

Summary of Submissions

1st GPPS Turbomachinery CFD Workshop (GPPS 2021)

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Imperial College London



TECHNISCHE
UNIVERSITÄT
DARMSTADT

**Imperial College
London**

Motivation (Untold)

“CFD is a reliable workhorse for turbomachinery” ... but is that so?

How did you predict
the performance map
so well? Any special
sauces?

I have mixed up all
the CFD settings but
still a bit short on the
pressure ratio...

You may try solver A
with model B and
option C turned on...

Oh, you may try this
tip gap size and that
map data.

Solver D with model
E and a coarse mesh
will also work...

These data are from
private emails of the
authors though...



Reasons of Inconsistency

CFD side:

- Commercial solvers: intellectual property
- Version control of models
(turbulence models; R-S interfaces; wall functions, etc.)
- Potential bugs in the solver
(lack of data for validation and verification)
- Difference in user inputs
(preferred mesh, models, etc.)

Exp side:

- Limit of Exp technique in the 90s
- Version control of data
- Limit availability of data in public

Solution: Open-Source

SU2
code

HiFiLES
High-Order CFD
Simulation

Open ∇ FOAM



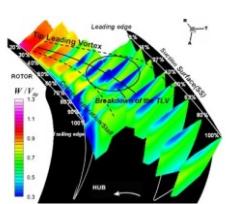
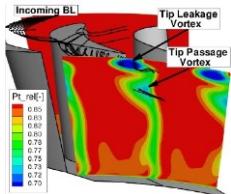
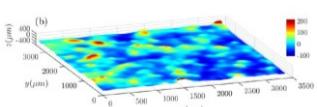
CFL3D
Version 6



NEKTAR++
SPECTRAL/HP ELEMENT FRAMEWORK

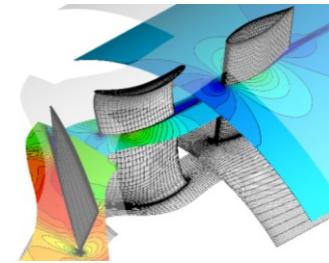
code.saturne

CFD solvers



Common research models

GPPS 1st Turbomachinery CFD Workshop



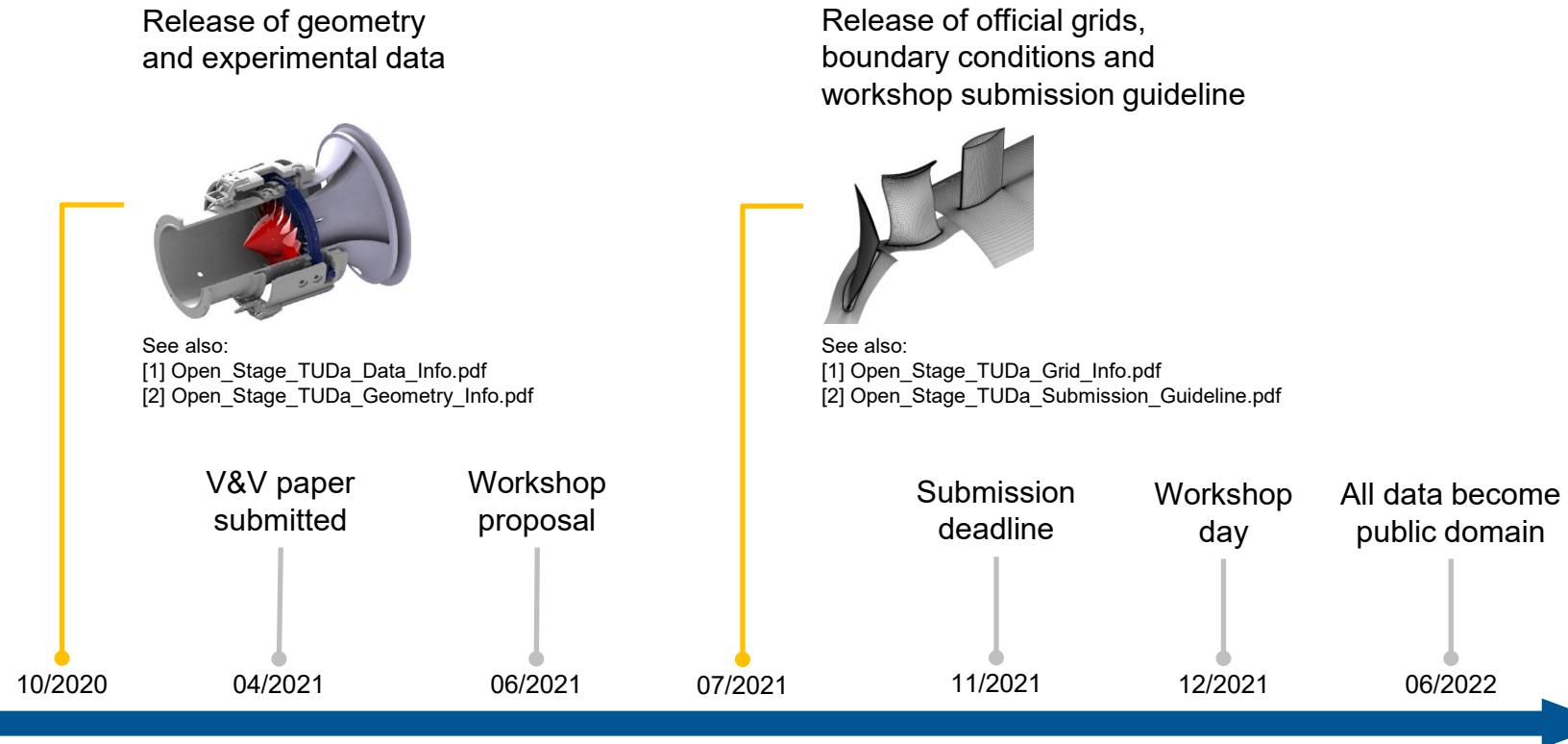
⋮

Validation & verification campaign

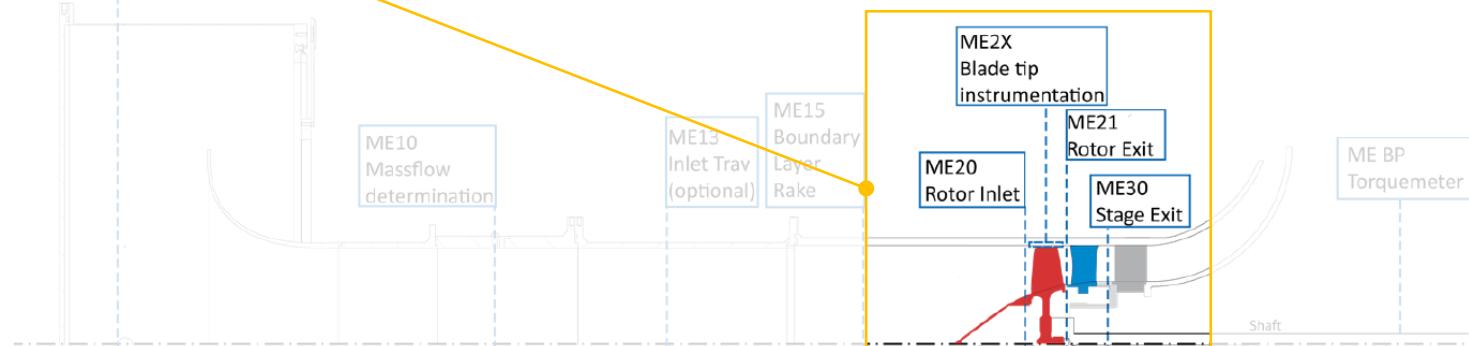
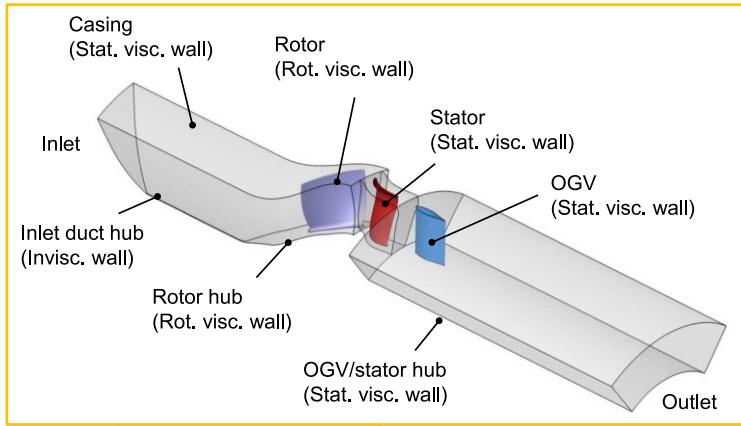
Scope of GPPS CFD workshop series

Design of the Workshop

Timeline



Flow Domain and Boundary Conditions



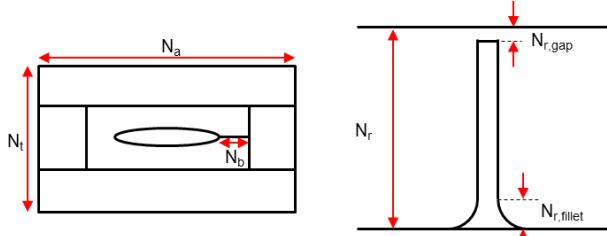
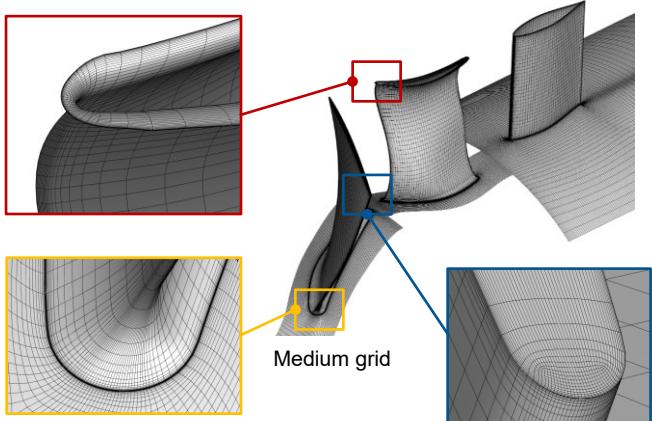
Major differences between CFD model and EXP

- The **axial-to-radial duct** is simplified as an axial duct.
- The **stator hub cavity flow** is not considered.
- Changes of the **inlet profile** are not considered.
- Changes of **blade tip gap size** are not considered.

