Lab Notes

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January 24, 2017

# Contents

1	To :	Do	2
	1.1	Coding	2
	1.2	Theoretical	2
	1.3	Papers	2
2	Fas	ter Solvers	3
	2.1	Fast WENO Oscillation Indicator Calculation	3
	2.2	Approximating Interface Terms in FV	4
	2.3	Analytical Results for Basis Vectors	4
	2.4	Operator Splitting	5
	2.5	Distortion ODEs	7
		2.5.1 Linearized Distortion ODEs Solver	7
		2.5.2 Linearized Reduced Distortion ODE Solver	8
	2.6	Primitive WENO and DG Reconstruction	9
	2.7	Change to Row-Major Ordering	9
3	Slov	w Flow	21
	3.1	Studying numerical smearing with slow flow past a barrier	21
4	RG	FM	22

## To Do

### 1.1 Coding

- Test split-WENO in 2D
- Implement in CUDA
- Solid EOSs
- Implement Barton's damage model
- Test compressible Euler vs GPR use narrowing domain from Toro's book
- Try conservative formulation [Peshkov,Grmela,Romenski]

### 1.2 Theoretical

- Investiage approximate Riemann solvers (e.g. Dumbser's HLLEM)
- Convergence of conservation of mass in RGFM

## 1.3 Papers

- Isobaric cookoff (make cookoff the focus)
- Split solver vs ADER-WENO
- Application of ADER-WENO to Barton's solid model (with Tome)
- HPR-RGFM paper (solve stationarity of interface solver under some conditions)
- Application of ADER-WENO to equations in other areas of Physics, Biology, & Economics

## Faster Solvers

### 2.1 Fast WENO Oscillation Indicator Calculation

The WENO oscillation indicator is defined as:

$$o = \Sigma_{mn} w_m w_n \tag{2.1}$$

where  $w_i$  are the WENO coefficients calculated for a particular stencil, and:

$$\Sigma_{mn} = \sum_{\alpha=1}^{N} \int_{0}^{1} \psi_{m}^{(\alpha)} \psi_{n}^{(\alpha)} \tag{2.2}$$

By considering that:

$$o = \sum_{\alpha=1}^{N} \int_{0}^{1} \left( \frac{d^{\alpha} w}{dx^{\alpha}} \right)^{2} > 0$$
 (2.3)

we have that  $\Sigma$  is symmetric positive definite. Thus, it has a Cholesky decomposition  $\Sigma = LL^T$ . Thus:

$$o = \left\| w^T L \right\|^2 \tag{2.4}$$

L can be precalculated, and o calculated quickly as:

```
1: o = 0

2: \mathbf{for} \ j = 1...n \ \mathbf{do}

3: tmp = 0

4: \mathbf{for} \ i = j...n \ \mathbf{do}

5: tmp = tmp + w(i) * L(i,j)

6: \mathbf{end} \ \mathbf{for}

7: o = o + tmp * tmp

8: \mathbf{end} \ \mathbf{for}
```

### 2.2 Approximating Interface Terms in FV

Instead of calculating the following:

$$\int D(q^{-}(x_{0},t),q^{+}(x_{0},t)) dt$$
(2.5)

I propose calculating the following:

$$D\left(\frac{1}{\Delta t} \int q^{-}\left(x_{0}, t\right) dt, \frac{1}{\Delta t} \int q^{+}\left(x_{0}, t\right) dt\right)$$

$$(2.6)$$

This obtains a large speedup with no discernable difference in the results of Stokes' First Problem.

### 2.3 Analytical Results for Basis Vectors

For N=1, the Gauss-Legendre nodes on [0,1] are  $\left\{\frac{1}{2}\left(1-\frac{1}{\sqrt{3}}\right),\frac{1}{2}\left(1+\frac{1}{\sqrt{3}}\right)\right\}$ . Thus:

$$\psi_1(x) = -\sqrt{3}x + \frac{1+\sqrt{3}}{2}$$
 (2.7a)

$$\psi_2(x) = \sqrt{3}x + \frac{1 - \sqrt{3}}{2}$$
 (2.7b)

$$\psi_1(1) = \frac{1 - \sqrt{3}}{2} \tag{2.8a}$$

$$\psi_2(1) = \frac{1+\sqrt{3}}{2}$$
 (2.8b)

