



Simulation of TUDa-GLR-OpenStage by HGAE

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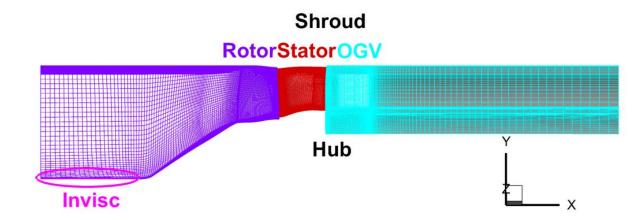
HGAE(hybrid grid aeroelasticity environment)

- ☐ A three-dimensional (3D) unstructured finite-volume compressible flow solver
 - Modeling complex geometry with high fidelity based on a hybrid grid method
 - Solving RANS equations in the rotating frame
 - Roe's upwind scheme with MUSCL extrapolation(second-order accuracy)
 - Implicit temporal discretization and dual time-stepping technique(second-order accuracy)
 - One-equation Spalart-Allmaras (S-A) turbulence model
 - Massively Parallel Processing: MPI2(Win/LINUX)
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The HGAE code has been developed and used more than 15 years, and has been validated for various aerodynamic and aeroelastic cases.

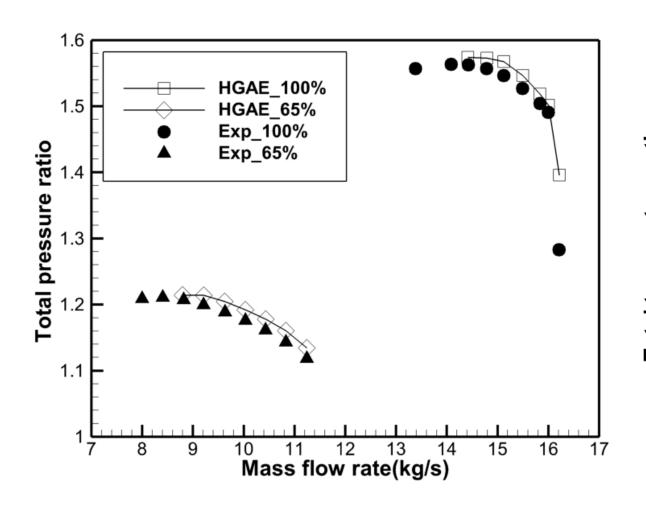
CFD—Setup

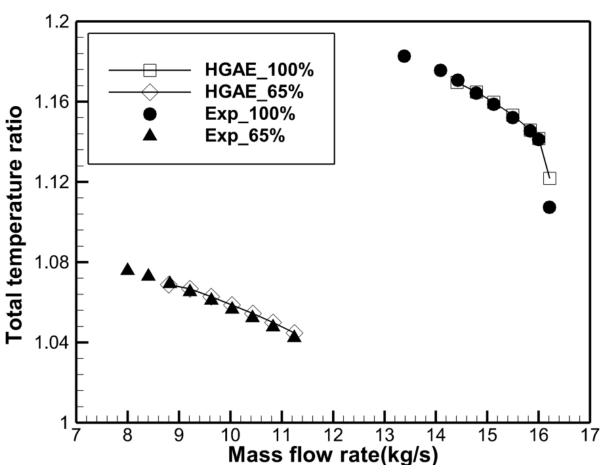
- ☐ Grid Information
 - Official medium grid
- **□** RANS Flow Solver Information
 - Roe scheme
 - SA turbulence model
 - No use of wall function
 - Mixing plane for rotor-stator interface
 - Idea gas
 - Jacobi solver
- **□** Boundary conditions
 - Inlet: from InletBC.input file $\tilde{v} = 0.198508e-4$
 - Outlet: radial equilibrium backpressure



