

HIGH FREQUENCY COMMUNICATION SYSTEMS

Lecture 8

Hasan T Abbas & Qammer H Abbasi Spring 2021

LECTURE OUTLINE

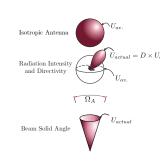
- · Array Directivity
- · Planar Antenna Arrays
- · Feeding Networks
- · Software-defined Radio

1

DIRECTIVITY

- · Recall *directivity* describes the antenna radiation in a given direction
 - · We use the radiation intensity $[U(\theta,\phi)=1/2\operatorname{Re}(\vec{\mathbf{E}}\times\vec{\mathbf{H}}^*)\cdot r^2\,\widehat{\mathbf{r}}] \text{ to assess the power radiated in a given direction per unit solid angle}$
- · We define the directivity as:

$$\begin{split} D = & \frac{4\pi}{\Omega_{\text{A}}} \\ \text{where,} & \Omega_{\text{A}} = \iint |\textit{EF}(\theta,\phi)|^2 |\textit{AF}(\theta,\phi)|^2 \mathrm{d}\Omega \\ & \mathrm{d}\Omega = \sin\theta \, \mathrm{d}\theta \, \mathrm{d}\phi \end{split}$$



Lets first consider a uniformly excited, uniformly spaced linear array where all the elements are *isotropic* (EF = 1). From the previous lecture, we have:

$$|AF|^2 = \left| \frac{\sin N\psi/2}{N\sin \psi/2} \right|^2 \equiv \frac{1}{N} + \frac{1}{N^2} \sum_{m=1}^{N-1} (N-m)\cos m\psi \tag{1}$$

Knowing,

$$\psi = kd\cos\theta + \alpha \implies \sin\theta \,d\theta = -\frac{1}{kd}\,d\psi$$

The beam solid angle Ω_A then becomes:

$$\Omega_{A} = \int_{0}^{2\pi} d\phi \int_{0}^{\pi} |AF(\theta)|^{2} d\theta = 2\pi \int_{kd+\alpha}^{-kd+\alpha} |AF(\psi)|^{2} \left(\frac{-1}{kd}\right) d\psi$$

$$= \frac{2\pi}{kd} \int_{-kd+\alpha}^{kd+\alpha} |AF(\psi)|^{2} d\psi \tag{2}$$

4

SOME FURTHER COMPUTATION

Solving (1) and (2) we get:

$$\begin{split} \Omega_{A} &= \frac{2\pi}{kd} \left[\frac{1}{N} \int_{-kd+\alpha}^{kd+\alpha} \mathrm{d}\psi + \frac{2}{N^2} \sum_{m=1}^{N-1} (N-m) \int_{-kd+\alpha}^{kd+\alpha} \cos m\psi \mathrm{d}\psi \right] \\ &= \frac{2\pi}{kd} \left[\frac{1}{N} \psi \bigg|_{-kd+\alpha}^{kd+\alpha} + \frac{2}{N^2} \sum_{m=1}^{N-1} (N-m) \frac{\sin m\psi}{m} \bigg|_{-kd+\alpha}^{kd+\alpha} \right] \\ &= \frac{2\pi}{kd} \left[\frac{1}{N} (2kd) + \frac{2}{N^2} \sum_{m=1}^{N-1} \frac{N-m}{m} [\sin m(kd+\alpha) - \sin m(-kd+\alpha)] \right] \end{split}$$

Using the trigonometric identity, $\sin(a+b) = \sin a \cos b + \cos a \sin b$, we get:

$$\Omega_{A} = \frac{4\pi}{N} + \frac{4\pi}{N^2} \sum_{m=1}^{N-1} \frac{N-m}{mkd} 2\cos m\alpha \sin mkd$$

The directivity for broadside and end-fire arrays is thus:

$$D = \frac{4\pi}{\Omega_A} = \frac{1}{\frac{1}{N} + \frac{1}{N^2} \sum_{m=1}^{N-1} \frac{N-m}{mkd} 2\cos m\alpha \sin mkd}$$

For arrays such as the Hanson-Woodyard arrays, there is an additional renormalisation factor that accounts for the excess phase delay, δ ,

$$D_{\text{General}} = \frac{\left|\frac{\sin(N\delta/2)}{N\sin\delta/2}\right|^2}{\frac{1}{N} + \frac{1}{N^2} \sum_{m=1}^{N-1} \frac{N-m}{mkd} 2\cos m\alpha \sin mkd}$$
(3)

In general, the directivity from (3) can be visualised as:

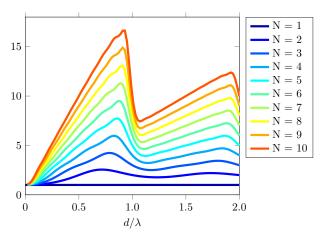
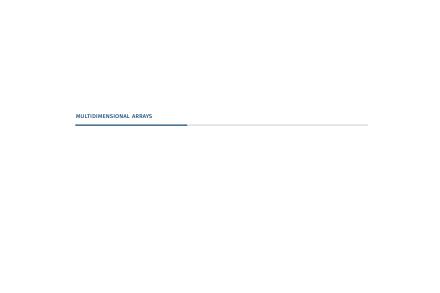


Figure 1: Seeing the directivity as a function of element spacing d and number of elements N.



