

HIGH FREQUENCY COMMUNICATION SYSTEMS

Lecture 3

Hasan T Abbas & Qammer H Abbasi Spring 2021

LECTURE OUTLINE

- · Antennas and Radiation
- · Potential Functions
- · Antenna Characteristics

1

SOURCES OF ELECTROMAGNETIC FIELDS

- · A distribution of currents and charges can generate and radiate electromagnetic fields
 - \cdot The distribution is typically localised in a region of space
 - · As an example, a simple wire can act as an antenna
- · We are interested in determining the electromagnetic fields in space, given a current distribution

- Antennas are most widely used for wireless communications
- Modern antenna invention is attributed to Heinrich Hertz (1887)
 - Radio system was developed by Guglielmo Marconi (1897)
- Due to the duality principle, an antenna can also act as a receiver to FM radiation

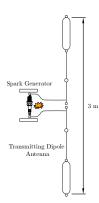




Figure 1: The Hertz's invention

- We need a disturbance in the EM fields
 - Most commonly, this is caused by a time-varying electric current
- The disturbance also depends on the nature of the antenna
 - For a wire antenna, the discontinuities at the ends cause radiation

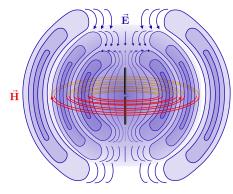


Figure 2: Antenna Radiation Mechanism

• There are mainly two ways to find the radiated fields from a given current distribution

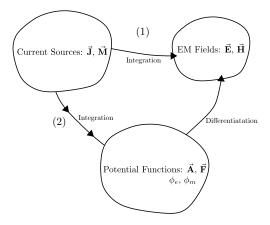


Figure 3: Two ways to find the radiated EM fields

- · Solving EM fields directly using the Maxwell's equations is often very difficult, especially in the spatial domain
- · The introduction of scalar (ϕ) and vector $\vec{\bf A}$ potential functions simplify the process
- · We start from the fact:
 - · Magnetic field is divergence-less (${f \nabla}\cdot{f B}=0$). We can therefore, say that:

$$\nabla \cdot \nabla \times \vec{\mathbf{A}} \equiv 0$$

$$\Rightarrow \vec{\mathbf{H}} = \frac{1}{\mu} \nabla \times \vec{\mathbf{A}}$$

We can write the Ampere's law as:

$$\nabla \times \vec{\mathbf{E}} = -j\omega\mu\vec{\mathbf{H}} = j\omega\nabla \times \vec{\mathbf{A}}$$
$$\nabla \times (\vec{\mathbf{E}} + j\omega\vec{\mathbf{A}}) = 0$$

Knowing that the $\nabla \times (-\nabla \phi) \equiv 0$, we set:

$$\vec{\mathbf{E}} + j\omega \vec{\mathbf{A}} = -\nabla \phi$$
$$\vec{\mathbf{E}} = -\nabla \phi - j\omega \vec{\mathbf{A}}$$

- \cdot ϕ is the electric scalar potential and its a function of position.
- · If we know $\vec{\bf A}$ and ϕ , we can find $\vec{\bf E}$ and $\vec{\bf H}$

- · We still need to figure out how to find the potentials, $\vec{\bf A}$ and ϕ for a given current density $\vec{\bf J}$.
- For this we move back to Maxwell's equations and find a relationship

$$\nabla \times \vec{\mathbf{H}} = j\omega\varepsilon\vec{\mathbf{E}} + \vec{\mathbf{J}}$$

$$\nabla \times (\nabla \times \vec{\mathbf{A}}) = j\omega\mu\varepsilon\vec{\mathbf{E}} + \mu\vec{\mathbf{J}}$$

$$\nabla \times \nabla \times \vec{\mathbf{A}} = j\omega\mu\varepsilon (-j\omega\vec{\mathbf{A}} - \nabla\phi) + \mu\vec{\mathbf{J}}$$

