Lab Notes

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### To Do

### 1.1 Coding

- Test split-WENO in 2D
- Implement in CUDA
- Solid EOSs
- Implement Barton's damage model
- Test compressible Euler vs GPR use narrowing domain from Toro's book
- Try conservative formulation [Peshkov,Grmela,Romenski]

#### 1.2 Theoretical

- Investiage approximate Riemann solvers (e.g. Dumbser's HLLEM)
- Convergence of conservation of mass in RGFM

### 1.3 Papers

- Isobaric cookoff (make cookoff the focus)
- Split solver vs ADER-WENO
- Analytical results for GPR split solver
- Application of ADER-WENO to equations in other areas of Physics, Biology, & Economics
- HPR-RGFM paper (solve stationarity of interface solver under some conditions)

## Faster Solvers

### 2.1 Fast WENO Oscillation Indicator Calculation

The WENO oscillation indicator is defined as:

$$o = \Sigma_{mn} w_m w_n \tag{2.1}$$

where  $w_i$  are the WENO coefficients calculated for a particular stencil, and:

$$\Sigma_{mn} = \sum_{\alpha=1}^{N} \int_{0}^{1} \psi_{m}^{(\alpha)} \psi_{n}^{(\alpha)} \tag{2.2}$$

By considering that:

$$o = \sum_{\alpha=1}^{N} \int_{0}^{1} \left( \frac{d^{\alpha} w}{dx^{\alpha}} \right)^{2} > 0 \tag{2.3}$$

we have that  $\Sigma$  is symmetric positive definite. Thus, it has a Cholesky decomposition  $\Sigma = LL^T$ . Thus:

$$o = \left\| w^T L \right\|^2 \tag{2.4}$$

L can be precalculated, and o calculated quickly as:

```
1: o = 0

2: \mathbf{for} \ j = 1...n \ \mathbf{do}

3: tmp = 0

4: \mathbf{for} \ i = j...n \ \mathbf{do}

5: tmp = tmp + w(i) * L(i,j)

6: \mathbf{end} \ \mathbf{for}

7: o = o + tmp * tmp

8: \mathbf{end} \ \mathbf{for}
```

### 2.2 Approximating Interface Terms in FV

Instead of calculating the following:

$$\int D(q^{-}(x_{0},t),q^{+}(x_{0},t)) dt \qquad (2.5)$$

I propose calculating the following:

$$D\left(\frac{1}{\Delta t} \int q^{-}\left(x_{0}, t\right) dt, \frac{1}{\Delta t} \int q^{+}\left(x_{0}, t\right) dt\right)$$

$$(2.6)$$

This obtains a large speedup with no discernable difference in the results of Stokes' First Problem.

### 2.3 Analytical Results for Basis Vectors

For N=1, the Gauss-Legendre nodes on [0,1] are  $\left\{\frac{1}{2}\left(1-\frac{1}{\sqrt{3}}\right),\frac{1}{2}\left(1+\frac{1}{\sqrt{3}}\right)\right\}$ . Thus:

$$\psi_1(x) = -\sqrt{3}x + \frac{1+\sqrt{3}}{2}$$
 (2.7a)

$$\psi_2(x) = \sqrt{3}x + \frac{1 - \sqrt{3}}{2}$$
 (2.7b)

$$\psi_1(1) = \frac{1 - \sqrt{3}}{2} \tag{2.8a}$$

$$\psi_2(1) = \frac{1+\sqrt{3}}{2}$$
 (2.8b)

$$\psi_1(1) \psi_1(1) = 1 - \frac{\sqrt{3}}{2}$$
 (2.9a)

$$\psi_1(1)\,\psi_2(1) = -\frac{1}{2}$$
 (2.9b)

$$\psi_2(1) \,\psi_2(1) = 1 + \frac{\sqrt{3}}{2}$$
 (2.9c)

$$\int_{m}^{m+1} \psi_1(x) dx = \frac{-\sqrt{3}}{2} (2m+1) + \frac{1+\sqrt{3}}{2} = \frac{1}{2} - m\sqrt{3}$$
 (2.10a)

$$\int_{m}^{m+1} \psi_2(x) dx = \frac{\sqrt{3}}{2} (2m+1) + \frac{1-\sqrt{3}}{2} = \frac{1}{2} + m\sqrt{3}$$
 (2.10b)

The WENO matrices are:

$$\begin{pmatrix} \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} - \sqrt{3} & \frac{1}{2} + \sqrt{3} \end{pmatrix}, \begin{pmatrix} \frac{1}{2} + \sqrt{3} & \frac{1}{2} - \sqrt{3} \\ \frac{1}{2} & \frac{1}{2} \end{pmatrix}$$
 (2.11)

