



University
of Glasgow

HIGH-FREQUENCY COMMUNICATION SYSTEMS

Lecture 3

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- Antennas and Radiation
- Potential Functions
- Antenna Characteristics

- A distribution of currents and charges can generate and **radiate electromagnetic fields**
 - The distribution is typically localised in a region of space
 - As an example, a simple wire can act as an *antenna*
- We are interested in determining the electromagnetic fields in space, given a current distribution

ANTENNA

- Antennas are most widely used for wireless communications
- Modern antenna invention is attributed to Heinrich Hertz (1887)
 - Radio system was developed by Guglielmo Marconi (1897)
- Due to the *duality* principle, an antenna can also act as a receiver to EM radiation

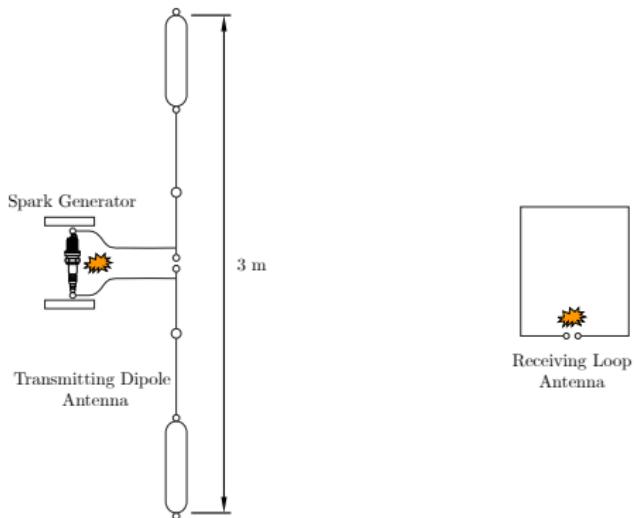


Figure 1: The Hertz's invention

- We need a **disturbance** in the EM fields
 - Most commonly, this is caused by a time-varying electric current
- The disturbance also depends on the nature of the antenna
 - For a wire antenna, the discontinuities at the ends cause radiation

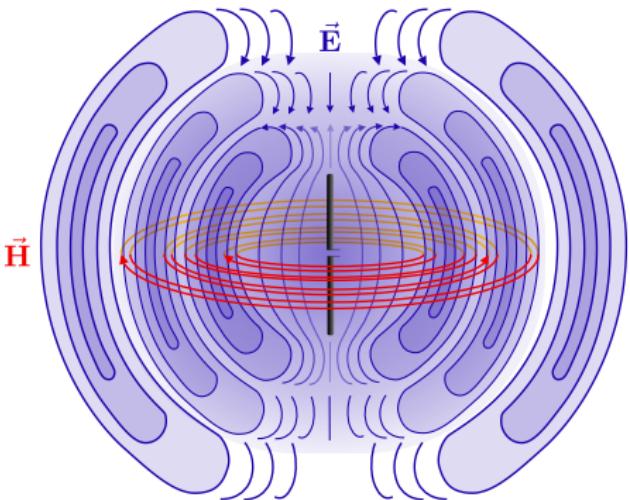


Figure 2: Antenna Radiation Mechanism

- There are mainly two ways to find the radiated fields from a given current distribution

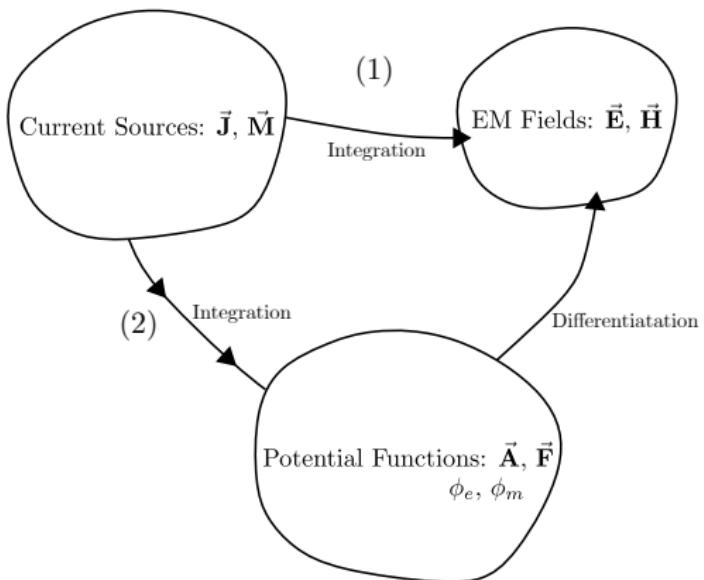


Figure 3: Two ways to find the radiated EM fields

- Solving EM fields directly using Maxwell's equations is often very difficult, especially in the spatial domain
- The introduction of scalar (ϕ) and vector $\vec{\mathbf{A}}$ potential functions simplify the process
- We start from the fact:
 - Magnetic field is divergence-less ($\nabla \cdot \vec{\mathbf{B}} = 0$). We can, therefore, say that:

