Lab Notes

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## To Do

### 1.1 Coding

- Test split-WENO in 2D
- Implement in CUDA
- Solid EOSs
- Implement Barton's damage model
- Test compressible Euler vs GPR use narrowing domain from Toro's book
- Try conservative formulation [Peshkov,Grmela,Romenski]

### 1.2 Theoretical

- Investiage approximate Riemann solvers (e.g. Dumbser's HLLEM)
- Convergence of conservation of mass in RGFM

### 1.3 Papers

- Isobaric cookoff (make cookoff the focus)
- Split solver vs ADER-WENO
- Application of ADER-WENO to Barton's solid model (with Tome)
- HPR-RGFM paper (solve stationarity of interface solver under some conditions)
- Application of ADER-WENO to equations in other areas of Physics, Biology, & Economics

## Faster Solvers

### 2.1 Fast WENO Oscillation Indicator Calculation

The WENO oscillation indicator is defined as:

$$o = \Sigma_{mn} w_m w_n \tag{2.1}$$

where  $w_i$  are the WENO coefficients calculated for a particular stencil, and:

$$\Sigma_{mn} = \sum_{\alpha=1}^{N} \int_{0}^{1} \psi_{m}^{(\alpha)} \psi_{n}^{(\alpha)} \tag{2.2}$$

By considering that:

$$o = \sum_{\alpha=1}^{N} \int_{0}^{1} \left( \frac{d^{\alpha} w}{dx^{\alpha}} \right)^{2} > 0$$
 (2.3)

we have that  $\Sigma$  is symmetric positive definite. Thus, it has a Cholesky decomposition  $\Sigma = LL^T$ . Thus:

$$o = \left\| w^T L \right\|^2 \tag{2.4}$$

L can be precalculated, and o calculated quickly as:

```
1: o = 0

2: \mathbf{for} \ j = 1...n \ \mathbf{do}

3: tmp = 0

4: \mathbf{for} \ i = j...n \ \mathbf{do}

5: tmp = tmp + w(i) * L(i,j)

6: \mathbf{end} \ \mathbf{for}

7: o = o + tmp * tmp

8: \mathbf{end} \ \mathbf{for}
```

### 2.2 Approximating Interface Terms in FV

Instead of calculating the following:

$$\int D(q^{-}(x_{0},t),q^{+}(x_{0},t)) dt$$
(2.5)

I propose calculating the following:

$$D\left(\frac{1}{\Delta t} \int q^{-}\left(x_{0}, t\right) dt, \frac{1}{\Delta t} \int q^{+}\left(x_{0}, t\right) dt\right)$$

$$(2.6)$$

This obtains a large speedup with no discernable difference in the results of Stokes' First Problem.

### 2.3 Analytical Results for Basis Vectors

For N=1, the Gauss-Legendre nodes on [0,1] are  $\left\{\frac{1}{2}\left(1-\frac{1}{\sqrt{3}}\right),\frac{1}{2}\left(1+\frac{1}{\sqrt{3}}\right)\right\}$ . Thus:

$$\psi_1(x) = -\sqrt{3}x + \frac{1+\sqrt{3}}{2}$$
 (2.7a)

$$\psi_2(x) = \sqrt{3}x + \frac{1 - \sqrt{3}}{2}$$
 (2.7b)

$$\psi_1(1) = \frac{1 - \sqrt{3}}{2} \tag{2.8a}$$

$$\psi_2(1) = \frac{1+\sqrt{3}}{2}$$
 (2.8b)

$$\psi_1(1) \psi_1(1) = 1 - \frac{\sqrt{3}}{2}$$
 (2.9a)

$$\psi_1(1)\,\psi_2(1) = -\frac{1}{2}$$
 (2.9b)

$$\psi_2(1) \,\psi_2(1) = 1 + \frac{\sqrt{3}}{2}$$
 (2.9c)

$$\int_{m}^{m+1} \psi_1(x) dx = \frac{-\sqrt{3}}{2} (2m+1) + \frac{1+\sqrt{3}}{2} = \frac{1}{2} - m\sqrt{3}$$
 (2.10a)

$$\int_{m}^{m+1} \psi_2(x) dx = \frac{\sqrt{3}}{2} (2m+1) + \frac{1-\sqrt{3}}{2} = \frac{1}{2} + m\sqrt{3}$$
 (2.10b)

