}
 \end{aligned}$$



Governing Equations

- Computational approach: Reynolds-Averaged Navier Stokes (RANS) with k-epsilon model.

- Navier-Stokes – Body and Surface forces present:

$$-\rho \left(\frac{D\vec{v}}{Dt} \right) = \rho \nabla \Phi + \nabla p + \eta \nabla^2 \vec{v} \qquad \frac{D}{Dt} \equiv \frac{\partial}{\partial t} + (\vec{v} \cdot \nabla)$$

- Turbulence – For internal flow: $Re \geq 2300$

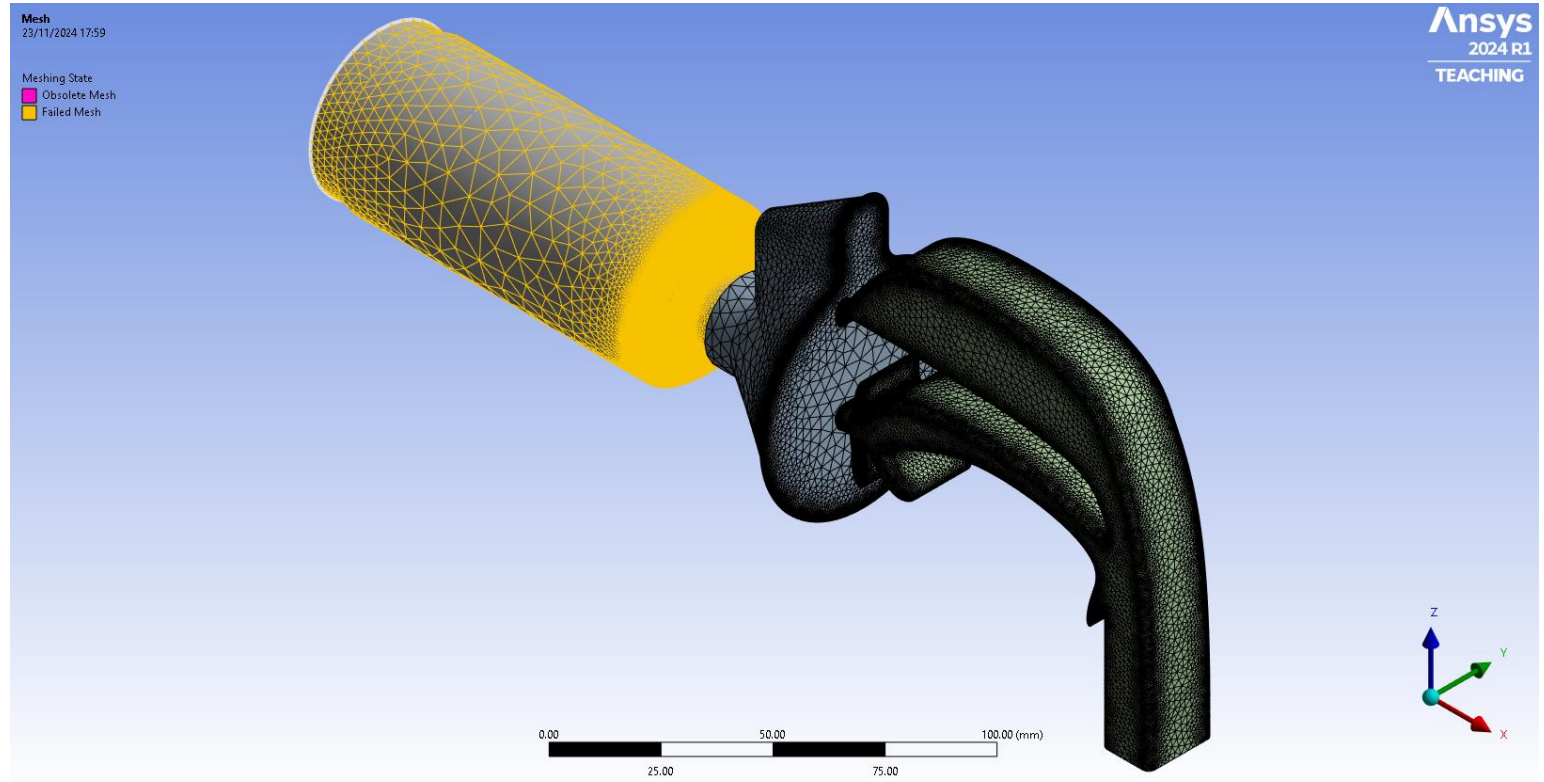
- $Re_{Salbutamol/Air} = \frac{\rho u L}{\mu} = \frac{1.07 \times 1.724 \times 119 \times 10^{-3}}{1.7894 \times 10^{-5}} = 12269$



Default Mesh for Initial design

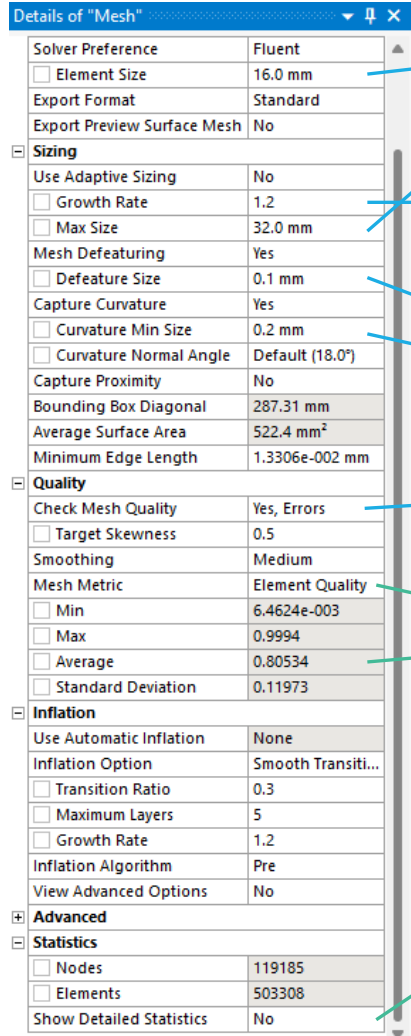
The default meshing option is inadequate:

- High number of Elements
- The Mesh fails



Mesh Size (mm)	Number of Elements	Aspect Ratio	Skewness	Orthogonal Quality	Element Quality
Default	1,141,767	1.9014	0.2419	0.7568	0.8274

