

# PID Tuning – Frequency Response Method

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## 1. INTRODUCTION

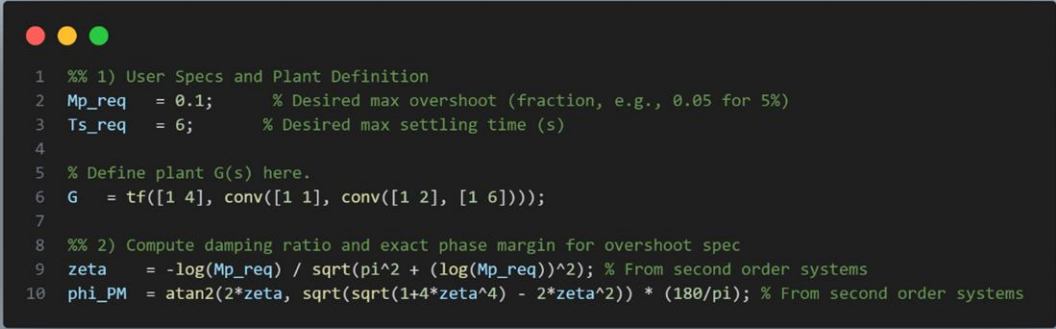
PID controllers are fundamental in control systems due to their versatility and ease of implementation. Among various tuning methods, the **frequency-response approach** provides a direct link between time-domain performance and frequency-domain stability measures, such as phase margin and crossover frequency.

This report first outlines the standard frequency-domain PID tuning method. Then, it presents a semi-automated implementation based on **second-order system approximations**, enabling control over **maximum overshoot** and **settling time** through systematic calculations.

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## 2. CLASSICAL FREQUENCY-RESPONSE PID TUNING

### 2.1 Design Specifications



```
1 %% 1) User Specs and Plant Definition
2 Mp_req = 0.1; % Desired max overshoot (fraction, e.g., 0.05 for 5%)
3 Ts_req = 6; % Desired max settling time (s)
4
5 % Define plant G(s) here.
6 G = tf([1 4], conv([1 1], conv([1 2], [1 6])));
7
8 %% 2) Compute damping ratio and exact phase margin for overshoot spec
9 zeta = -log(Mp_req) / sqrt(pi^2 + (log(Mp_req))^2); % From second order systems
10 phi_PM = atan2(2*zeta, sqrt(sqrt(1+4*zeta^4) - 2*zeta^2)) * (180/pi); % From second order systems
```

Define time-domain specifications:

- Maximum overshoot:  $M_p$  (e.g., 0.05 for 5%)
- Settling time:  $T_s$  (in seconds)

These are then converted into frequency-domain targets:

- Damping ratio  $\zeta$  based on overshoot:

$$\zeta = \frac{-\ln(M_p)}{\sqrt{\pi^2 + (\ln M_p)^2}}$$

- Required phase margin  $\phi_{PM}$  for a second-order approximation:

$$\phi_{PM} = \tan^{-1} \left( \frac{2\zeta}{\sqrt{\sqrt{1 + 4\zeta^4} - 2\zeta^2}} \right)$$

- Target open-loop phase at crossover frequency:

$$\angle L(j\omega_c) = -180^\circ + \phi_{PM}$$

## 2.2 Crossover Frequency Selection

```

1 %% 2.1) Frequency response of the plant and crossover frequency
2 wgrid = logspace(-2, 2, 5000);
3 [~, ph] = bode(G, wgrid); ph = squeeze(ph);
4 logw = log10(wgrid);
5 logw_c = interp1(ph, logw, targetPhase, 'linear');
6 wc = 10^logw_c;
7 magGwc = abs(evalfr(G, 1j*wc)); % Evaluates the plant G magnitude at wc in frequency domain.
8 fprintf('-->Computed crossover frequency: wc = %.3f rad/s\n', wc);

```

The crossover frequency  $\omega_c$  is chosen where the plant's phase response matches the above target phase. At that frequency, the magnitude of the open-loop transfer function is forced to 1 by adjusting the proportional gain  $K_p$ .