Official Grids

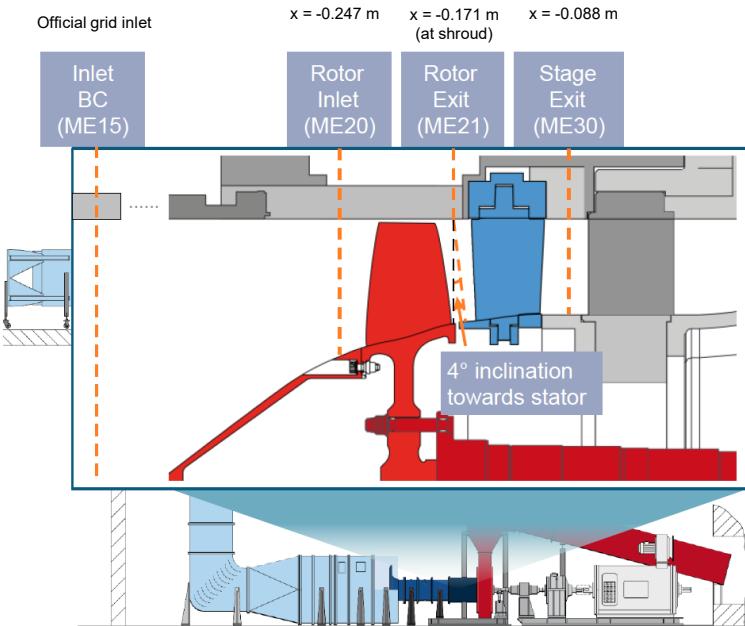
Major features of official grids

- All grid cells are **hexahedron**.
- **Five sets of grids (uniformly refined)** in structured/unstructured .cgns format and .trb format.
- Boundary layers are refined with an average $y^+ < 3$
- **Tip gap and fillets** are considered.



	Grid name	UltraCoarse	Coarse	Medium	Fine	UltraFine
Rotor	Total radial grid point	37	53	81	121	181
	Tip gap radial grid point	9	13	21	33	49
	Hub fillet radial grid point	9	13	17	29	45
	Total tangential grid point	29	41	65	93	145
	Total axial grid point	41	61	97	141	213
	Boundary layer grid point	9	13	21	29	45
	Tip gap O-grid point	5	9	13	21	29
Stator	Total grid point (million)	0.12	0.28	1.08	3.36	11.77
	Total radial grid point	41	65	93	137	201
	Tip/hub fillet radial grid point	9	13	21	29	49
	Total tangential grid point	17	29	41	69	101
	Total axial grid point	37	53	85	129	189
	Boundary layer grid point	9	13	21	29	45
	Tip gap O-grid point	5	9	13	21	29
OGV	Total grid point (million)	0.04	0.16	0.53	1.80	5.81
	Total radial grid point	-	-	77	-	-
	Total tangential grid point	-	-	81	-	-
	Total axial grid point	-	-	77	-	-
	Boundary layer grid point	-	-	17	-	-
	Total grid point (million)	-	-	0.85	-	-

Flow Quantities of Interest



Collected data:

- **characteristics.csv**

Corrected_speed(RPM), Corrected_mass_flow(kg/s), pt_AA_15(Pa),
pt_MA_15(Pa), Tt_AA_15(K), Tt_MA_15(K), pt_AA_30(Pa), pt_MA_30(Pa),
Tt_AA_30(K), Tt_MA_30(K), ptr_AA_15_30, Ttr_AA_15_30, Ttr_MA_15_30,
Isentropic_Efficiency_15_30

- **profile_ME21.csv**

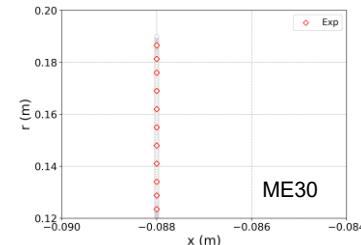
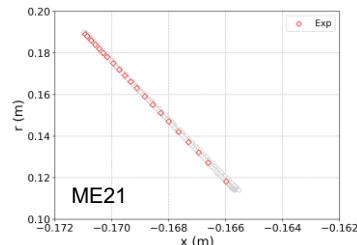
Corrected_mass_flow(kg/s), r_21(m), x_21(m), Span, alpha(deg),
gamma(deg), pt_AA_21(Pa), ptr_AA_15_21

- **profile_ME30.csv**

Corrected_mass_flow(kg/s), r_30(m), x_30(m), Span, pt_AA_30(Pa),
Tt_AA_30(K), ptr_AA_15_30, Ttr_AA_15_30

Quality control:

- Post-process check
- Location check



CFD Setup Form

Collected CFD setup info:

• Grid details

Number of grid nodes, y^+

• Flow solver numerical schemes

Advection scheme, turbulence model, wall function, rotor-stator interface model

• Boundary conditions

Inlet profile (mean flow quantities; turbulence model quantities), outlet boundary condition

• Convergence history

Mass flow convergence at PE/NS conditions

1. Participant Information

First name:	[REDACTED]
Last name:	[REDACTED]
Organization:	[REDACTED]
Email:	[REDACTED]

Type of model for turbulence quantities*: (e.g., frozen rotor, mixing plane)	mixing plane
If not listed above, please briefly describe the rotor-stator interface model and include a major reference to it:	
* Mean flow quantities are ρ , T , u_x , u_y , u_z , etc.; turbulence quantities are eddy viscosity, k , ω , etc.	

2. Grid Information

If this submission used an official grid:

Grid name (e.g., medium, fine, etc.):	fine
---------------------------------------	------

If this submission used an in-house grid:

Average y^+ of the first layer grid:	
Number of grid points in the rotor domain:	
Number of grid points in the stator domain:	
Type of grid element: (e.g., hexahedron, tetrahedron, etc.)	

3. RANS Flow Solver Information

(1) General:

Solver name:	NUMECA FineTurbo
Major reference(s) (optional):	

(6) Other details (optional):

Fluid model (e.g., real gas, idea gas):	idea gas
Linear system solver (e.g., Jacobi, etc.):	Incomplete Lower Upper(ILU)
Have you verified your solver in NASA 2D flat plate against established RANS solvers? (yes/no)	

4. Boundary conditions

(1) Inlet:

How were the mean flow quantities determined? (e.g., from InletBC.input file; uniform inlet at standard conditions)	from InletBC.input file
How was the turbulence quantity(s) determined? (e.g., values and units of inlet k and ω)	$k = 35 \text{ m}^2/\text{s}^2$ $\epsilon = 2.0 \times 10^3 \text{ m}^2/\text{s}^3$

(2) Outlet (optional):

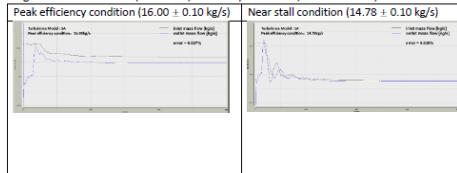
What type of boundary condition is used? (e.g., uniform backpressure, radial equilibrium backpressure, mass flow, Riemann, etc.)	radial equilibrium backpressure
--	---------------------------------

(3) Periodic boundary (optional):

Have you checked the periodicity of mean flow quantities? (yes/no)	yes
Have you checked the periodicity of turbulence quantities? (yes/no)	yes

5. Convergence History

A figure of mass flow rate (rotor inlet, rotor exit/stator inlet, and stator exit) versus iteration



(5) Rotor-stator interface model:

Type of model for mean flow quantities*: (e.g., frozen rotor, mixing plane, non-reflecting (Giles))	mixing plane
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Submission Statistics

Submission Statistics

47 characteristic curves submitted by **9** authors from **6** institutes

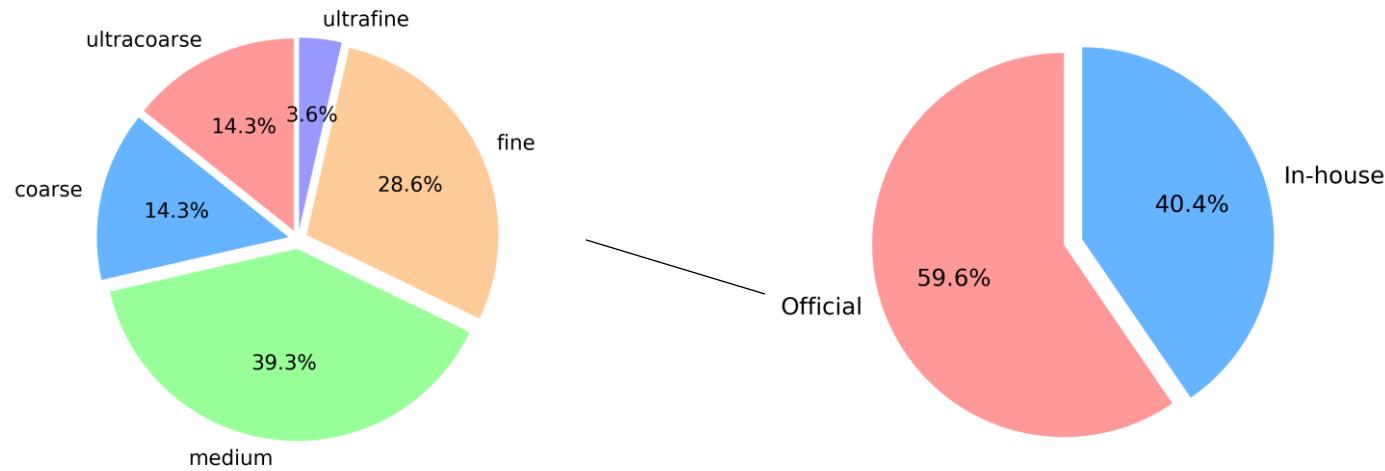
- 41 curves at 100% speed, 6 curves at 65% speed
- 5 universities and 1 research institute

