

High Scanning-Rate Periodic Leak-Wave Antennas using Complementary Microstrip-Slotline Stubs

Jianwen Chen, Qingfeng Zhang*

Southern University of Science and Technology, Shenzhen, China

Email: *zhang.qf@sustc.edu.cn

Abstract - A series-fed patch (SFP) array leaky-wave antenna can realize the frequency scanning. To increase the scanning rate, we add complementary microstrip-slotline stubs between the patches. The complementary microstrip-slotline stub is an all-pass filter and its group delay is smooth and continuous, and it maintains a flat magnitude response within an ultra-wide bandwidth. It significantly increases the slope of phase versus frequency and hence the scanning rate when cascading with the series-fed patch leaky-wave antennas. Three examples are provided in comparison with the conventional one. The results show that the new leaky-wave antennas increase the scanning rate by 42%-72%.

Index Terms —group delay, series-fed patch (SFP) array, leaky-wave antennas, dispersive delay line, microstrip line, slotline.

I. INTRODUCTION

LEAKY-WAVE antennas (LWAs) have been applied in many communication systems or radars at microwave frequency because they have a lot of advantages such as low cost, simple configuration, light weight, easy manufacturing and integrability with other electronic components [1]. Therefore, since nineteenth century, they have been widely studied and used in many fields [2], [3]. A typical example of these applications is millimeter-wave imaging systems. Usually they require the antennas with high scanning-rate within a narrow bandwidth so that the system is simple [4]. Leaky wave antennas are attractive for imaging applications due to their simple feeding network and system architecture.

Leaky-wave antennas can be broadly classified into periodic and continuous structures [5]. Periodic leak-wave antennas are achieved by introducing periodic perturbations, such as short-circuited stubs, dielectric gratings, and slot oriented structures. Continuous leaky-wave antennas are based on fast-wave transmission lines, e.g. metallic waveguides. One important feature of leaky-wave antennas is that it scans the beam as the frequency changes. Usually, it requires several gigahertz to scans the half space, and thus the scanning rate is low. A high scanning rate antenna is highly demand in narrow-band applications. One possible way is to employ all-pass delay lines [6]-[9]. However, C-section structures requires stripline implementation, which make the fabrication difficult.

This paper presents an approach to increase the scanning rate using complementary microstrip-slotline stubs, which has a smooth and continuous group delay curve and a flat

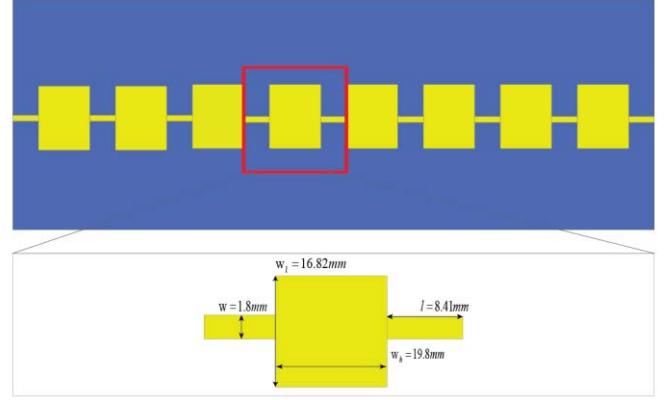


Fig. 1. The series-fed patch (SFP) array antenna (the permittivity of the substrate is $\epsilon_r = 2.2$ and the height is $h = 1.5\text{mm}$).

magnitude response in a wide frequency band [10]. The advantages of this structure are simple structure, wide operational bandwidth and easy fabrication.

II. PERIODIC SERIES-PATCH LEAKY-WAVE ANTENNA

Fig. 1 shows the structure of the periodic series-fed patch (SFP) leaky-wave antenna that we use in this paper. We consider that the antenna structures are terminated by matched loads, so as to operate in a traveling-wave regime. Following the standard frequency-angle scanning law [2], [11-12], we have

$$\theta_{\text{MB}}(\omega) = \sin^{-1} \left[\frac{\beta_n(\omega)}{k_0} \right] = \sin^{-1} \left[\frac{c\beta_n(\omega)}{\omega} \right] \quad (1a)$$

with

$$\beta_n(\omega) = \beta_0(\omega) + n \frac{2\pi}{p} \quad (1b)$$

where $\theta_{\text{MB}}(\omega)$ is the main-beam radiation angle, $\beta_n(\omega)$ presents the n^{th} space harmonic, ω is the angular frequency, c is the speed of light in free space, $k_0 = \omega/c$ is the free-space wavenumber, p is the period of the structure.

