



University
of Glasgow

HIGH FREQUENCY COMMUNICATION SYSTEMS

Lecture 1

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PRELIMINARY INFORMATION

COURSE TEAM



(a) Dr Qammer H Abbasi



(b) Dr Hasan T Abbas

MOTIVATION - CHANG'E NO. 4



Panoramic View of the Chang'e No. 4 Lander on the Moon.

- We will award the best students for best overall performance and best project.



(c) Overall Prize



(d) Project Competition

- Introduction to Millimetre wave (mmWave) and Terahertz (THz) Frequency Communication Systems
- Theory of Electromagnetic (EM) wave propagation
- Channel Modelling Schemes
- Antenna Analysis & Design

- State of the art of electromagnetic simulation strategies for THz devices
- Application of solid-state structures and novel 2D materials in mmWave and THz device technologies
- Antenna design with emphasis on phased arrays used for beamforming
- Wireless Propagation models of mmWave and THz communication channels

At the end of the course you will be able to:

1. Recognise the physical limitations of electromagnetic wave propagation and the need to move to higher frequencies in next generation mobile communication.
2. Analyse the wireless channel models to characterise a cellular communication environment.
3. Use electromagnetic simulation techniques to study antennas and wave propagation.
4. Design complex antenna systems with specific beamforming needs for mobile environments.

COURSE ASSESSMENTS

Assessment	Weightage
Homework	30%
Final Exam	30%
Term Project	30%
Class Participation	10%

COURSE ASSESSMENTS DETAILS

Homework	3 Assignments in total
Final Exam	2 Questions – 1 hour long
Term Project	Design a mmWave Cubesat antenna
Class Participation	Attendance and participation in the discussions

YOUR FIRST TASK

- Make a project plan for the mmWave Cubesat antenna
- You will be marked individually but are welcome to work as a team
- Prepare a Gantt chart for the project
- Come up with an expected budget of the project

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- You can work in groups of 2 or 3

THE RADIO SPECTRUM

DESCRIPTIONS

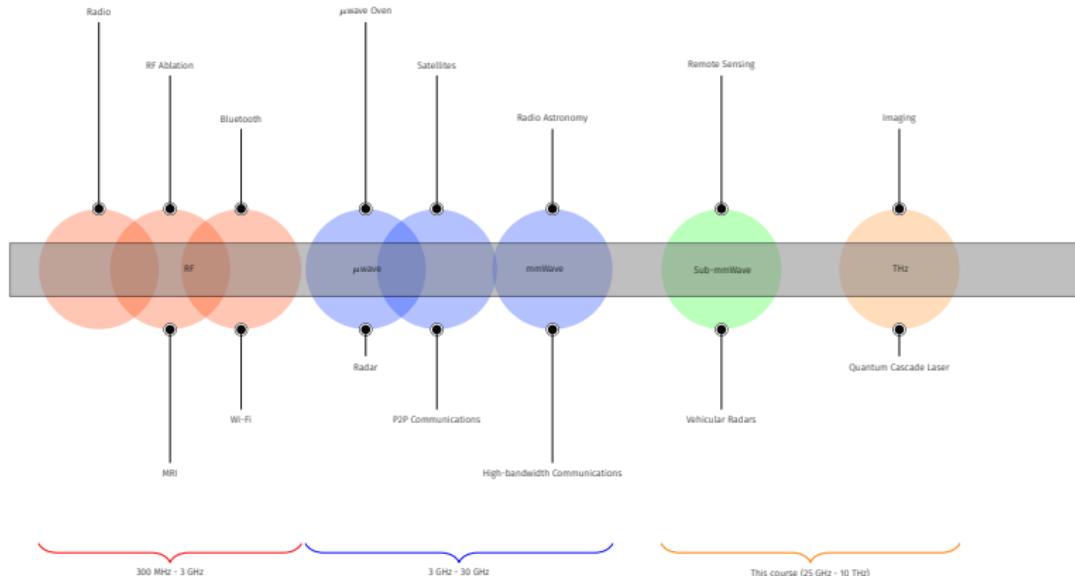


Figure 1: The electromagnetic wave spectrum

- EM theory deals with the study of charges
- Charges at rest or more importantly in motion