9 CFD solvers

- 3 commercial solvers: Ansys CFX, Fine/Turbo, Turbostream
- 1 open-source solver: SU2
- 5 in-house solvers: ASPAC, HADES, HGAE, MAP, TurboXD

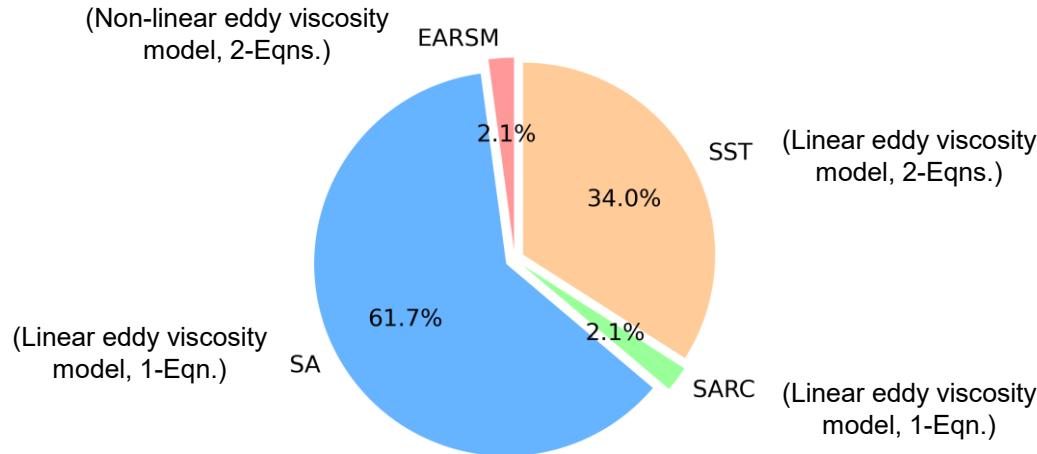
Submission Statistics

Grid usage: 60% using official grids, 40% using in-house grids.



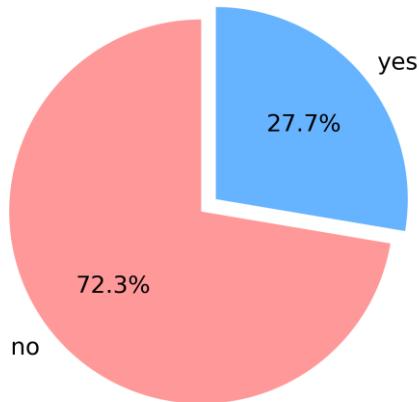
Submission Statistics

Turbulence model: SA and SST are most popular



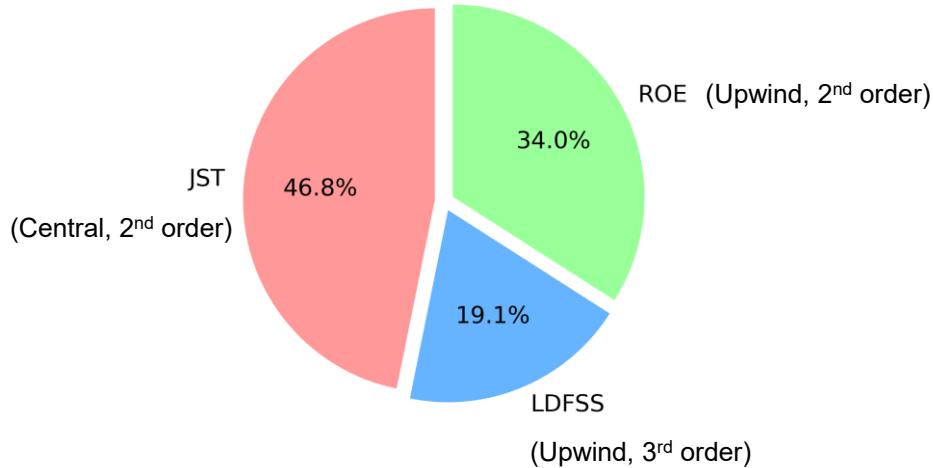
Submission Statistics

Wall functions: 30% uses wall function and 70% does not



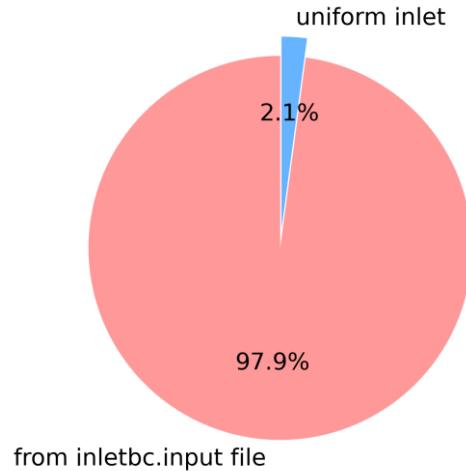
Submission Statistics

Advection scheme: All submission are $\geq 2^{\text{nd}}$ order accurate in space



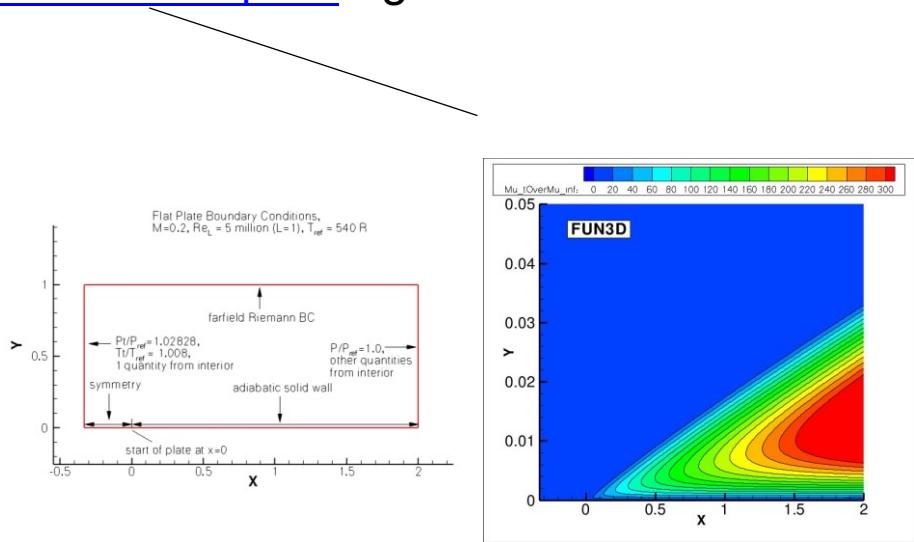
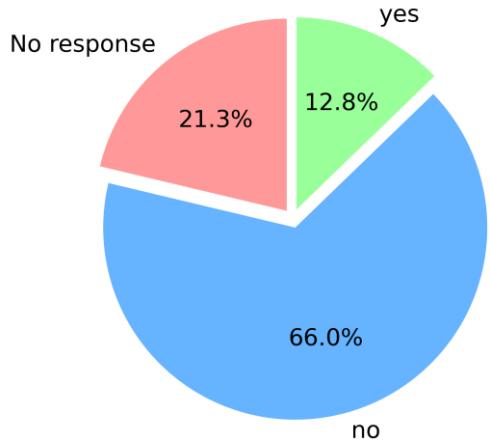
Submission Statistics

Inlet boundary conditions: most submissions used official .bc file for mean flow quantities



Submission Statistics

Have you verified your solver in [NASA 2D flat plate](#) against established RANS solvers? (yes/no)



Validation: Experiment versus CFD

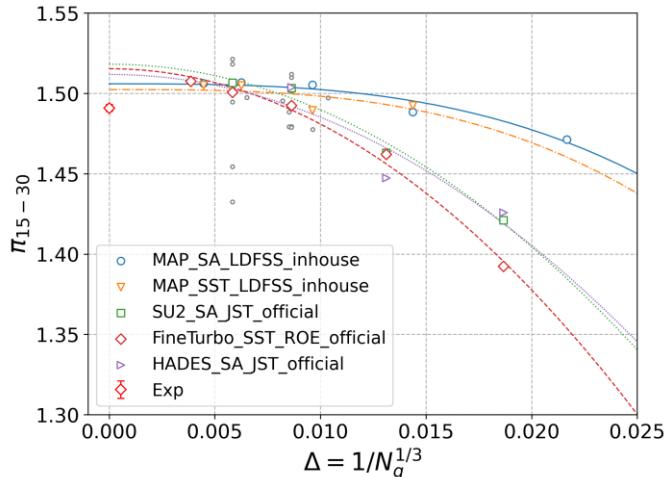
Grid Independence

- Estimate discretization error

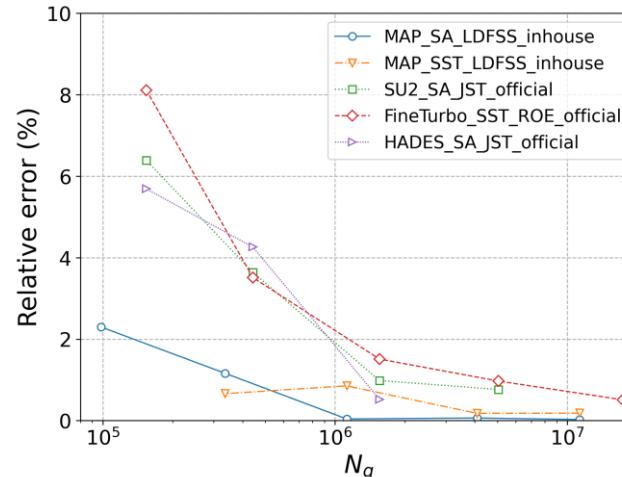
$$q = \underline{k\Delta^n} + q_{ideal}$$
$$\varepsilon_q = \left(\frac{q}{q_{ideal}} - 1 \right) \times 100\%$$

discretization error

- Design speed, peak efficiency ($m=16.00 \pm 0.10 \text{kg/s}$)



q flow quantity of interest
q_{ideal} ideal flow quantity of interest free of discretization error
Δ grid spacing
n order of spatial accuracy of advection scheme



