1 Mathematical Formulation

The geometry considered is a thin film of Silicon in the domain $-L/2 \le X \le L/2$ and $0 \le Y \le H$. Consider a certain particle, initially located at the coordinate **X**. During deformation, this particle follows a path

$$\boldsymbol{x} = \boldsymbol{x}(\boldsymbol{X}, t) \tag{1}$$

Let u(X,t) be the displacement of a material particle located at X. Then

$$\boldsymbol{u}(\boldsymbol{X},t) = \boldsymbol{x}(\boldsymbol{X},t) - \boldsymbol{X} = [u(\boldsymbol{X},t), v(\boldsymbol{X},t), w(\boldsymbol{X},t)]^{\mathsf{T}}$$
(2)

Let the deformation gradient be denoted by \mathbf{F} .

$$\mathbf{F} = \frac{\partial \mathbf{x}}{\partial \mathbf{X}} = \nabla_{\mathbf{X}} \mathbf{u} + \mathbf{I} \tag{3}$$

$$\mathbf{E} = \frac{1}{2} (\mathbf{F}^\mathsf{T} \mathbf{F} - \mathbf{I}) \tag{4}$$

Assuming plane strain deformation,

$$\mathbf{F} = \begin{bmatrix} 1 + \frac{\partial u}{\partial X} & \frac{\partial u}{\partial Y} & 0\\ \frac{\partial v}{\partial X} & 1 + \frac{\partial v}{\partial \partial Y} & 0\\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} F_{11} & F_{12} & 0\\ F_{21} & F_{22} & 0\\ 0 & 0 & F_{33} \end{bmatrix}$$
 (5)

Decomposition of deformation gradient

$$\mathbf{F} = \mathbf{F}^{\text{el}}\mathbf{F}^{\text{inel}} \tag{6}$$

where \mathbf{F}^{el} and \mathbf{F}^{inel} are the deformation gradients due to elastic deformation and inelastic deformation respectively.

The inelastic deformation gradient tensor, $\mathbf{F}^{\mathrm{inel}}$, has contribution from two sources - Deformation due to concentration gradient and Viscoplastic deformation.

$$\mathbf{F}^{\text{inel}} = \mathbf{F}^{c}\mathbf{F}^{p} \tag{7}$$

1.1 Viscoplastic Deformation

$$\dot{\mathbf{F}}^{p} = (J)^{-1} \frac{3}{2} \frac{\mathbf{M_{0}^{el}} \mathbf{F}^{p}}{\sigma_{\text{eff}}} \dot{d}_{0} \langle \frac{\sigma_{\text{eff}}}{\sigma_{\text{f}}} - 1 \rangle^{m}$$
(8)

$$\mathbf{M}_{\mathbf{0}}^{\mathrm{el}} = J(\mathbf{F}^{\mathrm{el}})^{\mathsf{T}} \boldsymbol{\tau} (\mathbf{F}^{\mathrm{el}})^{-\mathsf{T}}$$
(9)

 \mathbf{F}^{p} is assumed to be of the following form:

$$\mathbf{F}^{\mathbf{p}} = \begin{bmatrix} \lambda_{xx} & \lambda_{xy} & 0\\ \lambda_{yx} & \lambda_{yy} & 0\\ 0 & 0 & \lambda_{zz} \end{bmatrix}$$
 (10)

since, $det(\mathbf{F}^p) = 1$

$$\lambda_{zz} = 1/(\lambda_{xx}\lambda_{yy} - \lambda_{xy}\lambda_{yx}) \tag{11}$$

1.2 Deformation due to concentration gradient

$$\mathbf{F}^{c} = (J^{c})^{1/3}\mathbf{I} \tag{12}$$

where
$$J^c = 1 + 3\eta \chi_{\text{max}} \tilde{c}$$
 (13)

$$\mathbf{F}^{\text{inel}} = \mathbf{F}^{\text{p}} \mathbf{F}^{\text{c}} \tag{14}$$

$$\mathbf{F}^{\text{el}} = \mathbf{F}((\mathbf{F}^{\text{p}}\mathbf{F}^{\text{c}}))^{-1} \tag{15}$$

$$\mathbf{E}^{\text{el}} = \frac{1}{2} \left[(\mathbf{F}^{\text{el}})^{\mathsf{T}} \mathbf{F}^{\text{el}} - \mathbf{I} \right]$$
 (16)

Let **P** and **S** denote the first and second Piola-Kirchhoff stress tensors respectively.

$$W(\mathbf{F}, c) = \frac{J^c}{2} \frac{E(c)}{1 + \nu} \left(\frac{\nu}{1 - 2\nu} (\operatorname{tr} \mathbf{E}^{el})^2 + \operatorname{tr}(\mathbf{E}^{el} \mathbf{E}^{el}) \right)$$
(17)

$$\mathbf{S}^{\text{el}} = J^{c}(2\mu_{\text{si}}(c)\mathbf{E}^{\text{el}} + \lambda_{\text{si}}(c)\text{tr}(\mathbf{E}^{\text{el}})\mathbf{I})$$
(18)

$$\mathbf{S} = (\mathbf{F}^{c})^{-1}(\mathbf{F}^{p})^{-1}\mathbf{S}^{el}(\mathbf{F}^{p})^{-\mathsf{T}}(\mathbf{F}^{c})^{-\mathsf{T}}$$
(19)

$$\mathbf{P} = \mathbf{FS} \tag{20}$$

(21)

Let σ denote the Cauchy stress tensor. Then

$$\boldsymbol{\sigma} = (J)^{-1} \mathbf{P} \mathbf{F}^{\mathsf{T}} \tag{22}$$

where,
$$J = \det(\mathbf{F})$$
 (23)

Let ${m au}$ denote the deviatoric part of the Cauchy stress, ${m \sigma}$; then

$$\tau = \sigma - (1/3) \operatorname{tr}(\sigma) \mathbf{I} \tag{24}$$

(25)

Let $\sigma_{\rm eff}$ denote the von Mises stress. Then:

$$\sigma_{\text{eff}} = \sqrt{\frac{3}{2}(\tau_{11}^2 + \tau_{22}^2 + \tau_{33}^2 + 2 + \tau_{12}^2)}$$
 (26)

