

# Steady RANS Simulation of the TUDa-GLR-OpenStage Using the Opensource Code SU2

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### Content

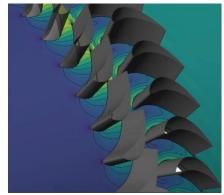
- ☐ The open-source code SU2
- □ Computation Setup
- □ Overall Performance
- □ Radial Profiles

### The Open-Source Code SU2

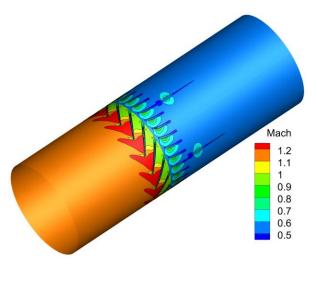
#### ☐ Features of SU2

- Adjoint Optimization
- Compressible Flow from start
- Unstructured grid
- Dynamic Mesh
- **□** Turbo Features of open SU2 up to now
  - Multi-stage RANS
  - Axial/Radial turbomachinery
  - Harmonic Balance
  - Body Force









**TUDa-GLR-OpenStage** 

Validated with Aachen Turbine case and NASA Rotor 67/Stage 35 and some cascade configurations on aerodynamics and aeroelasiticity\*\*

\*Vitale, S., M. Pini, and Piero Colonna. "Multistage turbomachinery design using the discrete adjoint method within the open-source software su2." *Journal of Propulsion and Power* 36.3 (2020): 465-478.

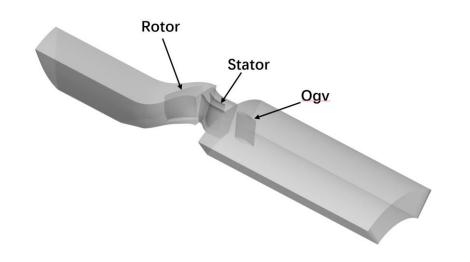
\*\*Yan, C., Wang, B., He, X., Zhao, F., Zheng, X., Vahdati, M., and Zheng, X. "Extension and Validation of the Turbomachinery Capabilities of SU2 Open Source Computational Fluid Dynamic Code." . Journal of Turbomachinery.(2024); 146(6).

### **□** Grids

• Geometry with rotor pinch included



	Ultracoarse	Coarse	Medium	Fine	Ultrafine
Rotor	0.11	0.30	1.05	3.29	11.60
Stator	0.04	0.15	0.51	1.76	5.71
OGV			8.24		

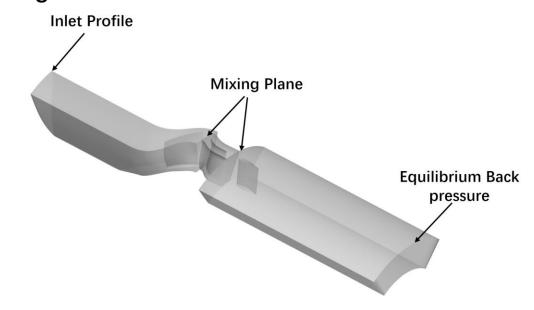


#### **□** RANS Solver

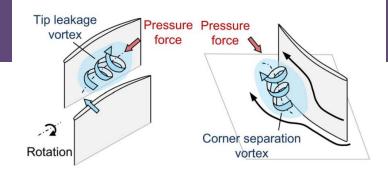
- JST convective scheme
- FGMRES linear solver
- Turbulence model: SST-2003/1994, SA, SA-PGOmega\*
- Without wall function

#### **□** Boundary Conditions

- Inlet: official inlet profile
- Outlet: radial equilibrium static pressure
- Mixing Plane Interface



\*He, X., Zhao, F., and Vahdati, M. (September 19, 2022). "A Turbo-Oriented Data-Driven Modification to the Spalart-Allmaras Turbulence Model."



#### **□** PGOmega

Fig. 1 Illustration of compressor blockage cells

He, X., Zhao, F., and Vahdati, M. (September 19, 2022). "A Turbo-Oriented Data-Driven Modification to the Spalart–Allmaras Turbulence Model."