$$\psi_1(1) \psi_1(1) = 1 - \frac{\sqrt{3}}{2}$$
 (2.9a)

$$\psi_1(1)\,\psi_2(1) = -\frac{1}{2}$$
 (2.9b)

$$\psi_2(1) \,\psi_2(1) = 1 + \frac{\sqrt{3}}{2}$$
 (2.9c)

$$\int_{m}^{m+1} \psi_1(x) dx = \frac{-\sqrt{3}}{2} (2m+1) + \frac{1+\sqrt{3}}{2} = \frac{1}{2} - m\sqrt{3}$$
 (2.10a)

$$\int_{m}^{m+1} \psi_2(x) dx = \frac{\sqrt{3}}{2} (2m+1) + \frac{1-\sqrt{3}}{2} = \frac{1}{2} + m\sqrt{3}$$
 (2.10b)

The WENO matrices are:

$$\begin{pmatrix} \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} - \sqrt{3} & \frac{1}{2} + \sqrt{3} \end{pmatrix}, \begin{pmatrix} \frac{1}{2} + \sqrt{3} & \frac{1}{2} - \sqrt{3} \\ \frac{1}{2} & \frac{1}{2} \end{pmatrix}$$
 (2.11)

The inverses are:

$$\frac{1}{\sqrt{3}} \begin{pmatrix} \sqrt{3} + \frac{1}{2} & -\frac{1}{2} \\ \sqrt{3} - \frac{1}{2} & \frac{1}{2} \end{pmatrix}, \frac{1}{\sqrt{3}} \begin{pmatrix} \frac{1}{2} & \sqrt{3} - \frac{1}{2} \\ -\frac{1}{2} & \sqrt{3} + \frac{1}{2} \end{pmatrix}$$
 (2.12)

The weights for both nodes are 0.5 so  $\int_0^1 \psi_i \psi_j dx = \frac{\delta_{ij}}{2}$  and  $\int_0^1 \psi_i \psi_j' dx = (-1)^j \frac{\sqrt{3}}{2}$ .

$$I_{11} - I_2^T = \frac{1}{2} \begin{pmatrix} 2 - \sqrt{3} & -1 \\ -1 & 2 + \sqrt{3} \end{pmatrix} - \frac{1}{2} \begin{pmatrix} -\sqrt{3} & -\sqrt{3} \\ \sqrt{3} & \sqrt{3} \end{pmatrix}$$

$$= \frac{1}{2} \begin{pmatrix} 2 & -(1 - \sqrt{3}) \\ -(1 + \sqrt{3}) & 2 \end{pmatrix}$$
(2.13)

$$(I_{11} - I_2^T)^{-1} = \frac{1}{3} \begin{pmatrix} 2 & 1 - \sqrt{3} \\ 1 + \sqrt{3} & 2 \end{pmatrix}$$
 (2.14)

Using a precalculated, analytical form of U in the DG predictor for N=1 obtains a ~30% speedup on Stokes' First Problem.

### 2.4 Operator Splitting

Noting that  $\frac{d\rho}{dt} = 0$  over the ODE time step, we must solve the following system:

$$\frac{dA_{ij}}{dt} = \frac{-\psi_{ij}}{\theta_1(\tau_1)} = \frac{-3}{\tau_1} |A|^{\frac{5}{3}} A \operatorname{dev}(G)$$
(2.15a)

$$\frac{dJ_i}{dt} = \frac{-H_i}{\theta_2(\tau_2)} = -\frac{1}{\tau_2} \frac{T\rho_0}{T_0\rho} J_i$$
(2.15b)

Many different solvers can be used to solve the homogeneous part of the system. So far, this has been tested with SLIC, WENO, and DG. A split-WENO scheme seems to be the fastest and most accurate method available. The results using split-WENO to solve Stokes' First Problem with N=1 are shown in 2.1. These results are comparable to the corresponding results using ADER-WENO, as seen in 2.2.

The results of using a 3rd-order split-WENO scheme to solve Stokes' First Problem are shown in 2.3. Note the close agreement with the Navier-Stokes solution, closely matching the result using ADER-WENO. The split-WENO scheme took 15 times less CPU time than the ADER-WENO scheme.