Finding optimum Mesh Size – Method



Will be varied to find the optimum size

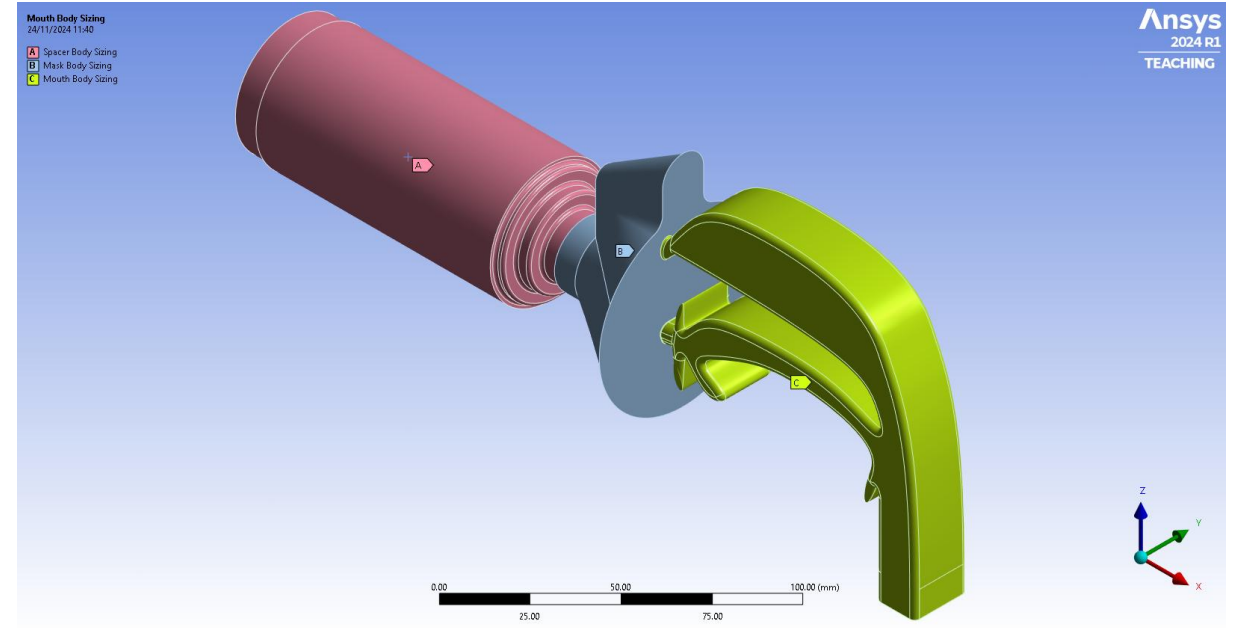
Standard growth rate to avoid abrupt changes in adjacent mesh elements

Limited to the geometry of the CAD

Lowest possible value with valid mesh

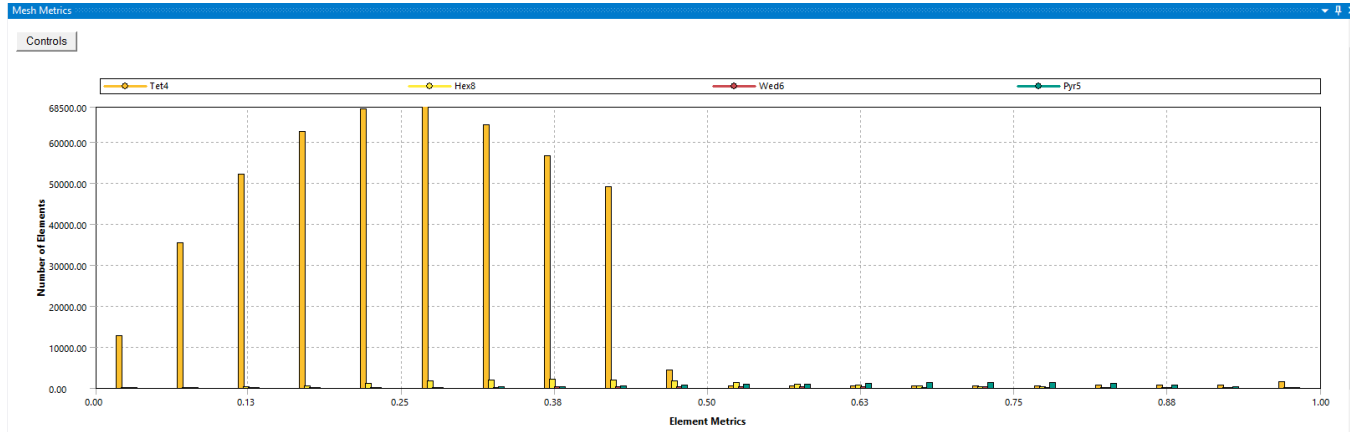
Properties and their values can be found for each mesh

Detailed of the number of nodes and elements can be seen.



Location	Mesh Method	Defeature size	Local Minimum Size
Spacer Volume	Hex Dominant	0.75 mm	1.2 mm
Mask Volume	Hex Dominant	0.5 mm	0.8 mm
Mouth Volume	Patch Conforming	0.3 mm	0.5 mm

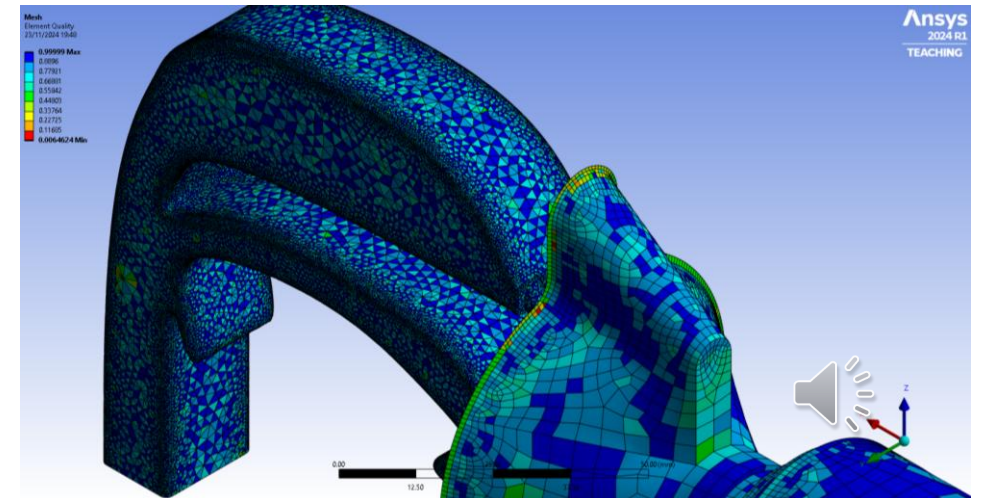
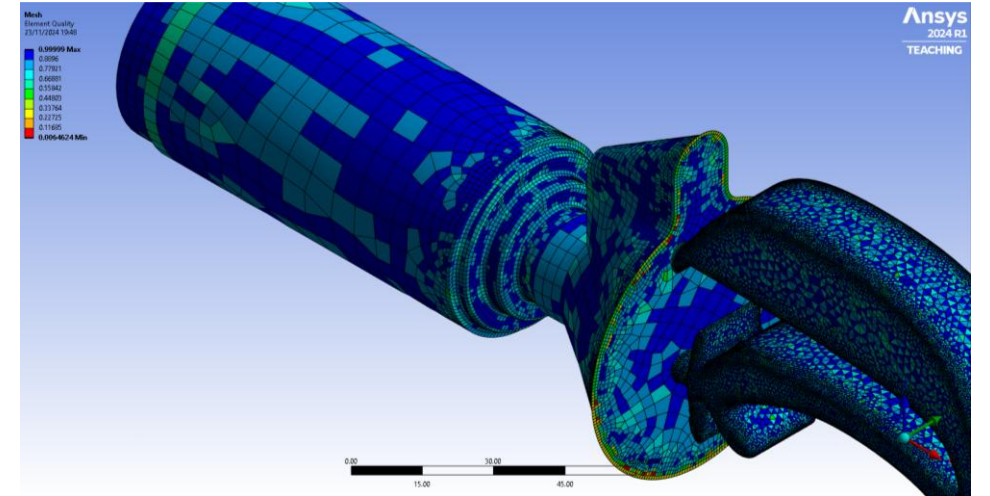
Varying Mesh Size for Initial Design