The inverses are:

$$\frac{1}{\sqrt{3}} \begin{pmatrix} \sqrt{3} + \frac{1}{2} & -\frac{1}{2} \\ \sqrt{3} - \frac{1}{2} & \frac{1}{2} \end{pmatrix}, \frac{1}{\sqrt{3}} \begin{pmatrix} \frac{1}{2} & \sqrt{3} - \frac{1}{2} \\ -\frac{1}{2} & \sqrt{3} + \frac{1}{2} \end{pmatrix}$$
 (2.12)

The weights for both nodes are 0.5 so  $\int_0^1 \psi_i \psi_j dx = \frac{\delta_{ij}}{2}$  and  $\int_0^1 \psi_i \psi_j' dx = (-1)^j \frac{\sqrt{3}}{2}$ .

$$I_{11} - I_2^T = \frac{1}{2} \begin{pmatrix} 2 - \sqrt{3} & -1 \\ -1 & 2 + \sqrt{3} \end{pmatrix} - \frac{1}{2} \begin{pmatrix} -\sqrt{3} & -\sqrt{3} \\ \sqrt{3} & \sqrt{3} \end{pmatrix}$$

$$= \frac{1}{2} \begin{pmatrix} 2 & -(1 - \sqrt{3}) \\ -(1 + \sqrt{3}) & 2 \end{pmatrix}$$
(2.13)

$$(I_{11} - I_2^T)^{-1} = \frac{1}{3} \begin{pmatrix} 2 & 1 - \sqrt{3} \\ 1 + \sqrt{3} & 2 \end{pmatrix}$$
 (2.14)

Using a precalculated, analytical form of U in the DG predictor for N=1 obtains a ~30% speedup on Stokes' First Problem.

### 2.4 Operator Splitting

Noting that  $\frac{d\rho}{dt} = 0$  over the ODE time step, we must solve the following system:

$$\frac{dA_{ij}}{dt} = \frac{-\psi_{ij}}{\theta_1(\tau_1)} = \frac{-3}{\tau_1} |A|^{\frac{5}{3}} A \operatorname{dev}(G)$$
(2.15a)

$$\frac{dJ_i}{dt} = \frac{-H_i}{\theta_2(\tau_2)} = -\frac{1}{\tau_2} \frac{T\rho_0}{T_0\rho} J_i$$
(2.15b)

Many different solvers can be used to solve the homogeneous part of the system. So far, this has been tested with SLIC, WENO, and DG. A split-WENO scheme seems to be the fastest and most accurate method available. The results using split-WENO to solve Stokes' First Problem with N=1 are shown in 2.1. These results are comparable to the corresponding results using ADER-WENO, as seen in 2.2.

The results of using a 3rd-order split-WENO scheme to solve Stokes' First Problem are shown in 2.3. Note the close agreement with the Navier-Stokes solution, closely matching the result using ADER-WENO. The split-WENO scheme took 15 times less CPU time than the ADER-WENO scheme.

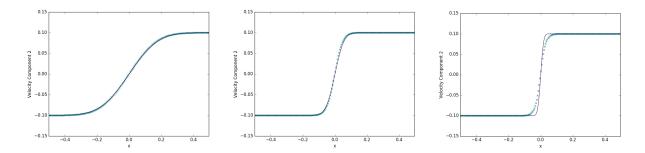


Figure 2.1: Results of solving Stokes' First Problem ( $\mu=10^{-2}, \mu=10^{-3}, \mu=10^{-4}$ ) with a split-WENO scheme (N=1)

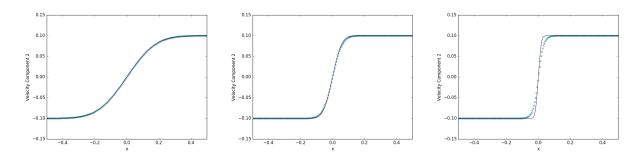


Figure 2.2: Results of solving Stokes' First Problem ( $\mu = 10^{-2}, \mu = 10^{-3}, \mu = 10^{-4}$ ) with a ADER-WENO scheme (N = 1)

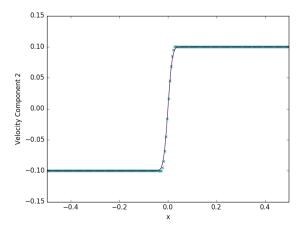


Figure 2.3: Results of solving Stokes' First Problem ( $\mu=10^{-4}$ ) with a split-WENO scheme (N=2)