The WENO matrices are:

$$\begin{pmatrix} \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} - \sqrt{3} & \frac{1}{2} + \sqrt{3} \end{pmatrix}, \begin{pmatrix} \frac{1}{2} + \sqrt{3} & \frac{1}{2} - \sqrt{3} \\ \frac{1}{2} & \frac{1}{2} \end{pmatrix}$$
 (2.11)

The inverses are:

$$\frac{1}{\sqrt{3}} \begin{pmatrix} \sqrt{3} + \frac{1}{2} & -\frac{1}{2} \\ \sqrt{3} - \frac{1}{2} & \frac{1}{2} \end{pmatrix}, \frac{1}{\sqrt{3}} \begin{pmatrix} \frac{1}{2} & \sqrt{3} - \frac{1}{2} \\ -\frac{1}{2} & \sqrt{3} + \frac{1}{2} \end{pmatrix}$$
 (2.12)

The weights for both nodes are 0.5 so  $\int_0^1 \psi_i \psi_j dx = \frac{\delta_{ij}}{2}$  and  $\int_0^1 \psi_i \psi_j' dx = (-1)^j \frac{\sqrt{3}}{2}$ .

$$I_{11} - I_2^T = \frac{1}{2} \begin{pmatrix} 2 - \sqrt{3} & -1 \\ -1 & 2 + \sqrt{3} \end{pmatrix} - \frac{1}{2} \begin{pmatrix} -\sqrt{3} & -\sqrt{3} \\ \sqrt{3} & \sqrt{3} \end{pmatrix}$$

$$= \frac{1}{2} \begin{pmatrix} 2 & -(1 - \sqrt{3}) \\ -(1 + \sqrt{3}) & 2 \end{pmatrix}$$
(2.13)

$$(I_{11} - I_2^T)^{-1} = \frac{1}{3} \begin{pmatrix} 2 & 1 - \sqrt{3} \\ 1 + \sqrt{3} & 2 \end{pmatrix}$$
 (2.14)

Using a precalculated, analytical form of U in the DG predictor for N=1 obtains a ~30% speedup on Stokes' First Problem.

#### 2.4 Distortion ODEs

#### 2.4.1 Linearized Distortion ODEs Solver

Note that  $A^* = \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}}I$  is a stationary point of the ODE for A. Linearizing the ODE around  $A^*$  gives:

$$\frac{dA}{dt} \approx J_A (A^*) (A - A^*) \qquad (2.15)$$

$$= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{5}{3}} \left(\left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{in} \delta_{mj} + \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{jn} \delta_{im} + \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{im} \delta_{jn} - \frac{1}{3} \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{im} \delta_{jn} \delta_{kl} \delta_{kl} - \frac{2}{3} \left(\frac{\rho}{\rho_0}\right)^{\frac{2}{3}} \delta_{ij} \delta_{mn}\right) \times \left(A_{mn} - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn}\right) \\
= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right) \left(A_{mn} - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn}\right) \\
= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(A_{mn} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right) - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \delta_{mn} \left(\delta_{in} \delta_{mj} + \delta_{im} \delta_{jn} - \frac{2}{3} \delta_{ij} \delta_{mn}\right)\right) \\
= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(A_{ji} + A_{ij} - \frac{2}{3} \operatorname{tr}(A) \delta_{ij} - \left(\frac{\rho}{\rho_0}\right)^{\frac{1}{3}} \left(\delta_{ij} + \delta_{ij} - 2\delta_{ij}\right)\right) \\
= \frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \left(A + A^T - \frac{2}{3} \operatorname{tr}(A) I\right)$$

The matrix for this system, in row-major form, is:

$$\frac{-3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}} \begin{pmatrix}
\frac{4}{3} & 0 & 0 & 0 & -\frac{2}{3} & 0 & 0 & 0 & -\frac{2}{3} \\
0 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
0 & 0 & 1 & 0 & 0 & 0 & 1 & 0 & 0 \\
0 & 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
-\frac{2}{3} & 0 & 0 & 0 & \frac{4}{3} & 0 & 0 & 0 & -\frac{2}{3} \\
0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\
0 & 0 & 1 & 0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\
-\frac{2}{3} & 0 & 0 & 0 & -\frac{2}{3} & 0 & 0 & 0 & \frac{4}{3}
\end{pmatrix} \tag{2.16}$$