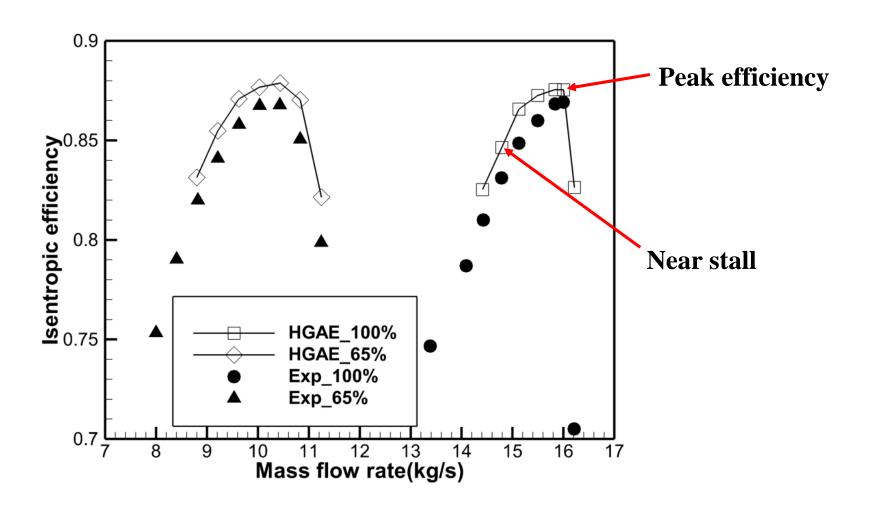
1.5 Stage computational domain

Compressor Characteristics

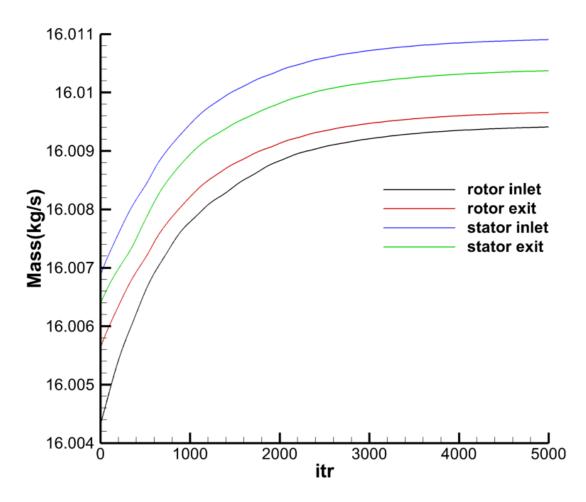




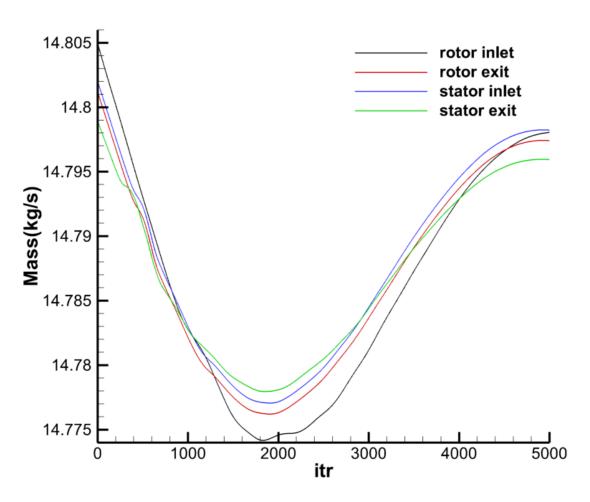
Compressor Characteristics



Convergence History(100% speed)

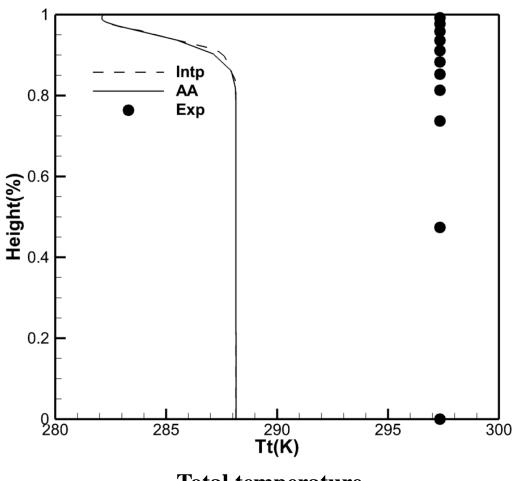


Peak efficiency condition (16.00 \pm 0.10 kg/s)