This configuration consists of 8 unit cells and the working frequency range is from 5.2 GHz to 6.2 GHz. Fig. 2 and Fig. 3 show the simulated scattering parameters and beam scanning property of this antenna, respectively.

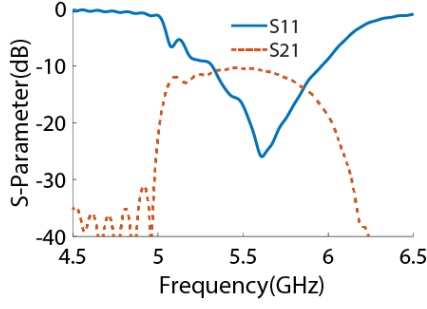


Fig. 2. The S-parameter of the SFP leaky-wave antenna.

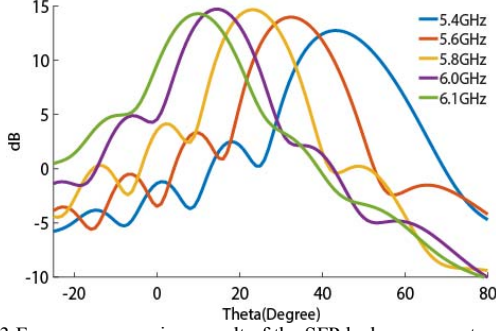


Fig. 3. Frequency scanning result of the SFP leaky-wave antenna.

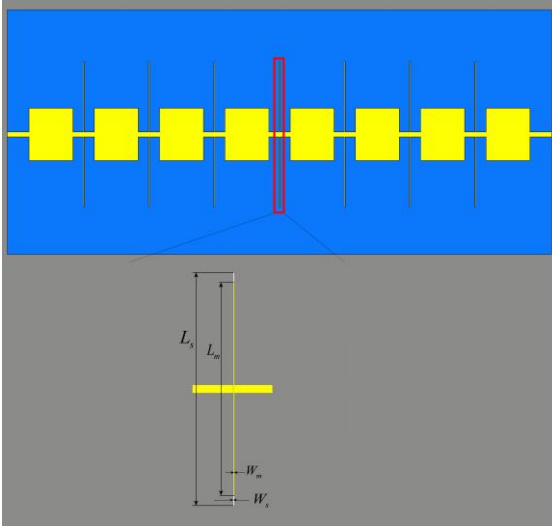


Fig. 4. The proposed new leaky-wave antenna with complementary microstrip-slotline stubs ($W_s = W_m = 0.2\text{mm}$).

III. LEAKY-WAVE ANTENNA WITH COMPLEMENTARY MICROSTRIP-SLOTLINE STUBS

To increase the scanning rate, we propose a new leaky-wave antenna in Fig. 4, which is realized by inserting complementary microstrip-slotline stubs between the series patch elements. The microstrip-slotline stub, as shown in the zoomed figure of Fig. 4, is composed of an open stub and slotline on the ground plane with equal widths ($W_m = W_s$) but different lengths (L_s longer than L_m). Fig. 5 and 6 show the S-parameters and group delay of this microstrip-slotline stub, respectively. Note that it exhibits a flat magnitude within a wide frequency band and a group delay peak at some specific frequencies. By aligning the peak group delay with the operational frequency band of the SFP antenna, we can increase the scanning rate.

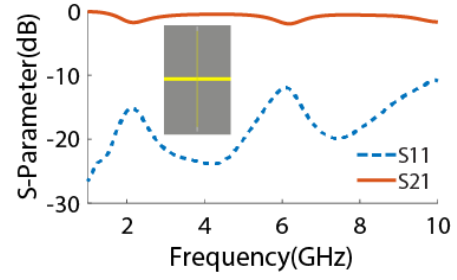


Fig. 5. S-parameter of the complementary microstrip-slotline stub

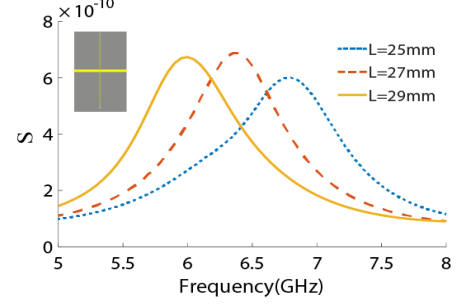


Fig. 6. Group delays for different lengths L_m .

