

An Introduction to Discontinuous Galerkin Methods

Module 3B: To Higher-Orders - Discrete System

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Numerical Quadrature (Gauss)

Hermite Interpolation (and quadrature)

Truncation error/exact quadrature

GL Lagrange Orthogonality

Local Mapping Function (Jacobian)

Mass Matrix- Diagonalization

Log differentiation

Stiffness Integral

Numerical Flux (Extrapolated)

Assembly of System

RK4 Time discretization

Investigate p-Convergence

Numerical Quadrature (Gauss)

- ▶ We now have a method for generating a robust arbitrary order solution approximation, but unlike before it isn't practical to analytically pre-calculate all the integrals.
- ▶ We can use a numerical quadrature technique to do this instead, able to integrate arbitrary functions
- ▶ If we call the interpolation of a function Inf then we assume that for a sufficiently accurate interpolation, we can use the interpolation of the function wherever we could use the function itself before. This is in general $M-1$ order accurate.

$$f \approx Inf = \sum_{i=0}^M f(x_i) L_i(x) \quad (1)$$

$$\int f \approx \int Inf = \int \sum_{i=0}^M f(x_i) L_i(x) = \sum_{i=0}^M f(x_i) \int L_i(x) = \sum_{i=0}^M f(x_i) w_i \quad (2)$$

Hermite Interpolation (and quadrature)

- ▶ Recall: Hermite interpolation includes derivatives of interpolated function as well
- ▶ Consider a Hermite interpolation polynomial that includes first derivatives as well, the interpolation would be $2M - 1$ accurate. The quadrature using this polynomial would look like:

$$\int f dx \approx \sum_{i=0}^M f(x_i)w_i + \sum_{i=0}^M \left[f'(x_i) \int (x - x_i)L_i^2(x) dx \right] \quad (3)$$

- ▶ It turns out if we choose our quadrature/interpolation points to be the Legendre roots, the integral for the second term is zero. Thus no first derivative terms are needed for the Hermite quadrature, even though it is $2M - 1$ order accurate.

Truncation error/exact quadrature

- ▶ It is important to consider error sources from the approximation to the solution and integrals, these can affect convergence
- ▶ Three main error sources in quadrature: aliasing, truncation, and inexact quadrature
- ▶ Aliasing occurs if the function is not sampled frequently enough, it is assumed that the sol'n is sufficiently smooth and the discretization suitably fine to avoid this in most cases
- ▶ Truncation is unavoidable except where the exact function is of equal or lesser order than the interpolation/quadrature. Higher order terms present in the exact function are left off.
- ▶ Inexact quadrature occurs when the total polynomial order of the product of the interpolated functions undergoing quadrature exceeds the exactness of the quadrature. For Gauss-Legendre quadrature this isn't a problem for one and even two functions in the integrand. Each function is of order $M-1$ and the quadrature is exact for $2M-1$, so the quadrature is able to exactly integrate the interpolation

GL Lagrange Orthogonality

- ▶ A final useful property of the Lagrange basis with Legendre interpolation points is orthogonality
- ▶ The product of two $M - 1$ order Lagrange bases can be rearranged to be a Legendre poly of order M and a remainder polynomial of order $M - 2$
- ▶ The remainder polynomial can be expressed as a linear combination of Legendre polys all of order $< M$, all are orthogonal to the order M Legendre, so

$$\int_{-1}^1 L_i(x)L_j(x) dx = \delta_{ij}w_i \quad (4)$$

Local Mapping Function (Jacobian)

- ▶ The domain of orthogonality for Legendre polynomials (and by extension GL Lagrange) is $[-1, 1]$
- ▶ Elements may be arbitrary sizes though, we'd like to be able to transform $x \in [x_L, x_R] \rightarrow X \in [-1, 1]$ by means of a mapping $x = g(X)$ and it's inverse $X = G(x)$

$$x = g(X) = \frac{X + 1}{2} \Delta x + x_L, \quad X = G(x) = \frac{2(x - x_L)}{\Delta x} + 1 \quad (5)$$

- ▶ Applying a change of variables for the mapping

$$\int_{x_L}^{x_R} L_i(x) L_j(x) dx \rightarrow \int_{-1}^1 L_i(g(X)) L_j(g(X)) g' dX \quad (6)$$

- ▶ $J = g' = \frac{\Delta x}{2}$ is called the determinant of the Jacobian matrix

Mass Matrix- Diagonalization

- ▶ We have done what seems like quite a bit of tangential work, but it now pays off

$$\sum_{i=0}^M \frac{d\tilde{q}_i}{dt} \int_k \psi_i(x) \phi_j(x) dx = \sum_{i=0}^M \frac{d\tilde{q}_i}{dt} \int_I L_i(X) L_j(X) \frac{\Delta x}{2} dX \quad (7)$$

$$= \frac{\Delta x}{2} \sum_{i=0}^M \frac{dq_i}{dt} \delta_{ij} w_i = \frac{\Delta x}{2} q'_j w_j \quad \text{for all } j \quad (8)$$

