

# Numpy code for calculating multi-component adsorption isotherms using ideal adsorbed solution theory

Jurn Heinen

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## 1 Computer code

Multicomponent adsorption isotherms are frequently predicted from single component isotherms using the well-known ideal adsorbed solution theory (IAST) introduced by Myers and Prausnitz.[1] The advantage of IAST is also that it is able to compute mixture adsorption using any molar composition. Here, we consider a binary mixture only.

IAST is based on three assumptions: (1) all adsorbates have access to the same surface area of the sorbent, (2) the sorbent is inert, and (3) the mixture in the adsorbed phase behaves as an ideal solution at constant temperature and spreading pressure.

The spreading pressure  $\pi$  can be thought of as the negative of the surface tension and can be calculated via the Gibbs isotherm[1]

$$\frac{\pi A}{RT} = \int_0^{P_i^0} \frac{q_i}{P} dP \quad (1)$$

with  $A$  the surface area of the sorbent,  $R$  the gas constant,  $T$  the temperature,  $P_i^0$  the partial pressure for component  $i$  at the spreading pressure,  $q_i$  the single component  $i$  adsorption isotherm and  $P_i$  the component pressure of the bulk phase. The fugacity coefficient is set to one. Here,  $q_i$  is fitted to a Langmuir isotherm  $q_i = q_{\text{sat},i} b_i P / (1 + b_i P)$ . Integrating equation (1) analytically gives

$$\int_0^{P_i^0} \frac{q_i}{P} dP = q_{\text{sat},i} \ln \left( 1 + b_i P_i^0 \right). \quad (2)$$

For arbitrary defined isotherm models, it might be necessary to perform the integration numerically. At equilibrium, the spreading pressures of all components are equivalent. Therefore, for a two-component system the following relation holds

$$q_{\text{sat},1} \ln \left( 1 + b_1 \frac{P y_1}{x_1} \right) - q_{\text{sat},2} \ln \left( 1 + b_2 \frac{P y_2}{1 - x_1} \right) = 0 \quad (3)$$

with  $x_2 = 1 - x_1$ . The adsorbed-vapour phase is described by an analog of Raoult's law

$$\frac{P y_i}{x_i} = P_i^0 \quad (4)$$

with  $x_i$  being the mole fraction of component  $i$  in the adsorbed phase. Listing 1 shows a routine that solves equation (3) for  $x_1$  using the analytical expression.

Listing 1: Find root of equation (3) and obtain  $x_1$  using analytical integrating of the Gibbs isotherm.

```

1 def iastLangmuirAnalytical(x, data):
2     P, y, isotherm = data[0], data[1], data[2]
3
4     isotherm1 = isotherm[0]
5     isotherm2 = isotherm[1]
6
7     f = isotherm1[0]*np.log(1+isotherm1[1]*y[0]*P/x) - isotherm2[0]*np.log(
8         1+isotherm2[1]*((y[1]*P)/(1 - x)))
9     return f
10
11 f = fsolve(iastLangmuirAnalytical, x0, args=data)
12 x[0] = f
13 x[1] = 1 - x[0]
```

The scipy function *fsolve()* returns the root of the function *iastLangmuirAnalytical()*. This root is  $x_1$  and for a two-component mixture  $x_2 = 1 - x_1$ . Also, equation (1) can also be integrated numerically to obtain  $x_1$  and  $x_2$ . Listing 2 shows this procedure using *integrate.quad()* method from scipy.

Here, the upper integration limits are unknown. Both integrals should be equal. Using *fsolve()*, the upper limit is found.

Listing 2: Numerical integration of the Gibbs isotherm to obtain  $x_1$  and  $x_2$ .

```

1 def iastLangmuirNumerical(x, data):
2     P, y, isotherm = data[0], data[1], data[2]
3
4     isotherm1 = isotherm[0]
5     isotherm2 = isotherm[1]
6
7     f1, err1 = integrate.quad(langmuirNumerical, 0, y[0]*P/x,
8                               args=(isotherm1))
9     f2, err2 = integrate.quad(langmuirNumerical, 0, y[1]*P/(1-x),
10                               args=(isotherm2))
11
12     f = f1 - f2
13     return f
```

Next, the total adsorption capacity  $q_T$  is obtained from

$$\frac{1}{q_T} = \sum_i^N \frac{x_i}{q_i(P_i^0)} \quad (5)$$

with  $q_i = x_i q_T$ . Here,  $q_i$  (not  $q_i(P_i^0)$ ) is the actual adsorbed amount of component  $i$  in the mixture. In the code, it is given as follows:

Listing 3: Compute the mixture adsorption isotherms based on equation (5).

```

1 q = langmuir(P*(S.y/x), S.params)
2
3 qtot = 1.0/np.sum(x/q)
4 q_mix = qtot * x
```

Remember that the variables  $x$  and  $S.y$  are numpy arrays!