**2.3 Proposal of SA-PG** $_{\omega}$  **Model.** To start with, the flow topologies of compressor blockage cells are illustrated in Fig. 1. A compressor blockage cell is typically formed by the tip leakage vortex or the corner separation vortex, both of which are featured by 3D swirling motion, flow stagnation, and adverse pressure gradient. In the blockage cells, the relative vorticity vector is almost aligned with the pressure gradient vector, which generally points from the upstream suction surface (SS) to the downstream pressure surface (PS). Based on these observations, an empirical compressor blockage identifier is proposed in Eq. (8)

$$\hat{p}_{\omega} = \left| \frac{\partial p}{\partial x_i} \frac{\omega_i}{\Omega} \right| / \frac{\rho^2 W^3}{\mu \text{Re}_{ref}}$$
 (8)

Finally, the compressor blockage identifier  $\hat{p}_{\omega}$  is applied to boost eddy viscosity of the original SA model by multiplying the modified strain rate  $\hat{S}$  with the  $\beta_{p\omega}$  function

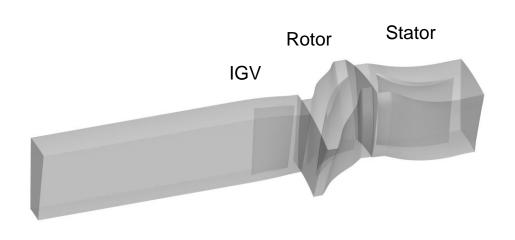
$$\beta_{p\omega}(\hat{p}_{\omega}) = \begin{cases} 1 + c_{p\omega 1} \tanh(c_{p\omega 2} \hat{p}_{\omega}^{c_{p\omega 3}}) & \text{if } \frac{\partial p}{\partial x_i} w_i \ge 0\\ 1 & \text{otherwise} \end{cases}$$
(9)

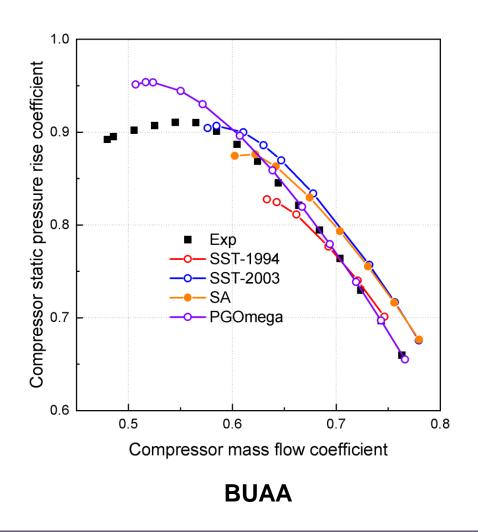
#### **□** PGOmega

```
pgomega by Xiao He 2022
  if (options.pgomga) {
    su2double dpds = 0, dpomg = 0, omg = 0, velocityMag = 0;
   su2double Velocity_Rel[3] = {0.0, 0.0, 0.0};
   su2double Vorticity_Rel[3] = {0.0, 0.0, 0.0};
   su2double RotationalVelocity[3] = {0.0, 0.0, 0.0};
   su2double RotationVelocityCrossR[3] = {0.0, 0.0, 0.0};
   for (int iDim = 0; iDim < nDim; iDim++) {</pre>
     RotationalVelocity[iDim] = config->GetRotation_Rate(iDim) / config->GetOmega_Ref();
    GeometryToolbox::CrossProduct( RotationalVelocity,Coord_i, RotationVelocityCrossR);
    for (int iDim = 0; iDim < nDim; iDim++) {</pre>
     Velocity_Rel[iDim] = V_i[idx.Velocity() + iDim] - RotationVelocityCrossR[iDim];
     Vorticity_Rel[iDim] = Vorticity_i[iDim] - RotationalVelocity[iDim];
    velocityMag = max(GeometryToolbox::Norm(3, Velocity_Rel), 0.001);
   omg = max(GeometryToolbox::Norm(3, Vorticity_Rel), 0.001);
    for (int iDim = 0; iDim < nDim; iDim++) dpds += PrimVar Grad i lidx.Pressure() [iDim] * Velocity Rel[iDim]; You, 3周前 * Uncommitted changes
    if (dpds >= 0.0) {
     su2double RefReynold = 1.0e6;
      dpomg = GeometryToolbox::DotProduct(3, PrimVar_Grad_i[idx.Pressure()], Vorticity_Rel) * laminar_viscosity *
             RefReynold / (omg * pow(velocityMag, 3) * pow(density, 2)); // reynold should be modified
      var.beta_PGO = var.cpw1 * tanh(var.cpw2 * pow(dpomg, var.cpw3));
    SetPgomegaBridge(dpomg);
Omega::get(Vorticity_i, nDim, PrimVar_Grad_i + idx.Velocity(), var);
```