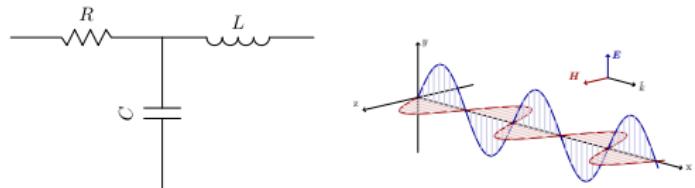


Figure 2: Circuit and Electromagnetic Theories

- Circuit theory is actually a subset of EM theory
- We apply *lumped* circuit theory when wavelength λ is much larger than circuit dimensions
 - Parasitic elements are negligible

THE MAXWELL'S EQUATIONS

- Set of four linear equations
 - Linearity helps multiple users access one radio link (tower).
- James Clerk Maxwell predicted wave propagation (1866)
- Heinrich Hertz (1886) experimentally proved the results in a lab
- Kick-started radio wave communications
- Comprehensive in explaining EM phenomena

- We use this form to describe the fields *at any point in space and time.*
- We call them field equations
- Widely used to solved wave phenomena.

$$\nabla \times \vec{\mathbf{E}} = -\frac{\partial \vec{\mathbf{B}}}{\partial t} - \vec{\mathbf{M}} \quad (\text{Faraday's Law})$$

$$\nabla \times \vec{\mathbf{H}} = \frac{\partial \vec{\mathbf{D}}}{\partial t} + \vec{\mathbf{J}} \quad (\text{Ampere's Law})$$

$$\nabla \cdot \vec{\mathbf{E}} = \rho_e / \varepsilon_0 \quad (\text{Gauss' Law})$$

$$\nabla \cdot \vec{\mathbf{H}} = \rho_m / \mu_0 \quad (\text{Flux Law})$$

- The current density, $\vec{\mathbf{J}} = \vec{\mathbf{J}}_i + \vec{\mathbf{J}}_d + \vec{\mathbf{J}}_c$
- In statics, $\frac{\partial}{\partial t}$ is zero.

- We use this form to describe the fields over *an extended region of space.*
- Not widely used.

$$\oint_C \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \iint_S \vec{B} \cdot d\vec{S} \quad (\text{Faraday's Law})$$

$$\oint_C \vec{H} \cdot d\vec{l} = \iint_S \vec{J} \cdot d\vec{S} + \frac{\partial}{\partial t} \iint_S \vec{D} \cdot d\vec{S} \quad (\text{Ampere's Law})$$

$$\iint_S \vec{D} \cdot d\vec{S} = \iiint_V \rho_e \, dV = \phi_e \quad (\text{Gauss' Law})$$

$$\iint_S \vec{B} \cdot d\vec{S} = \iiint_V \rho_m \, dV = \phi_m \quad (\text{Flux Law})$$

How the flux densities (electric \vec{D} , magnetic \vec{B}) and field intensities (electric \vec{E} , magnetic \vec{H}) are related.

For simple (isotropic) materials, we have a simple linear relationship:

$$\vec{D} = \epsilon \vec{E} \text{ [C m}^{-2}\text{]} \quad \text{(Dielectric Material)}$$

$$\vec{B} = \mu \vec{H} \text{ [Wb m}^{-2}\text{]} \quad \text{(Magnetic Material)}$$

$$\vec{J} = \sigma \vec{E} \text{ [A m}^{-2}\text{]}$$

- ϵ and μ are the permittivity and permeability of a given material respectively. For simple (isotropic and homogeneous) materials, these are real numbers.
- At higher frequencies, we need to consider the material polarizability.

- We can extract many material properties from ε and μ .

The speed of light:

$$c = \sqrt{\frac{1}{\mu\varepsilon}}$$

The characteristic impedance:

$$\eta = \sqrt{\frac{\mu}{\varepsilon}}$$

The refractive index:

$$n = \sqrt{\mu\varepsilon}$$

- Most materials are considered non-magnetic ($\mu_r = 1$).
- Further properties at nanoscale EM

In real life, there are many types of media. Generally,

$$\vec{D}(\vec{r}, t) = \epsilon(\vec{r}) \vec{E}(\vec{r}, t) [\text{C m}^{-2}]$$

Anisotropic materials:

$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \begin{bmatrix} \epsilon_{xx} & \epsilon_{xy} & \epsilon_{xz} \\ \epsilon_{yx} & \epsilon_{yy} & \epsilon_{yz} \\ \epsilon_{zx} & \epsilon_{zy} & \epsilon_{zz} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}$$

The permittivity ϵ is a tensor (or matrix) as properties depend on the direction.