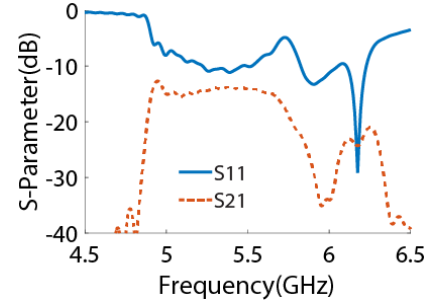


Fig. 7. S-parameter of the overall leaky-wave antenna in Fig. 4.

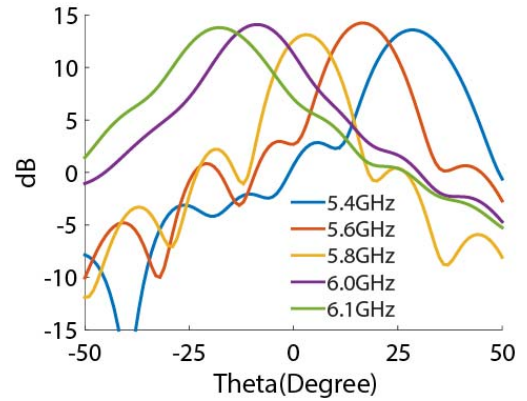


Fig. 8. Scanning beams of the antenna ($L_m = 26.4\text{mm}$, $L_s = 28\text{mm}$).

Fig. 7 shows the scattering parameters of the overall leaky-wave antenna including both microstrip-slotline stubs and SFPs. By comparing it with Fig. 2, one finds that the reflection is slightly degraded after inserting microstrip-slotline stubs. To verify the scanning rate of the new antenna, we design three different microstrip-slotline stubs, namely stub 1, stub 2 and stub 3. Their scanning responses are shown in Figs. 8-10. Note that, the scanning range clearly increases

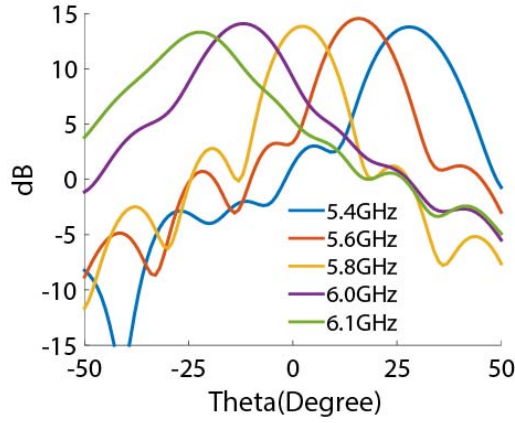


Fig.9. Scanning beams of the antenna ($L_m=26.4\text{mm}$, $L_s=29\text{mm}$).

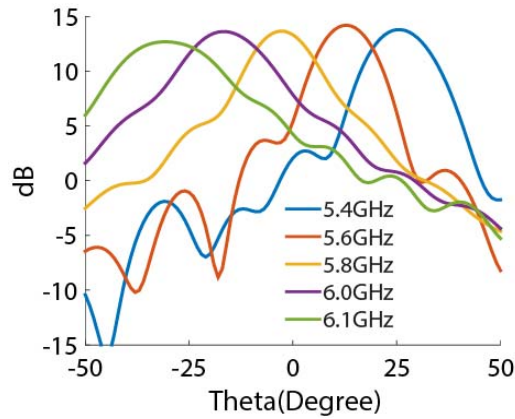


Fig.10. Scanning beams of the antenna ($L_m=27\text{mm}$, $L_s=29\text{mm}$).