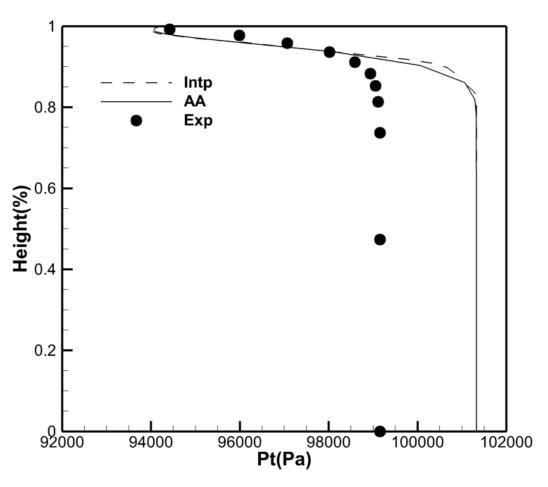


Near stall condition (14.78 \pm 0.10 kg/s)

ME15—PE100%

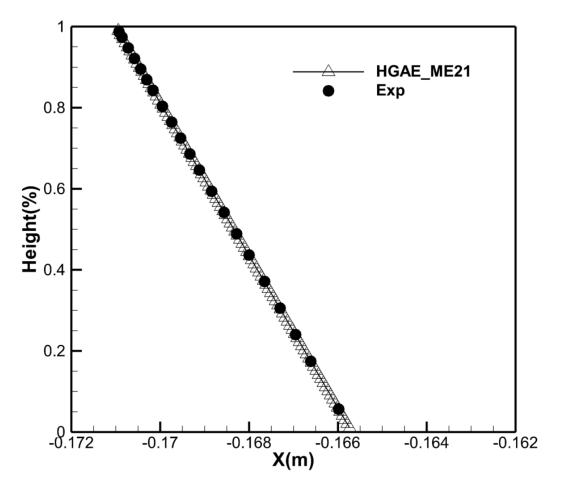


Total temperature



Total pressure

ME21—PE100%

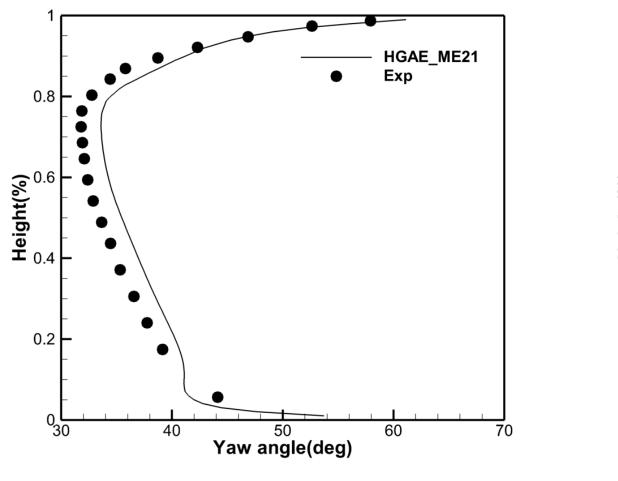


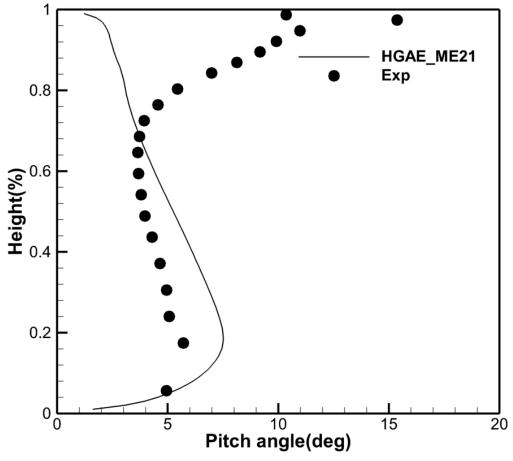
0.8 **Height(%)** HGAE_ME21 0.2 Exp 0 <u>لـــ</u> 1.2 1.35 1.4 1.45 Total pressure ratio 1.25 1.3 1.5 1.55 1.6