#### 2.5 Distortion ODEs

#### 2.5.1 Linearized Distortion ODEs Solver

Note that  $A^* = \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}}I$  is a stationary point of the ODE for A. Linearizing the ODE around  $A^*$  gives:

$$\frac{dA}{dt} \approx J_A(A^*)(A - A^*)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{5}{3}} \left(\left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{in} \delta_{mj} + \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{jn} \delta_{im} + \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{im} \delta_{jn} - \frac{1}{3} \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{im} \delta_{jn} \delta_{kl} \delta_{kl} - \frac{2}{3} \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{ij} \delta_{mn}\right)$$

$$\times \left(A_{mn} - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right) \left(A_{mn} - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(A_{mn} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right) - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(\left(A_{ji} + A_{ij} - \frac{2}{3} \operatorname{tr}(A) \delta_{ij}\right) - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \left(\delta_{ij} + \delta_{ij} - 2\delta_{ij}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(A + A^T - \frac{2}{3} \operatorname{tr}(A) I\right)$$

The matrix for this system, in row-major form, is:

$$\frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \begin{pmatrix}
\frac{4}{3} & 0 & 0 & 0 & -\frac{2}{3} & 0 & 0 & 0 & -\frac{2}{3} \\
0 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
0 & 0 & 1 & 0 & 0 & 0 & 1 & 0 & 0 \\
0 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
-\frac{2}{3} & 0 & 0 & 0 & \frac{4}{3} & 0 & 0 & 0 & -\frac{2}{3} \\
0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\
0 & 0 & 1 & 0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\
-\frac{2}{3} & 0 & 0 & 0 & -\frac{2}{3} & 0 & 0 & 0 & \frac{4}{3}
\end{pmatrix} \tag{2.17}$$

The eigenvalues and eigenvectors are:

$$\{0, 0, 0, 0, -2k, -2k, -2k, -2k, -2k\} \tag{2.18}$$

where  $k = \frac{3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}}$ . Thus, the solution is:

$$\frac{A_{12} - A_{21}}{2} \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{A_{13} - A_{31}}{2} \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ -1 & 0 & 0 \end{pmatrix} + \frac{A_{23} - A_{32}}{2} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{pmatrix} \\
+ \frac{A_{11} + A_{22} + A_{33}}{3} \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \\
+ \frac{2A_{22} - A_{11} - A_{33}}{3} e^{-2kt} \begin{pmatrix} -1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{2A_{33} - A_{11} - A_{22}}{3} e^{-2kt} \begin{pmatrix} -1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \\
+ \frac{A_{12} + A_{21}}{2} e^{-2kt} \begin{pmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{A_{13} + A_{31}}{2} e^{-2kt} \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} + \frac{A_{23} + A_{32}}{2} e^{-2kt} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \end{pmatrix}$$

This is equal to:

$$\frac{1}{2}(A - A^{T}) + \frac{\operatorname{tr}(A)}{3}I + e^{-2kt}\left(\frac{1}{2}(A + A^{T}) - \frac{\operatorname{tr}(A)}{3}I\right)$$
 (2.21)

Results with Stokes' First Problem look good with this linearisation. The ODE step takes a negligible amount of time, meaning that if accuracy is maintained to second order, the solver is now fast enough.

#### 2.5.2 Linearized Reduced Distortion ODE Solver

Taking system (??), note that the Jacobian of the system is given by:

$$J = -k \begin{pmatrix} 4x_1 - x_2 - x_3 & -x_1 & -x_1 \\ -x_2 & 4x_2 - x_3 - x_1 & -x_3 \\ -x_3 & -x_3 & 4x_3 - x_1 - x_2 \end{pmatrix}$$
(2.22)

Evaluated at stationary point  $x_i = \sqrt[3]{c}$  we have:

$$J(\mathbf{x_0}) = -k\sqrt[3]{c} \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix}$$
 (2.23)

Thus, the system is linearized to:

$$\frac{dx}{dt} \approx -k\sqrt[3]{c} \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix} \begin{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} - \sqrt[3]{c} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \end{pmatrix} 
= k\sqrt[3]{c} \begin{pmatrix} -2 & 1 & 1 \\ 1 & -2 & 1 \\ 1 & 1 & -2 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$
(2.24)

The eigenvalues of this system matrix are  $\{-3k\sqrt[3]{c}, -3k\sqrt[3]{c}, 0\}$  and the eigenvectors are:

$$\begin{pmatrix} -1 \\ 0 \\ 1 \end{pmatrix}, \begin{pmatrix} 0 \\ -1 \\ 1 \end{pmatrix}, \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \tag{2.25}$$

Thus, the linearized solution is:

$$x(t) = \frac{-2x_1 + x_2 + x_3}{3} e^{-3k\sqrt[3]{c}t} \begin{pmatrix} -1\\0\\1 \end{pmatrix} + \frac{x_1 - 2x_2 + x_3}{3} e^{-3k\sqrt[3]{c}t} \begin{pmatrix} 0\\-1\\1 \end{pmatrix} + \frac{x_1 + x_2 + x_3}{3} \begin{pmatrix} 1\\1\\1 \end{pmatrix}$$
(2.26)

This may represent a faster way to calculate the evolution of the stretch terms of A. Note that some kind of normalization will probably be necessary, as:

$$\frac{x_1 + x_2 + x_3}{3} \ge (x_1 x_2 x_3)^{\frac{1}{3}} \tag{2.27}$$

with equality if and only if  $x_1 = x_2 = x_3$ .