## 2.3 Controller Formulas

```

1 case 'PID'
2     Kp = 1 / magGwc;
3     Ti_base = 10 / wc;    Ti = Ti_base * scaleIntTI;
4     Ki = Kp / Ti;
5     Td = 1 / (10*wc);
6     Kd = Kp * Td;
7     C = pid(Kp, Ki, Kd);
8     ctrlStr = sprintf('-->PID (Kp=%.3f, Ki=%.3f, Kd=%.3f, Ti=%.3f)', ...
9                     Kp, Ki, Kd, Ti);

```

Based on the plant characteristics and the selected  $\omega_c$ , controller gains are calculated as follows:

- P Controller:

$$K_p = \frac{1}{|G(j\omega_c)|}$$

- **PI Controller:**

$$C(s) = K_p \left( 1 + \frac{1}{T_i s} \right), \quad T_i = \frac{10}{\omega_c}$$

- **PID Controller:**

$$C(s) = K_p \left( 1 + \frac{1}{T_i s} + T_d s \right), \quad T_i = \frac{10}{\omega_c}, \quad T_d = \frac{1}{10\omega_c}$$

## 2.4 Performance Evaluation

```

1 % Compute performance metrics
2 info = stepinfo(T);
3 Tr    = info.RiseTime;           % Rise Time (10%-90%)
4 Ts    = info.SettlingTime;
5 Mp    = info.Overshoot;
6 ess   = abs(1 - dcgain(T));
7 [Gm, PM, Wgm, Wpm] = margin(L);

```

The closed-loop system is:

$$T(s) = \frac{C(s)G(s)}{1 + C(s)G(s)}$$

Performance metrics such as rise time  $T_r$ , settling time  $T_s$ , overshoot  $M_p$ , and steady-state error  $e_{ss}$  are computed from the step response. Phase margin and gain margin are evaluated from the loop transfer function.

## 3. SEMI-SMART PID TUNING USING SECOND-ORDER APPROXIMATIONS

This MATLAB-based method automates tuning and checks performance specifications through a frequency-domain approach, incorporating:

- Explicit **overshoot and settling time constraints**

- **Second-order approximation** of the system for performance estimation
- Handling of **integrators** in the plant

### 3.1 Inputs and Setup

- Specify desired  $M_p$  and  $T_s$
- Define the plant  $G(s)$  using `tf(...)`
- Detect and account for **integrators** by scaling  $T_i$

### 3.2 Frequency Domain Computation

- Calculate  $\zeta$  and  $\phi_{PM}$  from  $M_p$
- Use interpolation to find the crossover frequency  $\omega_c$  where the plant phase matches  $-180^\circ + \phi_{PM}$
- Evaluate plant magnitude at  $\omega_c$  to compute controller gains