- ▶ We've reduced the full mass matrix into a diagonal mass matrix with all other terms zero, compared to Module 2 solver case the mass matrix is trivially invertible. We have: $\frac{\Delta x}{2} \mathbf{q}' \mathbf{M}$ where $\mathbf{M}_{jj} = w_j$

Log differentiation

- ▶ We can get a closed form expression for $L'_j(x)$ in the stiffness term by using logarithmic differentiation
- ▶ The main idea is that in general $f'/f = \ln(f)$ so applying this to our Lagrange basis

$$L'_j(x) = L_j \sum_{r=0, r \neq j}^N \frac{1}{x - x_r} \quad (9)$$

- ▶ using our previous function code for " $Lag(x)$ " we can get a general expression $dLag = @ (x, nv)$
 $Lag(x, nv) .* sum(1 ./ bsxfun(@minus, x, nn(nv, :, :)), 3)$
- ▶ We need a more involved method for evaluation at the interp points (see dLagrange.m)

Stiffness Integral

- ▶ We now have a routine for calculating L'_j , and suitable quadrature; we can evaluate the stiffness integral

$$\int_k \sum_{i=0}^M \left[c\tilde{q}_i \psi_i(x) \right] \phi'_j(x) dx = \sum_{i=0}^M c\tilde{q}_i \int_I L_i(X) L'_j(X) dX \quad (10)$$

- ▶ No Jacobian term from the mapping. The derivative in the integrand produces a complementary $1/J$ that cancels due to the change of variables.
- ▶ No tricks to be had for reducing the stiffness matrix, it is a full matrix. We have: $c\mathbf{K}_{ji} \tilde{\mathbf{q}}$

Numerical Flux (Extrapolated)

- ▶ One downside of using Gauss-Legendre points is there are no points on the boundary
- ▶ It is easy to calculate the boundary solution values from the solution interpolation at the left end (same idea for the right)

$$\tilde{q}(x_L) = \sum_{i=0}^M \tilde{q}_i L_i(x_L) \quad (11)$$

- ▶ Call $L_i(x_L) = L_{iL}$, the vector notation is then $\tilde{q}_L = \mathbf{L}_{iL}^T \tilde{\mathbf{q}}$
- ▶ So that our numerical flux vector is $\hat{\mathbf{f}} = c(\tilde{q}_R^k \mathbf{L}_{jR} - \tilde{q}_R^{k-1} \mathbf{L}_{jL})$
- ▶ Lobatto alternative gives boundary points, but would make the mass matrix a full matrix. Inversion is likely more expensive than interpolation

Assembly of System

- ▶ We can now combine the mass, stiffness, and numerical flux terms

$$\frac{\Delta x}{2} \mathbf{q}' \mathbf{M} + \hat{\mathbf{f}} - c \mathbf{K}_{ji} \tilde{\mathbf{q}} = 0 \quad (12)$$

- ▶ solving for q'

$$\tilde{\mathbf{q}}' = \frac{2}{\Delta x} (c \mathbf{K}_{ji} \tilde{\mathbf{q}} - \hat{\mathbf{f}}) \mathbf{M}^{-1} \quad (13)$$

- ▶ it is also possible to represent it componentwise easily thanks to the diagonal mass matrix

$$\tilde{q}'_j = \frac{2}{w_j \Delta x} (c \mathbf{K}_{j-} \tilde{\mathbf{q}} - \hat{f}_j) \quad (14)$$

RK4 Time discretization

- ▶ Compared to the simple linear DG solver, we'd like to use a higher order time discretization, Runge-Kutta 4th order: RK4. We can express as a function: $\tilde{\mathbf{q}}'(\tilde{\mathbf{q}})$ from our discrete system. RK4 consists of 4 trial steps:

$$k_1 = \tilde{\mathbf{q}}'(\tilde{\mathbf{q}}) \Delta t$$

$$k_2 = \tilde{\mathbf{q}}'(\tilde{\mathbf{q}} + \frac{k_1}{2}) \Delta t$$

$$k_3 = \tilde{\mathbf{q}}'(\tilde{\mathbf{q}} + \frac{k_2}{2}) \Delta t$$

$$k_4 = \tilde{\mathbf{q}}'(\tilde{\mathbf{q}} + k_3) \Delta t$$

$$\mathbf{q}(t+1) = \mathbf{q} + \frac{k_1}{6} + \frac{k_2}{3} + \frac{k_3}{3} + \frac{k_4}{6}$$

Investigate p-Convergence

- ▶ How does the p-convergence rate compare with h-convergence?
- ▶ Does the smoothness of the initial sol'n seem to effect the rate of convergence? (e.g. $\sin(x)$ vs gaussian curve)
- ▶ Does h or p refinement seem to be more efficient?