1.3 CZM Equations in Deepro's thesis

$$\Delta = \sqrt{\Delta_n^2 + \Delta_t^2} \tag{27}$$

$$T_n = K_n(1 - d)\langle \Delta_n \rangle \tag{28}$$

$$T_t = K_t(1 - d)\Delta_t \tag{29}$$

$$d = \begin{cases} 0 & \text{if } \Delta < \delta_{e,c} \\ \frac{\delta e}{\Delta} \left(\frac{\Delta - \delta_{e,c}}{\delta e - \delta_{e,c}} \right) & \text{if } \delta_{e,c} < \Delta < \delta e \\ 1 & \text{if } \Delta > \delta_e \end{cases}$$
 (30)

$$\delta_e \neq \sqrt{\left(\frac{2G_n}{\sigma_{\text{max}}}\right)^2 + \left(\frac{2G_t}{\tau_{\text{max}}}\right)^2} \tag{31}$$

$$\delta_{e,c} \neq \sqrt{\left(\frac{\sigma_{max}}{K_n}\right)^2 + \left(\frac{\tau_{max}}{K_t}\right)^2} \tag{32}$$

(33)

1.4 CZM Equations in COMSOL

$$\boldsymbol{u} = \{0, 0, \langle g_n \rangle\} + \mathbf{T}_b^{-\mathsf{T}} \cdot \Delta \boldsymbol{g}_t \tag{34}$$

$$u_m = \|\boldsymbol{u}\| \tag{35}$$

$$u_{\text{m, max}} = \max(u_m, u_{\text{m, max}}^{\text{old}})$$
 - same over the boundary or varies locally? (36)

$$\mathbf{f} = \mathbf{k}\mathbf{u}(1-d)$$
; Nominal traction (37)

$$u_{0t} = \frac{\sigma_{0t}}{k_{\rm n}} \tag{38}$$

$$u_{0s} = \frac{\sigma_{0s}}{k_t} \tag{39}$$

$$u_{0\text{m}} = u_{0\text{t}} u_{0\text{s}} \sqrt{\frac{u_m^2}{\langle u_{\text{I}} \rangle^2 u_{0\text{s}}^2 + u_{\text{II}}^2 u_{0\text{t}}^2}} - \text{why does it contain time varying quantities?}$$
 (40)

$$\beta = \frac{u_{\rm II}}{u_{\rm I}} - \text{constant ?} \tag{41}$$

$$u_{\rm mf} = \begin{cases} \frac{2(1+\beta^2)}{u_{\rm 0m}} \left[\left(\frac{k_n}{G_{ct}} \right)^{\alpha} + \left(\frac{\beta^2 k_t}{G_{cs}} \right)^{\alpha} \right]^{-\frac{1}{\alpha}} & \text{if } u_{\rm I} > 0\\ \frac{2G_{\rm cs}}{\sigma_s} & \text{if } u_{\rm I} < 0 \end{cases}$$

$$(42)$$

(43)

1.4.1 variable names in COMSOL

Variables in Decohesion node

$$u0t = \frac{\sigma_t}{k_n}$$
, Damage initiation displacement, tension (44)

$$u0s = \frac{\sigma_s}{k_{teq}}$$
, Damage initiation displacement, Shear (45)

$$u0m_{ap1} = \text{Damage initiation displacement, Mixed Mode}$$
 (46)

$$uft = \frac{2G_{ct}}{\sigma_t}$$
, Failure displacement, tension (47)

$$ufs = \frac{2G_{cs}}{\sigma_s}$$
, Failure displacement, Shear (48)

$$ufm_{ap1} =$$
Failure displacement, Mixed Mode (49)

$$u_{I_{an1}} = \text{Mode I displacement jump}$$
 (50)

$$u_{II_{ap1}} = \text{Mode II displacement jump}$$
 (51)

$$dmg_{ap1} = dmg = Damage (52)$$

$$dmg_{ratio_{ap1}} = \frac{um_{max_{ap1}} - u0m_{ap1}}{ufm_{ap1} - u0m_{ap1}}, \text{ Damage evolution ratio}$$
(53)

Stress equilibrium equation:

$$\nabla_{\mathbf{X}} \cdot \mathbf{P} = 0. \tag{54}$$

Mass conservation equation:

$$\frac{\partial c}{\partial t} = -\nabla_{\boldsymbol{X}} \cdot \boldsymbol{j} \tag{55}$$

1.5 Non-Dimensionalization

$$\tilde{c} = c/c_{\text{max}} \qquad \qquad \tilde{\boldsymbol{j}} = \boldsymbol{j}H/(c_{\text{max}}D_0)$$
 where, $c_{\text{max}} = \chi_{\text{max}}/V_m^B$
$$\tilde{u} = u/H \qquad \qquad \tilde{v} = v/H$$

$$\tilde{X} = X/H \qquad \qquad \tilde{Y} = Y/H$$

$$\tilde{t} = D_0 t/H^2 \qquad \qquad \tilde{\mu}_{\text{si}}, \tilde{\lambda}_{\text{si}} = \mu_{\text{si}}/E_0, \lambda_{\text{si}}/E_0$$

$$\tilde{E}(c) = E_{\text{si}}(1 + \eta_{\text{E}}\chi_{\text{max}}\tilde{c})/E_0, \text{ where } E_0 = \frac{R_g T}{V_m^b}$$

$$\tilde{\sigma}_0 = \frac{\sigma_0}{E_0}$$

$$\tilde{K} = \frac{KH}{E_0}$$

$$\tilde{G}_0 = \frac{G_0}{HE_0}$$

$$\tilde{\delta}_{\text{initiation}} = \frac{\delta_{\text{initiation}}}{H}$$

$$\tilde{\delta}_{\text{failure}} = \frac{\delta_{\text{failure}}}{H}$$

Definition of the state of charge

$$soc = \frac{\int_{-L/2}^{L/2} \int_{0}^{H} \tilde{c} dy dx}{LH}$$

$$= H^{2} \frac{\int_{-L/2H}^{L/2H} \int_{0}^{1} \tilde{c}(\tilde{x}, \tilde{y}) d\tilde{y} d\tilde{x}}{LH}$$

$$= H \frac{\int_{-L/2H}^{L/2H} \int_{0}^{1} \tilde{c}(\tilde{x}, \tilde{y}) d\tilde{y} d\tilde{x}}{L}$$

$$= H \frac{\int_{-L/2H}^{L/2H} \int_{0}^{1} \tilde{c}(\tilde{x}, \tilde{y}) d\tilde{y} d\tilde{x}}{L}$$

$$(58)$$

$$=H^{2}\frac{\int_{-L/2H}^{L/2H}\int_{0}^{1}\tilde{c}(\tilde{x},\tilde{y})\mathrm{d}\tilde{y}\mathrm{d}\tilde{x}}{LH}$$
(57)

$$=H\frac{\int_{-L/2H}^{L/2H} \int_0^1 \tilde{c}(\tilde{x}, \tilde{y}) d\tilde{y} d\tilde{x}}{L}$$
(58)