#### Primitive WENO and DG Reconstruction 2.6

As suggested in [?], the WENO and DG can be performed in primitive variables, which is less computationally expensive than evaluating fluxes using conserved variables. Achieves around 20% speedup in DG step, at double cost in WENO step. Minimal speedup in FV step, as both primitive and conserved variables must be calculated for the flux updates. Not enough.

#### 2.7Change to Row-Major Ordering

The original GPR papers state the equations for A in column-major order, probably because the authors use Fortran. For C++ and Python implementations it is faster to work in row-major order. ~10% speedup was achieved by implementing this.

The GPR equations are:

$$\frac{\partial \rho}{\partial t} + \frac{\partial (\rho v_k)}{\partial x_k} = 0 \tag{2.28a}$$

$$\frac{\partial (\rho E)}{\partial t} + \frac{\partial (\rho E v_k + (p \delta_{ik} - \sigma_{ik}) v_i + q_k)}{\partial x_k} = 0$$

$$\frac{\partial (\rho v_i)}{\partial t} + \frac{\partial (\rho v_i v_k + p \delta_{ik} - \sigma_{ik})}{\partial x_k} = 0$$
(2.28b)

$$\frac{\partial (\rho v_i)}{\partial t} + \frac{\partial (\rho v_i v_k + p \delta_{ik} - \sigma_{ik})}{\partial x_k} = 0$$
 (2.28c)

$$\frac{\partial A_{ij}}{\partial t} + \frac{\partial (A_{ik}v_k)}{\partial x_j} + v_k \left( \frac{\partial A_{ij}}{\partial x_k} - \frac{\partial A_{ik}}{\partial x_j} \right) = -\frac{\psi_{ij}}{\theta_1(\tau_1)}$$
(2.28d)

$$\frac{\partial (\rho J_i)}{\partial t} + \frac{\partial (\rho J_i v_k + T \delta_{ik})}{\partial x_k} = -\frac{\rho H_i}{\theta_2(\tau_2)}$$
(2.28e)

Under row-major ordering, we have:

$$F_{1} = \begin{pmatrix} \rho v_{1} \\ \rho v_{1}E + v_{1}p - \sigma_{1m}v_{m} + q_{1} \\ \rho v_{1}^{2}E + v_{2}p - \sigma_{1m}v_{m} + q_{1} \\ \rho v_{1}^{2}P + p - \sigma_{11} \\ \rho v_{1}v_{2} - \sigma_{12} \\ \rho v_{1}v_{3} - \sigma_{13} \\ A_{1m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ 0 \\ 0 \\ \rho J_{1}v_{1} + T \\ \rho J_{2}v_{1} \\ \rho J_{3}v_{1} \end{pmatrix} \qquad F_{2} = \begin{pmatrix} \rho v_{2} \\ \rho v_{2}E + v_{2}p - \sigma_{2m}v_{m} + q_{2} \\ \rho v_{2}V_{3} - \sigma_{21} \\ \rho v_{2}v_{3} - \sigma_{22} \\ \rho v_{2}v_{3} - \sigma_{23} \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ \rho J_{1}v_{2} \\ \rho J_{2}v_{2} + T \\ \rho J_{3}v_{2} \end{pmatrix} \qquad F_{3} = \begin{pmatrix} \rho v_{3} \\ \rho v_{3}E + v_{3}p - \sigma_{3m}v_{m} + q_{3} \\ \rho v_{1}v_{3} - \sigma_{31} \\ \rho v_{2}v_{3} - \sigma_{32} \\ \rho v_{2}^{2}P - \sigma_{33} \\ 0 \\ 0 \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ \rho J_{1}v_{3} \\ \rho J_{2}v_{3} \\ \rho J_{3}v_{3} + T \end{pmatrix}$$

$$S = -\frac{1}{\theta_{1}(\tau_{1})} \begin{pmatrix} 0\\0\\0\\0\\0\\\psi_{11}\\\psi_{12}\\\psi_{13}\\\psi_{21}\\\psi_{22}\\\psi_{23}\\\psi_{33}\\0\\0\\0\\0\end{pmatrix} - \frac{1}{\theta_{2}(\tau_{2})} \begin{pmatrix} 0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\\rho H_{1}\\\rho H_{2}\\\rho H_{3} \end{pmatrix}$$
(2.34)

$$\Psi_{ij} = \rho v_i v_j - \sigma_{ij} \tag{2.35a}$$

$$\Psi_{ij} = \rho v_i v_j - \sigma_{ij}$$

$$\Phi_{ij}^k = \rho v_k \psi_{ij} - v_m \frac{\partial \sigma_{mk}}{\partial A_{ij}}$$
(2.35a)