Grid Independence

- Estimate discretization error

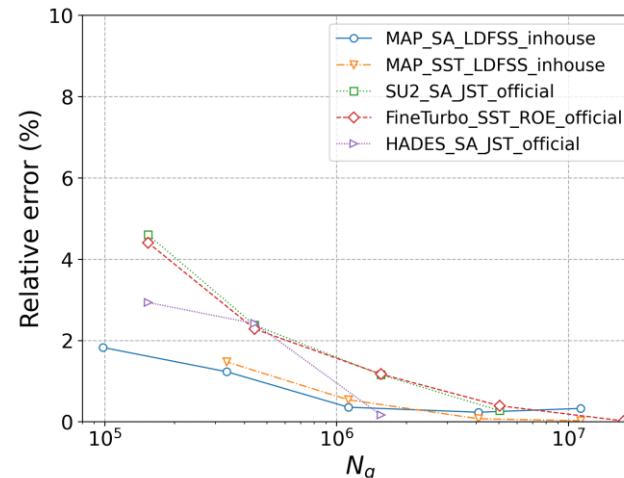
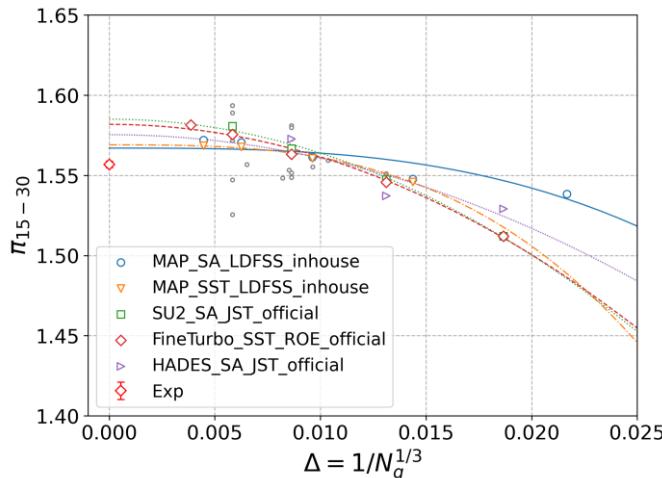
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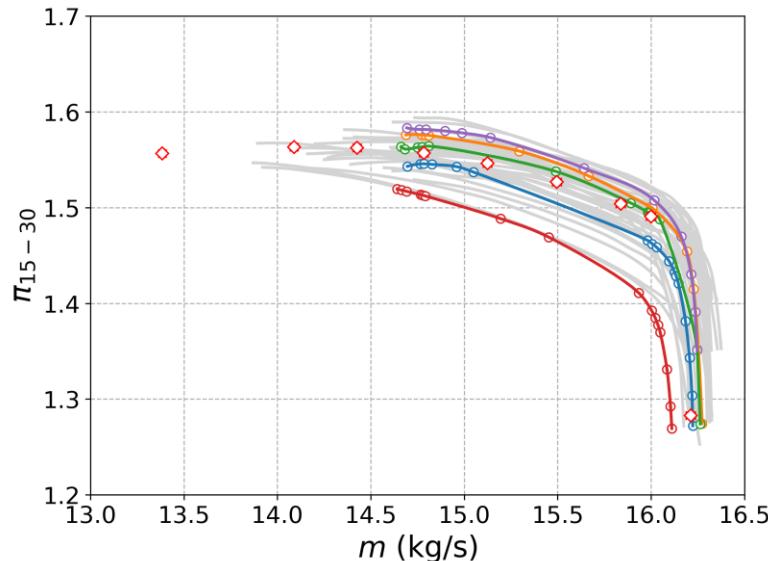
q	flow quantity of interest
q_{ideal}	ideal flow quantity of interest free of discretization error
Δ	grid spacing
n	order of spatial accuracy of advection scheme

- Design speed, near stall ($m=14.78 \pm 0.10 \text{kg/s}$)