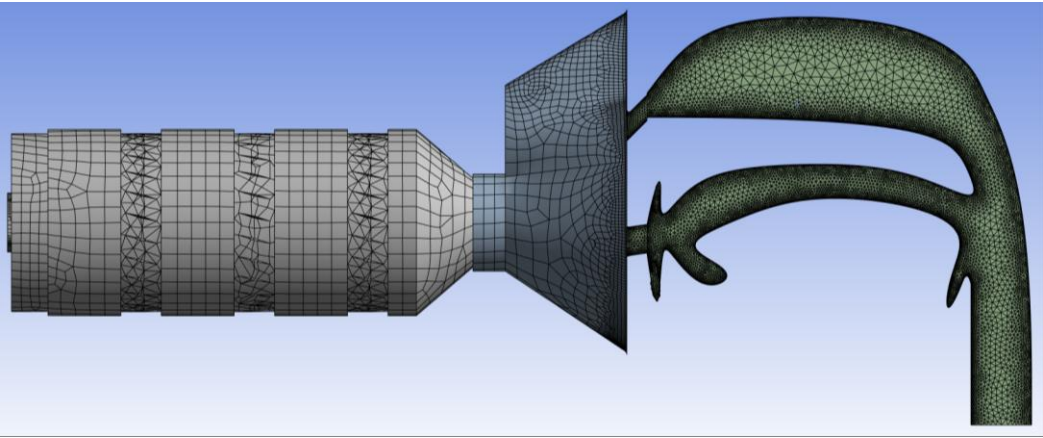
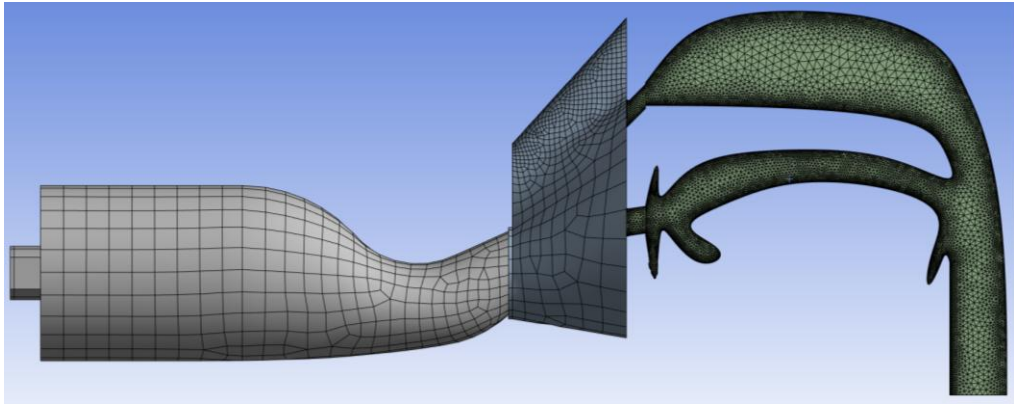
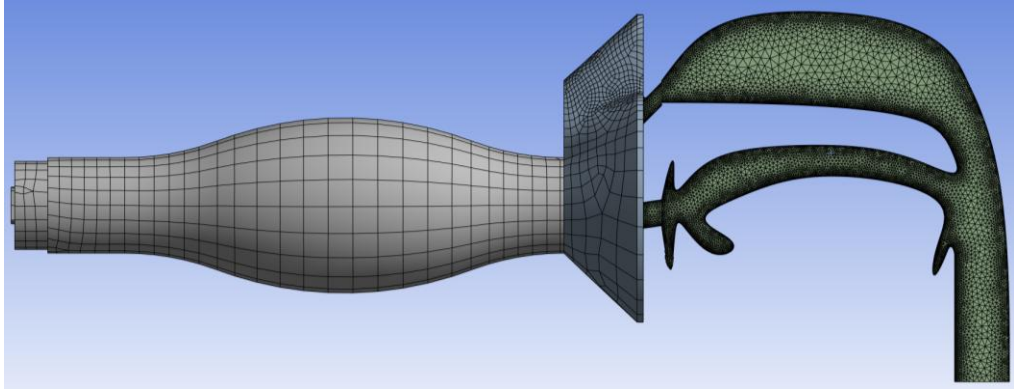
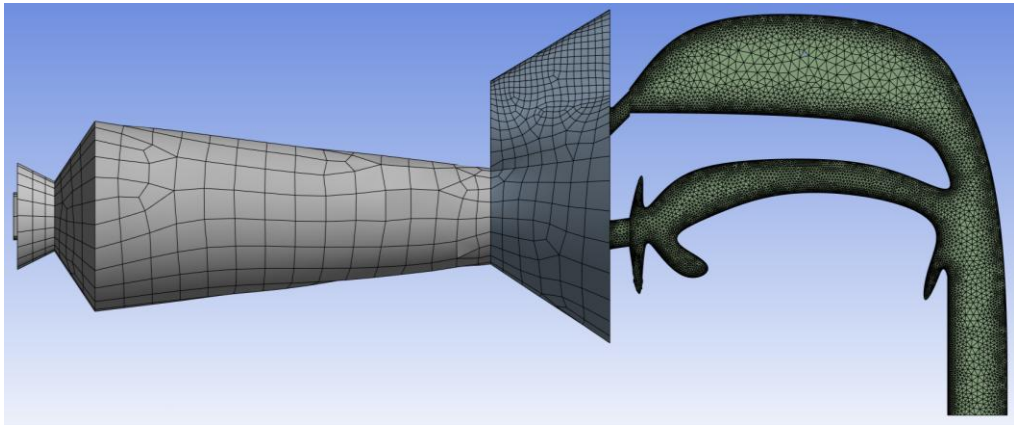


$$\text{Average Metric} = \sum \frac{\text{Metric} \times n_i}{n}$$

where n is the number of elements

Mesh Size (mm)	Number of Elements	Aspect Ratio	Skewness	Orthogonal Quality	Element Quality
16	503,308	2.0772	0.2730	0.7334	0.8053
12	503,456	2.1290	0.2747	0.7318	0.8042
8	503,813	2.0613	0.2731	0.7331	0.8056
4	507,966	2.1024	0.2742	0.7334	0.8030





Design	Number of Elements	Aspect Ratio	Skewness	Orthogonal Quality	Element Quality
Tapered	481,829	1.9265	0.25776	0.74292	0.81704
Pear Shape	486,293	1.9434	0.25948	0.74178	0.81528
Inclined Outlet	488,125	1.9409	0.25942	0.74207	0.81565
Guide Vanes	508,911	2.2861	0.27787	0.72855	0.80159



Calculation, Initialisation and Setup Conditions

General

Mesh

Scale...