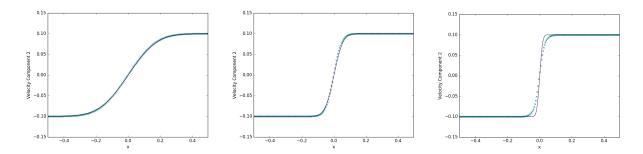


Figure 2.1: Results of solving Stokes' First Problem ( $\mu=10^{-2}, \mu=10^{-3}, \mu=10^{-4}$ ) with a split-WENO scheme (N=1)

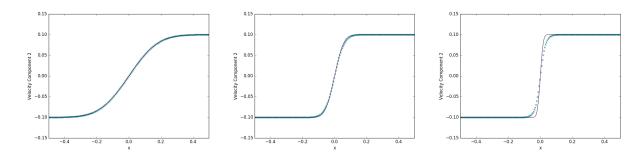


Figure 2.2: Results of solving Stokes' First Problem ( $\mu = 10^{-2}, \mu = 10^{-3}, \mu = 10^{-4}$ ) with a ADER-WENO scheme (N = 1)

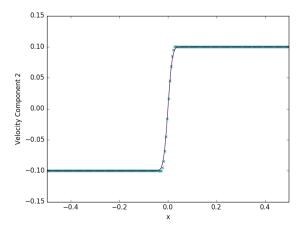


Figure 2.3: Results of solving Stokes' First Problem ( $\mu = 10^{-4}$ ) with a split-WENO scheme (N = 2)

#### 2.5 Distortion ODEs

#### 2.5.1 Linearized Distortion ODEs Solver

Note that  $A^* = \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} I$  is a stationary point of the ODE for A. Linearizing the ODE around  $A^*$  gives:

$$\frac{dA}{dt} \approx J_A(A^*)(A - A^*) \qquad (2.16)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{5}{3}} \left(\left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{in} \delta_{mj} + \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{jn} \delta_{im} + \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{im} \delta_{jn} - \frac{1}{3} \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{im} \delta_{jn} \delta_{kl} \delta_{kl} - \frac{2}{3} \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{ij} \delta_{mn}\right)$$

$$\times \left(A_{mn} - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right) \left(A_{mn} - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(A_{mn} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right) - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(\left(A_{ji} + A_{ij} - \frac{2}{3} \operatorname{tr}(A) \delta_{ij}\right) - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \left(\delta_{ij} + \delta_{ij} - 2\delta_{ij}\right)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(A + A^T - \frac{2}{3} \operatorname{tr}(A) I\right)$$

The matrix for this system, in row-major form, is:

$$\frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \begin{pmatrix}
\frac{4}{3} & 0 & 0 & 0 & -\frac{2}{3} & 0 & 0 & 0 & -\frac{2}{3} \\
0 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
0 & 0 & 1 & 0 & 0 & 0 & 1 & 0 & 0 \\
0 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
-\frac{2}{3} & 0 & 0 & 0 & \frac{4}{3} & 0 & 0 & 0 & -\frac{2}{3} \\
0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\
0 & 0 & 1 & 0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\
-\frac{2}{3} & 0 & 0 & 0 & -\frac{2}{3} & 0 & 0 & 0 & \frac{4}{3}
\end{pmatrix} \tag{2.17}$$

The eigenvalues and eigenvectors are:

$$\{0, 0, 0, 0, -2k, -2k, -2k, -2k, -2k\} \tag{2.18}$$

where  $k = \frac{3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}}$ . Thus, the solution is:

$$\frac{A_{12} - A_{21}}{2} \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{A_{13} - A_{31}}{2} \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ -1 & 0 & 0 \end{pmatrix} + \frac{A_{23} - A_{32}}{2} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{pmatrix} \\
+ \frac{A_{11} + A_{22} + A_{33}}{3} \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \\
+ \frac{2A_{22} - A_{11} - A_{33}}{3} e^{-2kt} \begin{pmatrix} -1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{2A_{33} - A_{11} - A_{22}}{3} e^{-2kt} \begin{pmatrix} -1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \\
+ \frac{A_{12} + A_{21}}{2} e^{-2kt} \begin{pmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{A_{13} + A_{31}}{2} e^{-2kt} \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} + \frac{A_{23} + A_{32}}{2} e^{-2kt} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \end{pmatrix}$$

This is equal to:

$$\frac{1}{2}(A - A^{T}) + \frac{\operatorname{tr}(A)}{3}I + e^{-2kt}\left(\frac{1}{2}(A + A^{T}) - \frac{\operatorname{tr}(A)}{3}I\right)$$
(2.21)

Results with Stokes' First Problem look good with this linearisation. The ODE step takes a negligible amount of time, meaning that if accuracy is maintained to second order, the solver is now fast enough.