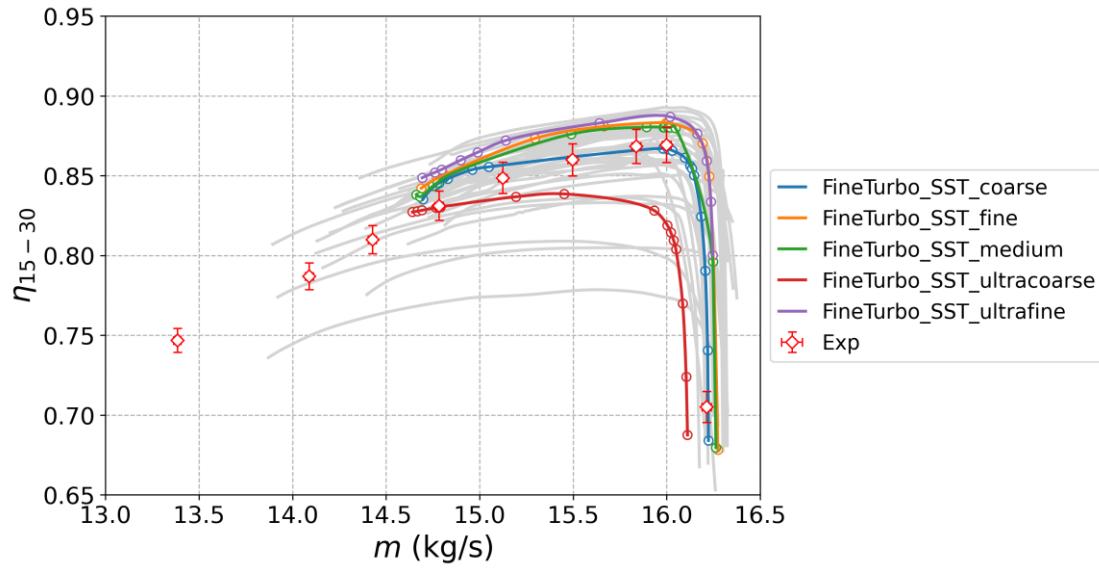


Grid Independence

- Convergence on performance MAP



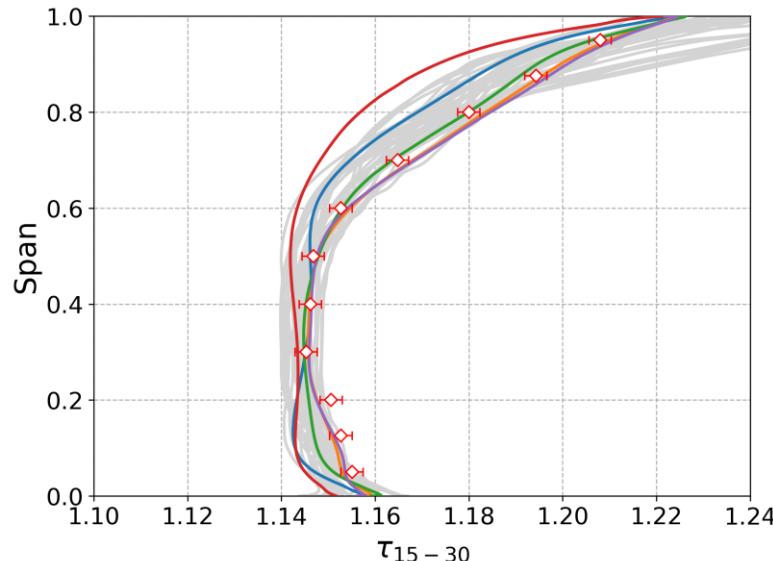
Total pressure ratio



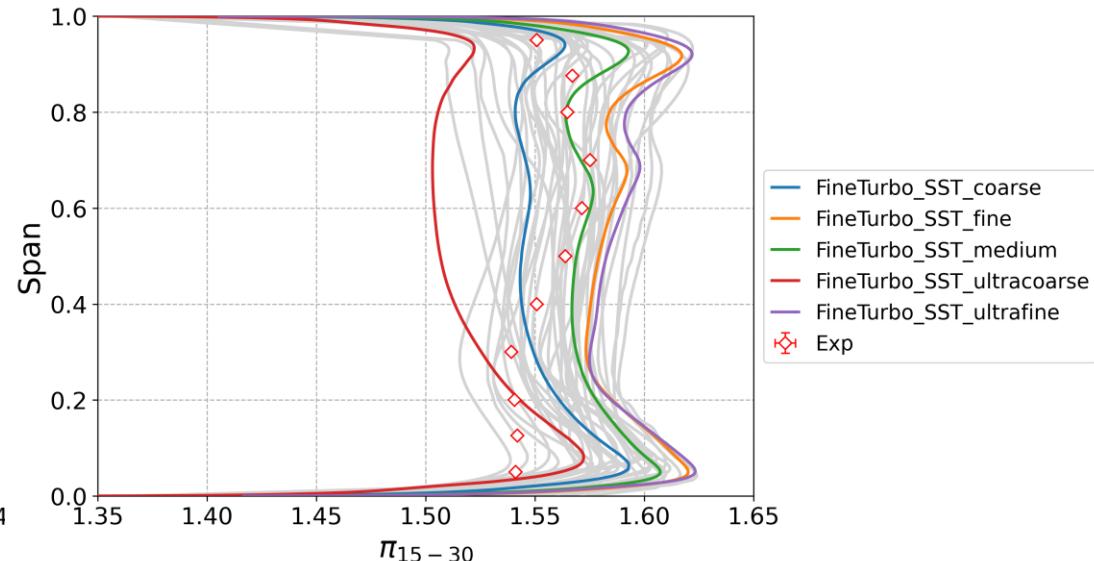
Design speed

Grid Independence

- Convergence on stage exit (ME30) spanwise profiles



Total temperature ratio

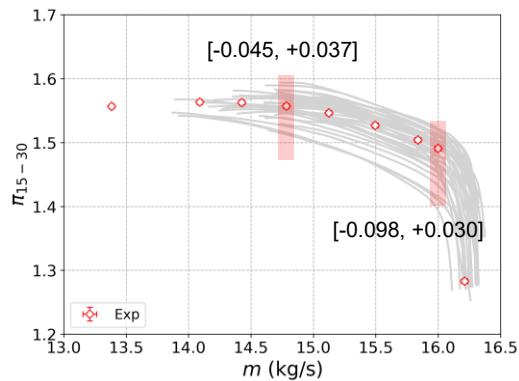


Total pressure ratio

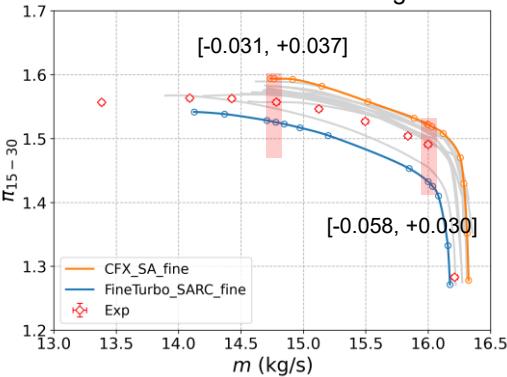
Design speed, near stall ($m=14.78 \pm 0.10 \text{kg/s}$)

Total Pressure Ratio Characteristics

All data

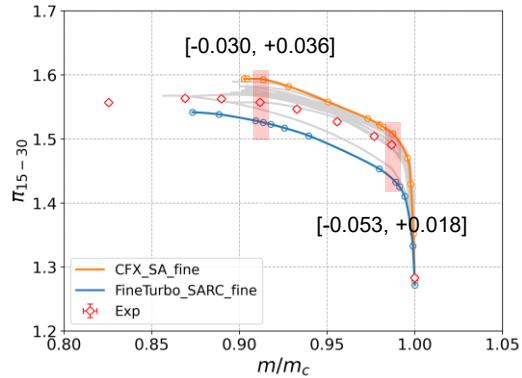


Exclude coarse grid ($N_g \geq 3M$)



Design speed

Normalize mass flow

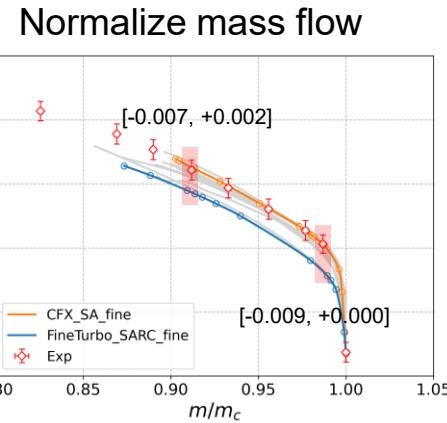
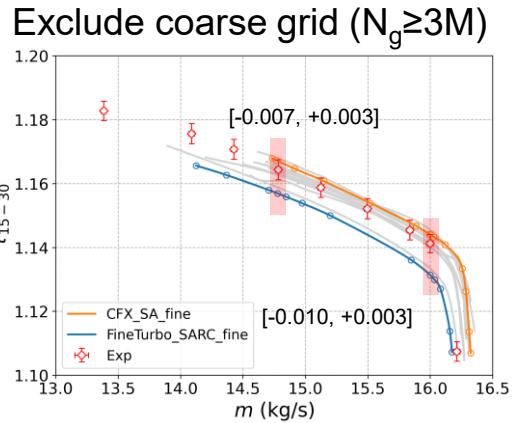
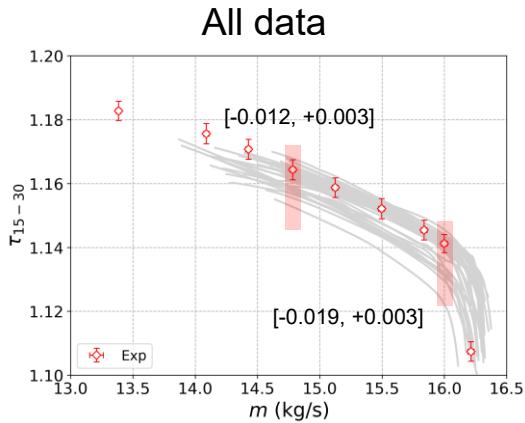


- Discretization
- Uncertainty in inlet BC
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- Periodic and R-S BC
- Other geometric uncertainties

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Total Temperature Ratio Characteristics



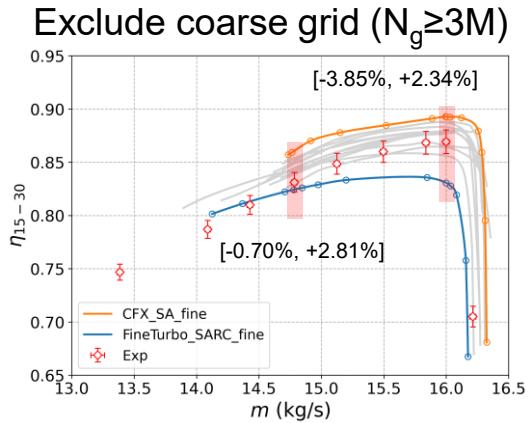
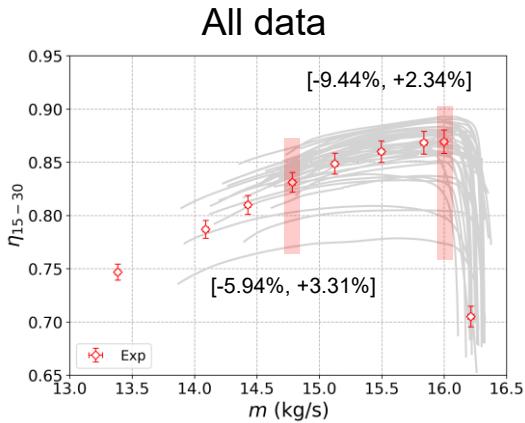
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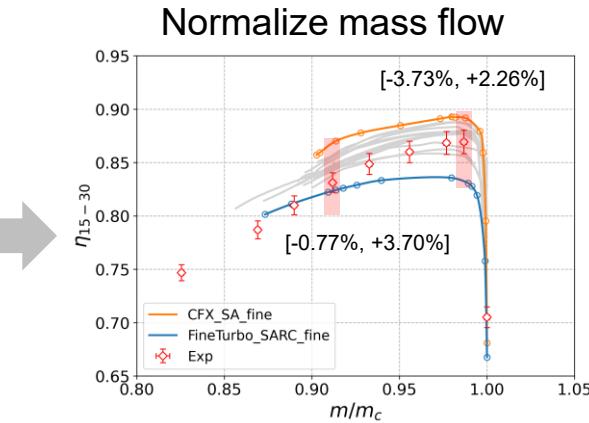
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ISENTROPIC EFFICIENCY CHARACTERISTICS



Design speed



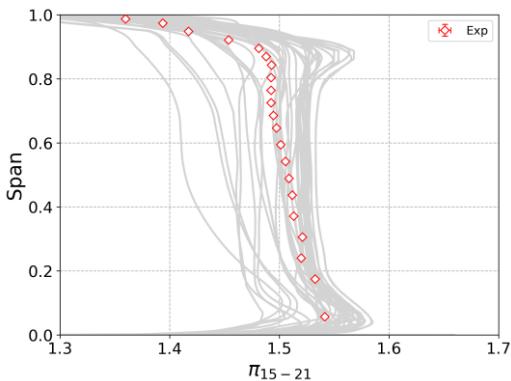
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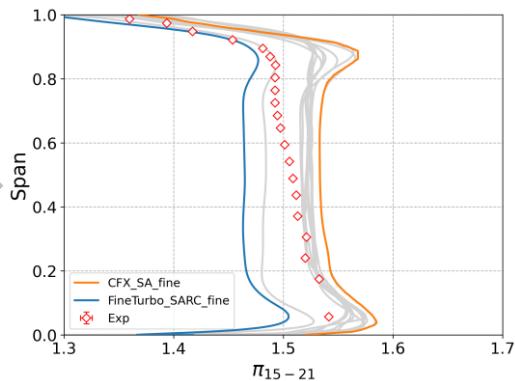
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Rotor Exit (ME21) Total Pressure Ratio Profile

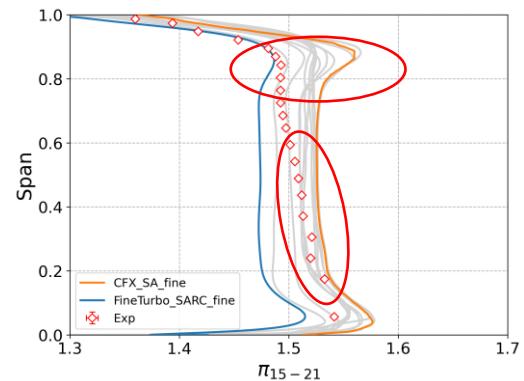
All data ($m=16.00 \pm 0.10 \text{ kg/s}$)



Exclude coarse grid ($N_g \geq 3M$)