Check

Report Quality

Display...

Units...

Solver

Type

Pressure-Based

Density-Based

Velocity Formulation

Absolute

Relative

Time

Steady

Transient

☒ Gravity

Gravitational Acceleration

X [m/s²]

0

Y [m/s²]

0

Z [m/s²]

-9.81

Gravity and Time Conditions

Models

Multiphase (Off)

Energy (On)

Viscous (Realizable k-ε, Standard Wall Fn)

Radiation (Off)

Heat Exchanger (Off)

Species (Off)

Discrete Phase (On)

Injections

Erosion Dynamic Mesh

Solidification & Melting (Off)

Virtual Blade Model (Off)

Acoustics (Off)

Structure (Off)

Eulerian Wall Film (Off)

Potential/Electrochemistry (Off)

Battery Model (Off)

Energy and Viscous Input Parameters

Hybrid Initialization

General Settings

Turbulence Settings

Species Settings

Number of Iterations

20

Explicit Under-Relaxation Factor

Scalar Equation-0

1

Scalar Equation-1

1

Reference Frame

Relative to Cell Zone

Absolute

Initialization Options

☐ Use Specified Initial Pressure on Inlets

☐ Use External-Aero Favorable Settings

☐ Maintain Constant Velocity Magnitude

Hybrid Initialisation Conditions

Hybrid Initialization

General Settings

Turbulence Settings

Species Settings

☒ Averaged Turbulent Parameters

Turbulence Intensity [%]

5

Viscosity Ratio

10

Hybrid Initialisation Turbulence Conditions

Checking case topology...

-This case has both inlets & outlets

-Pressure information is not available at the boundaries.

Case will be initialized with constant pressure

iter	scalar-0
1	1.000000e+00
2	1.287338e-04
3	1.885722e-05
4	4.273223e-06
5	5.038013e-06
6	1.797860e-06
7	1.241736e-05
8	1.988474e-06
9	8.031669e-07
10	5.212931e-06
11	8.500169e-07
12	3.664107e-07
13	2.493054e-06
14	4.070227e-07
15	1.757193e-07
16	1.209482e-06
17	1.975868e-07
18	8.535913e-08
19	5.907275e-07
20	9.653385e-08

Hybrid initialization is done.

Hybrid Initialisation Iterations

Run Calculation

Check Case...

Update Dynamic Mesh...

Pseudo Time Settings

Fluid Time Scale

Time Step Method

Automatic

Time Scale Factor

1

Length Scale Method

Conservative

Verbosity

0

Parameters

Number of Iterations

200

Reporting Interval

1

Profile Update Interval

1

Solution Processing

Statistics

☐ Data Sampling for Steady Statistics

Data File Quantities...

Solution Advancement

Calculate

Run Calculation Conditions

Fluent Launcher

Ansys

Home

General Options

Parallel Settings

Remote

Scheduler

Environment

Dimension

2D

3D

Solver Options

☒ Double Precision

☐ Do not show this panel again

Parallel (Local Machine)

Solver Processes

2

Solver Processes Input Parameters

Home

General Options

Parallel Settings

Remote

Scheduler

Environment

Interconnects

default

Solver GPGPUs per Machine (Offload Mode)

1

MPI Types

default

☐ Select IP Interface

Run Types

☒ Shared Memory On Local Machine

☐ Distributed Memory on a Cluster

Solver GPGPUs per machine Input Parameters



Boundary Conditions

Inlet Conditions	
Velocity Magnitude (m/s)	1.724
Specification Method	Intensity and Viscosity Ratio
Turbulent Intensity (%)	5
Turbulent Viscosity Ratio	10
Temperature (°C)	25
Discrete Phase Type	Escape

Outlet Conditions	
Backflow Reference Frame	Absolute
Gauge Pressure (Pa)	0
Specification Method	Intensity and Viscosity Ratio
Turbulent Intensity (%)	5
Turbulent Viscosity Ratio	10
Backflow Total Temp (°C)	25
Discrete Phase Type	Escape

Wall Conditions	
Wall Motion	Stationary
Shear Condition	No Slip
Roughness Model	Standard
Roughness Height (m)	0
Roughness Constant	0.5
Temperature (°C)	25
Discrete Phase Type	Trap

Average number of breaths for 3 – 5 year olds = 28 breaths per minute

Inspiratory Flow Rate for 2 – 12 year olds (Q_1) = $30 \frac{L}{min} = 0.0005 \frac{m^3}{s}$

Inlet Area of Spacer(A_1) = $0.00029 m^2$

Inlet Velocity = $\frac{Q_1}{A_1} = \frac{0.0005}{0.00029} = 1.724 \frac{m}{s}$



DPM/ Injection Conditions

Discrete Phase Model

Interaction

☒ Interaction with Continuous Phase

☐ Update DPM Sources Every Flow Iteration

DPM Iteration Interval

1

Particle Treatment

☐ Unsteady Particle Tracking

Contour Plots for DPM Variables

☐ Mean Values

Tracking

Physical Models

UDF

Numerics

Parallel

Tracking Parameters

Max. Number of Steps

50000

☐ Specify Length Scale

Step Length Factor

5

Tracking Option

☒ High-Res Tracking

DPM Tracking Conditions

Point Properties

Physical Models

Turbulent Dispersion

Parcel

Wet C

Momentum Exchange

Drag Law

spherical

Heat Exchange

Heat Transfer Coefficient

Ranz-Marshall

☐ Rough Wall Model

Particle Rotation

☐ Enable Rotation

DPM Physical Model Conditions

Tracking

Physical Models

UDF

Options

☐ Thermophoretic Force

☐ Saffman Lift Force

☐ Virtual Mass Force

☐ Pressure Gradient Force

☒ Erosion/Accretion

☐ Two-Way Turbulence Coupling

☐ DEM Collision

☐ Stochastic Collision

☐ Breakup

☐ Volume Displacement

DPM Erosion/ Accretion Conditions

Create/Edit Materials

Name

salbutamol-particles

Material Type

inert-particle

Order Materials by

☒ Name

☐ Chemical Formula

Chemical Formula

Fluent Inert Particle Materials

salbutamol-particles

Fluent Database...