$$=2H\frac{\int_0^{L/2H} \int_0^1 \tilde{c}(\tilde{x}, \tilde{y}) d\tilde{y} d\tilde{x}}{L}$$
 (59)

$$=\frac{2H}{L}\operatorname{intop1}(\tilde{c})\tag{60}$$

Equations in component form 1.7

$$\mathbf{F} = \begin{bmatrix} 1 + \frac{\partial \tilde{u}}{\partial \tilde{X}} & \frac{\partial \tilde{u}}{\partial \tilde{Y}} & 0\\ \frac{\partial \tilde{v}}{\partial \tilde{X}} & 1 + \frac{\partial \tilde{v}}{\partial \tilde{Y}} & 0\\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \tilde{F}_{11} & \tilde{F}_{12} & 0\\ \tilde{F}_{21} & \tilde{F}_{22} & 0\\ 0 & 0 & \tilde{F}_{33} \end{bmatrix}$$
(61)

$$\tilde{F}_{11}^{\text{el}} = (J^c)^{-1/3} \lambda_{zz} (\tilde{F}_{11} \lambda_{yy} - \tilde{F}_{12} \lambda_{yx})$$
(62)

$$\tilde{F}_{12}^{\text{el}} = (J^c)^{-1/3} \lambda_{zz} (\tilde{F}_{12} \lambda_{xx} - \tilde{F}_{11} \lambda_{xy})$$
(63)

$$\tilde{F}_{21}^{\text{el}} = (J^c)^{-1/3} \lambda_{zz} (\tilde{F}_{21} \lambda_{yy} - \tilde{F}_{22} \lambda_{yx}) \tag{64}$$

$$\tilde{F}_{22}^{\text{el}} = (J^c)^{-1/3} \lambda_{zz} (\tilde{F}_{22} \lambda_{xx} - \tilde{F}_{21} \lambda_{xy}) \tag{65}$$

$$\tilde{F}_{33}^{\text{el}} = (J^c)^{-1/3} (1/\lambda_{zz}) \tilde{F}_{33} \tag{66}$$

$$\tilde{E}_{11}^{\text{el}} = 0.5[(\tilde{F}_{11}^{\text{el}})^2 + (\tilde{F}_{21}^{\text{el}})^2 - 1] \tag{67}$$

$$\tilde{E}_{22}^{\text{el}} = 0.5[(\tilde{F}_{12}^{\text{el}})^2 + (\tilde{F}_{22}^{\text{el}})^2 - 1] \tag{68}$$

$$\tilde{E}_{33}^{\text{el}} = 0.5[(\tilde{F}_{33}^{\text{el}})^2 - 1] \tag{69}$$

$$\tilde{E}_{12}^{\text{el}} = 0.5[\tilde{F}_{11}^{\text{el}}\tilde{F}_{12}^{\text{el}} + \tilde{F}_{21}^{\text{el}}\tilde{F}_{22}^{\text{el}}] = \tilde{E}_{21}^{\text{el}}$$

$$(70)$$

$$\tilde{S}_{11}^{\text{el}} = J^{c} [2\tilde{\mu}_{\text{si}}(\tilde{c})\tilde{E}_{11}^{\text{el}} + \tilde{\lambda}_{\text{si}}(\tilde{c})(\tilde{E}_{11}^{\text{el}} + \tilde{E}_{22}^{\text{el}} + \tilde{E}_{33}^{\text{el}})]$$
(71)

$$\tilde{S}_{22}^{\text{el}} = J^{c} [2\tilde{\mu}_{\text{si}}(\tilde{c})\tilde{E}_{22}^{\text{el}} + \tilde{\lambda}_{\text{si}}(\tilde{c})(\tilde{E}_{11}^{\text{el}} + \tilde{E}_{22}^{\text{el}} + \tilde{E}_{33}^{\text{el}})]$$
(72)

$$\tilde{S}_{33}^{\text{el}} = J^{c} [2\tilde{\mu}_{\text{si}}(\tilde{c})\tilde{E}_{33}^{\text{el}} + \tilde{\lambda}_{\text{si}}(\tilde{c})(\tilde{E}_{11}^{\text{el}} + \tilde{E}_{22}^{\text{el}} + \tilde{E}_{33}^{\text{el}})]$$
(73)

$$\tilde{S}_{12}^{\text{el}} = J^c 2\tilde{\mu}_{\text{si}}(\tilde{c})\tilde{E}_{12}^{\text{el}} = \tilde{S}_{21}^{\text{el}} \tag{74}$$

(75)

$$\tilde{S}_{11} = (J^c)^{-2/3} \left[-\lambda_{xy} (\tilde{S}_{12}^{\text{el}} \lambda_{yy} - \tilde{S}_{22}^{\text{el}} \lambda_{xy}) + \lambda_{yy} (\tilde{S}_{11}^{\text{el}} \lambda_{yy} - \tilde{S}_{21}^{\text{el}} \lambda_{xy}) \right] \lambda_{zz}^2$$
(76)

$$\tilde{S}_{12} = (J^c)^{-2/3} [\lambda_{xx} (\tilde{S}_{12}^{\text{el}} \lambda_{yy} - \tilde{S}_{22}^{\text{el}} \lambda_{xy}) - \lambda_{yx} (\tilde{S}_{11}^{\text{el}} \lambda_{yy} - \tilde{S}_{21}^{\text{el}} \lambda_{xy})] \lambda_{zz}^2$$
(77)

$$\tilde{S}_{21} = (J^c)^{-2/3} [\lambda_{xy} (\tilde{S}_{12}^{\text{el}} \lambda_{yx} - \tilde{S}_{22}^{\text{el}} \lambda_{xx}) - \lambda_{yy} (\tilde{S}_{11}^{\text{el}} \lambda_{yx} - \tilde{S}_{21}^{\text{el}} \lambda_{xx})] \lambda_{zz}^2$$
(78)

$$\tilde{S}_{22} = (J^c)^{-2/3} \left[-\lambda_{xx} (\tilde{S}_{12}^{\text{el}} \lambda_{yx} - \tilde{S}_{22}^{\text{el}} \lambda_{xx}) + \lambda_{yx} (\tilde{S}_{11}^{\text{el}} \lambda_{yx} - \tilde{S}_{21}^{\text{el}} \lambda_{xx}) \right] \lambda_{zz}^2$$
(79)

$$\tilde{S}_{33} = (J^c)^{-2/3} \tilde{S}_{33}^{\text{el}} / \lambda_{zz}^2 \tag{80}$$

$$\tilde{P}_{11} = \tilde{F}_{11}\tilde{S}_{11} + \tilde{F}_{12}\tilde{S}_{21} \tag{81}$$