Continuing and using the vector identity,

$$\nabla \times \nabla \times \vec{\mathbf{A}} = \nabla \left(\nabla \cdot \vec{\mathbf{A}} - \nabla^2 \vec{\mathbf{A}} \right)$$
 and rearranging, we get,

$$\nabla^2 \vec{\mathbf{A}} + \omega^2 \mu \varepsilon \vec{\mathbf{A}} = -\mu \vec{\mathbf{J}} + \nabla \left(\nabla \cdot \vec{\mathbf{A}} + j\omega \mu \varepsilon \phi \right)$$

The solution is complete by defining $\vec{\mathbf{A}}$ in terms of ϕ through the Lorentz gauge,

$$\mathbf{\nabla \cdot \vec{A}} = -j\omega\mu\varepsilon\phi$$

The magnetic vector potential $\vec{\mathbf{A}}$ is finally expressed through an inhomogeneous vector wave equation:

$$\nabla^2 \vec{\mathbf{A}} + k^2 \vec{\mathbf{A}} = -\mu \vec{\mathbf{J}}$$

SUMMARY - THE POTENTIAL FUNCTION

- \cdot Given an electric current density $ec{\mathbf{J}}$
- · Solve for the magnetic vector potential \vec{A}
 - · Solve for \vec{E} and \vec{H}

There are some assumptions in this method, namely:

- · The space is homogeneous (only one material)
- \cdot The magnetic current density \vec{M} is zero.

- . We solve $\vec{\mathbf{A}}$ individually in terms of the scalar components (A_x,A_y,A_z)
- · For a forcing function p, the general solution (in terms of ψ) can be written as:

$$\nabla^2 \psi + k^2 \psi = -p \tag{1}$$

For a point source $(p = \delta(\vec{\mathbf{r}}))$, the solution of the above equation is called the *impulse response*. And this impulse response is also called the Green function of the differential equation

SOLVING FOR A GIVEN J

- · For a delta function, the solution of 1 is 0 everywhere except at the origin.
- Due to spherical symmetry, it is better to express the problem in the spherical coordinates.

$$\frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2\frac{\partial\psi}{\partial r}\right) = -k^2\psi$$

Substituting $\psi = G/r$, we get:

$$\frac{\partial^2 G}{\partial r^2} = k^2 G$$

$$G = C_1 e^{-jkr} + C_2 e^{+jkr}$$

In terms of ψ the solution becomes:

$$\psi = \frac{\mathsf{G}}{\mathsf{r}} = \frac{\mathsf{C}_1}{\mathsf{r}} \mathrm{e}^{-jk\mathsf{r}} + \frac{\mathsf{C}_2}{\mathsf{r}} \mathrm{e}^{+jk\mathsf{r}}$$

For sources displaced from the origin, we use:

- The fundamental type of antenna is the point electric dipole also known as the *The Hertzian Dipole*
- The current of a z-directed Hertzian dipole is expressed as:

$$J_Z(\vec{\mathbf{r}}) = \widehat{\mathbf{z}} l \, \mathrm{d} l \, \delta(\vec{\mathbf{r}})$$

The magnetic vector potential is given as:

$$\vec{\mathbf{A}} = \widehat{\mathbf{z}}\mu \frac{1}{4\pi} \, \mathrm{d}l \, \frac{\mathrm{e}^{-jkr}}{r}$$

For an arbitrary source, we have:

$$\vec{\mathbf{A}} = \frac{\mu}{4\pi} \int_{V} \vec{\mathbf{J}} \, \mathrm{d}V' \, \frac{\mathrm{e}^{-jkr}}{r}$$

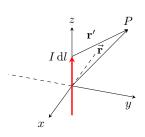


Figure 4: The Hertzian Dipole



THE RADIATION PATTERN

- · A graphical representation of the far-field radiation properties
- Pattern can be further described in E- (E_{θ}) and H- (H_{ϕ}) planes.