#### 2.5.2 Linearized Reduced Distortion ODE Solver

Taking system (??), note that the Jacobian of the system is given by:

$$J = -k \begin{pmatrix} 4x_1 - x_2 - x_3 & -x_1 & -x_1 \\ -x_2 & 4x_2 - x_3 - x_1 & -x_3 \\ -x_3 & -x_3 & 4x_3 - x_1 - x_2 \end{pmatrix}$$
(2.22)

Evaluated at stationary point  $x_i = \sqrt[3]{c}$  we have:

$$J(\mathbf{x_0}) = -k\sqrt[3]{c} \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix}$$
 (2.23)

Thus, the system is linearized to:

$$\frac{dx}{dt} \approx -k\sqrt[3]{c} \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix} \begin{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} - \sqrt[3]{c} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \end{pmatrix} 
= k\sqrt[3]{c} \begin{pmatrix} -2 & 1 & 1 \\ 1 & -2 & 1 \\ 1 & 1 & -2 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$
(2.24)

The eigenvalues of this system matrix are  $\{-3k\sqrt[3]{c}, -3k\sqrt[3]{c}, 0\}$  and the eigenvectors are:

$$\begin{pmatrix} -1\\0\\1 \end{pmatrix}, \begin{pmatrix} 0\\-1\\1 \end{pmatrix}, \begin{pmatrix} 1\\1\\1 \end{pmatrix} \tag{2.25}$$

Thus, the linearized solution is:

$$\boldsymbol{x}(t) = \frac{-2x_1 + x_2 + x_3}{3} e^{-3k\sqrt[3]{c}t} \begin{pmatrix} -1\\0\\1 \end{pmatrix} + \frac{x_1 - 2x_2 + x_3}{3} e^{-3k\sqrt[3]{c}t} \begin{pmatrix} 0\\-1\\1 \end{pmatrix} + \frac{x_1 + x_2 + x_3}{3} \begin{pmatrix} 1\\1\\1 \end{pmatrix}$$
(2.26)

This may represent a faster way to calculate the evolution of the stretch terms of A. Note that some kind of normalization will probably be necessary, as:

$$\frac{x_1 + x_2 + x_3}{3} \ge (x_1 x_2 x_3)^{\frac{1}{3}} \tag{2.27}$$

with equality if and only if  $x_1 = x_2 = x_3$ .

#### Primitive WENO and DG Reconstruction 2.6

As suggested in [?], the WENO and DG can be performed in primitive variables, which is less computationally expensive than evaluating fluxes using conserved variables. Achieves around 20% speedup in DG step, at double cost in WENO step. Minimal speedup in FV step, as both primitive and conserved variables must be calculated for the flux updates. Not enough.

#### 2.7Change to Row-Major Ordering

The original GPR papers state the equations for A in column-major order, probably because the authors use Fortran. For C++ and Python implementations it is faster to work in row-major order. ~10% speedup was achieved by implementing this.

The GPR equations are:

$$\frac{\partial \rho}{\partial t} + \frac{\partial \left(\rho v_k\right)}{\partial x_k} = 0 \tag{2.28a}$$

$$\frac{\partial (\rho E)}{\partial t} + \frac{\partial (\rho E v_k + (p \delta_{ik} - \sigma_{ik}) v_i + q_k)}{\partial x_k} = 0$$

$$\frac{\partial (\rho v_i)}{\partial t} + \frac{\partial (\rho v_i v_k + p \delta_{ik} - \sigma_{ik})}{\partial x_k} = 0$$
(2.28b)

$$\frac{\partial (\rho v_i)}{\partial t} + \frac{\partial (\rho v_i v_k + p \delta_{ik} - \sigma_{ik})}{\partial x_k} = 0$$
 (2.28c)

$$\frac{\partial A_{ij}}{\partial t} + \frac{\partial (A_{ik}v_k)}{\partial x_j} + v_k \left( \frac{\partial A_{ij}}{\partial x_k} - \frac{\partial A_{ik}}{\partial x_j} \right) = -\frac{\psi_{ij}}{\theta_1(\tau_1)}$$
(2.28d)

$$\frac{\partial \left(\rho J_{i}\right)}{\partial t} + \frac{\partial \left(\rho J_{i} v_{k} + T \delta_{ik}\right)}{\partial x_{k}} = -\frac{\rho H_{i}}{\theta_{2}\left(\tau_{2}\right)}$$
(2.28e)