$$\tilde{P}_{12} = \tilde{F}_{11}\tilde{S}_{12} + \tilde{F}_{12}\tilde{S}_{22} \tag{82}$$

$$\tilde{P}_{21} = \tilde{F}_{21}\tilde{S}_{11} + \tilde{F}_{22}\tilde{S}_{21} \tag{83}$$

$$\tilde{P}_{22} = \tilde{F}_{21}\tilde{S}_{12} + \tilde{F}_{22}\tilde{S}_{22} \tag{84}$$

$$\tilde{P}_{33} = \tilde{F}_{33}\tilde{S}_{33} \tag{85}$$

$$J = \tilde{F}_{33}(\tilde{F}_{11}\tilde{F}_{22} - \tilde{F}_{12}\tilde{F}_{21}) \tag{86}$$

$$\tilde{\sigma}_{11} = (\tilde{F}_{11}\tilde{P}_{11} + \tilde{F}_{12}\tilde{P}_{12})/J \tag{87}$$

$$\tilde{\sigma}_{12} = (\tilde{F}_{21}\tilde{P}_{11} + \tilde{F}_{22}\tilde{P}_{12})/J \tag{88}$$

$$\tilde{\sigma}_{21} = (\tilde{F}_{11}\tilde{P}_{21} + \tilde{F}_{12}\tilde{P}_{22})/J \tag{89}$$

$$\tilde{\sigma}_{22} = (\tilde{F}_{21}\tilde{P}_{21} + \tilde{F}_{22}\tilde{P}_{22})/J \tag{90}$$

$$\tilde{\sigma}_{33} = \tilde{F}_{33}\tilde{P}_{33}/J \tag{91}$$

(92)

$$\tilde{\tau}_{11} = \tilde{\sigma}_{11} - (\tilde{\sigma}_{11} + \tilde{\sigma}_{22} + \tilde{\sigma}_{33})/3 \tag{93}$$

$$\tilde{\tau}_{22} = \tilde{\sigma}_{22} - (\tilde{\sigma}_{11} + \tilde{\sigma}_{22} + \tilde{\sigma}_{33})/3 \tag{94}$$

$$\tilde{\tau}_{33} = \tilde{\sigma}_{33} - (\tilde{\sigma}_{11} + \tilde{\sigma}_{22} + \tilde{\sigma}_{33})/3 \tag{95}$$

$$\tilde{\tau}_{12} = \tilde{\tau}_{21} = \tilde{\sigma}_{12} \tag{96}$$

$$\tilde{\sigma}_{\text{eff}} = \sqrt{\frac{3}{2}(\tilde{\tau}_{11}^2 + \tilde{\tau}_{22}^2 + \tilde{\tau}_{33}^2 + 2\tilde{\tau}_{12}^2)}$$
(97)

$$\tilde{M}_{11}^{\rm el} = J[-\tilde{F}_{12}^{\rm el}(\tilde{F}_{11}^{\rm el}\tilde{\tau}_{12} + \tilde{F}_{21}^{\rm el}\tilde{\tau}_{22}) + \tilde{F}_{22}^{\rm el}(\tilde{F}_{11}^{\rm el}\tilde{\tau}_{11} + \tilde{F}_{21}^{\rm el}\tilde{\tau}_{21})]/(\tilde{F}_{11}^{\rm el}\tilde{F}_{22}^{\rm el} - \tilde{F}_{12}^{\rm el}\tilde{F}_{21}^{\rm el})$$
(98)

$$\tilde{M}_{12}^{\rm el} = J[\tilde{F}_{11}^{\rm el}(\tilde{F}_{11}^{\rm el}\tilde{\tau}_{12} + \tilde{F}_{21}^{\rm el}\tilde{\tau}_{22}) - \tilde{F}_{21}^{\rm el}(\tilde{F}_{11}^{\rm el}\tilde{\tau}_{11} + \tilde{F}_{21}^{\rm el}\tilde{\tau}_{21})]/(\tilde{F}_{11}^{\rm el}\tilde{F}_{22}^{\rm el} - \tilde{F}_{12}^{\rm el}\tilde{F}_{21}^{\rm el})$$
(99)

$$\tilde{M}_{21}^{\rm el} = J[-\tilde{F}_{12}^{\rm el}(\tilde{F}_{12}^{\rm el}\tilde{\tau}_{12} + \tilde{F}_{22}^{\rm el}\tilde{\tau}_{22}) + \tilde{F}_{22}^{\rm el}(\tilde{F}_{12}^{\rm el}\tilde{\tau}_{11} + \tilde{F}_{22}^{\rm el}\tilde{\tau}_{21})]/(\tilde{F}_{11}^{\rm el}\tilde{F}_{22}^{\rm el} - \tilde{F}_{12}^{\rm el}\tilde{F}_{21}^{\rm el})$$
(100)

$$\tilde{M}_{22}^{\text{el}} = J[\tilde{F}_{11}^{\text{el}}(\tilde{F}_{12}^{\text{el}}\tilde{\tau}_{12} + \tilde{F}_{22}^{\text{el}}\tilde{\tau}_{22}) - \tilde{F}_{21}^{\text{el}}(\tilde{F}_{12}^{\text{el}}\tilde{\tau}_{11} + \tilde{F}_{22}^{\text{el}}\tilde{\tau}_{21})]/(\tilde{F}_{11}^{\text{el}}\tilde{F}_{22}^{\text{el}} - \tilde{F}_{12}^{\text{el}}\tilde{F}_{21}^{\text{el}})$$

$$(101)$$

$$\tilde{M}_{33}^{\text{el}} = J\tilde{\tau}_{33} \tag{102}$$

Viscoplastic rates:

$$\dot{\lambda}_{xx} = \frac{3\dot{d}_0}{2J\tilde{\sigma}_{\text{eff}}} (\tilde{M}_{11}^{\text{el}} \lambda_{xx} + \tilde{M}_{12}^{\text{el}} \lambda_{yx}) H(\frac{\tilde{\sigma}_{\text{eff}}}{\tilde{\sigma}_{\text{f}}} - 1)^{\text{m}}$$
(103)

$$\dot{\lambda}_{xy} = \frac{3\dot{d}_0}{2J\tilde{\sigma}_{\text{eff}}} (\tilde{M}_{11}^{\text{el}} \lambda_{xy} + \tilde{M}_{12}^{\text{el}} \lambda_{yy}) H (\frac{\tilde{\sigma}_{\text{eff}}}{\tilde{\sigma}_{\text{f}}} - 1)^{\text{m}}$$
(104)