For a Hertzian dipole, the far-fields ($kr \gg 1$) are given as:

$$\vec{\mathbf{E}} = \hat{\boldsymbol{\theta}} \frac{j\omega\mu l \, \mathrm{d}l}{4\pi r} \sin(\theta)$$
$$\vec{\mathbf{H}} = \hat{\boldsymbol{\phi}} \frac{jkl \, \mathrm{d}l}{4\pi r} \sin(\theta)$$

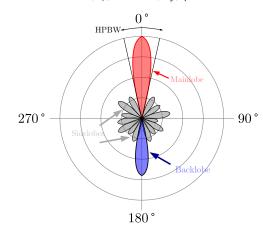


Figure 5: The Radiation Pattern

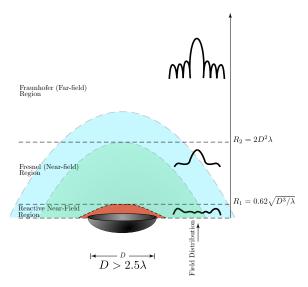
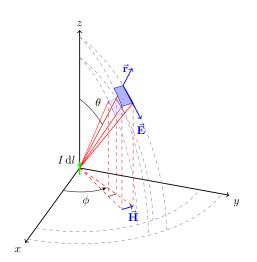


Figure 6: The Regions of Antenna Radiation

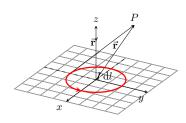
PLOTTING THE RADIATION PATTERN

- The graphical representation is easier in the spherical coordinates
- · We apply the Cartesian to Spherical coordinate transformation



Homework

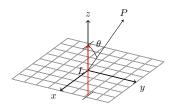
- · Derive the expressions of the electric and magnetic fields for a loop antenna oriented in the x-y plane as shown below
 - First derive the expression of the magnetic vector potential $\vec{\mathbf{A}}$
 - · Spherical coordinate transformation needs to be done on the operators and expressions.
- · Due on MS Teams on March 30.



EXAMPLE - THE UNIFORM LINE SOURCE

- · A line source with a uniform current along its extent
- · Say the line is z-directed and centered on the origin
- · The length of the line source is L

$$I(Z') = \begin{cases} I_0 & x' = 0, \quad y = 0, \quad |Z'| \le \frac{L}{2} \\ 0 & \text{elsewhere} \end{cases}$$



- · As the current is only in the z-direction, we only find the A_z component
- · For z-directed sources, $R \approx r z' \cos \theta$ for the phase term and $R \approx r$ in the magnitude term

$$A_{z} = \mu \int_{-L/2}^{L/2} I(z') \frac{e^{-jkR}}{4\pi R} dz'$$

$$= \mu \frac{e^{-jkr}}{4\pi r} \int_{-L/2}^{L/2} I_{0} e^{jk(z'\cos\theta)} dz'$$

$$= \mu \frac{I_{0} e^{-jkr}}{4\pi r} \frac{\sin[(kL/2)\cos\theta]}{(kL/2)\cos\theta}$$

The electric field is given as:

$$\begin{split} \vec{\mathbf{E}} &= -j\omega\vec{\mathbf{A}} - \frac{j}{\omega\mu\varepsilon}\nabla\left(\nabla\cdot\vec{\mathbf{A}}\right) \\ &= -j\omega\vec{\mathbf{A}} - (-j\omega\vec{\mathbf{A}}\cdot\hat{\mathbf{r}})\hat{\mathbf{r}} \\ &= j\omega\sin\theta\mathsf{A}_z\hat{\boldsymbol{\theta}} \\ &= \frac{j\omega\mu\mathsf{I}_0\mathsf{Le}^{-jkr}}{4\pi r}\sin\theta\frac{\sin\left[(k\mathsf{L}/2)\cos\theta\right]}{(k\mathsf{L}/2)\cos\theta}\hat{\boldsymbol{\theta}} \end{split}$$