Correct to $m/m_c = 0.9868$



Design speed, peak efficiency

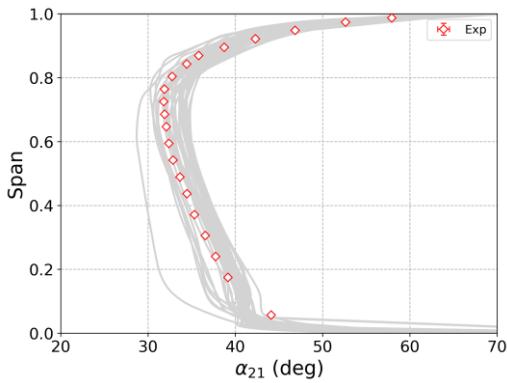
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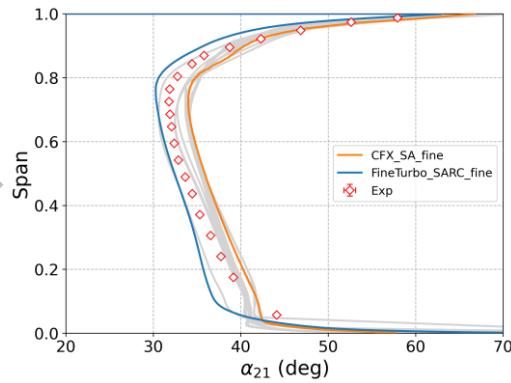
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Rotor Exit (ME21) Absolute Flow Angle Profile

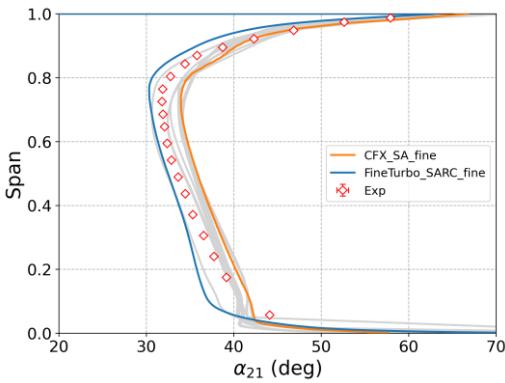
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Exclude coarse grid ($N_g \geq 3M$)



Correct to $m/m_c = 0.9868$



Design speed, peak efficiency

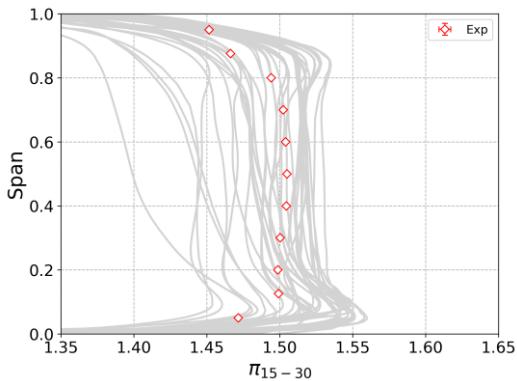
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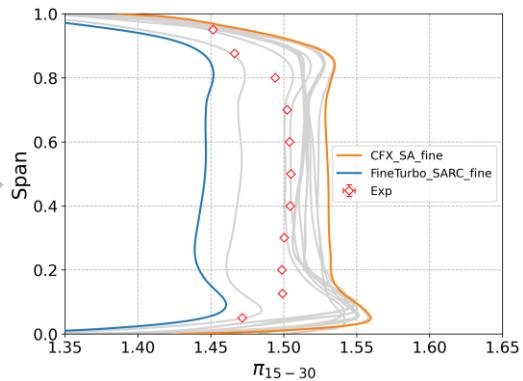
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Stator Exit (ME30) Total Pressure Ratio Profile

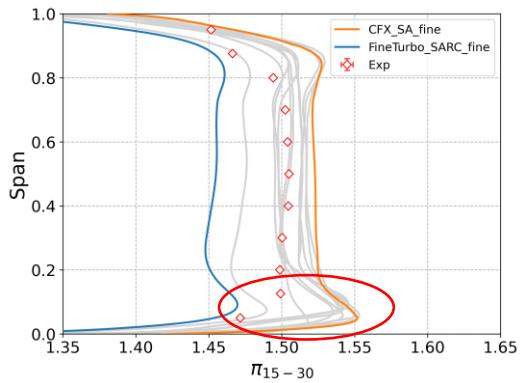
All data ($m=16.00 \pm 0.10 \text{kg/s}$)



Exclude coarse grid ($N_g \geq 3M$)



Correct to $m/m_c=0.9868$



Design speed, peak efficiency

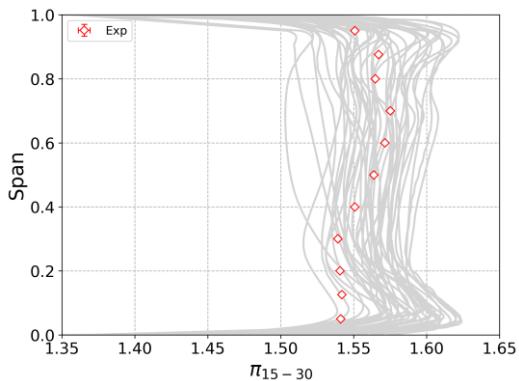
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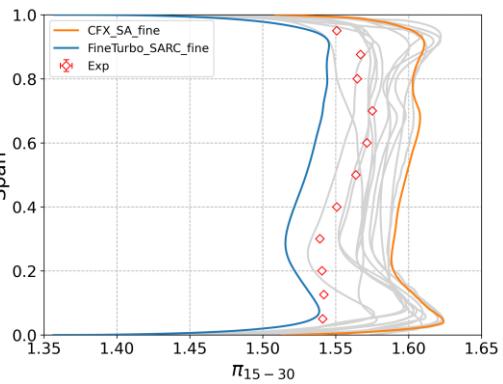
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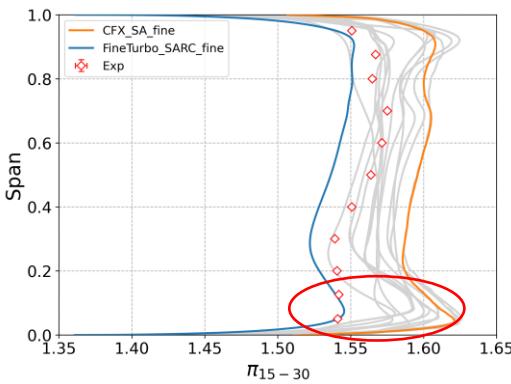
All data ($m=14.78 \pm 0.10 \text{ kg/s}$)



Exclude coarse grid ($N_g \geq 3M$)



Correct to $m/m_c = 0.9116$



Design speed, near stall

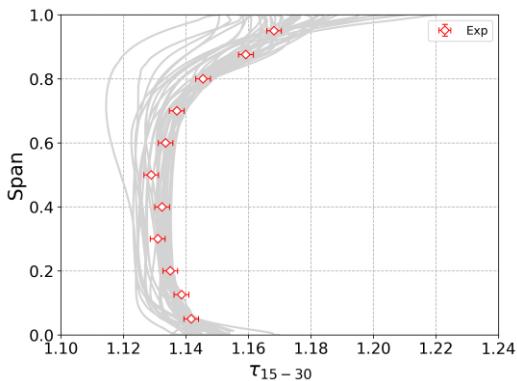
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- Uncertainty in inlet BC
- Uncertainty in throat area
- Turbulence model
- Periodic and R-S BC
- Other geometric uncertainties

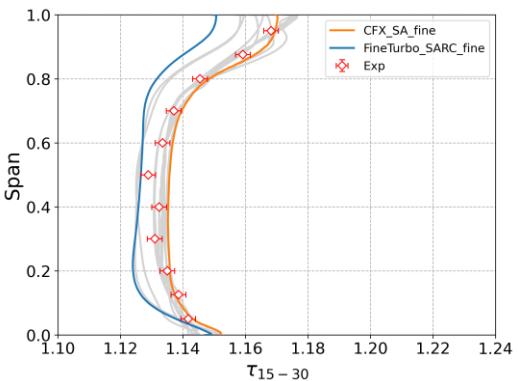
- Discretization
- Uncertainty in inlet BC
- Uncertainty in throat area
- Turbulence model
- Periodic and R-S BC
- Other geometric uncertainties

Stator Exit (ME30) Total Temperature Ratio Profile

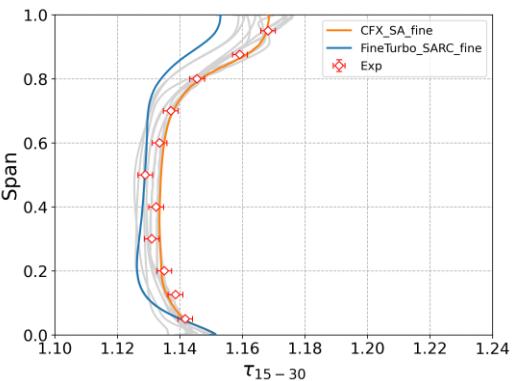
All data ($m=16.00 \pm 0.10 \text{ kg/s}$)



Exclude coarse grid ($N_g \geq 3M$)



Correct to $m/m_c = 0.9868$



Design speed, peak efficiency

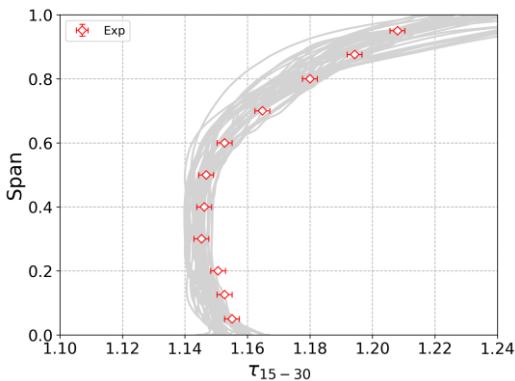
- Discretization
- Uncertainty in inlet BC
- Uncertainty in throat area
- Turbulence model
- Periodic and R-S BC
- Other geometric uncertainties

