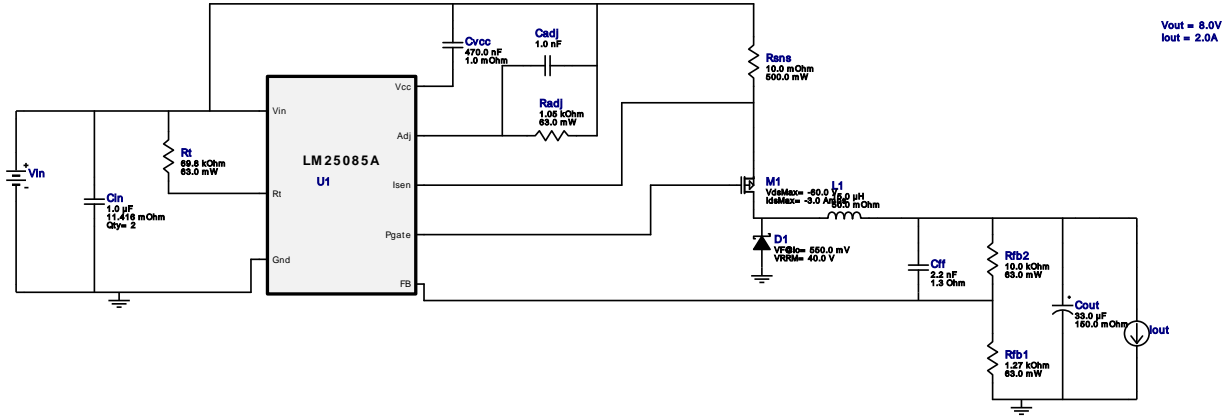


VinMin = 17.0V  
VinMax = 20.0V  
Vout = 8.0V  
Iout = 2.0A

Device = LM25085AMY/NOPB  
Topology = Buck  
Created = 2023-03-22 06:17:44.255  
BOM Cost = \$2.03  
BOM Count = 15  
Total Pd = 1.47W





## WEBENCH® Design Report

Design : 25 LM25085AMY/NOPB  
LM25085AMY/NOPB 17V-20V to 8.00V @ 2A



## Electrical BOM

Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cadj	Samsung Electro-Mechanics	CL21C102JBCNNNC Series= C0G/NP0	Cap= 1.0 nF VDC= 50.0 V IRMS= 0.0 A	1	\$0.01	0805 7 mm <sup>2</sup>
Cff	MuRata	GRM188R71E222KA01D Series= X7R	Cap= 2.2 nF ESR= 1.3 Ohm VDC= 25.0 V IRMS= 0.0 A	1	\$0.01	0603 5 mm <sup>2</sup>
Cin	TDK	C1005X5R1V105K050BC Series= X5R	Cap= 1.0 uF ESR= 11.416 mOhm VDC= 35.0 V IRMS= 1.483 A	2	\$0.03	0402 3 mm <sup>2</sup>
Cout	Panasonic	ATPH33MAHA Series= TPH	Cap= 33.0 uF ESR= 150.0 mOhm VDC= 10.0 V IRMS= 510.0 mA	1	\$0.32	CAPSMT_6_A09 11 mm <sup>2</sup>
Cvcc	Taiyo Yuden	TMK212BJ474KD-T Series= X5R	Cap= 470.0 nF ESR= 1.0 mOhm VDC= 20.0 V IRMS= 0.0 A	1	\$0.02	0805 7 mm <sup>2</sup>
D1	Fairchild Semiconductor	SS24FL	VF@Io= 550.0 mV VRRM= 40.0 V	1	\$0.09	SOD-123F 12 mm <sup>2</sup>
L1	NIC Components	NPI34W150MTRF	L= 15.0 uH 50.0 mOhm	1	\$0.25	IND_NPI34W 172 mm <sup>2</sup>
M1	Fairchild Semiconductor	FDC5614P	VdsMax= -60.0 V IdsMax= -3.0 Amps	1	\$0.25	SOT-23-6 15 mm <sup>2</sup>
Radj	Vishay-Dale	CRCW04021K05FKED Series= CRCW..e3	Res= 1.05 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm <sup>2</sup>
Rfb1	Vishay-Dale	CRCW04021K27FKED Series= CRCW..e3	Res= 1.27 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm <sup>2</sup>

Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Rfb2	Vishay-Dale	CRCW040210K0FKED Series= CRCW..e3	Res= 10.0 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm <sup>2</sup>
Rsns	Stackpole Electronics Inc	CSR1206FK10L0 Series= ?	Res= 10.0 mOhm Power= 500.0 mW Tolerance= 1.0%	1	\$0.11	 1206 11 mm <sup>2</sup>
Rt	Vishay-Dale	CRCW040269K8FKED Series= CRCW..e3	Res= 69.8 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm <sup>2</sup>
U1	Texas Instruments	LM25085AMY/NOPB	Switcher	1	\$0.87	 MUY08A 24 mm <sup>2</sup>

## Operating Values

#	Name	Value	Category	Description
1.	Cin IRMS	986.871 mA	Capacitor	Input capacitor RMS ripple current
2.	Cin Pd	5.559 mW	Capacitor	Input capacitor power dissipation
3.	Cout IRMS	140.689 mA	Capacitor	Output capacitor RMS ripple current
4.	Cout Pd	2.969 mW	Capacitor	Output capacitor power dissipation
5.	D1 Tj	68.33 degC	Diode	D1 junction temperature
6.	Diode Pd	638.83 mW	Diode	Diode power dissipation
7.	IC Pd	243.45 mW	IC	IC power dissipation
8.	IC Tj	41.199 degC	IC	IC junction temperature
9.	IC Tolerance	18.0 mV	IC	IC Feedback Tolerance
10.	ICThetaJA	46.0 degC/W	IC	IC junction-to-ambient thermal resistance
11.	Iin Avg	873.72 mA	IC	Average input current
12.	L Ipp	487.36 mA	Inductor	Peak-to-peak inductor ripple current
13.	L Pd	250.0 mW	Inductor	Inductor power dissipation
14.	M1 Pd	293.63 mW	Mosfet	M1 MOSFET total power dissipation
15.	M1 PdCond	202.42 mW	Mosfet	M1 MOSFET conduction losses
16.	M1 PdSw	91.207 mW	Mosfet	M1 MOSFET switching losses
17.	M1 Tj	52.755 degC	Mosfet	M1 MOSFET junction temperature
18.	Cin Pd	5.559 mW	Power	Input capacitor power dissipation
19.	Cout Pd	2.969 mW	Power	Output capacitor power dissipation
20.	Diode Pd	638.83 mW	Power	Diode power dissipation
21.	IC Pd	243.45 mW	Power	IC power dissipation
22.	L Pd	250.0 mW	Power	Inductor power dissipation
23.	M1 Pd	293.63 mW	Power	M1 MOSFET total power dissipation
24.	M1 PdCond	202.42 mW	Power	M1 MOSFET conduction losses
25.	M1 PdSw	91.207 mW	Power	M1 MOSFET switching losses
26.	Total Pd	1.474 W	Power	Total Power Dissipation
27.	BOM Count	15	System Information	Total Design BOM count
28.	Duty Cycle	41.925 %	System Information	Duty cycle
29.	Efficiency	91.562 %	System Information	Steady state efficiency
30.	FootPrint	281.0 mm <sup>2</sup>	System Information	Total Foot Print Area of BOM components
31.	Frequency	606.795 kHz	System Information	Switching frequency
32.	Iout	2.0 A	System Information	Iout operating point

#	Name	Value	Category	Description
33.	Mode	CCM	System Information	Conduction Mode
34.	Pout	16.0 W	System Information	Total output power
35.	SW Ipk	2.244 A	System Information	Peak switch current
36.	Total BOM	\$2.03	System Information	Total BOM Cost
37.	Vin	20.0 V	System Information	Vin operating point
38.	Vout	8.0 V	System Information	Operational Output Voltage
39.	Vout Actual	7.987 V	System Information	Vout Actual calculated based on selected voltage divider resistors
40.	Vout Tolerance	3.828 %	System Information	Vout Tolerance based on IC Tolerance (no load) and voltage divider resistors if applicable
41.	Vout p-p	73.167 mV	System Information	Peak-to-peak output ripple voltage