For media with loss, ϵ is a complex number.

- For dispersive media,
 $\epsilon = f(\omega)$.
- Unsuitable for communications
 - Material Dispersion causes pulse spreading
- We compute the dispersion relation for devices such as waveguides.
- However, naturally all materials are dispersive to some extent.

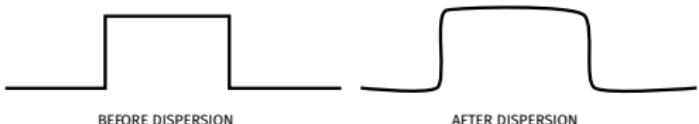


Figure 3: Frequency Dispersion

- Common circuit laws (Ohm's, KCL, and KVL) can be derived from the Maxwell's equations
- All circuit relations can be extracted

$$\vec{J}_c = \sigma \vec{E} \quad \Leftrightarrow \quad i = \frac{1}{R} v_R = G v_R \quad (\text{Ohm's Law})$$

$$\vec{B} = \mu \vec{H} \quad \Leftrightarrow \quad \phi_m = L i_L$$

$$\vec{M} = \mu \frac{\partial \vec{H}}{\partial t} \quad \Leftrightarrow \quad v_L = L \frac{\partial i_L}{\partial t}$$

$$\vec{D} = \epsilon \vec{E} \quad \Leftrightarrow \quad Q = Cv$$

$$\vec{J}_d = \epsilon \frac{\partial \vec{E}}{\partial t} \quad \Leftrightarrow \quad i_C = C \frac{\partial v}{\partial t}$$

$$\oint_C \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \iint_S \vec{B} \cdot d\vec{S} = -\frac{\partial \phi_m}{\partial t} \Leftrightarrow \sum v = -\frac{\partial \phi_m}{\partial t} = -L_s \frac{\partial i}{\partial t}$$

$$-V + V_R + V_L + V_C = -L_s \frac{\partial i}{\partial t}$$

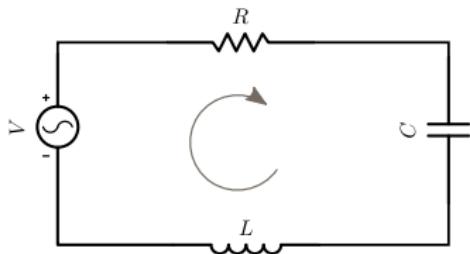


Figure 4: A Simple Circuit

- $L_s = 0$ when circuit dimensions are much smaller than the wavelength ($\Rightarrow \sum v = 0$).

CIRCUIT AND FIELD CONCEPT CORRESPONDENCE

Circuit	Field
Voltage V	Electric Field Intensity \vec{E}
Current I	Magnetic Field Intensity \vec{H}
Power $V \times I^*$	Poynting Vector Power Flow $\vec{E} \times \vec{H}^*$
Lab Project & Presentation	20%

You may have noticed loss of cell-phone reception when inside an elevator or driving through a tunnel.

EM wave propagation is governed by **boundary conditions**.

- We are interested in determining the fields in a given region in space
 - Use the integral forms to derive the boundary conditions
- Boundaries represent discontinuities in field values
 - The derivatives become undefined
- We break the fields into *tangential* and *normal* components