- Discretization
- Uncertainty in inlet BC
- Uncertainty in throat area
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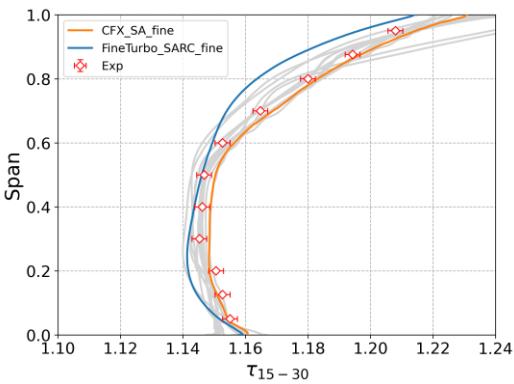
- Discretization
- Uncertainty in inlet BC
- Uncertainty in throat area
- Turbulence model
- Periodic and R-S BC
- Other geometric uncertainties

Stator Exit (ME30) Total Temperature Ratio Profile

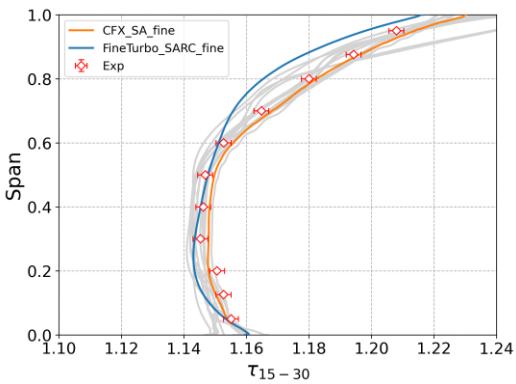
All data ($m=14.78 \pm 0.10 \text{kg/s}$)



Exclude coarse grid ($N_g \geq 3M$)



Correct to $m/m_c = 0.9116$



Design speed, near stall

- Discretization
- Uncertainty in inlet BC
- Uncertainty in throat area
- Turbulence model
- Periodic and R-S BC
- Other geometric uncertainties

- Discretization
- Uncertainty in inlet BC
- Uncertainty in throat area
- Turbulence model
- Periodic and R-S BC
- Other geometric uncertainties

- Discretization
- Uncertainty in inlet BC
- Uncertainty in throat area
- Turbulence model
- Periodic and R-S BC
- Other geometric uncertainties

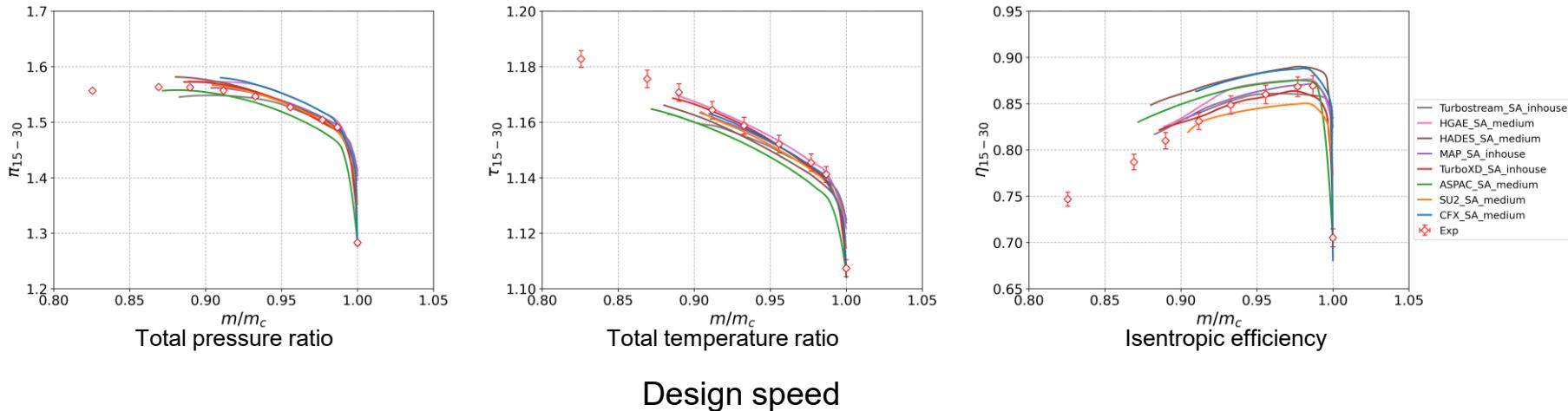
Verification: CFD versus CFD



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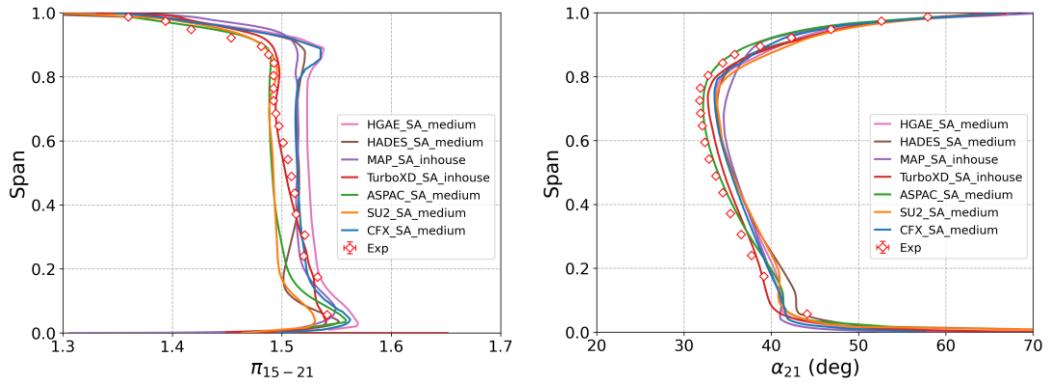
SA Model Verification: Performance Characteristics



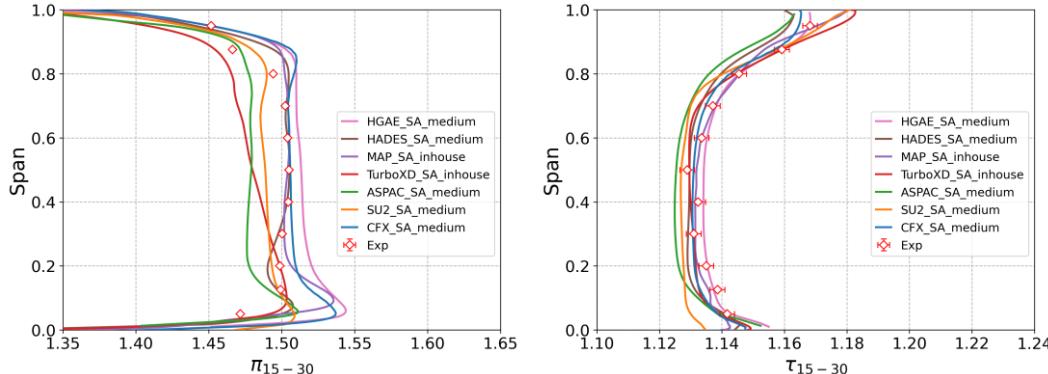
- No results are overlapping with each other (i.e., **verification goal not achieved**)
- Further communications on the implemented **SA model version** need to be made
- Further **V&V on low TRL cases** need to be made in future workshops (hopefully off-line)
- Effect of **wall function, SA inlet b.c. and SA advection term** needs to be investigated

SA Model Verification: Peak Efficiency Profiles

Rotor exit (ME21)



Stage exit (ME30)



* All data corrected to $m/m_c = 0.9868$

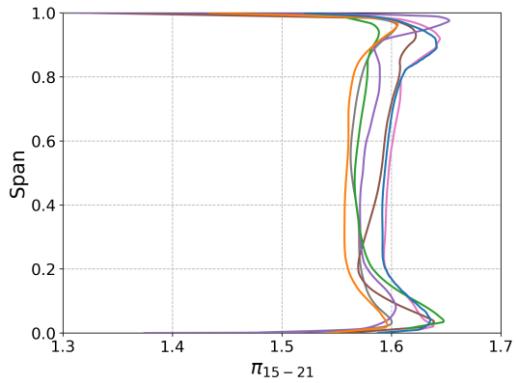


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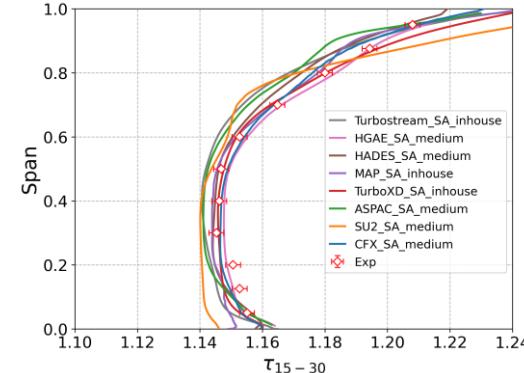
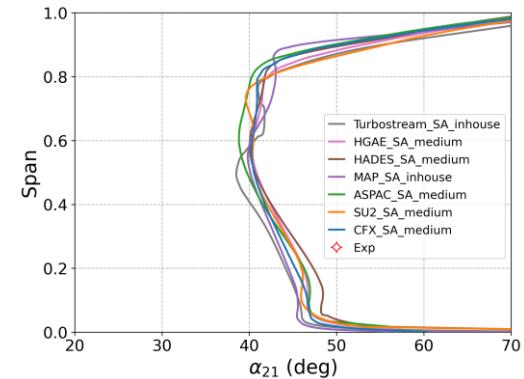
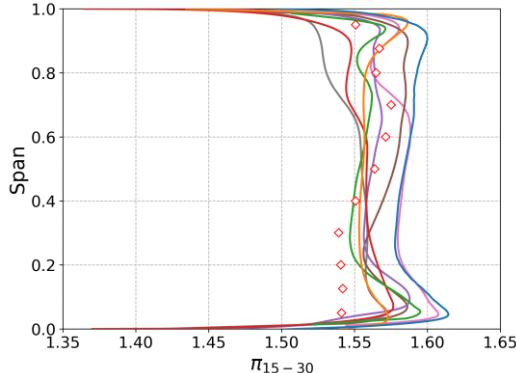
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SA Model Verification: Near Stall Profiles