$$\Omega_i = v_i \left( E + \rho E_\rho \right) - \frac{\sigma_{im} v_m}{\rho} + T_\rho H_i \tag{2.35c}$$

$$\Upsilon = \frac{\|\boldsymbol{v}\|^2 + \boldsymbol{H} \cdot \boldsymbol{J} - E - \rho E_{\rho}}{\rho E_p}$$
 (2.35d)

$$\tilde{\boldsymbol{H}} = E_{\boldsymbol{J}\boldsymbol{J}} \tag{2.35e}$$



 $\begin{smallmatrix} p_2 \\ p_2 \\ p_3 \\ p_4 \\ p_5 \\ p_6 \\ p_7 \\ p_8 \\ p_$  $\begin{matrix} 1 \\ + \rho E_t \\ v_1 \\ v_2 \\ v_3 \\ v_3 \\ v_3 \\ v_4 \\ v_4 \\ v_5 \\ v_6 \\$  $\frac{\partial Q}{\partial P}$ 

2.37

 $\frac{\partial P}{\partial Q}$ 

	0	$\rho v_1  H_3$	0	0	0	0	00	0	00	0	0 0	0 0	$\rho v_1$
CHAPTER 2.	FASTER SOLVERS	$\rho v_1 H_2$	0	0	0	0	0	0	0 0	0	0 0	0	0

S	$\rho v_1 H$	0	0	0	0	0	0	0	0	0	0	0	0	0	$\rho v_1$	0	
0	$\left(  ho v_1 H_1 + T  ilde{H}_1  ight)$	0	0	0	0	0	0	0	0	0	0	0	0	$\rho v_1$	0	0	(00 0)
0	$\Phi^1_{33}$	$-\frac{\partial \sigma_{11}}{A_{33}}$	$-\frac{\partial \sigma_{12}}{A_{33}}$	$-\frac{\partial \sigma_{13}}{A_{33}}$	0	0	0	0	0	0	$v_3$	0	0	0	0	0	
0	$\Phi^1_{32}$	$-\frac{\partial \sigma_{11}}{A_{32}}$	$-\frac{\partial \sigma_{12}}{A_{32}}$	$-\frac{\partial \sigma_{13}}{A_{32}}$	0	0	0	0	0	0	$v_2$	0	0	0	0	0	
0	$\Phi^1_{31}$	$-\frac{\partial \sigma_{11}}{A_{31}}$	$-\frac{\partial \sigma_{12}}{A_{31}}$	$-\frac{\partial \sigma_{13}}{A_{31}}$	.0	0	0	0	0	0	$v_1$	0	0	0	0	0	
0	$\Phi^1_{23}$	$-\frac{\partial \sigma_{11}}{A_{23}}$	$-\frac{\partial \sigma_{12}^{2}}{A_{23}}$	$-\frac{\partial \sigma_{13}^{2}}{A_{23}}$	0.0	0	0	$v_3$	0	0	0	0	0	0	0	0	
0	$\Phi^1_{22}$	$-\frac{\partial \sigma_{111}}{A_{22}}$	$-\frac{\partial \sigma_{12}}{A_{22}}$	$-\frac{\partial \sigma_{13}}{A_{22}}$	0	0	0	$v_2$	0	0	0	0	0	0	0	0	
0	$\Phi^1_{21}$	$-\frac{\partial \sigma_{111}}{A_{21}}$	$-\frac{\partial \tilde{\sigma_{12}}}{A_{21}}$	$-\frac{\partial \sigma_{13}^2}{A_{21}}$	0.21	0	0	$v_1$	0	0	0	0	0	0	0	0	
0	$\Phi^1_{13}$	$-\frac{\partial \sigma_{11}}{A_{13}}$	$-\frac{\partial \sigma_{12}}{A_{13}}$	$-\frac{\partial \sigma_{13}^{2}}{A_{13}}$	$v_3$	0	0	0	0	0	0	0	0	0	0	0	
		$-\frac{\partial \sigma_{11}}{A_{12}}$															
0	$\Phi^1_{11}$	$-\frac{\partial \sigma_{11}}{A_{11}}$	$-\frac{\partial \sigma_{12}^2}{A_{11}}$	$-\frac{\partial \sigma_{13}^2}{A_{11}}$	$v_1$	0	0	0	0	0	0	0	0	0	0	0	
0	$\Psi_{13}$	0	0	$\rho v_1$	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	0	
0	$\Psi_{12}$	0	$\rho v_1$	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	0	0	
θ	$(\Psi_{11}+\rho E+p)$	$2\rho v_1$	$ ho v_2$	$\rho v_3$	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	$\rho J_1$	$\rho J_2$	$\rho J_3$	
0	$(v_1 (\rho E_p + 1) + T_p H_1)$	1	0	0	0	0	0	0	0	0	0	0	0	$T_p$	0	0	
$/$ $v_1$	$\Omega_1$	$\frac{\Psi_{11}}{\rho}$	$\frac{\Psi^{'}12}{\rho}$	₩ <u>13</u>	.0	0	0	0	0	0	0	0	0	$v_1 J_1 + T_{ ho}$	$v_1J_2$	$\langle v_1 J_3 \rangle$	
						E G	$\frac{OF_1}{}$ =	$\partial P$				_					