$$\dot{\lambda}_{yx} = \frac{3\dot{d}_0}{2J\tilde{\sigma}_{\text{eff}}} (\tilde{M}_{21}^{\text{el}} \lambda_{xx} + \tilde{M}_{22}^{\text{el}} \lambda_{yx}) \mathbf{H} (\frac{\tilde{\sigma}_{\text{eff}}}{\tilde{\sigma}_{\text{f}}} - 1)^{\text{m}}$$
(105)

$$\dot{\lambda}_{yy} = \frac{3\dot{d}_0}{2J\tilde{\sigma}_{\text{eff}}} (\tilde{M}_{21}^{\text{el}} \lambda_{xy} + \tilde{M}_{22}^{\text{el}} \lambda_{yy}) H(\frac{\tilde{\sigma}_{\text{eff}}}{\tilde{\sigma}_{\text{f}}} - 1)^{\text{m}}$$
(106)

$$\dot{\lambda}_{zz} = \frac{3\dot{d}_0 \lambda_{zz}}{2J\tilde{\sigma}_{\text{eff}}} \tilde{M}_{33}^{\text{el}} H (\frac{\tilde{\sigma}_{\text{eff}}}{\tilde{\sigma}_{\text{f}}} - 1)^{\text{m}}$$
(107)

(108)

Viscoplastic rate equations in non-dimensional form:

$$\frac{d\lambda_{xx}}{dt} = \frac{1}{t_{\text{ref}}} \frac{d\lambda_{xx}}{d\tilde{t}} = \frac{3\dot{d}_0}{2J\tilde{\sigma}_{\text{eff}}} (\tilde{M}_{11}^{\text{el}} \lambda_{xx} + \tilde{M}_{12}^{\text{el}} \lambda_{yx}) H(\frac{\tilde{\sigma}_{\text{eff}}}{\tilde{\sigma}_{\text{f}}} - 1)^{\text{m}}$$
(109)

$$\frac{d\lambda_{xx}}{d\tilde{t}} = \frac{3\dot{\tilde{d}}_0}{2J\tilde{\sigma}_{\text{eff}}} (\tilde{M}_{11}^{\text{el}}\lambda_{xx} + \tilde{M}_{12}^{\text{el}}\lambda_{yx}) H(\frac{\tilde{\sigma}_{\text{eff}}}{\tilde{\sigma}_{\text{f}}} - 1)^{\text{m}}$$
(110)

where,
$$\dot{\tilde{d}}_0 = \dot{d}_0 t_{\text{ref}}$$
 (111)

Stress equilibrium Equation:

$$\nabla_{X} \cdot \mathbf{P} = \mathbf{0}. \tag{112}$$

$$\frac{\partial P_{11}}{\partial X} + \frac{\partial P_{12}}{\partial Y} = 0 \tag{113}$$

and,
$$\frac{\partial P_{21}}{\partial X} + \frac{\partial P_{22}}{\partial Y} = 0$$
 (114)

In non-dimensional form:

$$\frac{E_0}{H} \frac{\partial \tilde{P}_{11}}{\partial \tilde{X}} + \frac{E_0}{H} \frac{\partial \tilde{P}_{12}}{\partial \tilde{Y}} = 0 \tag{115}$$

and,
$$\frac{E_0}{H} \frac{\partial \tilde{P}_{21}}{\partial \tilde{X}} + \frac{E_0}{H} \frac{\partial \tilde{P}_{22}}{\partial \tilde{Y}} = 0$$
 (116)

So,

$$\frac{\partial \tilde{P}_{11}}{\partial \tilde{X}} + \frac{\partial \tilde{P}_{12}}{\partial \tilde{Y}} = 0 \tag{117}$$

and,
$$\frac{\partial \tilde{P}_{21}}{\partial \tilde{X}} + \frac{\partial \tilde{P}_{22}}{\partial \tilde{Y}} = 0$$
 (118)

Mass conservation Equation:

$$\frac{\partial c}{\partial t} = -\nabla_{\mathbf{X}} \cdot \mathbf{j} = -\left(\frac{\partial j_x}{\partial X} + \frac{\partial j_y}{\partial Y}\right) \tag{119}$$

For one way coupling:

$$\mathbf{j} = -D_0 \nabla_{\mathbf{X}} c \tag{120}$$

$$\tilde{j}_x = j_x H/(c_{\text{max}} D_0) \tag{121}$$

$$= -D_0 \frac{\partial c}{\partial X} H/(c_{\text{max}} D_0) \tag{122}$$

$$= -\frac{\partial \tilde{c}}{\partial \tilde{X}} \tag{123}$$

$$\tilde{j}_y = j_y H/(c_{\text{max}} D_0) \tag{124}$$

$$= -\frac{\partial \tilde{c}}{\partial \tilde{Y}} \tag{125}$$

For two way coupling:

$$\boldsymbol{j} = -\frac{1}{R_q T} \frac{D \chi_{\text{max}} \tilde{c}}{V_m^b} (F)^{-1} (F)^{-\mathsf{T}} \boldsymbol{\nabla}_{\boldsymbol{X}} \mu$$
 (126)

$$D = D_0 \exp(\frac{\alpha S_h}{E_0}) \tag{127}$$

$$\mu = \mu_0 + \mu_s \tag{128}$$

$$\mu_0 = R_g T \log(\gamma \tilde{c}) \tag{129}$$

$$\gamma = \frac{1}{1 - \tilde{c}} \exp\left(\frac{1}{R_o T} \left[2(A_0 - 2B_0)\tilde{c} - 3(A_0 - B_0)(\tilde{c}^2)\right]\right)$$
(130)

$$\mu_s = \frac{V_m^b}{V_{max}} \left[-\frac{1}{3} \frac{\partial J^c}{\partial \tilde{c}} \tilde{F}_{im}^{\text{el}} \tilde{F}_{in}^{\text{el}} C_{mnkl} \tilde{E}_{kl}^{\text{el}} + \frac{1}{2} \left(J^c \frac{\partial C_{ijkl}}{\partial \tilde{c}} + \frac{\partial J^c}{\partial \tilde{c}} C_{ijkl} \right) \tilde{E}_{ij}^{\text{el}} \tilde{E}_{kl}^{\text{el}} \right]$$
(131)

$$= (\mu_1 + \mu_2 + \mu_3)/\chi_{\text{max}} \tag{132}$$

$$\tilde{\mu} = \tilde{\mu}_0 + (\tilde{\mu}_1 + \tilde{\mu}_2 + \tilde{\mu}_3)/\chi_{\text{max}}$$
 (133)