- Common/include/option\_structure.hpp
- SU2\_CFD/include/numerics/CNumerics.hpp
- SU2\_CFD/include/numerics/turbulent/turb\_sources.hpp
- SU2\_CFD/include/variables/CTurbSAVariable.hpp
- SU2\_CFD/include/variables/CVariable.hpp
- SU2\_CFD/src/output/CFlowOutput.cpp
- SU2\_CFD/src/solvers/CTurbSASolver.cpp
- SU2\_CFD/src/variables/CTurbSAVariable.cpp

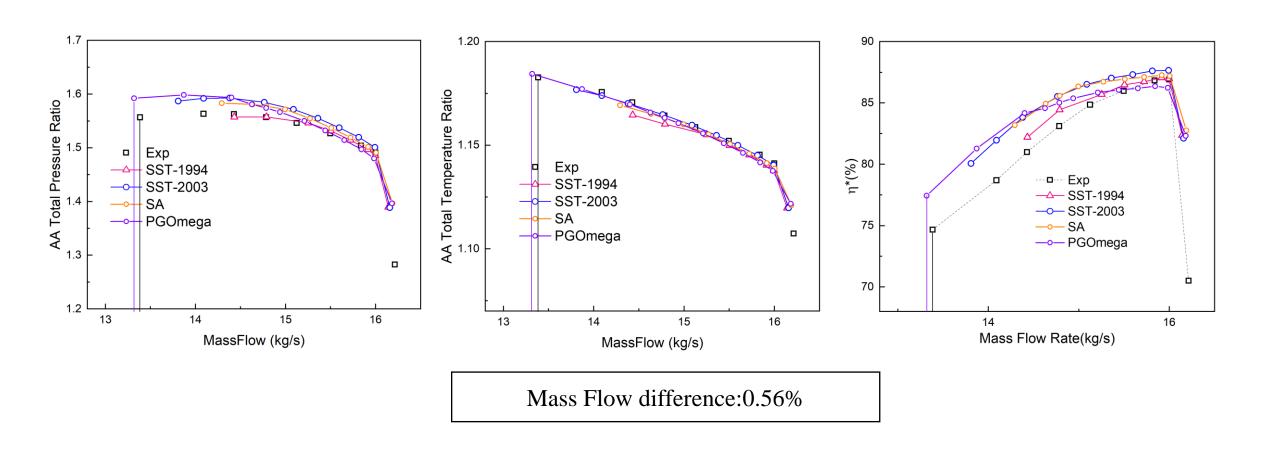
## PGOmega-BUAA



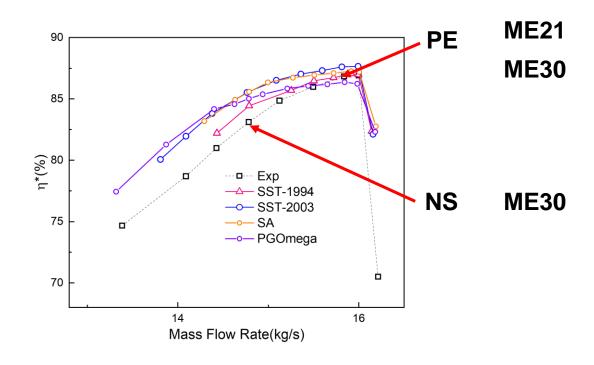


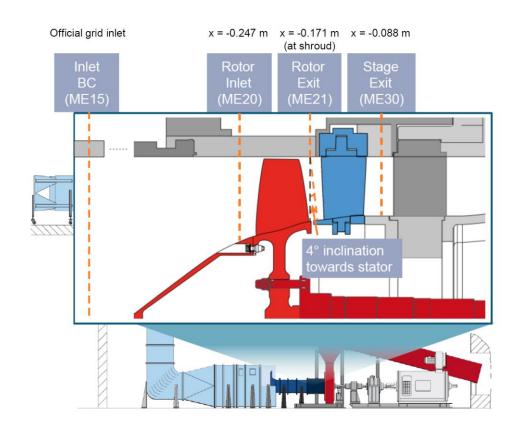
### **Overall Performance**

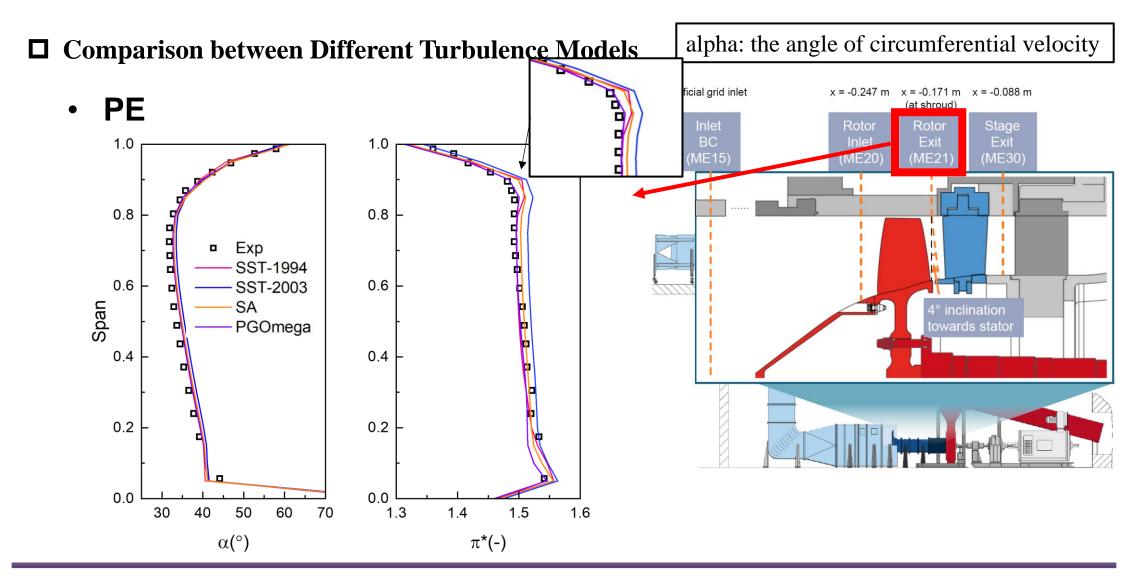
#### **□** Comparison between Different Turbulence Models