The eigenvalues and eigenvectors are:

$$\{0, 0, 0, 0, -2k, -2k, -2k, -2k, -2k\} \tag{2.17}$$

where  $k = \frac{3}{\tau_1} \left(\frac{\rho}{\rho_0}\right)^{\frac{7}{3}}$ . Thus, the solution is:

$$\frac{A_{12} - A_{21}}{2} \begin{pmatrix} 0 & 1 & 0 \\ -1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{A_{13} - A_{31}}{2} \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ -1 & 0 & 0 \end{pmatrix} + \frac{A_{23} - A_{32}}{2} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{pmatrix} \\
+ \frac{A_{11} + A_{22} + A_{33}}{3} \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \\
+ \frac{2A_{22} - A_{11} - A_{33}}{3} e^{-2kt} \begin{pmatrix} -1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{2A_{33} - A_{11} - A_{22}}{3} e^{-2kt} \begin{pmatrix} -1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \\
+ \frac{A_{12} + A_{21}}{2} e^{-2kt} \begin{pmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} + \frac{A_{13} + A_{31}}{2} e^{-2kt} \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} + \frac{A_{23} + A_{32}}{2} e^{-2kt} \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \end{pmatrix}$$

This is equal to:

$$\frac{1}{2}(A - A^{T}) + \frac{\operatorname{tr}(A)}{3}I + e^{-2kt}\left(\frac{1}{2}(A + A^{T}) - \frac{\operatorname{tr}(A)}{3}I\right)$$
 (2.20)

Results with Stokes' First Problem look good with this linearisation. The ODE step takes a negligible amount of time, meaning that if accuracy is maintained to second order, the solver is now fast enough.

#### 2.4.2 Linearized Reduced Distortion ODE Solver

Taking system (??), note that the Jacobian of the system is given by:

$$J = -k \begin{pmatrix} 4x_1 - x_2 - x_3 & -x_1 & -x_1 \\ -x_2 & 4x_2 - x_3 - x_1 & -x_3 \\ -x_3 & -x_3 & 4x_3 - x_1 - x_2 \end{pmatrix}$$
(2.21)

Evaluated at stationary point  $x_i = \sqrt[3]{c}$  we have:

$$J(x_0) = -k\sqrt[3]{c} \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix}$$
 (2.22)

Thus, the system is linearized to:

$$\frac{dx}{dt} \approx -k\sqrt[3]{c} \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix} \begin{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} - \sqrt[3]{c} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} \end{pmatrix} 
= k\sqrt[3]{c} \begin{pmatrix} -2 & 1 & 1 \\ 1 & -2 & 1 \\ 1 & 1 & -2 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$
(2.23)

The eigenvalues of this system matrix are  $\{-3k\sqrt[3]{c}, -3k\sqrt[3]{c}, 0\}$  and the eigenvectors are:

$$\begin{pmatrix} -1\\0\\1 \end{pmatrix}, \begin{pmatrix} 0\\-1\\1 \end{pmatrix}, \begin{pmatrix} 1\\1\\1 \end{pmatrix} \tag{2.24}$$

Thus, the linearized solution is:

$$\boldsymbol{x}(t) = \frac{-2x_1 + x_2 + x_3}{3} e^{-3k\sqrt[3]{c}t} \begin{pmatrix} -1\\0\\1 \end{pmatrix} + \frac{x_1 - 2x_2 + x_3}{3} e^{-3k\sqrt[3]{c}t} \begin{pmatrix} 0\\-1\\1 \end{pmatrix} + \frac{x_1 + x_2 + x_3}{3} \begin{pmatrix} 1\\1\\1 \end{pmatrix}$$
(2.25)

This may represent a faster way to calculate the evolution of the stretch terms of A. Note that some kind of normalization will probably be necessary, as:

$$\frac{x_1 + x_2 + x_3}{3} \ge (x_1 x_2 x_3)^{\frac{1}{3}} \tag{2.26}$$

with equality if and only if  $x_1 = x_2 = x_3$ .

#### Primitive WENO and DG Reconstruction 2.5

As suggested in [?], the WENO and DG can be performed in primitive variables, which is less computationally expensive than evaluating fluxes using conserved variables. Achieves around 20% speedup in DG step, at double cost in WENO step. Minimal speedup in FV step, as both primitive and conserved variables must be calculated for the flux updates. Not enough.

#### 2.6 Change to Row-Major Ordering

The original GPR papers state the equations for A in column-major order, probably because the authors use Fortran. For C++ and Python implementations it is faster to work in row-major order. ~10% speedup was achieved by implementing this.