Axial location

Total pressure ratio

ME21—PE100%



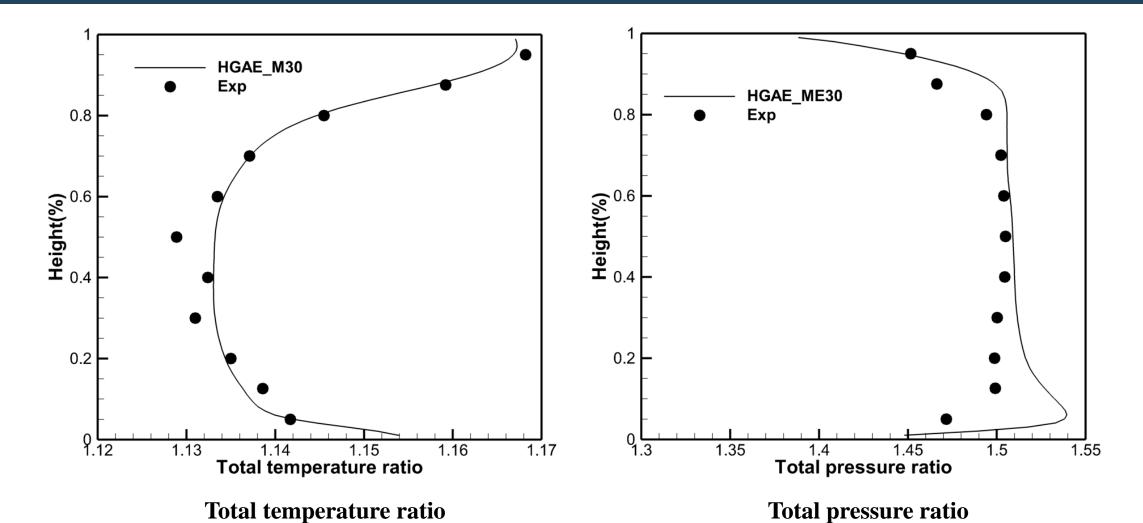


Yaw angle= arcta n(vt/vx)

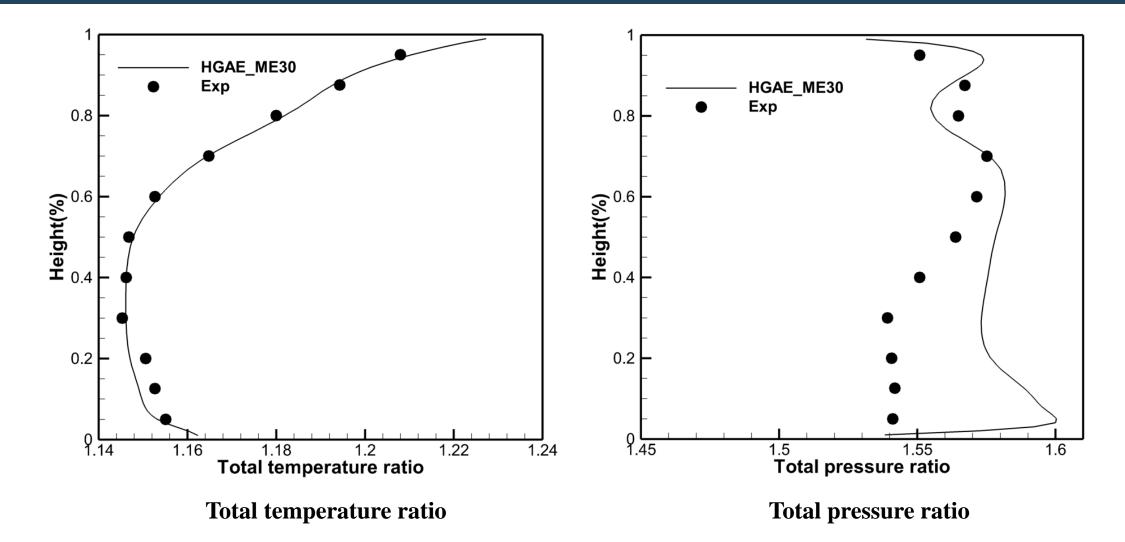
Pitch angle = arcta n(vr/vx)

 $vx \cdot vt$ and vr: axial, tangential and radial velocities in cylindrical coordinates.

ME30—PE100%



ME30—NS100%



Conclusions

- 1. With respect to the overall characteristics, the total temperature ratio calculated by HGAE shows a good agreement with the experimental results, while the total pressure ratio and isentropic efficiency are higher than the experimental results.
- 2. The compressor characteristics at the peak efficiency of the design speed agree well with the experimental results, whereas there are some deviations from the experimental results at the near stall point.
- 3. At the peak efficiency of the design speed, the total pressure ratio at 90% span and the pitch angle profiles have clear discrepancies with the experimental results at ME21 and the total pressure ratio at near 5% span is obviously different from the experimental results at ME30, which can also be found at the near stall point.



BeiHang University



Thanks