$$\tilde{\mu}_0 = \log(\gamma \tilde{c}) \tag{134}$$

$$\tilde{\mu}_{1} = -\frac{1}{6(J^{c})} \frac{\partial J^{c}}{\partial \tilde{c}} \left[\tilde{S}_{11}^{\text{el}} \tilde{E}_{11}^{\text{el}} + \tilde{S}_{22}^{\text{el}} \tilde{E}_{22}^{\text{el}} + 2 \tilde{S}_{12}^{\text{el}} \tilde{E}_{12}^{\text{el}} + \tilde{S}_{33}^{\text{el}} \tilde{E}_{33}^{\text{el}} \right]$$
(135)

$$\tilde{\mu}_2 = -\frac{1}{3(J^c)} \frac{\partial J^c}{\partial \tilde{c}} [\tilde{S}_{11}^{\text{el}} + \tilde{S}_{22}^{\text{el}} + \tilde{S}_{33}^{\text{el}}]$$
(136)

$$\tilde{\mu}_3 = \frac{1}{2} J^c \frac{\partial \tilde{C}_{ijkl}}{\partial \tilde{c}} \tilde{E}_{kl}^{\text{el}} \tilde{E}_{ij}^{\text{el}} \tag{137}$$

$$= \frac{1}{2} J^{c} [2\tilde{\mu}'_{si}(\tilde{c})\tilde{E}^{el}_{ij}\tilde{E}^{el}_{ij} + \tilde{\lambda}'_{si}(\tilde{c})(\tilde{E}^{el}_{11} + \tilde{E}^{el}_{22} + \tilde{E}^{el}_{33})\tilde{E}^{el}_{ij}\delta_{ij}]$$
(138)

$$= \frac{1}{2} J^{c} \left[2\tilde{\mu}'_{si}(\tilde{c}) \left((\tilde{E}_{11}^{el})^{2} + (\tilde{E}_{22}^{el})^{2} + (\tilde{E}_{33}^{el})^{2} + 2(\tilde{E}_{12}^{el})^{2} \right) + \tilde{\lambda}'_{si}(c) \left(\tilde{E}_{11}^{el} + \tilde{E}_{22}^{el} + \tilde{E}_{33}^{el} \right)^{2} \right]$$
(139)

$$\boldsymbol{j} = -\frac{D\chi_{\max}\tilde{c}}{V_m^b}\tilde{\mathbf{F}}^{-1}(\tilde{\mathbf{F}}^{-1})^\mathsf{T}\nabla_{\boldsymbol{X}}\tilde{\mu}$$
(140)

$$\tilde{j} = jHV_m^b/(\chi_{\text{max}}D_0) \tag{141}$$

$$= -\frac{D}{D_0} H \tilde{c} \tilde{\mathbf{F}}^{-1} (\tilde{\mathbf{F}}^{-1})^{\mathsf{T}} \nabla_{\mathbf{X}} \tilde{\mu}$$
(142)

$$\tilde{j}_x = \frac{-\bar{D}H\tilde{c}}{J^2} \left(\frac{\partial \tilde{\mu}}{\partial X} (\tilde{F}_{12}^2 + \tilde{F}_{22}^2) - \frac{\partial \tilde{\mu}}{\partial Y} (\tilde{F}_{11}\tilde{F}_{12} + \tilde{F}_{21}\tilde{F}_{22}) \right)$$

$$(143)$$

$$= \frac{-\bar{D}\tilde{c}}{J^2} \left(\frac{\partial \tilde{\mu}}{\partial \tilde{X}} (\tilde{F}_{12}^2 + \tilde{F}_{22}^2) - \frac{\partial \tilde{\mu}}{\partial \tilde{Y}} (\tilde{F}_{11}\tilde{F}_{12} + \tilde{F}_{21}\tilde{F}_{22}) \right)$$

$$(144)$$

$$\tilde{j}_y = \frac{-\bar{D}H\tilde{c}}{J^2} \left(\frac{\partial \tilde{\mu}}{\partial Y} (\tilde{F}_{11}^2 + \tilde{F}_{21}^2) - \frac{\partial \tilde{\mu}}{\partial X} (\tilde{F}_{11}\tilde{F}_{12} + \tilde{F}_{21}\tilde{F}_{22}) \right)$$

$$(145)$$

$$= \frac{-\bar{D}\tilde{c}}{J^2} \left(\frac{\partial \tilde{\mu}}{\partial \tilde{Y}} (\tilde{F}_{11}^2 + \tilde{F}_{21}^2) - \frac{\partial \tilde{\mu}}{\partial \tilde{X}} (\tilde{F}_{11}\tilde{F}_{12} + \tilde{F}_{21}\tilde{F}_{22}) \right)$$

$$(146)$$

(147)

In non-dimensional form:

$$c_{\max} \frac{D_0}{H^2} \frac{\partial \tilde{c}}{\partial \tilde{t}} = -\left(\frac{1}{H} \frac{\partial \tilde{j}_x}{\partial \tilde{X}} + \frac{1}{H} \frac{\partial \tilde{j}_y}{\partial \tilde{V}}\right) c_{\max} \frac{D_0}{H}$$
(148)

so,
$$\frac{\partial \tilde{c}}{\partial \tilde{t}} = -\left(\frac{\partial \tilde{j}_x}{\partial \tilde{X}} + \frac{\partial \tilde{j}_y}{\partial \tilde{Y}}\right)$$
 (149)

Secondary Variables (in DIS+SED) for the expression of flux in two-way coupling:

$$\tilde{\mathbf{F}}_{X} = \frac{\partial \tilde{\mathbf{F}}}{\partial \tilde{X}} = \begin{bmatrix}
\frac{\partial^{2} \tilde{u}}{\partial \tilde{X}^{2}} & \frac{\partial^{2} \tilde{u}}{\partial \tilde{X}^{2}} & 0 \\
\frac{\partial^{2} \tilde{v}}{\partial \tilde{X}^{2}} & \frac{\partial^{2} \tilde{v}}{\partial \tilde{X}^{2}} & 0 \\
0 & 0 & 0
\end{bmatrix}$$

$$\tilde{\mathbf{F}}_{Y} = \frac{\partial \tilde{\mathbf{F}}}{\partial \tilde{Y}} = \begin{bmatrix}
\frac{\partial^{2} \tilde{u}}{\partial \tilde{X}^{2}} & \frac{\partial^{2} \tilde{u}}{\partial \tilde{X}^{2}} & 0 \\
\frac{\partial^{2} \tilde{v}}{\partial \tilde{X}^{2}} & \frac{\partial^{2} \tilde{u}}{\partial \tilde{Y}^{2}} & 0 \\
\frac{\partial^{2} \tilde{v}}{\partial \tilde{X}^{2}} & \frac{\partial^{2} \tilde{v}}{\partial \tilde{Y}^{2}} & 0 \\
0 & 0 & 0
\end{bmatrix}$$
(150)