The GPR equations are:

$$\frac{\partial \rho}{\partial t} + \frac{\partial (\rho v_k)}{\partial x_k} = 0 \tag{2.27a}$$

$$\frac{\partial (\rho E)}{\partial t} + \frac{\partial (\rho E v_k + (p \delta_{ik} - \sigma_{ik}) v_i + q_k)}{\partial x_k} = 0$$

$$\frac{\partial (\rho v_i)}{\partial t} + \frac{\partial (\rho v_i v_k + p \delta_{ik} - \sigma_{ik})}{\partial x_k} = 0$$
(2.27b)

$$\frac{\partial (\rho v_i)}{\partial t} + \frac{\partial (\rho v_i v_k + p \delta_{ik} - \sigma_{ik})}{\partial x_k} = 0$$
 (2.27c)

$$\frac{\partial A_{ij}}{\partial t} + \frac{\partial (A_{ik}v_k)}{\partial x_j} + v_k \left( \frac{\partial A_{ij}}{\partial x_k} - \frac{\partial A_{ik}}{\partial x_j} \right) = -\frac{\psi_{ij}}{\theta_1(\tau_1)}$$
(2.27d)

$$\frac{\partial \left(\rho J_{i}\right)}{\partial t} + \frac{\partial \left(\rho J_{i} v_{k} + T \delta_{ik}\right)}{\partial x_{k}} = -\frac{\rho H_{i}}{\theta_{2}\left(\tau_{2}\right)}$$
(2.27e)

Under row-major ordering, we have:

$$\mathbf{Q} = \begin{pmatrix} \rho & \rho E & \rho v_1 & \rho v_2 & \rho v_3 & A_{11} & A_{12} & A_{13} & A_{21} & A_{22} & A_{23} & A_{31} & A_{32} & A_{33} & \rho J_1 & \rho J_2 & \rho J_3 \end{pmatrix}^T$$
(2.28a)  
$$\mathbf{P} = \begin{pmatrix} \rho & p & v_1 & v_2 & v_3 & A_{11} & A_{21} & A_{31} & A_{12} & A_{22} & A_{32} & A_{13} & A_{23} & A_{33} & J_1 & J_2 & J_3 \end{pmatrix}^T$$
(2.28b)

$$F_{1} = \begin{pmatrix} \rho v_{1} \\ \rho v_{1}E + v_{1}p - \sigma_{1m}v_{m} + q_{1} \\ \rho v_{1}^{2}E + v_{1}p - \sigma_{1m}v_{m} + q_{1} \\ \rho v_{1}^{2} + p - \sigma_{11} \\ \rho v_{1}v_{2} - \sigma_{12} \\ \rho v_{1}v_{3} - \sigma_{13} \\ A_{1m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ 0 \\ 0 \\ \rho J_{1}v_{1} + T \\ \rho J_{2}v_{1} \\ \rho J_{3}v_{1} \end{pmatrix} \qquad F_{2} = \begin{pmatrix} \rho v_{2} \\ \rho v_{2}E + v_{2}p - \sigma_{2m}v_{m} + q_{2} \\ \rho v_{2}V_{3} - \sigma_{21} \\ \rho v_{2}v_{3} - \sigma_{22} \\ \rho v_{2}v_{3} - \sigma_{23} \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ 0 \\ 0 \\ A_{3m}v_{m} \\ \rho J_{1}v_{2} \\ \rho J_{2}v_{2} + T \\ \rho J_{3}v_{2} \end{pmatrix} \qquad F_{3} = \begin{pmatrix} \rho v_{3} \\ \rho v_{3}E + v_{3}p - \sigma_{3m}v_{m} + q_{3} \\ \rho v_{1}v_{3} - \sigma_{31} \\ \rho v_{2}v_{3} - \sigma_{32} \\ \rho v_{2}^{2} + p - \sigma_{33} \\ 0 \\ 0 \\ 0 \\ A_{1m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{2m}v_{m} \\ 0 \\ 0 \\ 0 \\ A_{3m}v_{m} \\ \rho J_{1}v_{3} \\ \rho J_{2}v_{3} \\ \rho J_{3}v_{3} + T \end{pmatrix}$$

$$\Psi_{ij} = \rho v_i v_j - \sigma_{ij} \tag{2.34a}$$

$$\Psi_{ij} = \rho v_i v_j - \sigma_{ij}$$

$$\Phi_{ij}^k = \rho v_k \psi_{ij} - v_m \frac{\partial \sigma_{mk}}{\partial A_{ij}}$$
(2.34a)