Under row-major ordering, we have:

$$\mathbf{Q} = \begin{pmatrix} \rho & \rho E & \rho v_1 & \rho v_2 & \rho v_3 & A_{11} & A_{12} & A_{13} & A_{21} & A_{22} & A_{23} & A_{31} & A_{32} & A_{33} & \rho J_1 & \rho J_2 & \rho J_3 \end{pmatrix}^T$$

$$(2.29a)$$

$$\mathbf{P} = \begin{pmatrix} \rho & p & v_1 & v_2 & v_3 & A_{11} & A_{21} & A_{31} & A_{12} & A_{22} & A_{32} & A_{13} & A_{23} & A_{33} & J_1 & J_2 & J_3 \end{pmatrix}^T$$

$$(2.29b)$$

$$F_{1} = \begin{pmatrix} \rho v_{1} \\ \rho v_{1}E + v_{1}p - \sigma_{1m}v_{m} + q_{1} \\ \rho v_{1}^{2}E + v_{1}p - \sigma_{1m}v_{m} + q_{1} \\ \rho v_{1}^{2} + p - \sigma_{11} \\ \rho v_{1}v_{2} - \sigma_{12} \\ \rho v_{1}v_{3} - \sigma_{13} \\ A_{1m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ 0 \\ 0 \\ \rho J_{1}v_{1} + T \\ \rho J_{2}v_{1} \\ \rho J_{3}v_{1} \end{pmatrix} \qquad F_{2} = \begin{pmatrix} \rho v_{2} \\ \rho v_{2}E + v_{2}p - \sigma_{2m}v_{m} + q_{2} \\ \rho v_{2}V_{3} - \sigma_{21} \\ \rho v_{2}v_{3} - \sigma_{22} \\ \rho v_{2}v_{3} - \sigma_{23} \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ \rho J_{1}v_{2} \\ \rho J_{2}v_{2} + T \\ \rho J_{3}v_{2} \end{pmatrix} \qquad F_{3} = \begin{pmatrix} \rho v_{3} \\ \rho v_{3}E + v_{3}p - \sigma_{3m}v_{m} + q_{3} \\ \rho v_{1}v_{3} - \sigma_{31} \\ \rho v_{2}v_{3} - \sigma_{32} \\ \rho v_{2}^{2} + p - \sigma_{33} \\ 0 \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ \rho J_{1}v_{3} \\ \rho J_{2}v_{3} \\ \rho J_{3}v_{3} + T \end{pmatrix}$$

$$S = -\frac{1}{\theta_{1}(\tau_{1})} \begin{pmatrix} 0\\0\\0\\0\\0\\\psi_{11}\\\psi_{12}\\\psi_{13}\\\psi_{21}\\\psi_{22}\\\psi_{23}\\\psi_{31}\\\psi_{32}\\\psi_{33}\\0\\0\\0\end{pmatrix} - \frac{1}{\theta_{2}(\tau_{2})} \begin{pmatrix} 0\\0\\0\\0\\0\\0\\0\\0\\0\\0\\\rho H_{1}\\\rho H_{2}\\\rho H_{3} \end{pmatrix}$$

$$(2.34)$$

$$\Psi_{ij} = \rho v_i v_j - \sigma_{ij} \tag{2.35a}$$

$$\Psi_{ij} = \rho v_i v_j - \sigma_{ij}$$

$$\Phi_{ij}^k = \rho v_k \psi_{ij} - v_m \frac{\partial \sigma_{mk}}{\partial A_{ij}}$$
(2.35a)

$$\Omega_i = v_i \left( E + \rho E_\rho \right) - \frac{\sigma_{im} v_m}{\rho} + T_\rho H_i \tag{2.35c}$$

$$\Upsilon = \frac{\|\boldsymbol{v}\|^2 + \boldsymbol{H} \cdot \boldsymbol{J} - E - \rho E_{\rho}}{\rho E_p}$$
(2.35d)

$$\tilde{\boldsymbol{H}} = E_{\boldsymbol{J}\boldsymbol{J}} \tag{2.35e}$$

 $\begin{smallmatrix} p_2 \\ p_2 \\ p_3 \\ p_4 \\ p_5 \\ p_6 \\ p_7 \\ p_8 \\ p_$  $\begin{matrix} 1 \\ + \rho E_{t} \\ v_{1} \\ v_{2} \\ v_{3} \\ v_{3} \\ v_{3} \\ v_{3} \\ v_{3} \\ v_{4} \\ v_{5} \\ v_{7} \\ v_$  $\frac{\partial Q}{\partial P}$ 