		0	$\rho v_2 H_3$	0	0	0	0	0 0	0	0	0	0 0	0	0	0	P 02
CHAPTER 2.	FASTER SOLVER	RS	$r ilde{H}_2ig)$	`												
		0	$\left(\rho v_2 H_2 + 5\right)$	0	0	0	0	0 0	0	0	0	0 0	0	0	$\rho v_2$	(2.39)
		0	$\rho v_2 H_1$	0	0	0	0	0 0	0	0	0	0 0	0	$\rho v_2$	0 0	Þ
		0	$\Phi_{33}^2$	$-\frac{\partial \sigma_{21}}{A_{33}}$	$-\frac{\partial \sigma_{22}}{A_{33}}$	$-\frac{\partial \sigma_{23}}{A_{33}}$	0	00	0	0	0	0 %	° o	0	0 0	>
		0	$\Phi^2_{32}$	$-\frac{\partial \sigma_{21}}{A_{32}}$	$-\frac{\partial \sigma_{22}}{A_{32}}$	$-\frac{\partial \sigma_{23}}{A_{32}}$	0	0 0	0	0	0	0 %	0 0	0	0 0	Þ
		0	$\Phi_{31}^2$	$-\frac{\partial \sigma_{21}}{A_{31}}$	$-\frac{\partial \sigma_{22}}{A_{31}}$	$-\frac{\partial \sigma_{23}}{A_{31}}$	0	0 0	0	0	0	0 %	0	0	0 0	Þ
		0	$\Phi_{23}^2$	$-\frac{\partial \sigma_{21}}{A_{23}}$	$-\frac{\partial \sigma_{22}}{A_{23}}$	$-\frac{\partial \sigma_{23}}{A_{23}}$	0	0 0	0	$v_3$	0	0 0	0	0	0 0	Þ
		0	$\Phi^2_{22}$	$-\frac{\partial \sigma_{21}}{A_{22}}$	$-\frac{\partial \sigma_{22}}{A_{22}}$	$-\frac{\partial \sigma_{23}}{A_{22}}$	0	00	0	$v_2$	0	00	0	0	0 0	Þ
		0	$\Phi_{21}^2$	$-\frac{\partial \sigma_{21}}{A_{21}}$	$-\frac{\partial \sigma_{22}}{A_{21}}$	$-\frac{\partial \sigma_{23}^{2}}{A_{21}}$	0	0 0	0	$v_1$	0	o c	0	0	0 0	Þ
		0	$\Phi^2_{13}$	$-\frac{\partial \sigma_{21}}{A_{13}}$	$-\frac{\partial \sigma_{22}}{A_{13}}$	$-\frac{\partial \sigma_{23}}{A_{13}}$	0	<i>v</i> <sub>3</sub>	0	0	0	0 0	0	0	0 0	Þ
		0	$\Phi_{12}^2$	$-\frac{\partial \sigma_{21}}{A_{12}}$	$-\frac{\partial \sigma_{22}}{A_{12}}$	$-\frac{\partial \sigma_{23}}{A_{12}}$	0	$c_2$	0	0	0	00	0	0	0 0	Þ
		0	$\Phi_{11}^2$	$-\frac{\partial \sigma_{21}}{A_{11}}$	$-\frac{\partial \sigma_{22}}{A_{11}}$	$-\frac{\partial \sigma_{23}^{23}}{A_{11}}$	0	$c_1^0$	0	0	0	0 0	0	0	0 0	Þ
				0	0	$\rho v_2$	0.	$A_{13} = 0$	0	$A_{23}$	0	O A	0	0	0 0	
		d	$(\Psi_{22}+\rho E+p)$	$\rho v_1$	$2\rho v_2$	$\rho v_3$	0.	$A_{12} $	0	$A_{22}$	0	9.3	0	$ ho J_1$	$ ho J_2$	
		0	$\Psi_{21}$	$\rho v_2$	0	0	0 .	$A_{11}$	0	$A_{21}$	0	O A	0	0	0 0	>
		0	$(v_2 (\rho E_p + 1) + T_p H_2)$	0	1	0	0	0 0	0	0	0	0 0	0	0	$T_p$	Þ
		, 02	$\Omega_2$	$\frac{\Psi_{21}}{\rho}$	$\frac{\Psi_{22}}{\rho}$	<u>₩23</u>	.0	0 0	0	0	0	o c	0	$v_2J_1$	$v_2 J_2 + T_{ ho}$	2203
		,						$\partial F_2$								