$$\Omega_i = v_i \left( E + \rho E_\rho \right) - \frac{\sigma_{im} v_m}{\rho} + T_\rho H_i \tag{2.34c}$$

$$\Upsilon = \frac{\|\boldsymbol{v}\|^2 + \boldsymbol{H} \cdot \boldsymbol{J} - E - \rho E_{\rho}}{\rho E_p}$$
 (2.34d)

$$\tilde{\boldsymbol{H}} = E_{\boldsymbol{J}\boldsymbol{J}} \tag{2.34e}$$

 $\begin{smallmatrix} p_2 \\ p_2 \\ p_3 \\ p_4 \\ p_5 \\ p_6 \\ p_7 \\ p_8 \\ p_$  $\begin{matrix} 1 \\ + \rho E_t \\ v_1 \\ v_2 \\ v_3 \\ v_3 \\ v_4 \\ v_4 \\ v_5 \\ v_6 \\$  $\frac{\partial Q}{\partial P}$ 

2.36

	0	$\rho v_1  H_3$	0	0	0	0	0 0	0	00	0	00	000	$\rho v_1$
CHAPTER 2.	FASTER SOLVERS	$\rho v_1 H_2$	0	0	0	0	0 0	0 0	0 0	0	0 0	0 0	0

S	$\rho v_1 H_2$	0	0	0	0	0	0	0	0	0	0	0	0	0	$\rho v_1$	0	
0	$\left( ho v_1 H_1 + T  ilde{H}_1 ight)$	0	112 13 13	0	0	0	0	0	0	0	0	0	0	$\rho v_1$	0	0	1000
0	$\Phi^1_{33}$	$-\frac{\partial \sigma_{11}}{400}$	$-\frac{\frac{\delta^{133}}{\delta^{\sigma}12}}{A_{33}}$	$-\frac{\partial \sigma_{13}^{2}}{A_{22}}$	0	0	0	0	0	0	$v_3$	0	0	0	0	0	
0	$\Phi^1_{32}$	$-\frac{\partial \sigma_{11}}{455}$	$-\frac{\frac{\delta^{132}}{\delta^{\sigma}12}}{A_{32}}$	$-\frac{\partial \sigma_{13}}{A_{23}}$	0	0	0	0	0	0	$v_2$	0	0	0	0	0	
0	$\Phi^1_{31}$	$-\frac{\partial \sigma_{11}}{46i}$	$-\frac{\frac{\delta^{131}}{\delta^{\sigma_{12}}}}{A_{31}}$	$-\frac{\partial \sigma_{13}}{A_{31}}$	0.	0	0	0	0	0	$v_1$	0	0	0	0	0	
0	$\Phi^1_{23}$	$-\frac{\partial \sigma_{11}}{455}$	$-\frac{\frac{\delta^{7}23}{\delta^{\sigma}12}}{A_{23}}$	$-\frac{\partial \tilde{\sigma_{13}}}{A_{23}}$	0.5	0	0	$v_3$	0	0	0	0	0	0	0	0	
0	$\Phi^1_{22}$	$-\frac{\partial \sigma_{11}}{460}$	$-\frac{\frac{\partial^2 Z}{\partial \sigma_{12}}}{A_{22}}$	$-\frac{\partial \sigma_{13}^2}{A_{23}}$	0	0	0	$v_2$	0	0	0	0	0	0	0	0	
0	$\Phi^1_{21}$	$-\frac{\partial \sigma_{11}}{46.}$	$-\frac{\overset{\circ}{\partial}\overset{\circ}{\sigma}_{12}}{A_{21}}$	$-\frac{\partial \tilde{\sigma_{13}}}{A_{21}}$	0	0	0	$v_1$	0	0	0	0	0	0	0	0	
0	$\Phi^1_{13}$	$-\frac{\partial \sigma_{11}}{4.5}$	$-\frac{\delta^{113}_{113}}{A_{13}}$	$-\frac{\partial \sigma_{13}^{2}}{A_{13}}$	$v_3$	0	0	0	0	0	0	0	0	0	0	0	
0	$\Phi^1_{12}$	$-\frac{\partial \sigma_{11}}{\Delta_{10}}$	$-\frac{\delta^{112}_{112}}{A_{12}}$	$-\frac{\partial \sigma_{13}^2}{A_{13}}$	$v_2$	0	0	0	0	0	0	0	0	0	0	0	
0	$\Phi^1_{11}$	$-\frac{\partial \sigma_{11}}{A_{11}}$	$-\frac{\delta \sigma_{11}}{A_{11}}$	$-\frac{\partial \sigma_{13}^2}{A_{11}}$	$v_1$	0	0	0	0	0	0	0	0	0	0	0	
0	$\Psi_{13}$	0	0	$\rho v_1$	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	0	
			$\rho v_1$														
Ф	$(\Psi_{11}+\rho E+p)$	$2\rho v_1$	$\rho v_2$	$\rho v_3$	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	$\rho J_1$	$\rho J_2$	$\rho J_3$	
0	$(v_1 (\rho E_p + 1) + T_p H_1)$		0	0	0	0	0	0	0	0	0	0	0	$T_p$	0	0	
$\begin{array}{c} v_1 \\ \Omega_1 \\ \overline{V_{1,1}} \\ \overline{V_{1,2}} \\ \overline{V_{1,3}} \\ \overline{V_{1,3}} \\ \overline{V_{1,3}} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$														$\langle v_1 J_3 \rangle$			
						E C	$\frac{o\mathbf{r}_1}{} = $	$\partial P$									
							·										