(2.37)

		0	$\rho v_1 H_3$	0	0	0	0	0	0	0	0	0 0	0	0	$\rho v_1$
CHAPTER 2.	FASTER SOLVER	RS	$ov_1H_2$	0	0	0	0	0 0	0 0	0	0	0 0	0	0	$ \rho v_1 \\ 0 $

$$\frac{\partial F_1}{\partial P_1} = \begin{pmatrix} v_1 & v_1 & v_2 & v_1 & v_2 \\ v_1 & (v_1 (\rho E_p + 1) + T_p H_1) & (\Psi_{11} + \rho E_p + p) & \Psi_{12} & \Psi_{11} & \Phi_{12}^1 & \Phi_{12}^1 & \Phi_{21}^1 & \Phi_{2$$

	$\rho v_2 H_3 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
CHAPTER 2. FASTER SOLVE	$CRS = \begin{pmatrix} c & c & c & c & c & c & c & c & c & c$
	$ ho_{v_2H_1}$ $ ho_{v_2H_1}$ $ ho_{v_2H_2}$ $ ho_{v_2}$ $ ho_{v_2}$ $ ho_{v_2}$
	$\begin{array}{c} \Phi \\ \Phi_{33} \\ \Phi_{33} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi \\ \Phi_{32} \\ 0 \\ 32 \\ 32 \\ 32 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_{31} \\ \Phi_{31} \\ \Phi_{31} \\ -\frac{\rho_{321}}{2} \\ -\frac{\rho_{321}}{2} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	$\begin{array}{c} \Phi \\ \Phi_{22} \\ 0 \\ 22 \\ 0 \\ 22 \\ 12 \\ 12 \\ 12 \\ 12 \\$
	$\begin{array}{c} \Phi_{21} \\ \Phi_{21} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_{13} \\ \Phi_{13} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_{12} \\ \Phi_{12} \\ -621 \\ -872 \\ -12 \\ -12 \\ -12 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_{11}^2 \\ 0 \\ 0 \\ 111 \\ -\frac{\partial \sigma_{22}}{4711} \\ -\frac{\partial \sigma_{22}}{4711} \\ -\frac{\partial \sigma_{22}}{411} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ A_{13} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$ \begin{array}{c} \rho \\ \rho $
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	$ \begin{array}{c} 0 \\ (v_2 \ (\rho E_p + 1) + T_p H_2) \\ 0 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0$
	$\begin{pmatrix} v_2 \\ \Omega_2 \\ \frac{\Psi_{21}}{\Psi_{21}} \\ \frac{\Psi_{22}}{\Psi_{23}} \\ \frac{\Psi_{23}}{\Psi_{23}} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$
	$rac{\partial F_2}{\partial oldsymbol{P}} =$