$$\nabla \cdot \nabla \times \vec{\mathbf{A}} \equiv 0$$

$$\Rightarrow \vec{\mathbf{H}} = \frac{1}{\mu} \nabla \times \vec{\mathbf{A}}$$

We can write Ampere's law as:

$$\nabla \times \vec{\mathbf{E}} = -j\omega\mu\vec{\mathbf{H}} = j\omega\nabla \times \vec{\mathbf{A}}$$

$$\nabla \times (\vec{\mathbf{E}} + j\omega\vec{\mathbf{A}}) = 0$$

Knowing that the $\nabla \times (-\nabla\phi) \equiv 0$, we set:

$$\vec{\mathbf{E}} + j\omega \vec{\mathbf{A}} = -\nabla\phi$$

$$\vec{\mathbf{E}} = -\nabla\phi - j\omega \vec{\mathbf{A}}$$

- ϕ is the electric scalar potential and it's a function of position.
- If we know $\vec{\mathbf{A}}$ and ϕ , we can find $\vec{\mathbf{E}}$ and $\vec{\mathbf{H}}$

- We still need to figure out how to find the potentials, \vec{A} and ϕ for a given current density \vec{J} .
- For this we move back to Maxwell's equations and find a relationship

$$\nabla \times \vec{H} = j\omega\epsilon\vec{E} + \vec{J}$$

$$\nabla \times (\nabla \times \vec{A}) = j\omega\mu\epsilon\vec{E} + \mu\vec{J}$$

$$\nabla \times \nabla \times \vec{A} = j\omega\mu\epsilon (-j\omega\vec{A} - \nabla\phi) + \mu\vec{J}$$

Continuing and using the vector identity,

$\nabla \times \nabla \times \vec{A} = \nabla(\nabla \cdot \vec{A} - \nabla^2 \vec{A})$ and rearranging, we get,

$$\nabla^2 \vec{A} + \omega^2 \mu \varepsilon \vec{A} = -\mu \vec{J} + \nabla(\nabla \cdot \vec{A} + j\omega \mu \varepsilon \phi)$$

The solution is complete by defining \vec{A} in terms of ϕ through the Lorentz gauge,

$$\nabla \cdot \vec{A} = -j\omega \mu \varepsilon \phi$$

The magnetic vector potential \vec{A} is finally expressed through an inhomogeneous vector wave equation:

$$\nabla^2 \vec{A} + k^2 \vec{A} = -\mu \vec{J}$$

- Given an electric current density \vec{J}
- Solve for the magnetic vector potential \vec{A}
 - Solve for \vec{E} and \vec{H}

There are some assumptions in this method, namely:

- The space is homogeneous (only one material)
- The magnetic current density \vec{M} is zero.

- We solve \vec{A} individually in terms of the scalar components (A_x, A_y, A_z)
- For a forcing function p , the general solution (in terms of ψ) can be written as:

$$\nabla^2\psi + k^2\psi = -p \quad (1)$$

For a point source ($p = \delta(\vec{r})$), the solution of the above equation is called the *impulse response*. And this impulse response is also called the **Green function of the differential equation**

- For a delta function, the solution of 1 is 0 everywhere except at the origin.
- Due to spherical symmetry, it is better to express the problem in the spherical coordinates.

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right) = -k^2 \psi$$

Substituting $\psi = G/r$, we get:

$$\frac{\partial^2 G}{\partial r^2} = k^2 G$$

$$G = C_1 e^{-jkr} + C_2 e^{+jkr}$$

In terms of ψ the solution becomes:

$$\psi = \frac{G}{r} = \frac{C_1}{r} e^{-jkr} + \frac{C_2}{r} e^{+jkr}$$

For sources displaced from the origin, we use:

- The fundamental type of antenna is the point electric dipole also known as the *The Hertzian Dipole*
- The current of a z-directed Hertzian dipole is expressed as:

$$J_z(\vec{r}) = \hat{\mathbf{z}} I dl \delta(\vec{r})$$

The magnetic vector potential is given as:

$$\vec{\mathbf{A}} = \hat{\mathbf{z}} \mu \frac{I}{4\pi} dl \frac{e^{-jkr}}{r}$$

For an arbitrary source, we have:

$$\vec{\mathbf{A}} = \frac{\mu}{4\pi} \int_V \vec{\mathbf{J}} dV' \frac{e^{-jkr}}{r}$$