	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
CHAPTER 2. FASTER SOLVE	$RS \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 &$
	$ ho v_2 H_1$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	$\begin{array}{c} \Phi_{32} \\ \Phi_{32} \\ \Phi_{32} \\ \Phi_{32} \\ \end{array}$
	$\begin{array}{c} \Phi_2 \\ \Phi_3 \\ 0 \\ 311 \\ 0 \\ 311 \\ 0 \\ 311 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$
	$\begin{array}{c} \Phi_2 \\ \Phi_2 \\ \Phi_{23} \\ 0 \\ 23 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_2 \\ \Phi_2 \\ \rho_2 \\ \rho_2 \\ \rho_3 \\ \rho_4 \\ \rho_2 \\ \rho_2 \\ \rho_3 \\ \rho_4 \\ \rho_2 \\ \rho_4 \\ \rho_2 \\ \rho_4 \\ \rho_5 \\ \rho_6 \\$
	$\begin{array}{c} \Phi_2 \\ \Phi_2 \\ \Phi_2 \\ 0 \leq 21 \\ 0 \leq 21 \\ 0 \leq 21 \\ 0 \leq 21 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_2 \\ \Phi_1 \\ 0 \\ 113 \\ 0 \\ 212 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_2 \\ \Phi_{12} \\ 0 \\ 1_1 \\ 0 \\ 1_2 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$\begin{array}{c} \Phi_2 \\ \Phi_2 \\ 0 \\ 111 \\ 0 \\ 221 \\ 0 \\ 111 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $
	$\begin{array}{cccc} & & & & & & & & & & & & & & & & & $
	$\begin{array}{c} \rho \\ \rho \\ \rho v_1 \\ \rho v_1 \\ 2\rho v_2 \\ \rho v_3 \\ \rho v_3 \\ 0 \\ A_{12} \\ 0 \\ 0 \\ 0 \\ A_{22} \\ 0 \\ 0 \\ 0 \\ 0 \\ \rho J_1 \\ \rho J_2 \\ \rho J_3 \\ \rho J_4 \\ \rho J_5 \\ \rho J_$
	$\begin{array}{c} \Psi_{21} \\ \Psi_{21} \\ \rho v_2 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$(v_2 (\rho E_p + 1) + T_p H_2)$ $(v_2 (\rho E_p + 1) + T_p H_2)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(0)$ $(1)$ $(1)$ $(2)$ $(1)$ $(2)$ $(3)$ $(4)$ $(4)$ $(6)$ $(6)$ $(7)$ $(7)$ $(7)$ $(9)$ $(9)$ $(1)$
	$\begin{pmatrix} v_2 \\ \Omega_2 \\ \frac{\Psi_{21}}{2} \\ \frac{\Psi_{23}}{2} \\ \frac{\Psi_{23}}{2} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
	$rac{\partial F_2}{\partial oldsymbol{P}} =$