RS	$(\rho v_3 H_3)$	,														,	
0	$\rho v_3 H_2$	0	0	0	0	0	0	0	0	0	0	0	0	0	$\rho v_3$	0	(07.6)
0	$\rho v_3 H_1$	0	0	0	0	0	0	0	0	0	0	0	0	$\rho v_3$	0	0	
0	$\Phi_{33}^3$	$-\frac{\partial \sigma_{31}}{A_{33}}$	$-\frac{\partial \sigma_{32}}{A_{33}}$	- <u>A33</u>	0	0	0	0	0	0	0	0	$v_3$	0	0	0	
0	$\Phi^3_{32}$	$-\frac{\partial \sigma_{31}}{A_{32}}$	$-\frac{\partial \sigma_{32}}{A_{32}}$	- <u>8033</u>	0	0	0	0	0	0	0	0	$v_2$	0	0	0	
0	$\Phi_{31}^3$	$-\frac{\partial\sigma_{31}}{A_{31}}$	$-\frac{\partial \sigma_{32}}{A_{31}}$	- <u>8033</u>	0.0	0	0	0	0	0	0	0	$v_1$	0	0	0	
0	$\Phi_{23}^3$	$-\frac{\partial \sigma_{31}}{A_{23}}$	$-\frac{\partial \tilde{\sigma}_{32}^2}{A_{23}}$	$-\frac{\partial \sigma_{33}^2}{A_{23}}$	0	0	0	0	0	$v_3$	0	0	0	0	0	0	
0	$\Phi_{22}^3$	$-\frac{\partial \sigma_{31}}{A_{22}}$	$-\frac{\partial \sigma_{32}^2}{A_{22}}$	- <u>8033</u> - <u>A33</u>	0	0	0	0	0	$v_2$	0	0	0	0	0	0	
0	$\Phi_{21}^3$	$-\frac{\partial\sigma_{31}}{A_{21}}$	$-\frac{\partial \tilde{\sigma}_{32}^2}{A_{21}}$	- <u>8033</u> - <u>A31</u>	0	0	0	0	0	$v_1$	0	0	0	0	0	0	
0	$\Phi^3_{13}$	$-\frac{\partial \sigma_{31}}{A_{13}}$	$-\frac{\partial \sigma_{32}}{A_{13}}$	$-\frac{\partial \sigma_{33}}{A_{13}}$	0	0	$v_3$	0	0	0	0	0	0	0	0	0	
0	$\Phi^3_{12}$	$-\frac{\partial \sigma_{31}}{A_{12}}$	$-\frac{\partial \sigma_{32}^2}{A_{12}}$	$-\frac{\partial \sigma_{33}^2}{A_{13}}$	0	0	$v_2$	0	0	0	0	0	0	0	0	0	
0	$\Phi^3_{11}$	$-\frac{\partial \sigma_{31}}{A_{11}}$	$-\frac{\partial \sigma_{32}^2}{A_{11}}$	$-\frac{\partial \sigma_{33}}{A_{11}}$	0,1	0	$v_1$	0	0	0	0	0	0	0	0	0	
0	$(\Psi_{33}+\rho E+p)$	$\rho v_1$	$\rho v_2$	$2\rho v_3$	0	0	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	$ ho J_1$	$\rho J_2$	$\rho J_3$	
0	$\Psi_{32}$	0	$\rho v_3$	0	0	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	
θ	$\Psi_{31}$	$\rho v_3$	0	0	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	
0	$(v_3 (\rho E_p + 1) + T_p H_3)$	0	0	1	0	0	0	0	0	0	0	0	0	0	0	$T_p$	
/ v3	$\Omega_3$	<u>₩</u> 31	#32 p	433	.0	0	0	0	0	0	0	0	0	$v_3J_1$	$v_3J_2$	$\langle v_3 J_3 + T_\rho \rangle$	
						Li Ci	0.5	$\partial P$									

_																_	2.41)
-	⊃ -	0	0	0	0	0	0	0	0	0	0	0	0	0	0 1	$v_1$	.,
0 0	⊃ :	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$	0	
0 %	$\Gamma \alpha_{-}^{-}$	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$	0	0	
0	)	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{33}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{12}}{\partial A_{33}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{33}}$	0	0	0	0	0	0	0	0	$v_1$	0	0	0	
0	)	-10	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_1$	0	0	0	0	
0	)	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{31}}$	0	0	0	0	0	0	$v_1$	0	0	0	0	0	
0	0	-10	$-\frac{1}{\rho} \frac{\partial \sigma_{12}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{23}}$	0	0	0	0	0	$v_1$	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{12}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{22}}$	0	0	0	0	$v_1$	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{21}}$	-II	$-\frac{1}{\rho}\frac{\partial\sigma_{13}^{2}}{\partial A_{21}}$	0	0	0	$v_1$	0	0	0	0	0	0	0	0	
0	)	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{12}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{13}}$	0	0	$v_1$	0	0	0	0	0	0	0	0	0	
0				$-\frac{1}{\rho}\frac{\partial\sigma_{13}^{2}}{\partial A_{12}}$		$v_1$	0	0	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{12}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}^{-1}}{\partial A_{11}}$	$v_1$	0	0	0	0	0	0	0	0	0	0	0	
0	0	0	0	$v_1$	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	0	
0	0	0	$v_1$	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	0	0	
θ	$d\lambda$	$v_1$	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	0	0	
0	$v_1$	I 0	0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(\infty a+a)o}$	0	0	
$\begin{pmatrix} v_1 \\ 0 \end{pmatrix}$	0	$-\frac{\sigma_{11}}{\rho^2}$	$-\frac{\sigma_{12}}{\sigma^2}$	$-\frac{\sigma_{13}}{\rho^2}$	0	0	0	0	0	0	0	0	0	$-\frac{T}{o^2}$	0	0	
								$M_1 =$									