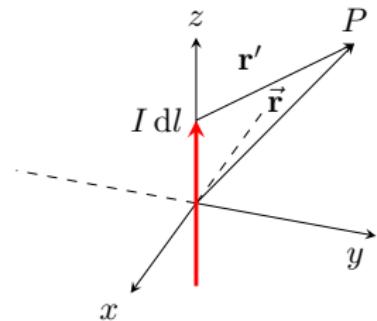


Figure 4: The Hertzian Dipole

ANTENNA CHARACTERISTICS AND PARAMETERS

- A graphical representation of the *far-field* radiation properties
- Pattern can be further described in *E*- (E_θ) and *H*- (H_ϕ) planes.

For a Hertzian dipole,
the far-fields ($kr \gg 1$)
are given as:

$$\vec{E} = \hat{\theta} \frac{j\omega\mu l dl}{4\pi r} \sin(\theta)$$

$$\vec{H} = \hat{\phi} \frac{jk l dl}{4\pi r} \sin(\theta)$$

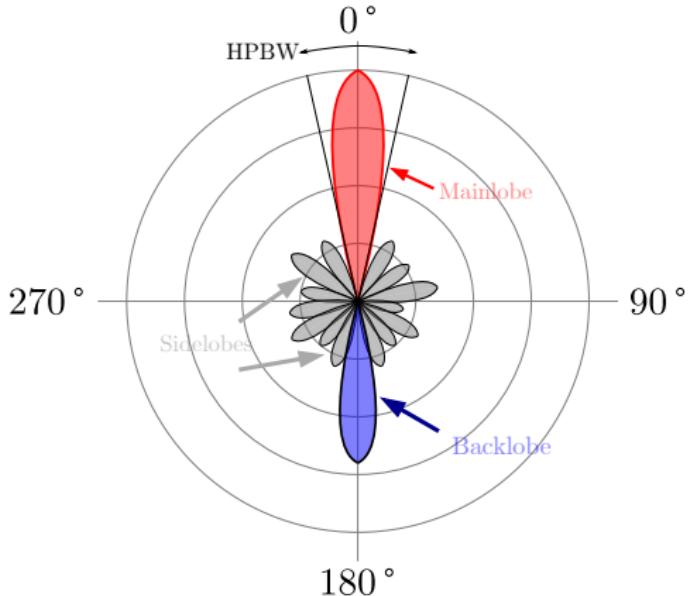


Figure 5: The Radiation Pattern

REGIONS OF RADIATION

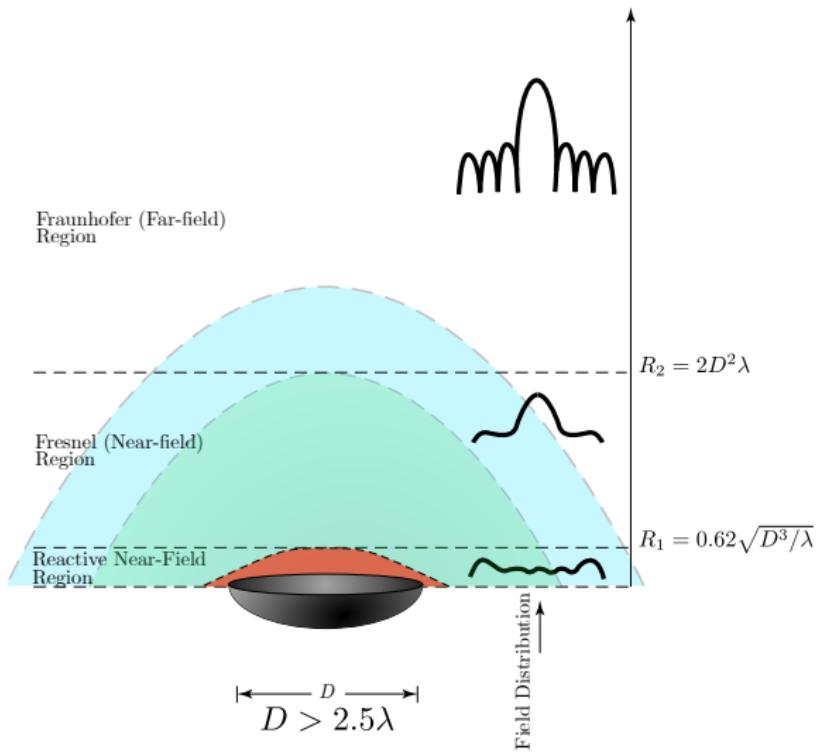
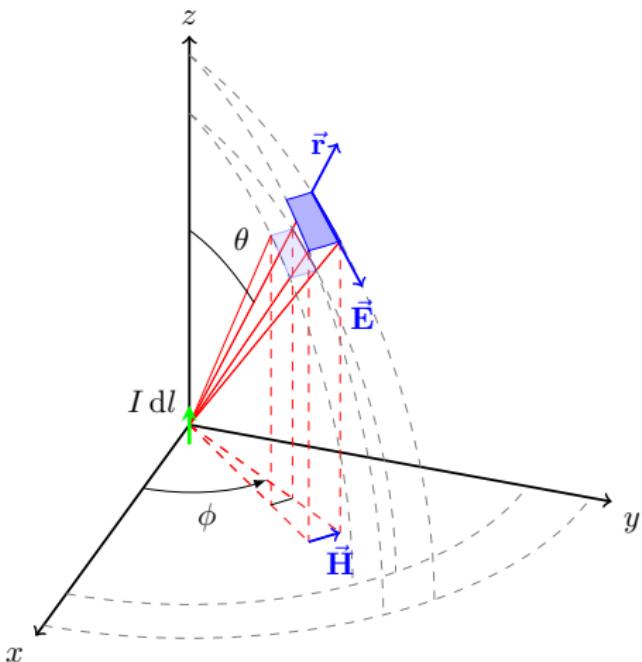