## 2 Example: equimolar methane/ethane mixture in ZIF-8 at 433 K.

In the directory 'data', you will find the input files and results of this section.

Figure 1 show the (a) single and (b) multi component adsorption isotherm of methane and ethane in ZIF-8 at 433 K. These adsorptions isotherms are calculated using grand-canonical Monte Carlo (GCMC) simulations[2], see subsection 2.1. The Langmuir isotherm parameters are presented in Table 1.

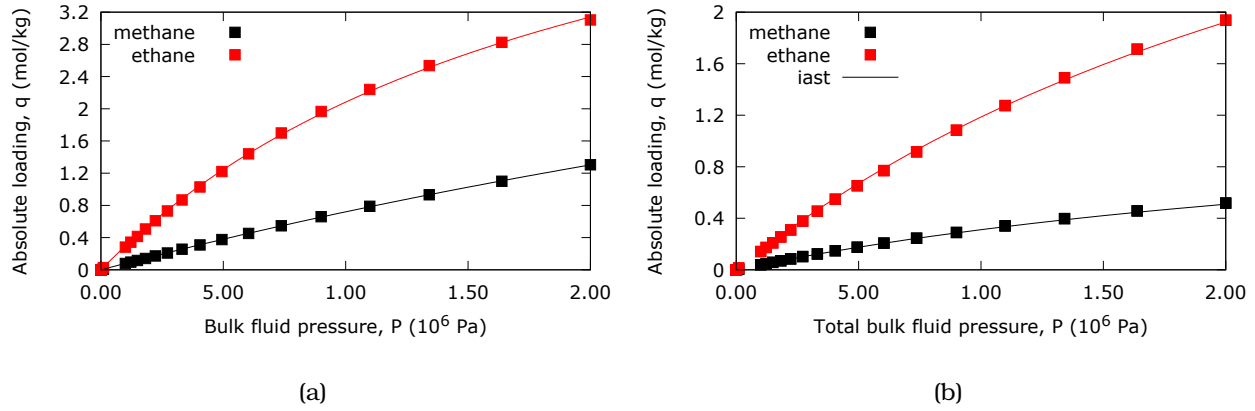


Figure 1: Adsorption isotherm of methane (black) and ethane (red) in ZIF-8 at 433 K. Data points are obtained from GCMC simulations. (a) Single component isotherm; solid lines are fitted Langmuir isotherms. (b) Multi component isotherms; solid lines are IAST predictions.

Table 1: Langmuir isotherm parameters of methane and ethane.

methane		ethane	
$q_{\text{sat},1}$ (mol/kg)	$b_1 \cdot 10^{-7}$ ( $\text{Pa}^{-1}$ )	$q_{\text{sat},2}$ (mol/kg)	$b_2 \cdot 10^{-7}$ ( $\text{Pa}^{-1}$ )
6.85	1.18	6.37	4.85

## 2.1 Grand-canonical Monte Carlo simulations for single component adsorption isotherms

Grand-canonical Monte Carlo simulations adsorbates (methane, ethane) are allowed to move between the open volumes of the crystalline unit cell of the porous material (ZIF-8) and an reservoir. After a considerable amount of insertions of the adsorbates into the unit cell, the chemical potentials of the adsorbates inside the porous material and of the reservoir are equal. The interactions of the adsorbate-adsorbate and adsorbate-porous material are calculated using force fields. These are *a priori* defined interactions between the various atom types.

The Van der Waals cut-off radius was set to 12.0 Å. To maintain the minimum image convention, a 2 x 2 x 2 unit cell was used with a lattice constant of  $a = 16.991$  Å. Non-bonding interactions are described using the Lennard-Jones potentials. For the framework, these are based on the DREIDING and UFF force field (GenericMOFs in RASPA-2.0) and for the adsorbates, the TraPPE force field is used. Note that the TraPPE force field is neutral, therefore no electrostatics are considered. The number of production cycles was set to 100000 and the number of initialization cycles to 50000. These are fairly standard settings but are sufficient for this system.

For more details on calculating adsorption properties using GCMC simulations the reader is referred to [3, 2, 4]

## References

- [1] A. L. Myers and J. M. Prausnitz. Thermodynamics of mixed-gas adsorption. *AIChE J.*, 11:121–127, 1965.
- [2] David Dubbeldam, Ariana Torres Knoop, and Krista S. Walton. On the inner workings of monte carlo codes. *Mol. Simul.*, 39(14-15):1253–1292, 2013.
- [3] Daank Frenkel and Berend Smit. *Understanding Molecular Simulation: From Algorithms to Applications*. Academic Press, 2 edition, 2001.
- [4] David Dubbeldam and Krista S. Walton. On the application of classical molecular simulations of adsorption in metal-organic frameworks. In Jianwen Jiang, editor, *Materials Modeling towards Engineering Applications*. Pan Stanford Publishing Pte Ltd., 2015.