### 3.3 Controller Loop

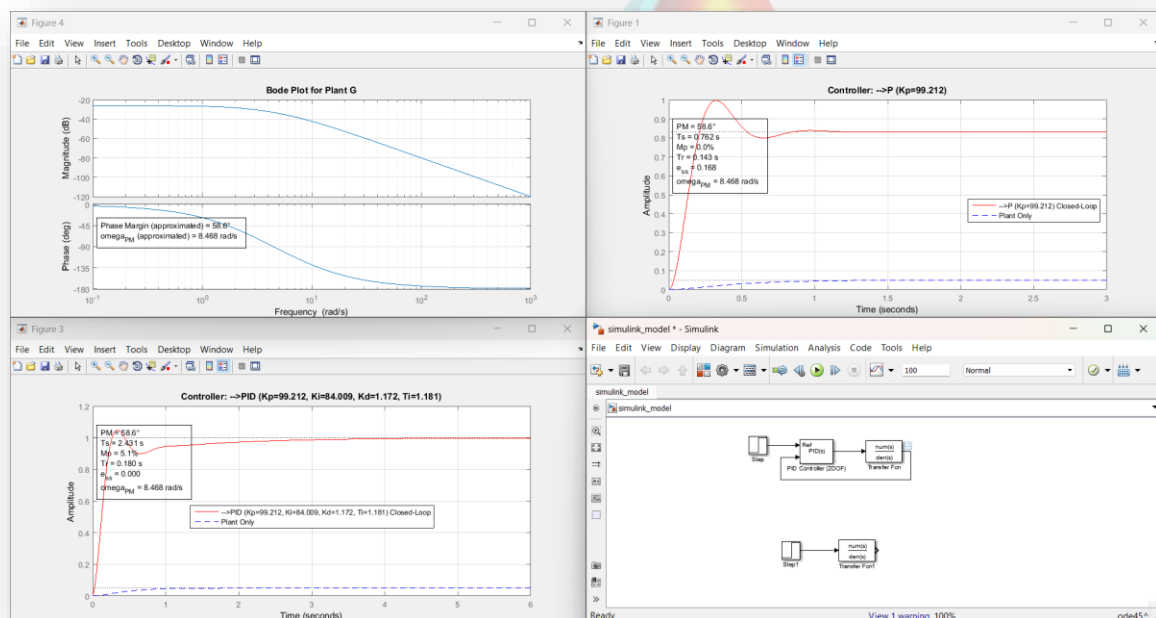
```

1  %% 3) Loop over controllers
2  controllers = {'P','PI','PID'};
3  figCount    = 0;
4  for i = 1:length(controllers)
5      switch controllers{i}
6          case 'P'
7              Kp = 1 / magGwc;
8              C = Kp;
9              ctrlStr = sprintf('-->P (Kp=%.3f)', Kp);
10
11         case 'PI'
12             Kp = 1 / magGwc;
13             Ti_base = 10 / wc;      Ti = Ti_base * scaleIntTI;
14             Ki = Kp / Ti;
15             C = tf([Kp*Ti, Kp], [Ti, 0]);
16             ctrlStr = sprintf('-->PI (Kp=%.3f, Ki=%.3f, Ti=%.3f)', Kp, Ki, Ti);
17
18         case 'PID'
19             Kp = 1 / magGwc;
20             Ti_base = 10 / wc;      Ti = Ti_base * scaleIntTI;
21             Ki = Kp / Ti;
22             Td = 1 / (10*wc);
23             Kd = Kp * Td;
24             C = pid(Kp, Ki, Kd);
25             ctrlStr = sprintf('-->PID (Kp=%.3f, Ki=%.3f, Kd=%.3f, Ti=%.3f)', ...
26                             Kp, Ki, Kd, Ti);
27     end

```

For each controller type (P, PI, PID):

- Compute gains using formulas above
- Build open-loop transfer function  $L(s) = C(s)G(s)$
- Evaluate closed-loop  $T(s)$  and extract:
  - $T_s$  (settling time)
  - $M_p$  (overshoot)
  - $T_r$  (rise time)
  - $e_{ss}$  (steady-state error)
- Check if specs are met:
  - If yes: plot response and print info
  - If no: discard controller



### 3.4 Visualizations and Results

- Annotated step response for successful controllers
- Bode plot of the plant with target phase margin and frequency
- Automatic rejection of controllers that do not meet both  $M_p$  and  $T_s$
- Simulink simulation if a controller is found viable.

#### 4. SUMMARY OF WORKFLOW

1. Define  $M_p$  and  $T_s$
  2. Model  $G(s)$
  3. Compute  $\zeta$ ,  $\phi_{PM}$ , and target phase
  4. Interpolate plant phase to find  $\omega_c$
  5. Compute controller gains
  6. Simulate step response
  7. Evaluate and select only valid controllers
  8. Showcase a quick Simulink simulation if a controller is found viable.
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#### 5. ADVANTAGES OF THE SEMI-SMART METHOD

- Directly links time-domain specifications to controller design
  - Automates gain calculation and performance verification
  - Adapts to integrating plants by modifying integral time
  - Avoids over-tuning or under-tuning by filtering out unsuitable designs
  - Easily extendable to more sophisticated methods or additional constraints
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#### 6. CONCLUSION

This report covers both traditional frequency-domain PID tuning for 2<sup>nd</sup> order systems and extends it in a practical semi-automated method using second-order system approximations for higher order systems. By integrating time-domain specifications into frequency-based controller design, this approach simplifies the tuning process while maintaining robust performance. The MATLAB implementation provides a flexible framework for applying these principles to a wide range of control systems.