Figure 6: The Regions of Antenna Radiation

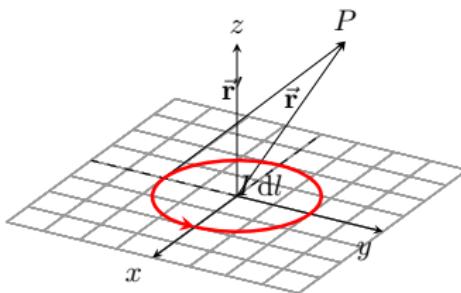
PLOTTING THE RADIATION PATTERN

- The graphical representation is easier in the spherical coordinates
- We apply the Cartesian to Spherical coordinate transformation



Homework

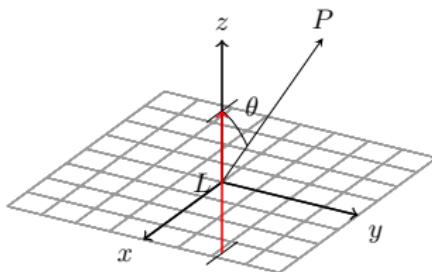
- Derive the expressions of the electric and magnetic fields for a loop antenna oriented in the $x - y$ plane as shown below
 - First derive the expression of the magnetic vector potential \vec{A}
 - Spherical coordinate transformation needs to be done on the operators and expressions.
- Due on MS Teams on March 30.



EXAMPLE - THE UNIFORM LINE SOURCE

- A line source with a uniform current along its extent
- Say the line is z-directed and centred on the origin
- The length of the line source is L

$$I(z') = \begin{cases} I_0 & x' = 0, \quad y = 0, \quad |z'| \leq \frac{L}{2} \\ 0 & \text{elsewhere} \end{cases}$$



- As the current is only in the z-direction, we only find the A_z component
- For z-directed sources, $R \approx r - z' \cos \theta$ for the phase term and $R \approx r$ in the magnitude term

$$\begin{aligned} A_z &= \mu \int_{-L/2}^{L/2} I(z') \frac{e^{-jkR}}{4\pi R} dz' \\ &= \mu \frac{e^{-jkr}}{4\pi r} \int_{-L/2}^{L/2} I_0 e^{jk(z' \cos \theta)} dz' \\ &= \mu \frac{I_0 e^{-jkr}}{4\pi r} \frac{\sin [(kL/2) \cos \theta]}{(kL/2) \cos \theta} \end{aligned}$$

The electric field is given as:

$$\begin{aligned}
 \vec{\mathbf{E}} &= -j\omega \vec{\mathbf{A}} - \frac{j}{\omega\mu\varepsilon} \nabla (\nabla \cdot \vec{\mathbf{A}}) \\
 &= -j\omega \vec{\mathbf{A}} - (-j\omega \vec{\mathbf{A}} \cdot \hat{\mathbf{r}}) \hat{\mathbf{r}} \\
 &= j\omega \sin \theta A_z \hat{\theta} \\
 &= \frac{j\omega \mu l_0 L e^{-jkr}}{4\pi r} \sin \theta \frac{\sin [(kL/2) \cos \theta]}{(kL/2) \cos \theta} \hat{\theta}
 \end{aligned}$$

The magnetic field can simply be found as:

$$H_\phi = \frac{E_\theta}{\eta}$$

- This describes the *complex power density* flowing out of a sphere of radius r
- It is real-valued and directed along the wave propagation direction

$$\vec{S} = \frac{1}{2} \vec{E} \times \vec{H}^*$$

- If \vec{E} is in the $\hat{\theta}$ and \vec{H} is in the $\hat{\phi}$ directions
- The Poynting vector will be radially directed.