TABLE I Comparison of Beam Angles and Ranges

	5.4GHz	5.8GHz	6.1GHz	Range
SFP	43°	23°	10°	33°
SFP with stub1	29°	3°	-18°	47°
SFP with stub2	28°	2°	-22°	50°
SFP with stub3	26°	-3°	-31°	57°

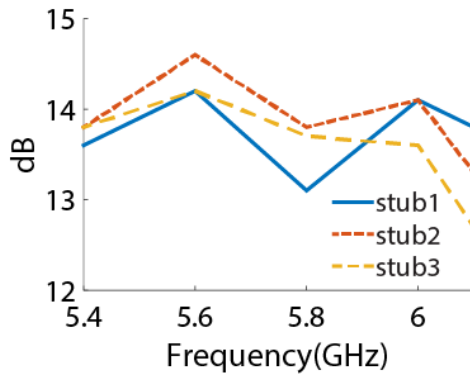


Fig. 11. The gain versus frequency responses of stub1, stub2 and stub3.

compared with the one without stubs in Fig. 3. To better see the improvement, Tab. I summarize the beam angles and ranges for different leaky-wave antennas from 5.4 GHz to 6.1 GHz. Note that, the scanning range of the original SFP without stubs is only 33°. Stub 1 has improved the scanning ranges by 42.4%, stub 2 has improved by 51.5%, and stub 3 has improved by 72.7%. Accordingly, one increases the scanning rate by employing the microstrip-slotline stubs in the conventional leaky-wave antennas. In general, the SFP leaky-wave antennas can be replaced by other configurations. Therefore, the proposed approach is a general technique to increase the scanning rate.

IV. CONCLUSION

A SFP leaky-wave antenna with complementary microstrip-slotline stubs has been proposed and illustrated. The complementary microstrip-slotline stub significantly increased the slope of phase versus frequency and hence the scanning rate when cascading with the series-fed patch leaky-wave antennas. Three examples were provided in comparison with the conventional one. The results revealed that the new leaky-wave antennas increased the scanning rate by 42%-72%.

ACKNOWLEDGMENT

This work is supported by Shenzhen Development and Reform Commission Funds ([2015]1939, [2015]944).

REFERENCES

- [1] Simon Otto, Andreas Rennings and Christophe Caloz, "Transmission Line Modeling and Asymptotic Formulas for Periodic Leaky-Wave Antennas Scanning Through Broadside", IEEE transactions on antennas and propagation, vol. 59, no. 10, October 2011
- [2] A. Hessel, Antenna Theory, Part II, R. E. Collin and R. F. Zucker, Eds. New York: McGraw-Hill, 1969, ch. 19
- [3] A. A. Oliner and D. R. Jackson, Antenna Engineering Handbook, J. Volakis, Ed., 4th ed. New York: McGraw-Hill, 2007.
- [4] Mohammadreza Ranjbar Naeini, Mohammad Fakharzadeh, Forouhar Farzaneh, "Travelling-Wave Ka-band Frequency Scanning Antennas For Millimeter-wave Imaging Applications", 8th International Symposium on Telecommunications (IST'2016), 2016.
- [5] D. R. Jackson, C. Caloz, and T. Itoh, "Leaky-wave antennas," Proc. IEEE, vol. 100, no. 7, pp. 2194–2206, Jul. 2012.
- [6] E. G. Cristal, "Analysis and exact design of cascaded commensurate transmission-line C-section all-pass networks," IEEE Trans. Microw. Theory Tech., vol. MTT-14, no. 6, pp. 285–291, Jun. 1966.
- [7] S. Gupta, A. Parsa, E. Perret, R. V. Snyder, R. J. Wenzel, and C. Caloz, "Group-delay engineered noncommensurate transmission line all pass network for analog signal processing," IEEE Trans. Microw. Theory Tech., vol. 58, no. 9, pp. 2392–2407, Sep. 2010.
- [8] R.L.Crane, "All-pass networks synthesis," IEEE Trans. Circuit Theory, vol. 15, no. 4, pp. 474–477, Dec. 1968.
- [9] K. Murase, R. Ishikawa, and K. Honjo, "Group delay equalized monolithic microwave integrated circuit amplifier for ultra-wideband based on right/left-handed transmission line design approach," Inst. Elec. Tech. Microw. Ant. Propag., vol. 3, no. 6, pp. 967–973, 2009.
- [10] Mrinal Kanti Mandal, Dominic Deslandes and Ke Wu, "Complementary Microstrip-Slotline Stub Configuration for Group Delay Engineering", IEEE microwave and wireless components letters, vol. 22, no. 8, August 2012
- [11] A. Hessel, Antenna Theory, Part II, R. E. Collin and R. F. Zucker, Eds. New York: McGraw-Hill, 1969, ch. 19
- [12] C. Caloz, D. R. Jackson, and T. Itoh, Frontiers in Antennas, F. Gross, Ed. New York: McGraw-Hill, 2010.