GRANTA MDS Database...

User-Defined Database...

Mixture

none

Properties

Density [kg/m³]

constant

1.07

Cp (Specific Heat) [J/(kg K)]

constant

1006.43

Salbutamol Injection Material Properties

DPM Injection Properties	
Injection Surface	Inlet
Injection Type	Surface
Particle Type	Inert
Diameter Distribution	Uniform
Velocity (m/s)	1.724
Diameter (m)	0.0004
Temperature (°C)	25
Total Flow Rate (kg/s)	1
Surface Options	Scale Flow Rate By Face Area

Point Properties

Physical Models

Turbulent Dispersion

Stochastic Tracking

Dispersion Model

discrete-random-walk

☐ Random Eddy Lifetime

Number of Tries

5

Time Scale Constant

0.15

Length Scale Constant

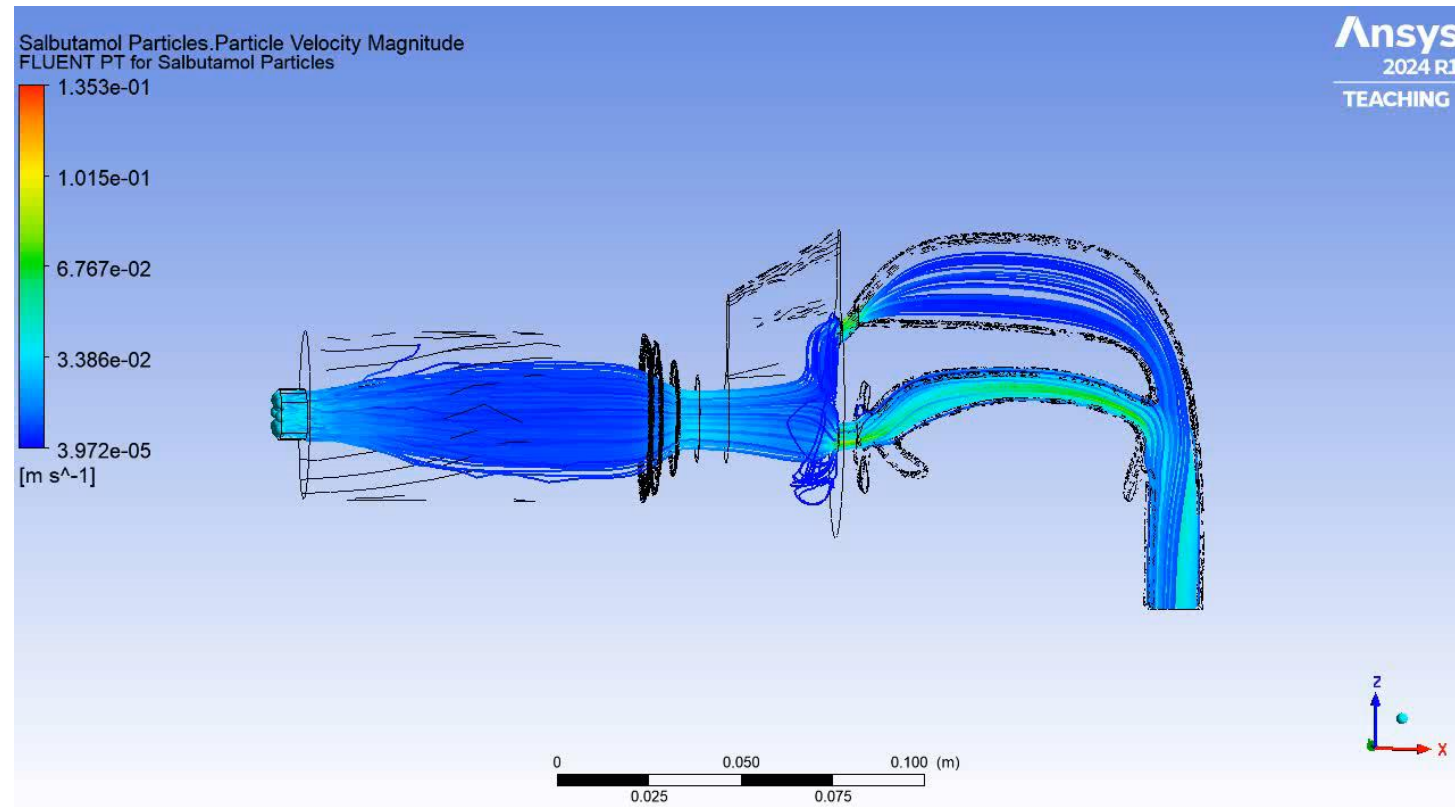
0.72

DPM Turbulence Conditions



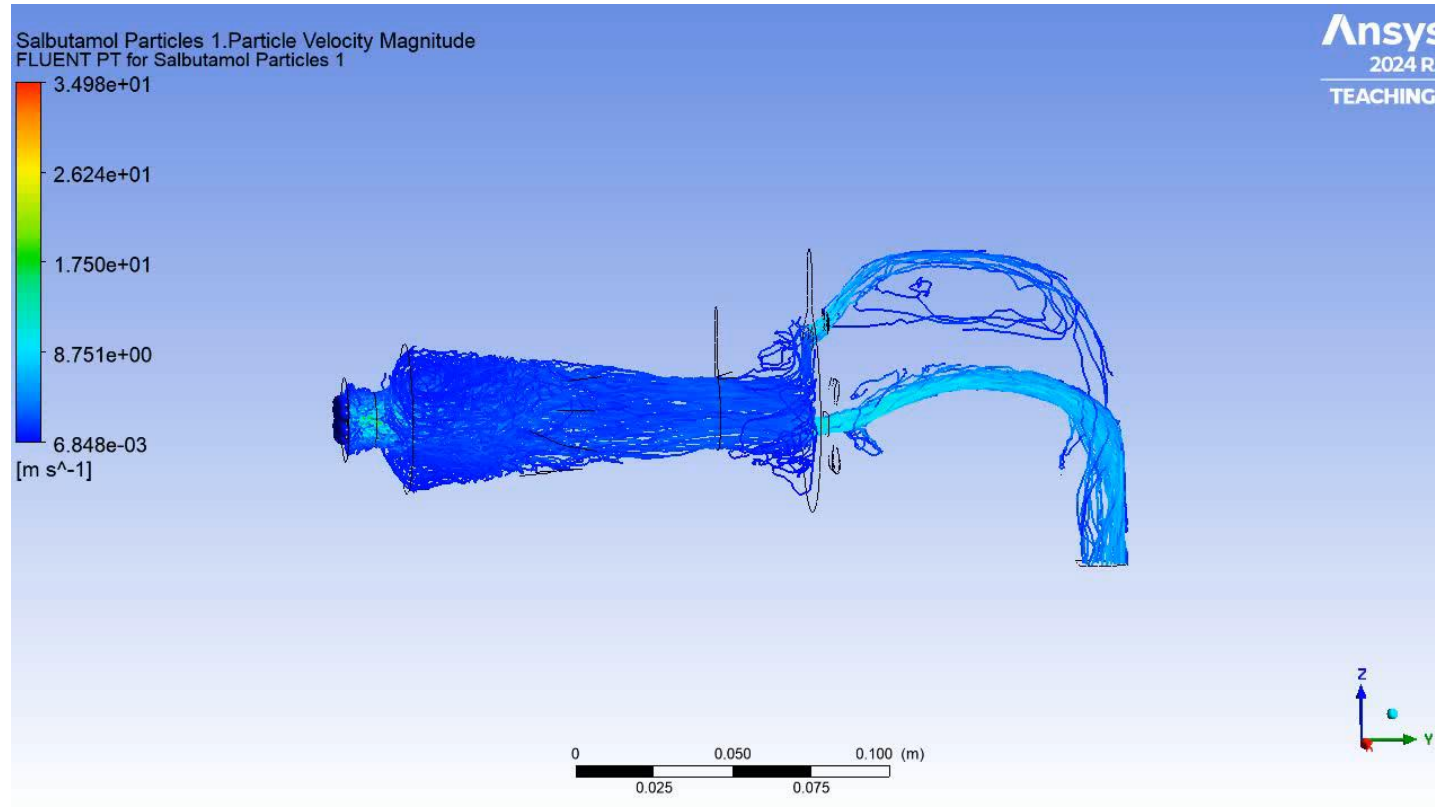
Initial Design Result

$$\text{Efficiency of Spacer} = \frac{\text{Particles Escaped}}{\text{Particles Tracked}} = \frac{562}{1200} = 46.83\%$$



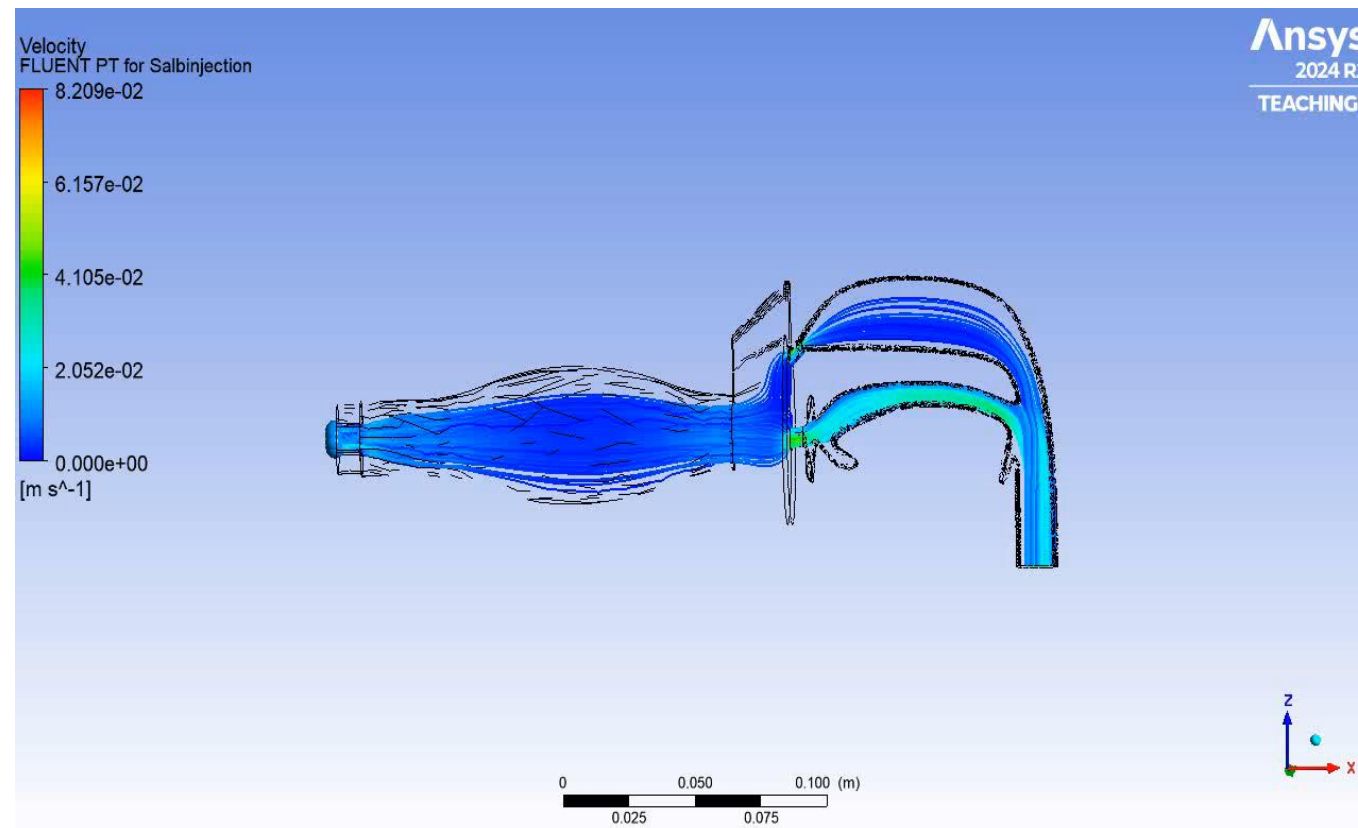
Tapered Spacer Result

$$\text{Efficiency of Spacer} = \frac{\text{Particles Escaped}}{\text{Particles Tracked}} = \frac{2109}{4400} = 47.93\%$$