## Design Inputs

Name	Value	Description
Iout	2.0	Maximum Output Current
VinMax	20.0	Maximum input voltage
VinMin	17.0	Minimum input voltage
VinTyp	18.0	Typical input voltage
Vout	8.0	Output Voltage
base_pn	LM25085A	Base Product Number
source	DC	Input Source Type
Ta	30.0	Ambient temperature

## WEBENCH® Assembly

### Component Testing

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of  $C_{in}$  and  $C_{out}$ , and the inductance and DC resistance of  $L1$  before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

### Soldering Component to Board

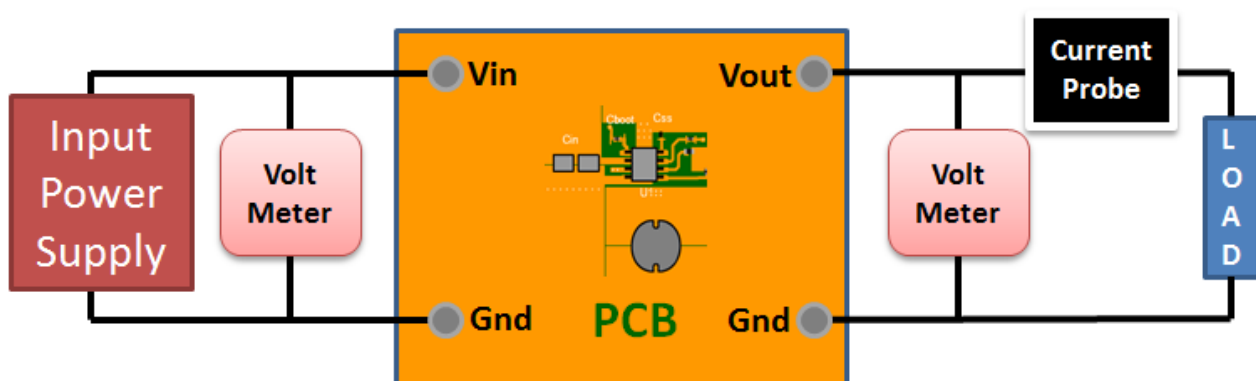
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab down to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

### Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 17.0V and set the input supply's current limit to zero. With the input supply off connect up the input supply to  $V_{in}$  and GND. Connect a digital volt meter and a load if needed to set the minimum load of the design from  $V_{out}$  and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

### Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between  $V_{in}$  and GND, a load is connected between  $V_{out}$  and GND and a current meter is connected in series between  $V_{out}$  and the load. The load must be able to handle at least rated output power + 50% ( 7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.