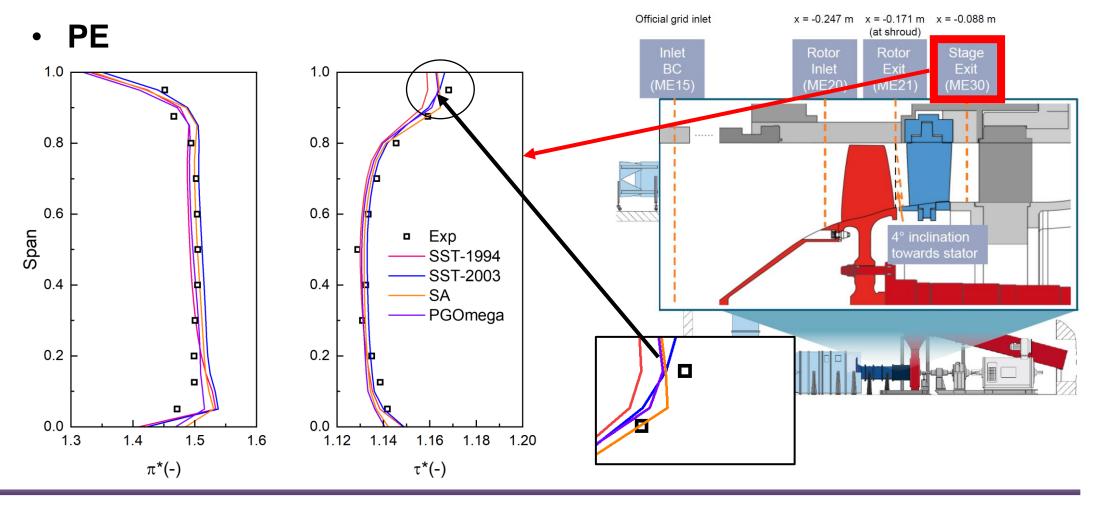
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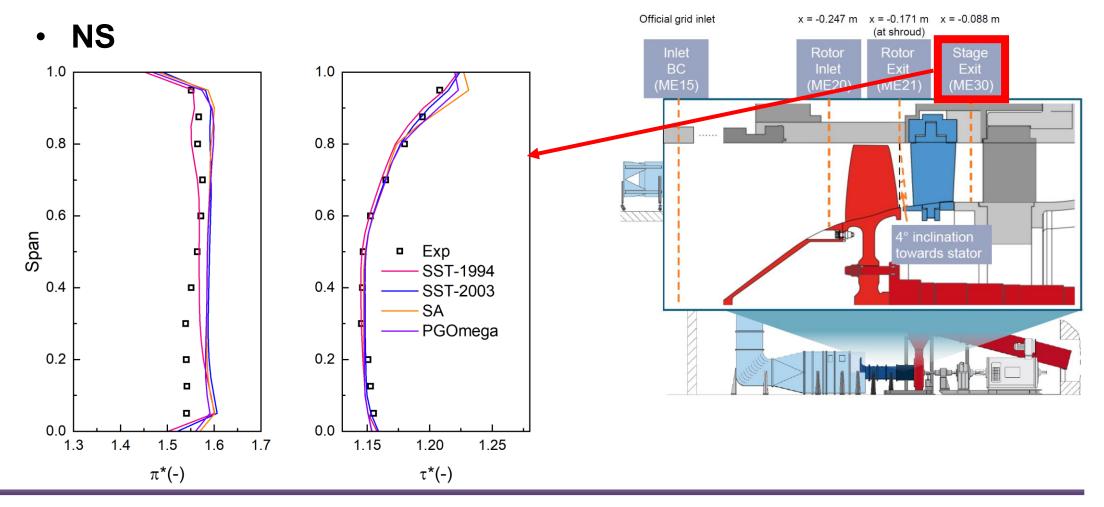




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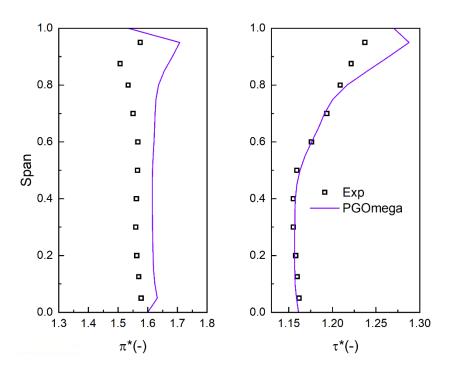
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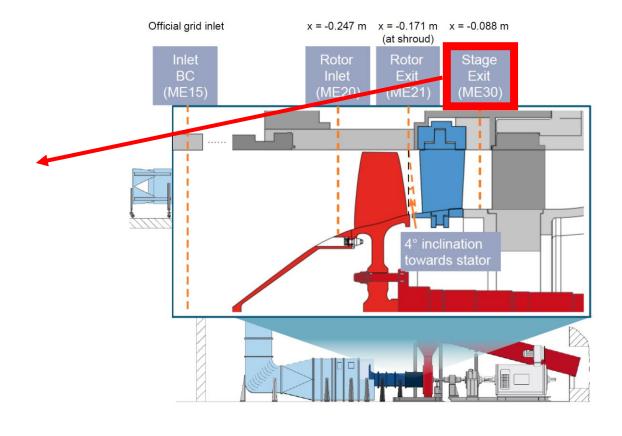


# Thanks

### **□** Comparison between Different Turbulence Models

Stall





### **□** Comparison between Different Turbulence Models