- Just like voltage and current ratio gives us impedance
- The ratio of electric and magnetic field components gives us the *intrinsic impedance*

$$\frac{E_\theta}{H_\phi} = \eta = \sqrt{\frac{\mu}{\epsilon}}$$

For free space, the value is $\eta_0 = 376.7 \Omega \approx 120\pi \Omega$

- The total power radiated by an antenna can be found from the Poynting vector
- We need to integrate over a surface

$$P = \iint_{S'} \vec{S} \cdot d\vec{S}' = 1/2 \operatorname{Re} \iint_{S'} (\vec{E} \times \vec{H}^*) \cdot d\vec{S}'$$

The dS' in spherical coordinates refers to a solid angle and for a given radius r can be expressed as:

$$dS' = r^2 \sin \theta \, d\theta \, d\phi$$

- Since the power varies with distance r , it is convenient to define the *radiation intensity*
- The radiation intensity is independent of the distance
- It is defined as the **power radiated in a given direction per unit solid angle**
 - It has units of watts per steradians

$$U(\theta, \phi) = \frac{1}{2} \operatorname{Re} \left(\vec{\mathbf{E}} \times \vec{\mathbf{H}}^* \right) \cdot r^2 \hat{\mathbf{r}}$$

- For a given antenna the directivity and gain describe in what direction the radiation is, as compared to an isotropic antenna
- For the isotropic antenna, the radiation pattern is uniform (ie) a circle
- Directivity is defined as the ratio of radiation intensity in a certain direction to the average radiation intensity

$$D = \frac{1}{2} \frac{\max \left[\operatorname{Re}(\vec{\mathbf{E}} \times \vec{\mathbf{H}}^*) \cdot \hat{\mathbf{r}} \right]}{P/4\pi r^2}$$

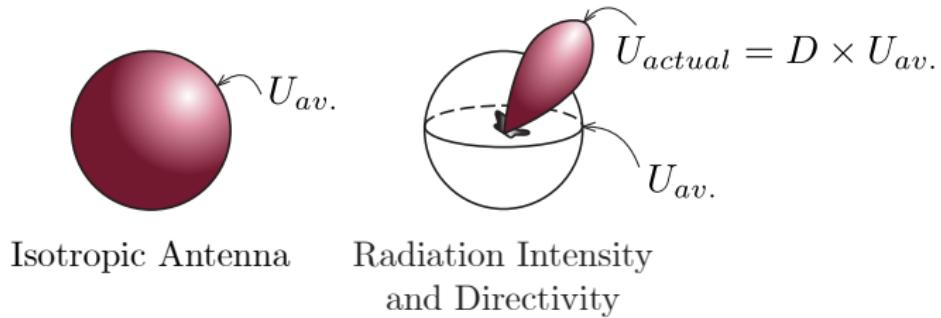


Figure 7: Relationship between Radiation Intensity and Directivity

- Although the directivity describes the radiation pattern of an antenna, we need a quantity that can be used when treating the antenna as a system
- Suppose the antenna is one component of a radio-frequency system that includes transmission lines and sources
- A parameter is helpful that determines how *efficiently* the antenna operates
 - In particular, how much input power is transferred into radiated power
- Antenna gain is defined as:

$$G = 4\pi \frac{U_m}{P_m}$$

We often describe it in terms of decibels:

$$G_{\text{dB}} = 10 \log G$$

- We can treat an antenna as an impedance with real and imaginary parts
 - The real part refers to how much radiation leaves the antenna (R_r) and how much dissipates as losses (R_o)
 - The imaginary part (X_A) determines the stored power in the near field.

$$Z_A = R_A + jX_A = (R_r + R_{ohm}) + jX_A$$

- Efficiency is a metric that determines the ratio of total desired power to the total power supplied
- Radiation efficiency of antennas is a measure of how much power is radiated

$$\epsilon_{rad} = \frac{P_{rad}}{P_{in}} = \frac{P_{rad}}{P_{rad} + P_{ohm}}$$