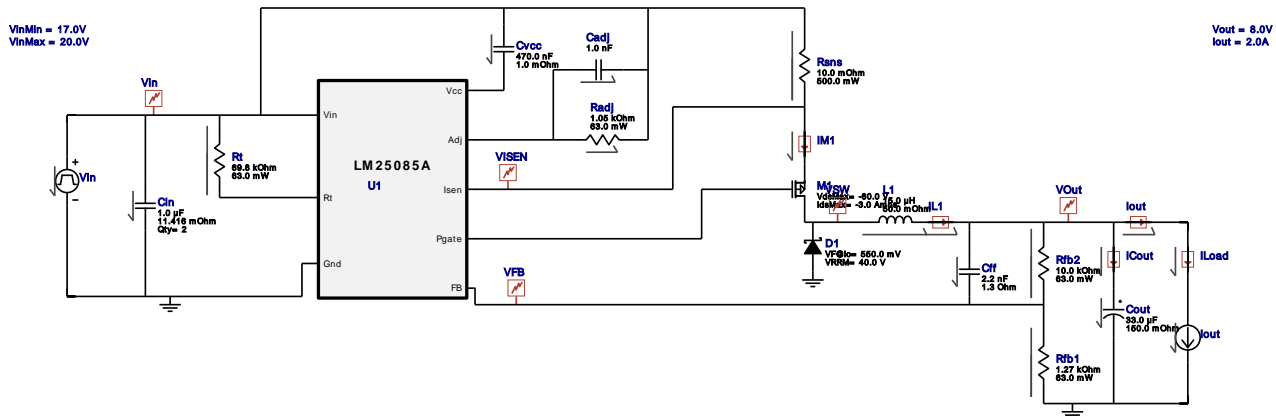


# WEBENCH® Electrical Simulation Report

Design Id = 25

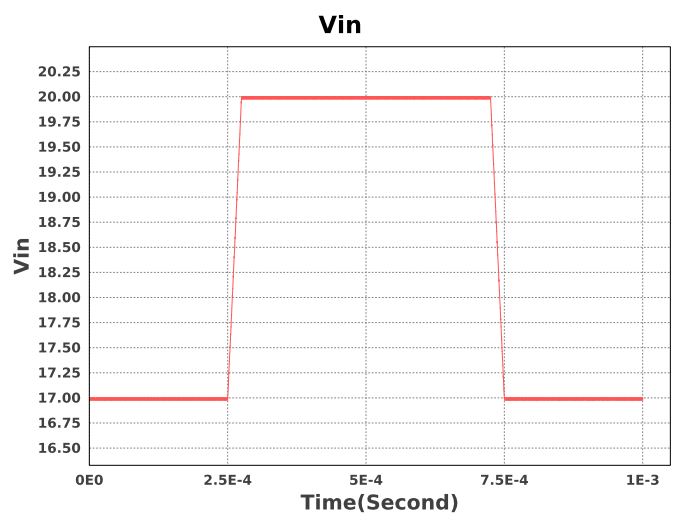
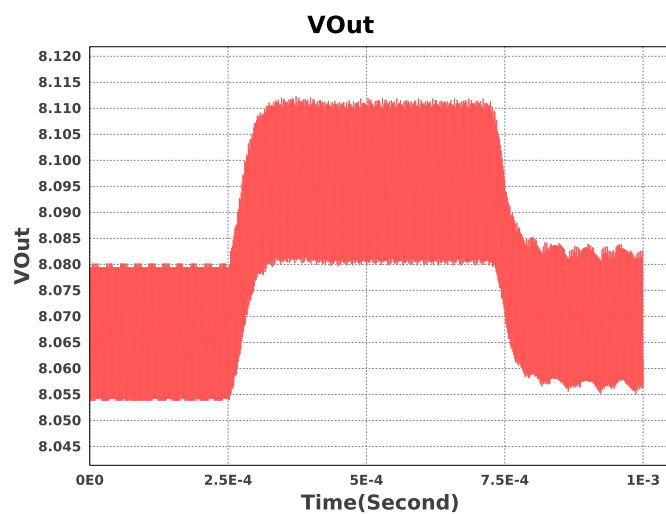
sim\_id = 3

Simulation Type = Input Transient



## Simulation Parameters

#	Name	Parameter Name	Description	Values
1.	Iout	I	Load Current	2.0 A



## Design Assistance

1. For a Constant On Time device to be stable, we need to provide a ripple at the feedback comparator. There are various methods to implement the ripple. Depending on the circuit complexity vs. the allowable ripple, we have three options to choose from. The simplest option, 'Low Complexity', would require only a high ESR cap at the output. This means that the BOM count will be small, but the output voltage ripple will be quite large. The 'optimal solution' would require a feed-forward cap in parallel with the upper feedback resistor to AC couple the ripple to the feedback node. This increases the BOM count slightly, but now we have more control over the output voltage ripple. If the output voltage requirement is very tight, then the best option is to go for the 'Low Output Ripple' solution. In this option we can go with very low ESR output caps and have very good control over the output voltage ripple

2. Master key : B9BB535380F6DCECC9D62E6CF388EC6F[v1]

3. **LM25085A** Product Folder : <http://www.ti.com/product/LM25085A> : contains the data sheet and other resources.

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