BOUNDARY CONDITIONS

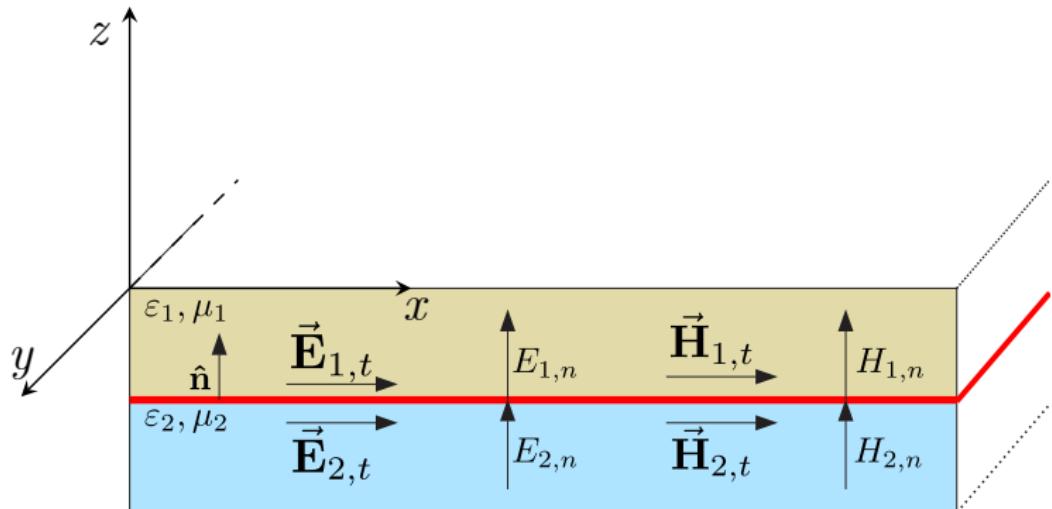


Figure 5: Boundary Conditions at an Interface

- The tangential components of the fields remain continuous along the boundary
- The normal components are discontinuous

$$\hat{\mathbf{n}} \times (\vec{\mathbf{E}}_1 - \vec{\mathbf{E}}_2) = \vec{\mathbf{M}}_s$$

$$\hat{\mathbf{n}} \cdot (\vec{\mathbf{D}}_2 - \vec{\mathbf{D}}_1) = \rho_{e,s}$$

Similarly,

$$\hat{\mathbf{n}} \times (\vec{\mathbf{H}}_1 - \vec{\mathbf{H}}_2) = -\vec{\mathbf{J}}_s$$

$$\hat{\mathbf{n}} \cdot (\vec{\mathbf{B}}_2 - \vec{\mathbf{B}}_1) = \rho_{m,s}$$

- For finite conductivity media ($\sigma_1, \sigma_2 \neq \infty$)
 - $\vec{J}_s, \vec{M}_s = 0, \rho_{e,s}, \rho_{m,s} = 0$

$$\hat{\mathbf{n}} \times (\vec{\mathbf{E}}_1 - \vec{\mathbf{E}}_2) = 0$$

$$\hat{\mathbf{n}} \times (\vec{\mathbf{H}}_2 - \vec{\mathbf{H}}_1) = 0$$

$$\hat{\mathbf{n}} \cdot (\vec{\mathbf{D}}_2 - \vec{\mathbf{D}}_1) = 0$$

$$\hat{\mathbf{n}} \cdot (\vec{\mathbf{B}}_2 - \vec{\mathbf{B}}_1) = 0$$

- For one PEC medium ($\sigma_1 = \infty$)
 - $\vec{E}_1 = \vec{H}_1 = 0$, All magnetic sources are zero

$$\hat{\mathbf{n}} \times \vec{E}_2 = 0$$

$$\hat{\mathbf{n}} \cdot \vec{H}_2 = \vec{J}_s$$

$$\hat{\mathbf{n}} \cdot \vec{D} = \rho_{e,s}$$

$$\hat{\mathbf{n}} \cdot \vec{B}_2 = 0$$

- In majority of cases, the time-variance of the fields is sinusoidal (time-harmonic).
- These time variations represented by $\exp(j\omega t)$
- We replace $\partial/\partial t$ by $j\omega$.

$$\nabla \times \vec{\mathbf{E}} = -j\omega \vec{\mathbf{B}}$$

$$\nabla \times \vec{\mathbf{H}} = j\omega \varepsilon \vec{\mathbf{E}} + \vec{\mathbf{J}}$$

$$\nabla \cdot \vec{\mathbf{E}} = \rho/\varepsilon$$

$$\nabla \cdot \vec{\mathbf{H}} = 0$$

- Wave Equations
- Dielectric Properties and Materials
- Nano-scale Electromagnetics