- So far, the 1D arrays we have looked at only yield beamscanning along one angle θ .
- Using multidimensional arrays, we can:
 - · Obtain pencil beams
 - Higher directivity and gain
 - Maneuver beams in both elevation and azimuthal planes.
- We can have elliptical or rectangular shapes in the 2D case

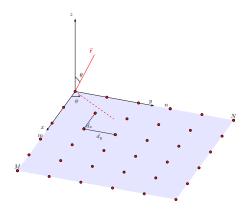


Figure 2: A 2D rectangular array.

Generally, the Array Factor for an 3D array can be described by first expressing the elements in the form of a position vector:

$$\hat{\mathbf{r'}}_{mn} = \widehat{\mathbf{x}} d_{mn} + \widehat{\mathbf{y}} y'_{mn} + \widehat{\mathbf{z}} z'_{mn}$$

Then,

$$AF(\theta,\phi) = \sum_{m=1}^{M} \sum_{n=1}^{N} I_{mn} \exp(j(k \hat{\mathbf{r}} \cdot \hat{\mathbf{r}'}_{mn} + \alpha_{mn}))$$

In the normalised form, we can write AF as:

$$\begin{split} \text{AF}(\theta,\phi) = & \frac{\sin M\psi_{\text{X}}/2}{M\sin\psi_{\text{X}}/2} \, \frac{\sin N\psi_{\text{y}}/2}{N\sin\psi_{\text{y}}/2} \\ \text{where,} \\ & \psi_{\text{X}} = & kd_{\text{X}}\sin\theta\cos\phi + \alpha_{\text{X}} \\ & \psi_{\text{y}} = & kd_{\text{y}}\sin\theta\sin\phi + \alpha_{\text{y}} \end{split}$$

Considering a 5×5 planar array with element spacings $d_{\rm x}=d_{\rm y}=\lambda/2$ and the phases $\alpha_{\rm x}=\alpha_{\rm y}=-\pi/(2\sqrt{2})$. The radiation pattern looks like:

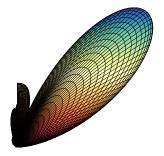


Figure 3: Radiation Pattern in the Cartesian coordinates.

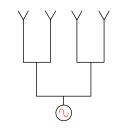


- The main benefit of phased array antennas is there is no need for mechanical motion.
 - · Beam can be steered using electronics
- A disadvantage is each antenna element must have a transmission path to the receiver
 - This is done both via hardware and software



Figure 4: Feeding Cables out of a Massive MIMO Phased Array Antenna

- Most common feeding network
 - · Also called parallel feed
- · We have equal line lengths to each element
 - Phase and amplitude are same across the elements
- Corporate feed can be operated at many frequencies
 - We call it wideband as the operation is independent of frequency



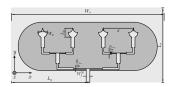


Figure 5: A Planar Inverted Cone Antenna Array ¹.

[&]quot;Abdoalbaset at Abohmra et al. "An Ultrawideband Microfabricated Gold-based Antenna Array for Terahertz Communication". In: IEE AWPL (2021). ISSN: 1548-5.

SERIES FEEDING NETWORK

- · Simplest feeding architecture
 - · Phase difference can be easily generated
- However, practically loss occurs along the series line
 - This results in unequal amplitudes across the elements
- By changing the frequency, the electrical line length of the feed is changed.
 - Due to this, we have dispersion that limits bandwidth

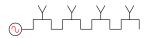


Figure 6: A series feeding network

THE HYBRID FEEDING NETWORK

- · Suitable for very large arrays
 - Additional phase shift is introduced commonly through diodes (PIN etc.)
- MEMS based switches can turn a particular arm on or off.
 - Such feeds can withstand high power inputs
- By changing the frequency, the electrical line length of the feed is changed.
 - Due to this, we have dispersion that limits bandwidth

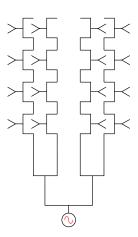


Figure 7: A hybrid corporate-series feeding network

OTHER FEEDING NETWORKS

- For millimetre wave communications, corporate and series feeding architectures become very complicated
- Other techniques such as sequentially rotated phase feeding networks are emerging as attractive candidates
 - · Each antenna element is physically rotated
 - Additionally, there is a phase shift to each element
- The advantage over corporate feeding network is that the resonant response can be obtained at a higher range of frequencies
 - · Ensures radiation pattern integrity

Figure 8: A sequentially rotated phase feeding network 1.

^{&#}x27;Chaojun Ma, Zu-Hui Ma, and Xiupu Zhang. "Millimeter-Wave Circularly Polarized Array Antenna Using Substrate-Integrated Gap Waveguide Sequentially Rotating Phase Feed", In: IEEE AWPL (2019). ISSN: 1548-5757.



- · A communication system consists of many layers of operations.
- · The physical layer is the most important of all.
- · Typically, physical layer processing is done via dedicated hardware
- · Radio is the technology through which signals are wirelessly transmitted and received
- · Software-defined radio has some or all physical layer functions implemented via hardware

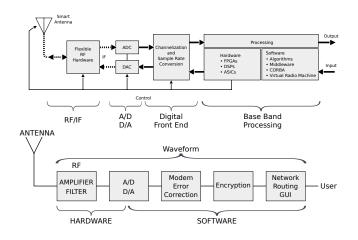


Figure 9: A Typical SDR workflow

- A graphical user interface consisting of flowgraphs through which different signal processing functions such as analog-digital conversion can be performed.
- Some additions let us writePython codes within each block
- The software is meant to interface with Universal Software Radio Peripheral (USRP) modules to construct a complete communication system.

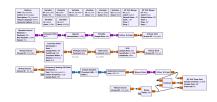


Figure 10: GNU Radio Interface.