		$\Gamma( ilde{H}_3)$
CHAPTER 2.	FASTER SOLVEI	$(p_{0})^{2} = (p_{0})^{2} + (p_{0})^{2} = (p_{0})^{2} + (p_{0})^{2} = $
		$ \rho v_3 H_2 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0$
		ho  otag bar = 0   ho  otag b
		$\begin{array}{c} \Phi_3 \\ \Phi_3 \\ \Phi_{333} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Phi_{33} \\ \Phi_{332} \\ \theta_{332} \\ \theta_{332} \\ \end{array}$ $\begin{array}{c} -\frac{\beta\sigma_{33}}{2} \\ -\frac{\beta\sigma_{33}}{2} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Phi_{3} \\ \Phi_{3} \\ \theta_{31} \\ \theta_{31} \\ \theta_{31} \\ \theta_{31} \\ \theta_{31} \\ \theta_{32} \\ \theta_{33} \\ \theta_{31} \\ \theta_{11} \\ \theta_{12} \\ \theta_{13} \\ \theta_{13} \\ \theta_{14} \\ \theta_{15} $
		$\begin{array}{c} \Phi_{33} \\ \Phi_{23} \\ \theta_{23} \\ \theta_{23$
		$\begin{array}{c} \Phi_3^3 \\ \Phi_{22}^3 \\ \theta_{22} \\ \theta_{33} \\ \theta_{32} \\ \theta_{33} \\ \theta_{34} \\ \theta_{35} \\ \theta_{3$
		$\begin{array}{c} \Phi_3 \\ \Phi_3 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Phi_{33} \\ 0 \\ 1_{13} \\ 0 \\ 0 \\ 1_{33} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Phi_3 \\ \Phi_{112} \\ 0 \\ 0 \\ 112 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Phi_{3} \\ \Phi_{11} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} 0 \\ \Psi_{33} + \rho E + p) \\ \rho v_1 \\ \rho v_2 \\ 2\rho v_3 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ A_{33} \\ \rho J_1 \\ \rho J_2 \\ \rho J_3 \\ \rho J_4 \end{array}$
		$ \begin{array}{c} \Psi_{32} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \rho \\ V_{311} \\ \rho v_3 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$(v_3 (\rho E_p + 1) + T_p H_3)$ $0$ $0$ $1$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$
		$\begin{pmatrix} v_3 \\ \Omega_3 \\ \frac{\Psi_{31}}{\sqrt{\rho}} \\ \frac{\psi_{\beta}}{\sqrt{\rho}} \\ \frac{\psi_{\beta}}{\sqrt{\rho}} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$
		$rac{\partial oldsymbol{F_3}}{\partial oldsymbol{P}} =$

00	_	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$ /	(2.41)
0	>	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$	0	
0 T 2.2 T	ıαı	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$	0	0	
0 0	<b>D</b>	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{33}}$	.⊢I o	$-\frac{1}{\rho}\frac{\partial \sigma_{13}}{\partial A_{23}}$	0	0	0	0	0	0	0	0	$v_1$	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{12}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{13}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_1$	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{12}}{\partial A_{21}}$	$\frac{1}{\rho} \frac{\partial \sigma_{13}}{\partial A_{31}}$	0	0	0	0	0	0	$v_1$	0	0	0	0	0	
0	0	$\frac{\partial \sigma_1}{\partial A_2}$	300 I	$-\frac{1}{\rho}\frac{\partial \sigma_{13}}{\partial A_{23}}$		0	0	0	0	$v_1$	0	0	0	0	0	0	
0 0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{13}}{\partial A_{22}}$	0	0	0	0	$v_1$	0	0	0	0	0	0	0	
0 0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{21}}$		$-\frac{1}{\rho}\frac{\partial \sigma_{13}}{\partial A_{21}}$	0	0	0	$v_1$	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{12}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{13}}{\partial A_{13}}$	0	0	$v_1$	0	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{12}}$	$-\frac{1}{9}\frac{\partial \sigma_{12}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{12}}$	0	$v_1$	0	0	0	0	0	0	0	0	0	0	
0	>	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{12}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{11}}$	$v_1$	0	0	0	0	0	0	0	0	0	0	0	
0	)	0	0	$v_1$	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	0	
0	>	0	$v_1$	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	0	0	
θ	$\Delta L$	$v_1$	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	0	0	
0 ;	$v_1$	<u>1</u>	0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(\infty a + a)^o}$	0	0	
$\begin{pmatrix} v_1 \\ 0 \end{pmatrix}$	) 	$-\frac{\sigma_{11}}{o^2}$	$-\frac{\sigma_{12}^{r}}{\sigma_{22}^{r}}$	$-\frac{\sigma_{13}}{\sigma^2}$	0	0	0	0	0	0	0	0	0	$-\frac{T}{o^2}$	0	o /	
								$M_1 =$									