		$rar{H}_3$
CHAPTER 2.	FASTER SOLVE	$\begin{pmatrix} v_3 & H_3 + T \tilde{H}_3 \\ 0 & & & & \\ 0 & & & & \\ 0 & & & & \\ 0 & & & &$
		$\begin{array}{c} 0 \\ \rho v_3 H_2 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} 0 \\ \rho v_3 H_1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Phi_3 \\ \Phi_{33} \\ \Phi_{33} \\ \Phi_{33} \\ \hline \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0$
		$\begin{array}{c} \Phi_{33} \\ \Phi_{332} \\ \theta_{332} \\ \theta_{332} \\ \theta_{332} \\ \theta_{332} \\ \theta_{332} \\ \theta_{0} \\ \theta_$
		$\begin{array}{c} 0 \\ \Phi_{31} \\ \Phi_{31} \\ \theta_{31} \\ \theta_{31} \\ \theta_{32} \\ \theta_{32} \\ \theta_{32} \\ \theta_{32} \\ \theta_{31} \\ \theta_{32} \\ \theta_{33} \\ \theta_{32} \\ \theta_{33} \\ \theta_{33} \\ \theta_{33} \\ \theta_{33} \\ \theta_{34} \\ \theta$
		$\begin{array}{c} \Phi_3 \\ \Phi_{23} \\ \theta_{23} \\ \theta_{332} \\ \theta_{332} \\ \theta_{332} \\ \theta_{332} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{cccccccccccccccccccccccccccccccccccc$
		$\begin{array}{c} \Phi_3 \\ \Phi_{21} \\ P_{21} \\ P_{31} \\$
		$\begin{array}{c} \Phi_3 \\ \Phi_{13} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Phi_3 \\ \Phi_{12} \\ \Phi_{12} \\ \Phi_{131} \\ \Phi_{131} \\ \Phi_{132} \\ \Phi_{132} \\ -\frac{\delta \sigma_{13}}{\delta \sigma_{33}} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$
		$\begin{array}{c} 0 \\ \Phi^3 \\ 111 \\ -\frac{\partial \sigma}{2} \\ 111 \\ -\frac{A}{11} \\ -\frac{A}{1} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$(\Psi_{33} + \rho E + p)$ $\rho v_{1}$ $\rho v_{2}$ $2\rho v_{3}$ $0$ $0$ $A_{13}$ $0$ $0$ $A_{23}$ $\rho J_{1}$ $\rho J_{2}$ $\rho J_{3}$
		$\begin{array}{c} \Psi_{32} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$\begin{array}{c} \Psi_{311} \\ \Psi_{911} \\ \rho v _3 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$(v_3 (\rho E_p + 1) + T_p H_3)$ $0$ $0$ $1$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$ $0$
		$\begin{pmatrix} v_3 \\ \Omega_3 \\ \frac{\Psi_{31}}{2} \\ \frac{\Psi_{32}}{2} \\ \frac{\Psi_{33}}{2} \\ \frac{\Psi_{33}}{2} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
		$rac{\partial F_3}{\partial oldsymbol{p}} =$

0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$ /	(2.40)
0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$	0	
$0 \\ \Gamma \alpha^2 T$	0	0	0	0	0	0	0	0	0	0	0	0	$v_1$	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{22}}$	7-10	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{33}}$	0	0	0	0	0	0	0	0	$v_1$	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{32}}$	ρI,	0	0	0	0	0	0	0	$v_1$	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}^{2}}{\partial A_{31}}$	0	0	0	0	0	0	$v_1$	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{12}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{23}}$	0	0	0	0	0	$v_1$	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{22}}$	0	0	0	0	$v_1$	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}^{2}}{\partial A_{21}}$	0	0	0	$v_1$	0	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{12}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{12}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}}{\partial A_{13}}$	0	0	$v_1$	0	0	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{12}}$	ı	- 1		$v_1$	0	0	0	0	0	0	0	0	0	0	
0 0	$-\frac{1}{\rho}\frac{\partial\sigma_{11}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{12}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{13}^{-1}}{\partial A_{11}}$	$v_1$	0	0	0	0	0	0	0	0	0	0	0	
0 0	0	0	$v_1$	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	0	
0 0	0	$v_1$	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	0	0	
$\frac{a\lambda}{d}$	$v_1$	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	0	0	
0	1 ⊣1 °	0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(a+a)^o}$	0	0	
$\begin{pmatrix} v_1 \\ 0 \end{pmatrix}$	$-\frac{\sigma_{11}}{\sigma^2}$	$-\frac{\sigma_{12}^{r}}{\sigma^{2}}$	$-\frac{\sigma_{13}}{\rho^2}$	0	0	0	0	0	0	0	0	0	$-\frac{1}{2}$	0	o /	
							$M_1 =$									