Rotor exit (ME21)



Stage exit (ME30)



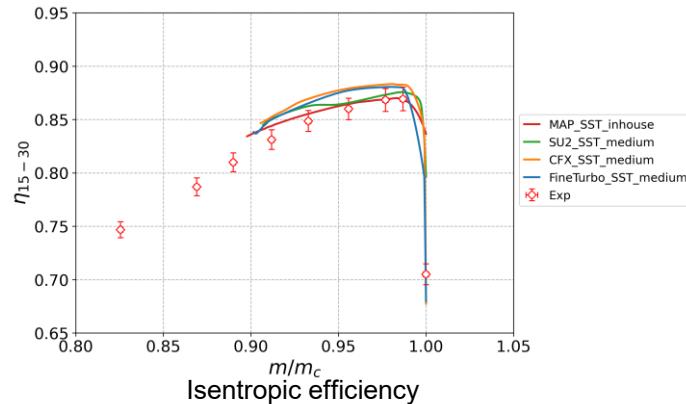
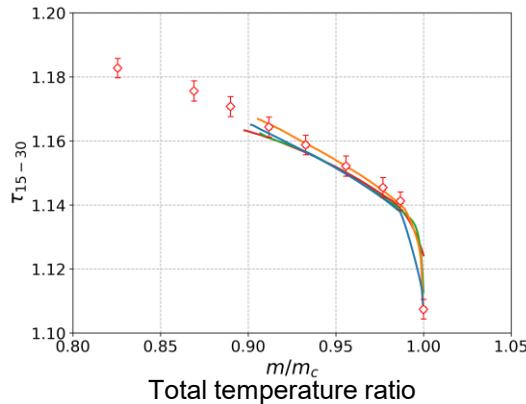
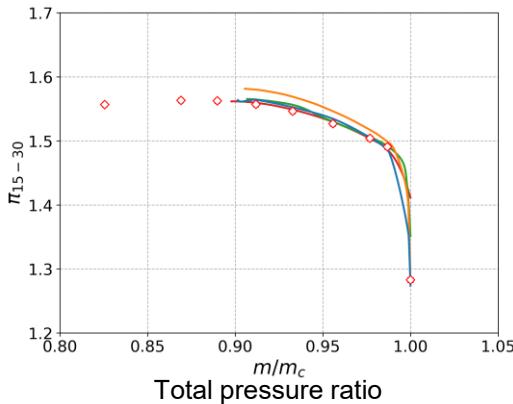
* All data corrected to $m/m_c=0.9116$



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SST Model Verification: Performance Characteristics

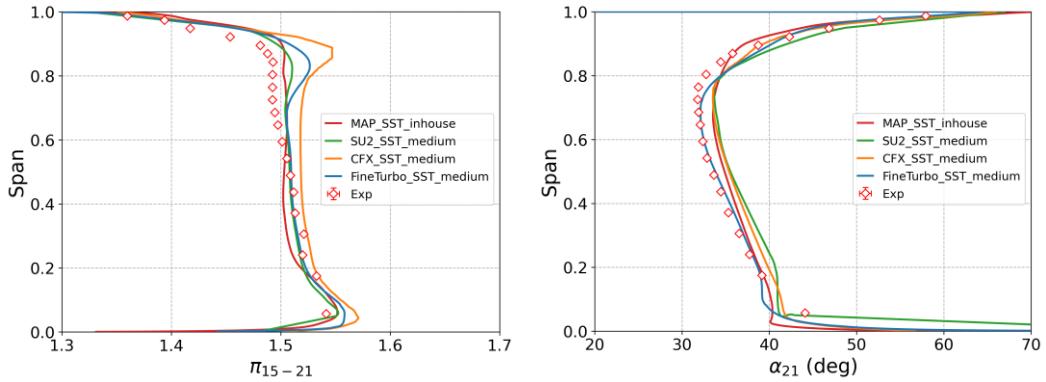


Design speed

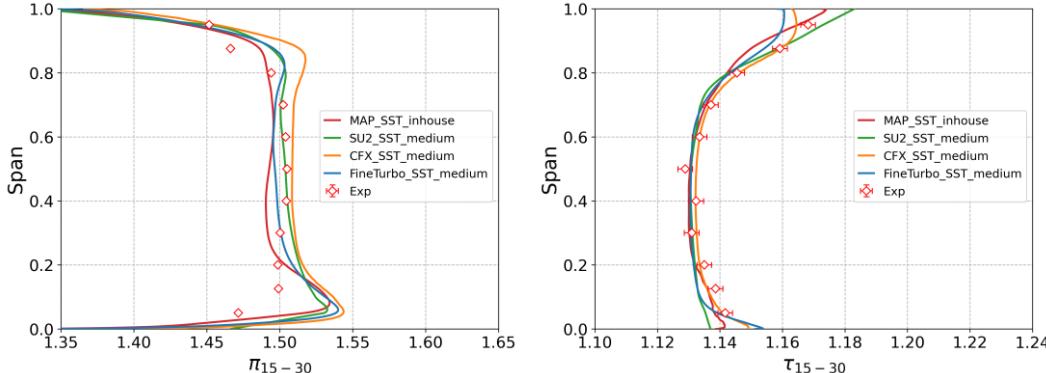
- Results match with each other (better than SA), but still not perfect
- Further communications on the implemented **SST model version** need to be made
- Further **V&V on low TRL cases** need to be made in future workshops (hopefully off-line)
- Effect of **wall function, SST inlet b.c. and SST advection term** needs to be investigated

SST Model Verification: Peak Efficiency Profiles

Rotor exit (ME21)



Stage exit (ME30)



* All data corrected to $m/m_c = 0.9868$

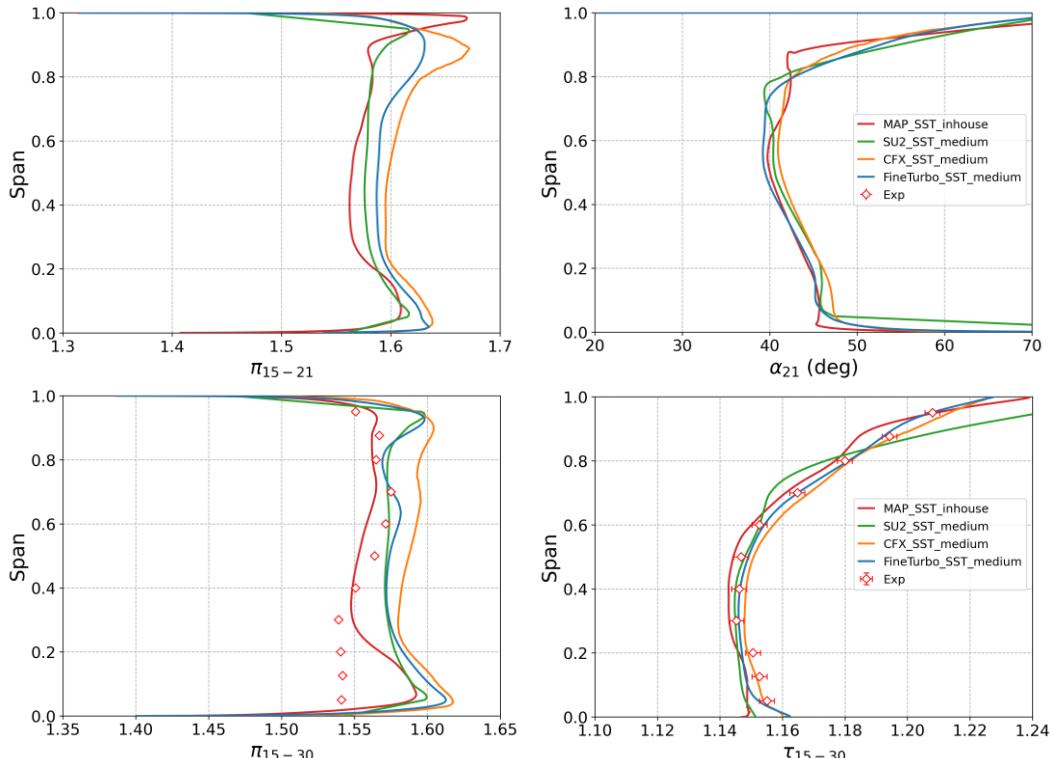


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SST Model Verification: Near Stall Profiles

Rotor exit (ME21)



Stage exit (ME30)

* All data corrected to $m/m_c = 0.9116$



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Conclusions

Conclusions

Validation (CFD vs. EXP)

- Overall uncertainty (different users and solvers, same inlet b.c., and refined grids)
Total pressure ratio: $\pm 2.5\%$; Total temperature ratio: $\pm 0.4\%$; Isentropic efficiency: $\pm 2.6\%$ (absolute)
- Major differences between CFD and EXP
Rotor exit: **near-tip TPR overshoot** (rotor tip geometrical uncertainty?); radial TPR gradient missed
Stator exit: **near-hub TPR overshoot** (stator hub cavity?)
- Most influential factors: grid density and turbulence model
Mind the “engineered” grid independence results: are the **grids refined uniformly**?
“Best-practice” turbulence model: how universal would that be? case-by-case? (more cases needed) solver-by-solver? (verification is essential)

Verification (CFD vs. CFD)

- SA model(s) in different solvers yield evidently different results
- SST model(s) in different solvers yield results similar to each other, but still not perfectly matched
- **Further V&V workshops on low TRL cases needed**

Summary of Submissions

1st GPPS Turbomachinery CFD Workshop (GPPS 2021)

Questions & Answers



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