_	_	_	_	_	_	_	_	_	_	_	_	_	_	_	_ <	2.42)
$^{\circ}_{ZT}$	0	0 (	0 (	0 (	0	0	0 (	0	0 (	0 (	0	0 (	0	2 (	y v	٣
$\begin{array}{ccc} & & 0 \\ & & \Gamma \alpha^2 T \end{array}$	0	0 (	0			0								$0$ $v_2$		
00	21 (	0 8 8 8	) [2]		0								v	0	0	
0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{33}}$	$-\frac{1}{\rho}\frac{\partial\sigma}{\partial A}$	$-\frac{1}{\rho}\frac{\partial\sigma}{\partial A}$	0	0	0	0	0	0	0	0	$v_2$	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{22}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}^{23}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_2$	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{22}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}^{23}}{\partial A_{31}}$	0	0	0	0	0	0	$v_2$	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{23}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{22}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}}{\partial A_{23}}$	0	0	0	0	0	$v_2$	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho} \frac{\partial \sigma_{21}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{22}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}^{23}}{\partial A_{22}}$	0	0	0	0	$v_2$	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}^{23}}{\partial A_{21}}$	0	0	0	$v_2$	0	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}}{\partial A_{13}}$	0	0	$v_2$	0	0	0	0	0	0	0	0	0	
	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{12}}$						0	0	0	0	0	0	0	0	0	
0 0	$\frac{1}{\rho} \frac{\partial \sigma_{21}}{\partial A_{11}}$						0	0	0	0	0	0	0	0	0	
0 0	0	0	$v_2$	0	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	
$\frac{d\lambda}{d}$	0	$v_2$	0	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	0	
0 0	$v_2$	0	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	0	
$v_2$	0	H 0	0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(a+a)o}$	0	
$\begin{pmatrix} v_2 \\ 0 \end{pmatrix}$	$-\frac{\sigma_{21}}{\sigma^2}$	$-\frac{\sigma_{22}^{r}}{\sigma^{22}}$	$-\frac{\sigma_{23}^{r}}{\rho^{2}}$	0	0	0	0	0	0	0	0	0	0	$-\frac{T}{o^2}$	· o	
							$M_2 =$									

$\Gamma lpha^2 T$		_	_	_	_	_	_	_	_	0	_	_	_	_	3	(2.43)
$\Gamma_{\alpha}$	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$\dot{v}$	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	0	
0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	0	0	
0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{33}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{33}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{33}}$	0	0	0	0	0	0	0	0	$v_3$	0	0	0	
0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_3$	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{31}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{31}}$	0	0	0	0	0	0	$v_3$	0	0	0	0	0	
0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{23}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}^{23}}{\partial A_{23}}$	0	0	0	0	0	$v_3$	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{22}}$	0	0	0	0	$v_3$	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}^2}{\partial A_{21}}$	0	0	0	$v_3$	0	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{32}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{13}}$	0	0	$v_3$	0	0	0	0	0	0	0	0	0	
0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{12}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{12}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{13}}$	0	$v_3$	0	0	0	0	0	0	0	0	0	0	
0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{32}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}^{23}}{\partial A_{11}}$	$v_3$	0	0	0	0	0	0	0	0	0	0	0	
$\frac{d\lambda}{d}$	0	0	$v_3$	0	0	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	
0 0	0	$v_3$	0	0	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	
0 0	$v_3$	0	0	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	
0	0	0	110	0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(n+n)o}$	34-434
$\begin{pmatrix} v_3 \\ 0 \end{pmatrix}$	$-\frac{\sigma_{31}}{\sigma^2}$	$-\frac{\sigma_{32}^r}{\sigma^2}$	$-\frac{\sigma_{33}^2}{\sigma_2^2}$	0	0	0	0	0	0	0	0	0	0	0		r
							$M_3 =$									

## Slow Flow

### 3.1 Studying numerical smearing with slow flow past a barrier

A checkerboard pattern appears around the corner of the barrier, leading to a crash, using reflective boundary conditions (in velocity) for the barrier. Do we need a staggered grid?

## RGFM

The RGFM does nothing without a temperature fix when applied to the heat conduction test. The linearisation upon which it is based results in a stationary solution when  $q_L = q_R$  and  $\sigma_L = \sigma_R$  initially. Barton's RGFM is similar. Should q be fixed? Maybe use analytical solution to heat equation at  $t = \Delta t$ ?

# Bibliography