The magnetic field can simply be found as:

$$H_{\phi} = \frac{E_{\theta}}{\eta}$$

- This describes the *complex power density* flowing out of a sphere of radius *r*
- · It is real-valued and directed along the wave propagation direction

$$\vec{\mathbf{S}} = \frac{1}{2}\vec{\mathbf{E}} \times \vec{\mathbf{H}^*}$$

- · If $\vec{\mathbf{E}}$ is in the $\hat{oldsymbol{ heta}}$ and $\vec{\mathbf{H}}$ is in the $\hat{oldsymbol{\phi}}$ directions
- The Poynting vector will be radially directed.

- · Just like voltage and current ratio gives us impedance
- The ratio of electric and magnetic field components give us the intrinsic impedance

$$\frac{\mathsf{E}_{\theta}}{\mathsf{H}_{\phi}} = \eta = \sqrt{\frac{\mu}{\varepsilon}}$$

For freespace, the value is $\eta_0=376.7\,\Omega\approx$ 120 $\pi\,\Omega$

- The total power radiated by an antenna can be found from the Poynting vector
- · We need to integrate over a surface

$$P = \iint_{S'} \vec{\mathbf{S}} \cdot dS' = 1/2 \operatorname{Re} \iint_{S'} (\vec{\mathbf{E}} \times \vec{\mathbf{H}^*}) \cdot dS'$$

The dS' in spherical coordinates refers to a solid angle and for a given radius r can be expressed as:

$$dS' = r^2 \sin \theta \, d\theta \, d\phi$$

- Since the power varies with distance *r*, it is convenient to define the *radiation intensity*
- · The radiation intensity is independent of the distance
- It is defined as the power radiated in a given direction per unit solid angle
 - · It has units of watts per steradians

$$U(\theta, \phi) = \frac{1}{2} \operatorname{Re} \left(\vec{\mathbf{E}} \times \vec{\mathbf{H}^*} \right) \cdot r^2 \hat{\mathbf{r}}$$

- For a given antenna the directivity and gain describe in what direction the radiation is, as compared to an isotropic antenna
- · For the isotropic antenna, the radiation pattern is uniform (ie) a circle
- Directivity is defined as the ratio of radiation intensity in a certain direction to the average radiation intensity

$$D = \frac{1}{2} \frac{\max \left[\text{Re}(\vec{\mathbf{E}} \times \vec{\mathbf{H}^*}) \cdot \hat{\mathbf{r}} \right]}{P/4\pi r^2}$$

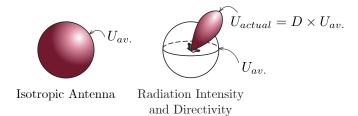


Figure 7: Relationship between Radiation Intensity and Directivity

- · Although the directivity describes the radiation pattern of an antenna, we need a quantity that can be used when treating antenna as a system
- Suppose the antenna is one component of a radio-frequency system that includes transmission lines and sources
- · A parameter is helpful that determines how *efficiently* the antenna operates
 - · In particular, how much input power is transferred into radiated power
- · Antenna gain is defined as:

$$G = 4\pi \frac{U_m}{P_m}$$

We often describe it in terms of decibels:

$$G_{\rm dB} = 10\log G$$

- · We can treat antenna as an impedance with real and imaginary parts
 - · The real part refers to the how much radiation leaves the antenna (R_r) and how much dissipates as losses (R_0)
 - · The imaginary part (X_A) determines the stored power in the near field.

$$Z_A = R_A + jX_A = (R_r + R_{ohm}) + jX_A$$

- · Efficiency is a metric that determines the ratio of total desired power to the total power supplied
- Radiation efficiency of antennas is a measure how much power is radiated

$$e_{rad} = \frac{P_{rad}}{P_{in}} = \frac{P_{rad}}{P_{rad} + P_{ohm}}$$