$$\tilde{\mathbf{F}}_{Y} = \frac{\partial \tilde{\mathbf{F}}}{\partial \tilde{Y}} = \begin{bmatrix} \frac{\partial^{2} \tilde{u}}{\partial \tilde{X} \tilde{Y}} & \frac{\partial^{2} \tilde{u}}{\partial \tilde{Y}^{2}} & 0\\ \frac{\partial^{2} \tilde{v}}{\partial \tilde{X} \tilde{Y}} & \frac{\partial^{2} \tilde{v}}{\partial \tilde{Y}^{2}} & 0\\ 0 & 0 & 0 \end{bmatrix}$$
(151)

$$\tilde{F}_{11_x}^{\text{el}} = -\frac{1}{3} (J^c)^{-4/3} \frac{dJ^c}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} F_{11} + (J^c)^{-1/3} F_{11_x}$$
(152)

$$\tilde{F}_{12_x}^{\text{el}} = -\frac{1}{3} (J^c)^{-4/3} \frac{dJ^c}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} F_{12} + (J^c)^{-1/3} F_{12_x}$$
(153)

$$\tilde{F}_{21_x}^{\text{el}} = -\frac{1}{3} (J^c)^{-4/3} \frac{dJ^c}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} F_{21} + (J^c)^{-1/3} F_{21_x}$$
(154)

$$\tilde{F}_{22_x}^{\text{el}} = -\frac{1}{3} (J^c)^{-4/3} \frac{dJ^c}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} F_{22} + (J^c)^{-1/3} F_{22_x}$$
(155)

$$\tilde{F}_{33a}^{\text{el}} = \tag{156}$$

$$\tilde{E}_{11}^{\text{el}} = \tilde{F}_{11}^{\text{el}} \tilde{F}_{11}^{\text{el}} + \tilde{F}_{21}^{\text{el}} \tilde{F}_{21}^{\text{el}} \tag{157}$$

$$\tilde{E}_{22_x}^{\text{el}} = \tilde{F}_{12}^{\text{el}} \tilde{F}_{12_x}^{\text{el}} + \tilde{F}_{22}^{\text{el}} \tilde{F}_{22_x}^{\text{el}} \tag{158}$$

$$\tilde{E}_{12_x}^{\text{el}} = 0.5[\tilde{F}_{11_x}^{\text{el}} \tilde{F}_{12}^{\text{el}} + \tilde{F}_{11}^{\text{el}} \tilde{F}_{12_x}^{\text{el}} + \tilde{F}_{21_x}^{\text{el}} \tilde{F}_{22_x}^{\text{el}} + \tilde{F}_{21_x}^{\text{el}} \tilde{F}_{22_x}^{\text{el}}] = \tilde{E}_{21_x}^{\text{el}}$$

$$(159)$$

$$\tilde{E}_{33_x}^{\rm el} = \tag{160}$$

$$\tilde{E}_{trace}^{\rm el} = \tilde{E}_{11}^{\rm el} + \tilde{E}_{22}^{\rm el} + \tilde{E}_{33}^{\rm el} \tag{161}$$

$$\tilde{E}_{trace_x}^{\rm el} = \tilde{E}_{11_x}^{\rm el} + \tilde{E}_{22_x}^{\rm el} + \tilde{E}_{33_x}^{\rm el} \tag{162}$$

$$\tilde{S}_{11_x}^{\text{el}} = \frac{dJ^c}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \frac{\tilde{S}_{11}^{\text{el}}}{J^c} + J^c \left(2 \frac{d\tilde{\mu}_{si}}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tilde{E}_{11}^{\text{el}} + 2\tilde{\mu}_{si} \tilde{E}_{11_x}^{\text{el}} + \frac{d\tilde{\lambda}_{si}}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tilde{E}_{trace}^{\text{el}} + \tilde{\lambda}_{si} \tilde{E}_{trace_x}^{\text{el}} \right)$$
(163)

$$\tilde{S}_{22_x}^{\text{el}} = \frac{dJ^c}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \frac{\tilde{S}_{22}^{\text{el}}}{J^c} + J^c \left(2 \frac{d\tilde{\mu}_{si}}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tilde{E}_{22}^{\text{el}} + 2\tilde{\mu}_{si} \tilde{E}_{22_x}^{\text{el}} + \frac{d\tilde{\lambda}_{si}}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tilde{E}_{trace}^{\text{el}} + \tilde{\lambda}_{si} \tilde{E}_{trace_x}^{\text{el}} \right)$$
(164)

$$\tilde{S}_{33_x}^{\text{el}} = \frac{dJ^c}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \frac{\tilde{S}_{33}^{\text{el}}}{J^c} + J^c \left(2 \frac{d\tilde{\mu}_{si}}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tilde{E}_{33}^{\text{el}} + 2\tilde{\mu}_{si} \tilde{E}_{33_x}^{\text{el}} + \frac{d\tilde{\lambda}_{si}}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tilde{E}_{trace}^{\text{el}} + \tilde{\lambda}_{si} \tilde{E}_{trace_x}^{\text{el}} \right)$$
(165)

$$\tilde{S}_{12_x}^{\text{el}} = 2\frac{dJ^c}{d\tilde{c}}\frac{\partial \tilde{c}}{\partial \tilde{\chi}}\tilde{\mu}_{si}\tilde{E}_{12}^{\text{el}} + 2J^c\frac{d\tilde{\mu}_{si}}{d\tilde{c}}\frac{\partial \tilde{c}}{\partial \tilde{\chi}}\tilde{E}_{12}^{\text{el}} + 2J^c\tilde{\mu}_{si}\tilde{E}_{12_x}^{\text{el}} = \tilde{S}_{21_x}^{\text{el}}$$

$$\tag{166}$$

$$\gamma = \frac{1}{1 - \tilde{c}} \exp\left(\frac{1}{R_q T} \left[2(A_0 - 2B_0)\tilde{c} - 3(A_0 - B_0)(\tilde{c}^2)\right]\right)$$
(167)

$$\frac{\partial \gamma}{\partial \tilde{X}} = \gamma_x = \frac{1}{(1 - \tilde{c})^2} \frac{\partial \tilde{c}}{\partial \tilde{X}} \exp(...) + \frac{1}{1 - \tilde{c}} \exp(...) \frac{1}{R_g T} [2(A_0 - 2B_0) \frac{\partial \tilde{c}}{\partial \tilde{X}} - 3(A_0 - B_0)(2\tilde{c} \frac{\partial \tilde{c}}{\partial \tilde{X}})]$$
(168)