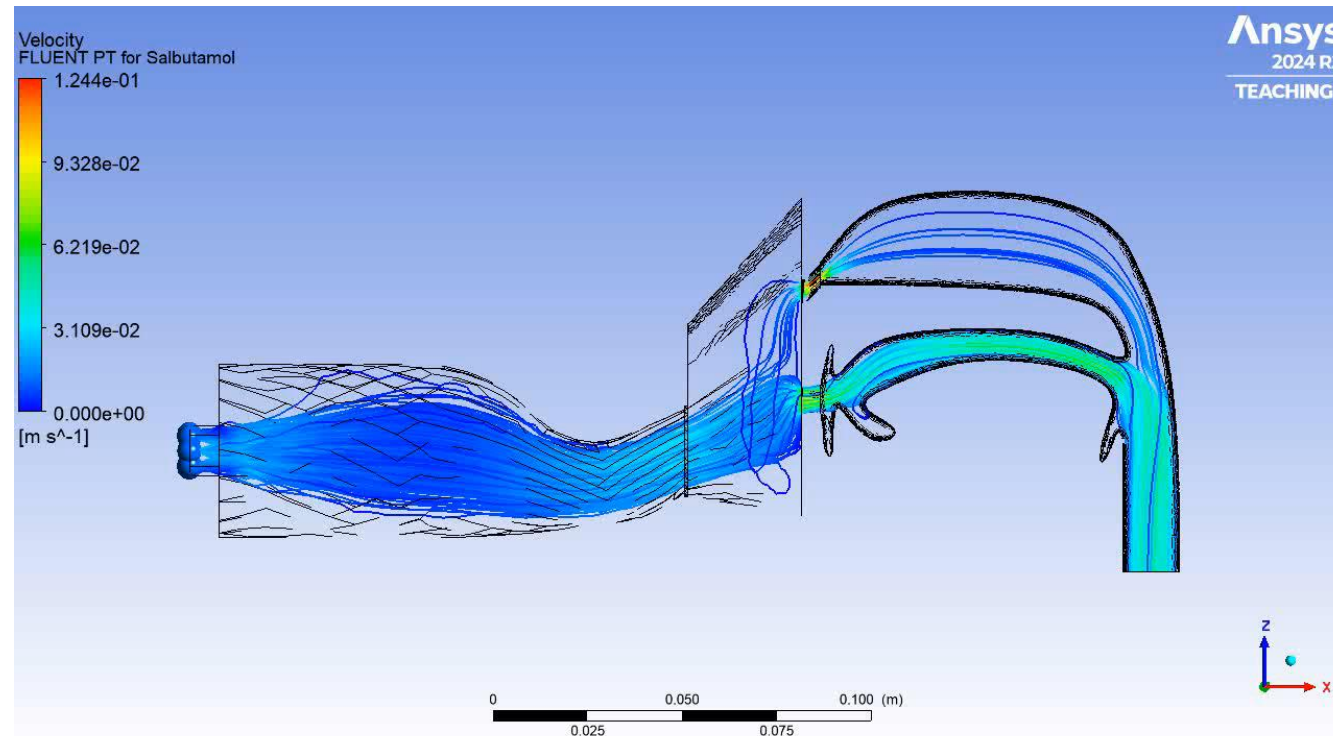
Pear-Shaped Spacer Result

$$\text{Efficiency of Spacer} = \frac{\text{Particles Escaped}}{\text{Particles Tracked}} = \frac{658}{900} = 73.11\%$$



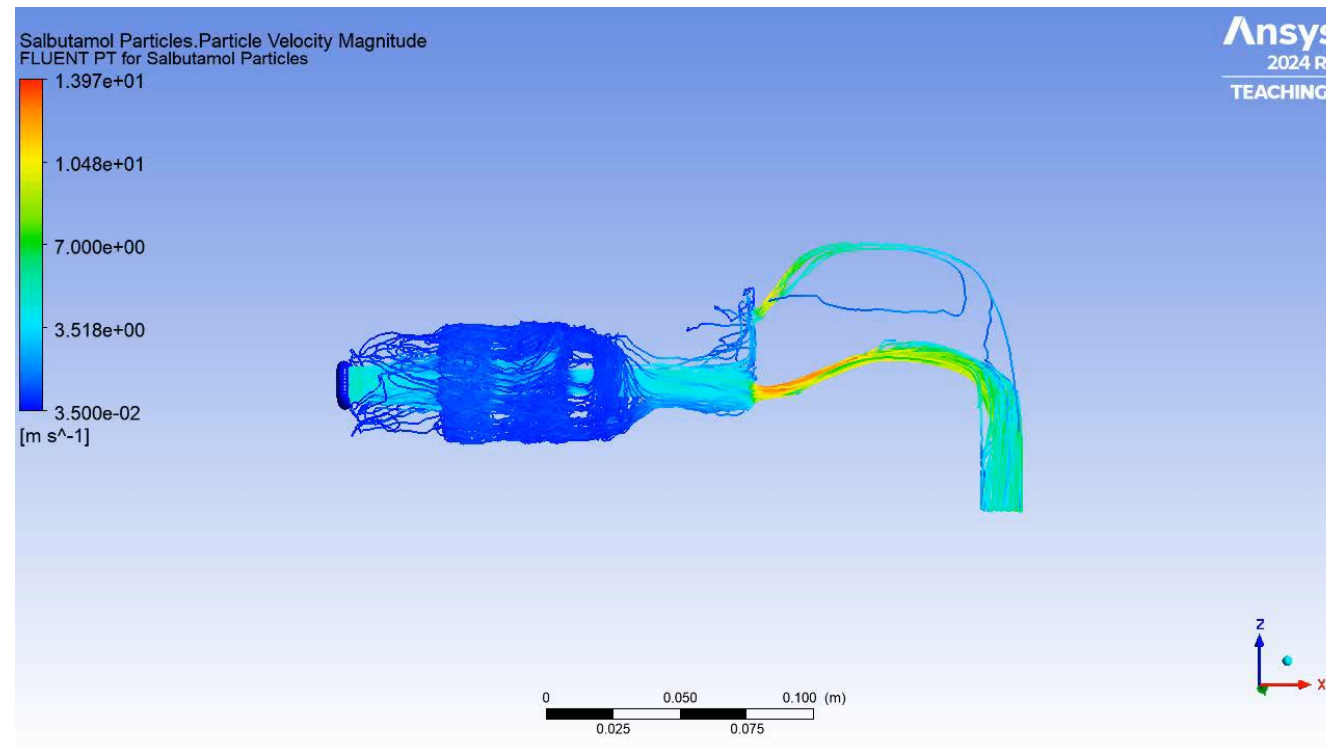
Inclined Outlet Spacer Result

$$\text{Efficiency of Spacer} = \frac{\text{Particles Escaped}}{\text{Particles Tracked}} = \frac{686}{990} = 69.29\%$$



Internal Guide Vanes Spacer Result

$$\text{Efficiency of Spacer} = \frac{\text{Particles Escaped}}{\text{Particles Tracked}} = \frac{283}{1120} = 25.27\%$$