_	_															_	.41)
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_2$	(2)
0	$\Gamma \alpha^2 I$	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_2$	0	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_2$	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{33}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{22}}{\partial A_{33}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}}{\partial A_{33}}$	0	0	0	0	0	0	0	0	$v_2$	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{32}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{22}^2}{\partial A_{32}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{23}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_2$	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}}{\partial A_{31}}$	0	0	0	0	0	0	$v_2$	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}^{22}}{\partial A_{23}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}}{\partial A_{23}}$	0	0	0	0	0	$v_2$	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{22}}{\partial A_{22}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}^{23}}{\partial A_{22}}$	0	0	0	0	$v_2$	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}^{2}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{23}^{23}}{\partial A_{21}}$	0	0	0	$v_2$	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}^{22}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}^{23}}{\partial A_{13}}$	0	0	$v_2$	0	0	0	0	0	0	0	0	0	
			$-\frac{1}{\rho}\frac{\partial\sigma_{22}^{22}}{\partial A_{12}}$					0	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{21}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{22}^{22}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{23}}{\partial A_{11}}$	$v_2$	0	0	0	0	0	0	0	0	0	0	0	
0	0	0	0	$v_2$	0	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	0	
θ	$d\lambda$	0	$v_2$	0	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	0	
0	0	$v_2$	0	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	0	
0	$v_2$	0	<del>1</del> 1 σ	0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(\infty a+a)\sigma}$	0	
/ v2	0	$-\frac{\sigma_{21}}{o^2}$	$-\frac{\sigma_{22}^{\prime}}{\rho^{2}}$	$-\frac{\sigma_{23}}{\rho^2}$	0	0	0	0	0	0	0	0	0	0	$-\frac{T}{o^2}$	· 0 /	
								$M_2 =$									

_																_	2.42)
0	$\Gamma \alpha^{2'}$	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	0	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	$v_3$	0	0	
0				$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{33}}$		0	0	0	0	0	0	0	$v_3$	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{32}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{32}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{33}}{\partial A_{32}}$	0	0	0	0	0	0	0	$v_3$	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{31}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{31}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{33}}{\partial A_{31}}$	0	0	0	0	0	0	$v_3$	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{23}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{23}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{33}}{\partial A_{23}}$	0	0	0	0	0	$v_3$	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{22}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{33}}{\partial A_{22}}$	0	0	0	0	$v_3$	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{21}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{32}}{\partial A_{21}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{33}}{\partial A_{21}}$	0	0	0	$v_3$	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{32}}{\partial A_{13}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{33}}{\partial A_{13}}$	0	0	$v_3$	0	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{12}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{12}}$	$-\frac{1}{\rho} \frac{\partial \sigma_{33}}{\partial A_{12}}$	0	$v_3$	0	0	0	0	0	0	0	0	0	0	
0	0	$-\frac{1}{\rho}\frac{\partial\sigma_{31}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial \sigma_{32}}{\partial A_{11}}$	$-\frac{1}{\rho}\frac{\partial\sigma_{33}}{\partial A_{11}}$	$v_3$	0	0	0	0	0	0	0	0	0	0	0	
θ	$d\lambda$	0	0	$v_3$	0	0	$A_{13}$	0	0	$A_{23}$	0	0	$A_{33}$	0	0	0	
0	0	0	$v_3$	0	0	0	$A_{12}$	0	0	$A_{22}$	0	0	$A_{32}$	0	0	0	
0	0	$v_3$	0	0	0	0	$A_{11}$	0	0	$A_{21}$	0	0	$A_{31}$	0	0	0	
0	$v_3$	0	0	-Π Φ	.0	0	0	0	0	0	0	0	0	0	0	$\frac{T}{(n+n)^{o}}$	(3)
/ v3	0	$-\frac{\sigma_{31}}{\rho^2}$	$-\frac{\sigma_{32}^2}{\sigma^2}$	$-\frac{\sigma_{33}^r}{\rho^2}$	0	0	0	0	0	0	0	0	0	0	0		2
								$M_3 =$									

## Slow Flow

### 3.1 Studying numerical smearing with slow flow past a barrier

A checkerboard pattern appears around the corner of the barrier, leading to a crash, using reflective boundary conditions (in velocity) for the barrier. Do we need a staggered grid?

## RGFM

The RGFM does nothing without a temperature fix when applied to the heat conduction test. The linearisation upon which it is based results in a stationary solution when  $q_L = q_R$  and  $\sigma_L = \sigma_R$  initially. Barton's RGFM is similar. Should q be fixed? Maybe use analytical solution to heat equation at  $t = \Delta t$ ?

# Bibliography