$$= \frac{1}{1-\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \gamma + \frac{\gamma}{R_g T} [2(A_0 - 2B_0) \frac{\partial \tilde{c}}{\partial \tilde{X}} - 3(A_0 - B_0)(2\tilde{c} \frac{\partial \tilde{c}}{\partial \tilde{X}})]$$
(169)

$$\tilde{\mu}_0 = \log(\gamma \tilde{c}) \tag{171}$$

$$\tilde{\mu}_{0_x} = \frac{1}{\gamma} \gamma_x + \frac{1}{\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tag{172}$$

$$\tilde{\mu}_{1} = -\frac{1}{6(J^{c})} \frac{\partial J^{c}}{\partial \tilde{c}} [\tilde{S}_{11}^{\text{el}} \tilde{E}_{11}^{\text{el}} + \tilde{S}_{22}^{\text{el}} \tilde{E}_{22}^{\text{el}} + 2\tilde{S}_{12}^{\text{el}} \tilde{E}_{12}^{\text{el}} + \tilde{S}_{33}^{\text{el}} \tilde{E}_{33}^{\text{el}}]$$
(173)

$$= -\frac{1}{2J^c} \eta \chi_{\text{max}} [\tilde{S}_{11}^{\text{el}} \tilde{E}_{11}^{\text{el}} + \tilde{S}_{22}^{\text{el}} \tilde{E}_{22}^{\text{el}} + 2\tilde{S}_{12}^{\text{el}} \tilde{E}_{12}^{\text{el}} + \tilde{S}_{33}^{\text{el}} \tilde{E}_{33}^{\text{el}}]$$
(174)

$$\tilde{\mu}_{1_x} = \left(-\frac{1}{2}\eta\chi_{\text{max}}\right) * \left(-\frac{1}{J^{c^2}}3\eta\chi_{\text{max}}\right) * \frac{\partial\tilde{c}}{\partial\tilde{X}}[...] - \frac{1}{2J^c}\eta\chi_{\text{max}}[...]_x \tag{175}$$

$$= -3\eta \chi_{\max} \frac{1}{J^c} \frac{\partial \tilde{c}}{\partial \tilde{\chi}} \tilde{\mu}_1 - \eta \chi_{\max} \frac{1}{2J^c} [\tilde{S}_{11_x}^{\text{el}} \tilde{E}_{11}^{\text{el}} + \tilde{S}_{11}^{\text{el}} \tilde{E}_{11_x}^{\text{el}} + \tilde{S}_{22_x}^{\text{el}} \tilde{E}_{22}^{\text{el}} + \tilde{S}_{22}^{\text{el}} \tilde{E}_{22_x}^{\text{el}}$$
(176)

$$+\tilde{S}_{33_x}^{\text{el}}\tilde{E}_{33}^{\text{el}} + \tilde{S}_{33}^{\text{el}}\tilde{E}_{33_x}^{\text{el}} + 2\tilde{S}_{12_x}^{\text{el}}\tilde{E}_{12}^{\text{el}} + 2\tilde{S}_{12}^{\text{el}}\tilde{E}_{12_x}^{\text{el}}]$$

$$(177)$$

$$\tilde{\mu}_2 = -\frac{1}{3(J^c)} \frac{\partial J^c}{\partial \tilde{c}} [\tilde{S}_{11}^{\text{el}} + \tilde{S}_{22}^{\text{el}} + \tilde{S}_{33}^{\text{el}}]$$
(178)

$$= -\frac{1}{I_c} \eta \chi_{\text{max}} [\tilde{S}_{11}^{\text{el}} + \tilde{S}_{22}^{\text{el}} + \tilde{S}_{33}^{\text{el}}]$$
 (179)

$$\tilde{\mu}_{2_x} = -\frac{3\eta \chi_{\text{max}}}{J^c} \frac{\partial \tilde{c}}{\partial \tilde{X}} \tilde{\mu}_2 - \frac{\eta \chi_{\text{max}}}{J^c} [\tilde{S}_{11_x}^{\text{el}} + \tilde{S}_{22_x}^{\text{el}} + \tilde{S}_{33_x}^{\text{el}}]$$
(180)

$$\tilde{\mu}_3 = \frac{1}{2} J^c \left[2\tilde{\mu}'_{si}(\tilde{c}) \left((\tilde{E}_{11}^{el})^2 + (\tilde{E}_{22}^{el})^2 + (\tilde{E}_{33}^{el})^2 + 2(\tilde{E}_{12}^{el})^2 \right) + \tilde{\lambda}'_{si}(c) \left(\tilde{E}_{11}^{el} + \tilde{E}_{22}^{el} + \tilde{E}_{33}^{el} \right)^2 \right]$$
(181)

$$\tilde{\mu}_{3_{x}} = \frac{dJ^{c}}{d\tilde{c}} \frac{\partial \tilde{c}}{\partial \tilde{X}} \frac{\tilde{\mu}_{3}}{J^{c}} + \frac{J^{c}}{2} \left[2\tilde{\mu}'_{\text{si}} (2\tilde{E}^{\text{el}}_{11}\tilde{E}^{\text{el}}_{11_{x}} + 2\tilde{E}^{\text{el}}_{22}\tilde{E}^{\text{el}}_{22_{x}} + 2\tilde{E}^{\text{el}}_{33}\tilde{E}^{\text{el}}_{33_{x}} + 4\tilde{E}^{\text{el}}_{12}\tilde{E}^{\text{el}}_{12_{x}}) + 2\tilde{\lambda}'_{\text{si}} (\tilde{E}^{\text{el}}_{trace}\tilde{E}^{\text{el}}_{trace_{x}})) \right]$$
(182)

$$\tilde{\mu}_x = \tilde{\mu}_{0_x} + (\tilde{\mu}_{1_x} + \tilde{\mu}_{2_x} + \tilde{\mu}_{3_x}) / \chi_{\text{max}}$$
(183)

1.8 Boundary and Initial Conditions

$$\tilde{c}(\tilde{X}, \tilde{Y}, 0) = 0 \tag{184}$$

$$\tilde{u}(\tilde{X}, \tilde{Y}, 0) = 0 \tag{185}$$

$$\tilde{v}(\tilde{X}, \tilde{Y}, 0) = 0 \tag{186}$$

$$\tilde{u}(\tilde{X},0,\tilde{t})=\tilde{v}(\tilde{X},0,\tilde{t})=0;$$
 all three other faces are traction free (187)

$$\tilde{j}_x(\tilde{X}, 1, \tilde{t}) = \tilde{j}_0(1 - \tilde{c}(\tilde{X}, 1, \tilde{t}));$$
 all three other faces are insulated from any flux (188)