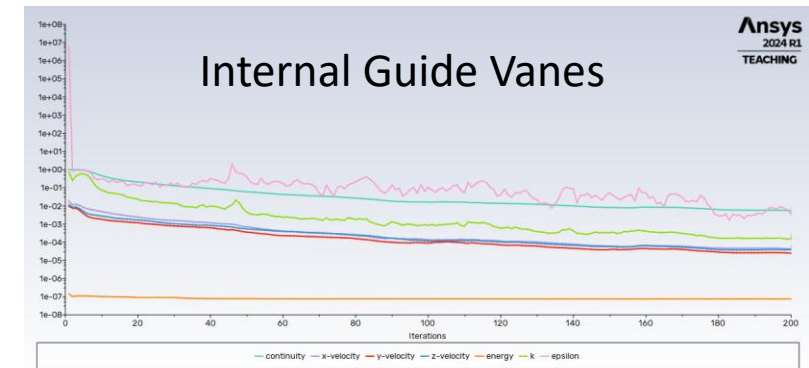
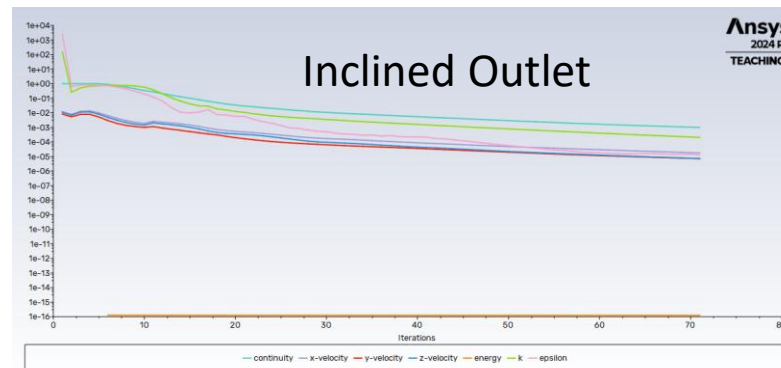
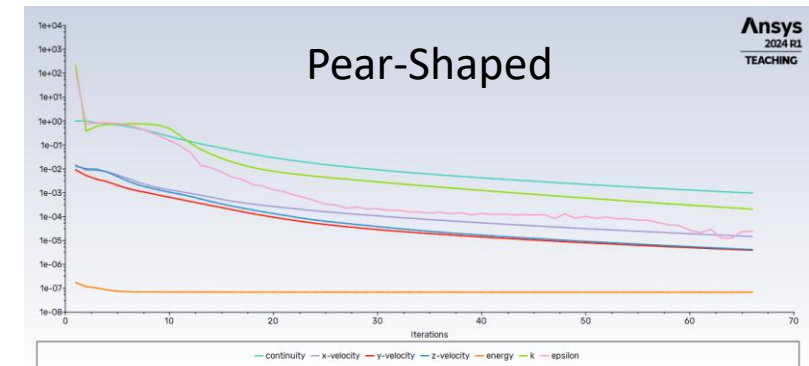
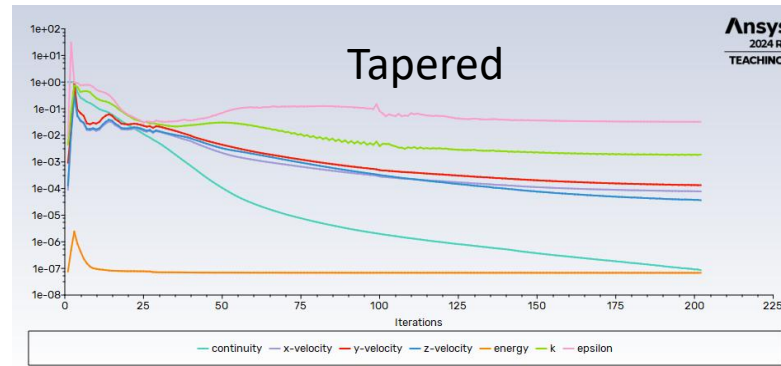
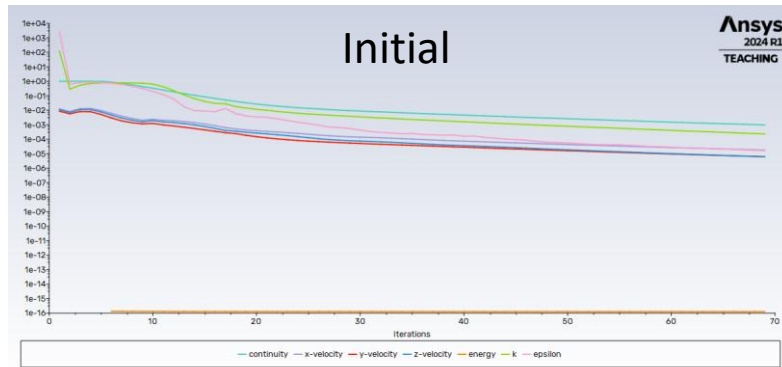


Comparison of Results

Spacer Type	Tracked Particles	Escaped Particles	Efficiency (%)
Initial	1200	562	46.83
Tapered	4400	2109	47.93
Pear-shaped	900	658	73.11
Inclined Outlet	990	686	69.29
Internal Guide Vanes	1120	283	25.27



Solver



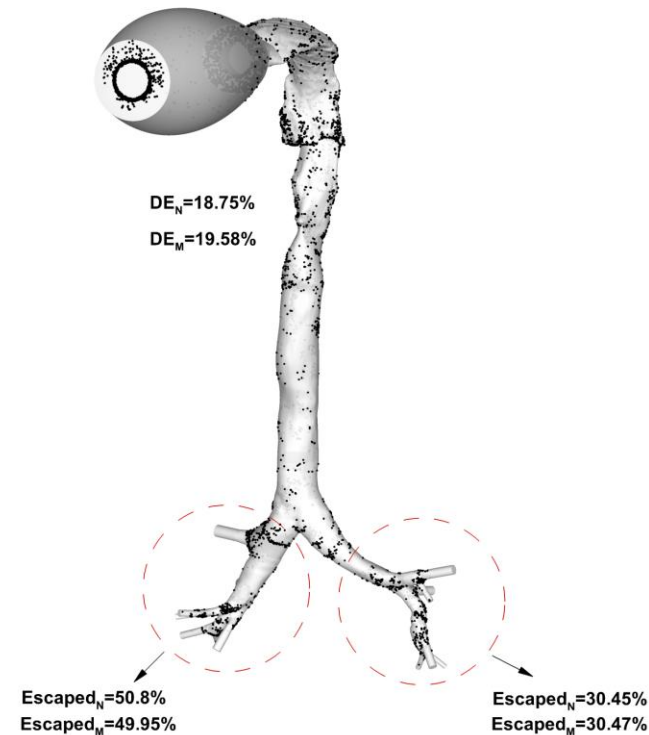
Validation

Advantages:

- Complies with regulations
- Turbulent model – k epsilon
- Mesh Resolution – default meshing

Things to Consider:

- Accuracy of human anatomy
- Using transient model instead of steady state
- Material and fluid properties



Limitations of model

- The computational cost of a transient model is too high (simulations take hours or crash). To address this, the model is simplified by choosing the steady-state option.
- The model for the mouth makes simplifications in CAD. We could outsource a more anatomy-correct model.
- The material for the wall boundary was chosen to be “honeycomb polycarbonate plastic” and modelled as smooth. Ideally, the mouth should be another material and have the associated roughness model.
- The fluid properties are mainly accounting for air instead of salbutamol, which slightly affects our efficiency values when solving.