_	_	_	_	_	_	_	_	_	_	_	_	_	_	_	_		2.42)
0	0  L	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_2$	3
0	$\Gamma \alpha^2$	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_2$	0	
0	0	0	0	0		0	0	0	0	0	0	0	0	$v_2$	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{33}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{22}^{22}}{\partial A_{33}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}}{\partial A_{33}}$	0	0	0	0	0	0	0	0	$v_2$	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{22}^{22}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_2$	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}^{2}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}^{23}}{\partial A_{31}}$	0	0	0	0	0	0	$v_2$	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{23}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{22}^{22}}{\partial A_{23}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{23}^{23}}{\partial A_{23}}$	0	0	0	0	0	$v_2$	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{22}^{22}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}^{23}}{\partial A_{22}}$	0	0	0	0	$v_2$	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}^{2}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}^{23}}{\partial A_{21}}$	0	0	0	$v_2$	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}^{23}}{\partial A_{13}}$	0	0	$v_2$	0	0	0	0	0	0	0	0	0	
		$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{12}}$						0	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}}{\partial A_{11}}$	$v_2$	0	0	0	0	0	0	0	0	0	0	0	
0	0	0	0	$v_2$	0	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	
θ	$d\lambda$	0	$v_2$	0	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	0	
0	0	$v_2$	0	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	0	
0	$v_2$	0	-1 σ	0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(\infty a+a)\sigma}$	0	
/ v2	0	$-\frac{\sigma_{21}}{\sigma^2}$	$-\frac{\sigma_{22}^{\prime}}{\rho^{2}}$	$-\frac{\sigma_{23}}{\rho^2}$	Ò	0	0	0	0	0	0	0	0	0	$-\frac{T}{o^2}$	· 0	
								$M_2 =$									

_	L															_	(2.43)
0	$\Gamma \alpha^2$	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	0	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	0	0	
0				$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{33}}$		0	0	0	0	0	0	0	$v_3$	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_3$	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{31}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{31}}$	0	0	0	0	0	0	$v_3$	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{23}}$	0	0	0	0	0	$v_3$	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{33}^2}{\partial A_{22}}$	0	0	0	0	$v_3$	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}^2}{\partial A_{21}}$	0	0	0	$v_3$	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{32}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{13}}$	0	0	$v_3$	0	0	0	0	0	0	0	0	0	
0				$-\frac{1}{\rho}\frac{\partial\sigma_{33}^{2}}{\partial A_{12}}$		~	0	0	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{32}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}^{1}}{\partial A_{11}}$	$v_3$	0	0	0	0	0	0	0	0	0	0	0	
θ	$d\lambda$	0	0	$v_3$	0	0	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	
0	0	0	$v_3$	0	0	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	
0	0	$v_3$	0	0	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	
0	$v_3$	0	0	<u>1</u>	.0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(\infty a+a)o}$	
/ v3	0	$-\frac{\sigma_{31}}{o^2}$	- 032 02	$-\frac{\sigma_{33}^2}{\rho^2}$	· 0	0	0	0	0	0	0	0	0	0	0	$-\frac{T}{o^2}$	L
								$M_3 =$									

## Slow Flow

### 3.1 Studying numerical smearing with slow flow past a barrier

A checkerboard pattern appears around the corner of the barrier, leading to a crash, using reflective boundary conditions (in velocity) for the barrier. Do we need a staggered grid?

# RGFM

The RGFM does nothing without a temperature fix when applied to the heat conduction test. The linearisation upon which it is based results in a stationary solution when  $q_L = q_R$  and  $\sigma_L = \sigma_R$  initially. Barton's RGFM is similar. Should q be fixed? Maybe use analytical solution to heat equation at  $t = \Delta t$ ?

# Bibliography